Mineral Resource Estimate and Update to a NI43-101 Technical Report for the Handeni Property centered at 37.97°E, 5.744°S, Tanga Province, Handeni District, Tanzania

Prepared for

East Africa Metals Inc.

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Standard Units & Abbreviations

% .... Percent
< .... Less than
> .... Greater than
° .... Degree
°C .... Degrees Celsius
µm .... Micrometre (micron)
a .... Year (annum)
Au .... Gold
cfm .... Cubic feet per minute
CIM .... Canadian Institute of Mining, Metallurgy and Petroleum
cm .... Centimetre
CPG .... Certified Professional Geologist (USA Designation)
d .... Day
dmt .... Dry metric tonne
ft .... Foot/feet
g .... Gram
G&A .... General & Administration
g/t .... Grams per tonne
gal .... Gallon
GPS .... Global Positioning System
h .... Hour
h/a .... Hours per year
ha .... Hectare (10,000 m^2)
HDPE .... High Density Polyethylene
hp .... Horsepower
in .... Inch(es)
k .... Kilo (thousand)
kg .... Kilogram
kg/m^2 .... Kilograms per square metre
kg/t .... Kilograms per tonne
km .... Kilometre
km^2 .... Square kilometre
kPa .... Kilopascals
kt .... Thousand tonnes
kV .... Kilovolt

kW .... Kilowatt
kWh .... Kilowatt hour
kWh/a .... Kilowatt hours per year
kWh/t .... Kilowatt hours per tonne
L .... Litre
L/s........ Litres per second
lb........ Pound(s)
LOM........ Life of Mine
m .... Metre
M .... Million
m/min........ Metres per minute
m/s........ Metres per second
m^2 .... Square metre
m^3 .... Cubic metre
m^3/t .... Cubic metres per tonne
Ma .... Million years ago
masl .... Metres above sea level
min........ Minute (time)
mL .... Millilitre
mm .... Millimetre
mo .... Month
Mt .... Million tonnes
MVA........ Megavolt ampere
MW .... Megawatt
MWh .... Megawatt hours
NI 43-101........ National Instrument 43-101
NPV .... Net Present Value
oz........ Ounce, Troy (31.1035 g)
P.Eng........ Professional Engineer (Canadian Designation)
P.Geo. .... Professional Geologist (Canadian Designation)
pH .... Acidity
ppm .... Parts per million
psi .... Pounds per square inch
QPs .... Qualified Persons
s........ Second (time)
SG .... Specific gravity
t........ Tonne (metric, 1,000 kg = 2205 lbs)
t/a .... Tonnes per year
t/h .... Tonnes per hour
t/m^3 .... Tonnes per cubic metre
tpd .... Tonnes per day
V .... Volt
wk .... Week

Drill Core Sizes

Size	Hole diameter, mm	Core diameter, mm
NQ	75.8	47.6
NTW	75.7	56.0
HQ	96	63.5

Source: Wikipedia

1 SUMMARY

This technical report is prepared for East Africa Metals Inc and presents an update to the June 2012 report which documented the independent initial mineral resource estimate for the Magambazi area of Canaco Resources Inc.'s ("Canaco") Handeni project in accordance with the requirements of National Instrument 43-101, '*Standards of Disclosure for Mineral Projects',* and the Canadian Institute of Mining, Metallurgy and Petroleum (CIM) Standards on Mineral Resources and Mineral Reserves, adopted by CIM Council, as amended.

The Handeni Property is located in the Tanga region of northeastern Tanzania, approximately 120 km west of Dar es Salaam and 30 km south of the town of Handeni, and is accessible by a combination of paved highway and all-weather unpaved roads from Dar es Salaam. The property mineral licences held by Canaco cover an area of approximately 96.22 km^2.

Situated in the Paleoproterozoic Usugaran/Ubendian Metamorphic Terrane, and along the northern extension of the north-trending Proterozoic Mozambique Mobile Belt, the Handeni area hosts the metamorphosed eastern extension of the Lake Victoria cratonic belt and, as such, it is considered prospective for Archean greenstone-related orogenic lode-gold mineralisation and deposits. The geology of the Handeni area is characterized by variably deformed amphibolite facies para- and ortho-gneisses, and amphibolites, with evidence for thrust faulting and the later development of a northwest trending mineralised shear zone in the northeastern portion of the property.

Previous mining activity on the property was restricted to artisanal hard rock and placer gold occurrences, with limited mineral exploration fieldwork conducted by Midland Minerals Corp. prior to Canaco acquiring the property in 2007. Since late 2007, Canaco has carried out programs of mineral exploration consisting of geophysical and remote sensing data collection, geologic mapping, soil surveying, surface (rock chip) sampling, petrologic studies, airborne magnetic and radiometric surveys, rotary air blast drilling, reverse circulation drilling and diamond drilling. These techniques were employed to facilitate understanding of local and regional geology, to collect sample materials, to identify the extent of gold mineralisation in the area and to allow quantification of the initial mineral resource presented in this report.

The exploration and drilling assay results were recorded in an electronic database and an independent review of the associated drilling, sampling, care and custody, sample preparation, laboratory, quality assurance/quality control and database procedures were completed under the scope of this technical report along with validation of the data itself. Further to that review, the quality of the gold analytical data are found here to be sufficiently reliable to support mineral resource estimation and the sample preparation, analysis and security have been generally performed in accordance with mineral exploration best practices and industry standards.

In 2009, mineral exploration diamond drilling at the Magambazi area identified encouraging gold occurrences, and in 2010 further drilling was carried out over much of the approximately 960 m strike length of the Magambazi hill. In 2010, mineral resource drilling was initiated on section lines that were spaced 40 m apart, to define the extent and quality of the observed gold mineralisation. By April 2012, 471 diamond drill holes had been drilled for a total of 121,846 m (including two abandoned holes totalling 80 m) on the Handeni property, of which 441 holes (113,863 m) were related to resource definition on Magambazi hill. Findings from 397 of these holes were used as the basis for the initial mineral resource estimate and the remainder of 44 holes were excluded due to pending QA/QC validation.

Diamond drilling in the Magambazi area, to-date, has identified gold mineralisation associated with a northwest trending structure that is interpreted to be the footwall of a metamorphosed and annealed high-angle fault zone, and a lower-grade stratabound gold mineralisation possibly related to a thrust plane. The lowest grade intercept reported in this work was 13.0 m containing 0.47 g/t Au, and the highest grade was 8.40 m containing 80.90 g/t Au. The longest intercept recorded was a 68.3 m interval that contained 1.90 g/t Au. From the 434 holes where assays have been reported by Canaco, a total of 289 holes were found to contain significant mineralised intervals measuring greater than 1.0 g/t Au.

In December 2011, Canaco commissioned an initial mineral resource estimate for the mineralised portion of the Magambazi area, which is the subject of this technical report. The mineral resource estimate was prepared by independent Qualified Person James N. Gray, P.Geo, of Advantage Geoservices Ltd. In support of this work, drilling data validation and historical context was provided by independent Qualified Persons Mr. Ian Farrelly, P.Geo. and Dr. Sandy Archibald, P.Geo. of Aurum Exploration Services. Mr. Gray, Mr. Farrelly and Dr. Archibald are each independent of Canaco and are Qualified Persons as defined by National Instrument 43-101. Along with Dr. Jim King of Jim King Consulting Inc., Canaco's independent Qualified Person for metallurgy and process design, each have reviewed, validated and approved publication of the technical information contained in this report and the associated news releases.

The initial mineral resource estimate for Magambazi was based on assay data available to February 29, 2012. Resource estimation was performed using Gemcom software. Uniform downhole 5 m composites were used to estimate 5 x 5 x 5 m blocks. The block size was selected to provide a reasonable level of selectivity in support of the low production rate (<6,000 tpd) anticipated for the project.

Gold grades were estimated by inverse distance cubed interpolation within two grade domains. Low-grade and potentially mineralised domains were derived by ordinary kriging of a 0.2 gram per tonne indicator applied to the composite data. Composite grades were capped in the two domains at 2.5 and 15 grams per tonne, respectively. The interpolation of indicators and of grade was carried out with a search oriented parallel to one of five interpreted structural trends. Rock densities were based on averages derived from more than 50,000 measurements. Resource classification was based on geometric parameters associated with sample location and drill density. Approximately 35% of the inferred category resource was downgraded from the indicated category due to unresolved QA/QC sample fails, which resulted in a decrease in confidence of the affected gold assays.

Measures were taken to validate that the mineral resource meets the condition of "reasonable prospects of economic extraction" as suggested under National Instrument 43-101. To this end, a pit shell was generated using a gold price of US$1,250 per ounce and an overall pit slope of 40° for the purpose of resource tabulation. Only blocks within the pit volume were included in this resource estimate. A cut-off grade of 0.5 gram per tonne was selected as the resource base case considering extraction by conventional surface mining and mineral processing methods. At a 0.5 gram per tonne gold cut-off grade Magambazi contains an indicated resource of 15.186 Mt grading 1.48 g/t Au (for 721,300 oz Au) plus an inferred resource 6.683 Mt grading 1.36 g/t Au (for 292,400 oz Au). For comparative purposes, other cut-off grades are included in Table 1.1.

Table 1.1: Magambazi Estimated Mineral Resource

Cut-off Grade (g/t)	Indicated			Inferred		
	Tonnes (kt)	Au (g/t)	Au (oz)	Tonnes (kt)	Au (g/t)	Au (oz)
0.30	19,685	1.23	777,500	9,256	1.09	324,500
0.40	17,218	1.36	750,300	7,831	1.23	308,800
0.50	**15,186**	**1.48**	**721,300**	**6,683**	**1.36**	**292,400**
0.60	13,392	1.60	689,900	5,593	1.52	273,400
0.70	11,884	1.72	658,700	4,791	1.67	256,800
1.00	8,593	2.07	570,600	3,058	2.14	210,700

In parallel with mineral resource estimation, Canaco has completed other work in support of the mineral resource estimate and in preparation for subsequent project stages. This work focused on understanding the metallurgical characteristics of gold mineralisation at the Magambazi area and on-going, environmental and socio-economic baseline studies.

The metallurgy of the Magambazi mineralisation was examined in a comprehensive, independent test program whose objectives included:

- confirmation of the free milling nature of the Magambazi area gold mineralisation;
- production of algorithms that relate gold recovery to the head grade of the mineralised material;
- investigation of the variability of the metallurgical response within the deposit;
- definition of an operable flowsheet for processing of material from the Magambazi deposit, including measurement of Bond Work Index, primary grind size, and cyanide leach conditions.

To this end, the deposit has been divided into four zones along strike, Zones A through D, and a variety of tests were conducted on representative composite samples to determine the metallurgical response and its variability across the zones. An extensive sampling program was undertaken to generate composite samples that would be representative of the Magambazi mineralisation as a whole and each zone in particular. Some 2,935 individual drill core intervals were selected as constituents for metallurgical testwork composites, representing 2,325 m of drill core. To maintain security and integrity of metallurgical samples, each drill core interval was kept segregated and shipped as an intact section of quartered core material to the metallurgical laboratory for processing.

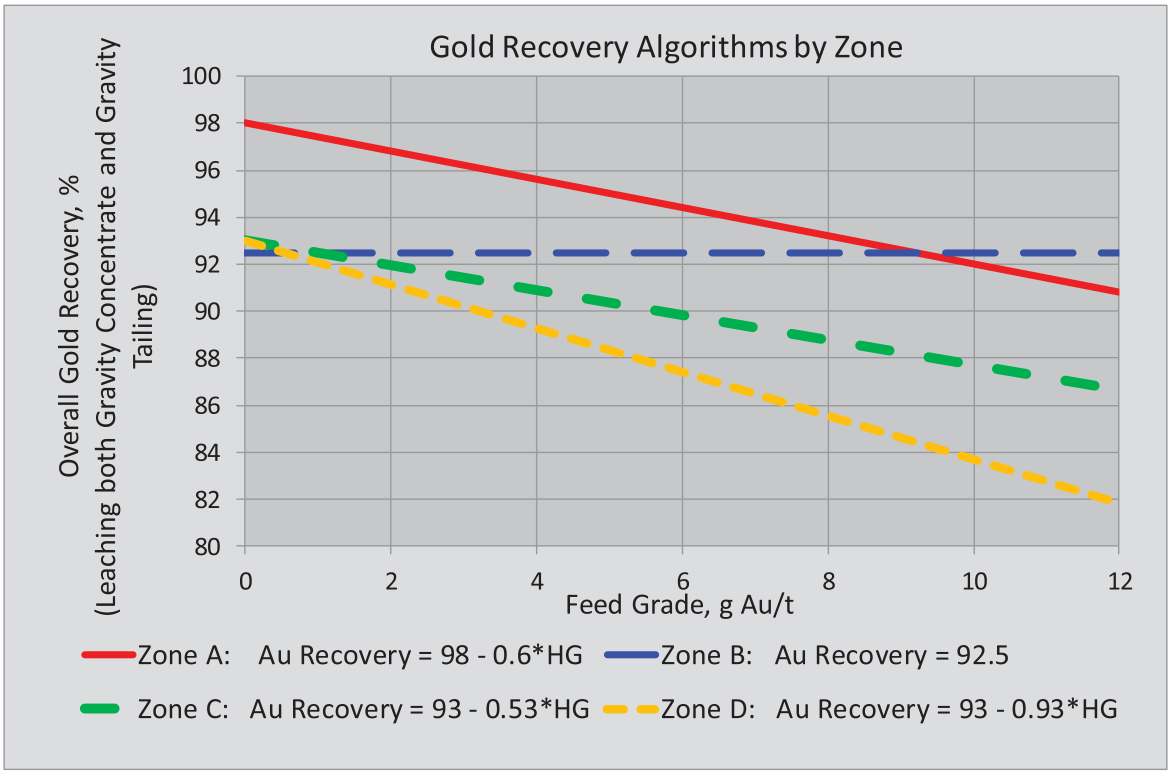
Through this work, it was found that mineralisation from the Magambazi area of the Handeni property may be processed using conventional gravity concentration and cyanide leaching to recover the contained gold. Composites representing a wide range of gold grades from each of these zones have been used to produce the gold recovery algorithms shown in Table 1.2 and in Figure 1.1.

Table 1.2: Gold Recovery Algorithms by Zone

Zone A	Overall Gold Recovery =	98 - 0.6*HG
Zone B	Overall Gold Recovery =	92.5
Zone C	Overall Gold Recovery =	93 - 0.53*HG
Zone D	Overall Gold Recovery =	93 - 0.93*HG

Note. Calculated recoveries are expressed in percent

Figure 1.1: Gold Recovery Algorithms by Zone



Further to the above points, it should be noted that:

- Gold recovery is lower for mineralisation originating in the north of the deposit, represented by Zones C and D, than in the South represented by Zones A and B.
- Gold recovery is reduced as the feed grade mineralisation increases. Gold in the Magambazi deposit is closely associated with arsenic and two arsenic minerals have been identified, namely arsenopyrite and lollingite. It is likely that the reduction in gold recovery is due to a change of mineralogy and gold distribution between these two minerals as the gold content of the mineralisation increases. This aspect of the mineralogy should be investigated further.
- Differences were observed between metallurgical composite sample grades predicted from drill core assays and those back-calculated from metallurgical results. Further metallurgical testwork should be completed to understand or reconcile these differences. This observation also indicates that the application of grade capping practices during the mineral resource estimation is appropriate in this case.
- The Magambazi area contains medium-hard mineralised material with an average Bond Work Index of 16.6. It is considered medium abrasive with an average abrasion index of 0.30.

The flowsheet suggested for processing mineralised material from the Magambazi area should comprise:

- Three stage crushing to a P80 of 6 mm.
- Single stage ball milling to a P80 product size of 180 to 200 µm, assuming the deposit might eventually be mined by open pit methods.
- Gravity concentration installed in the grinding circuit should be expected to recover approximately 70% of the gold in the plant feed into a gravity rougher concentrate representing approximately 2% of the mass feed. In this approach, the gravity concentrate should be subjected to cyanide leaching using a cyanide concentration of 2000 ppm for a residence time of 48 hours.
- The ground process feed, after removal of the gravity concentrate, (i.e. gravity tailings) should be subjected to cyanide leaching using a cyanide concentration of 500 ppm for a residence time of 24 hours. The cyanide leaching should be carried out in a series of eight tanks, the first two tanks operated as straight leach tanks with the remaining six tanks operated as carbon in pulp tanks in a carousel arrangement.
- Cyanide consumption in the testwork averaged 2.5 kg NaCN per tonne of gravity concentrate, and 0.10 kg NaCN per tonne of gravity tailing. The overall cyanide consumption ranged from 0.10 to 0.30 kg NaCN per tonne of Grade Composite feed. It should be noted that these consumptions are the specific cyanide requirement to leach the gold and they do not include cyanide that will inevitably be left in solution at the end of the gravity concentrate and gravity tailing leaches. Whilst every effort will be made to recycle cyanide from leach solutions, the actual plant cyanide consumptions would be expected to be closer to 4 kg NaCN per tonne of gravity concentrate and 0.35 kg NaCN per tonne of gravity tailing. Based on the relative weights of gravity concentrate on gravity tailing, this calculates to an overall consumption of

0.43 kg NaCN per tonne of plant feed. A consumption of 0.50 kg NaCN per tonne feed is suggested for use in calculating operating costs.

- Lime consumption ranged from 1.5 to 5.0 kg CaO per tonne of gravity concentrate, with the highest consumption measured for Zone D material. Lime consumption ranged from 0.5 to 1.0 kg CaO per tonne of gravity tailing. The overall lime consumption ranged from 0.5 to 1.1 kg CaO per tonne of plant feed. A consumption of 1.00 kg CaO per tonne plant feed is suggested for use in calculating operating costs

To minimize the amount of material subjected to cyanide leaching, as an alternative approach to the above flowsheet, preliminary testwork has been carried out on low-grade and high-grade master composites of Zones A through D, to investigate whether satisfactory gold recoveries could be collected into a combined gravity concentrate and flotation concentrate that represented a small weight percentage of the plant feed.

For the low-grade master composite, 96.4% of the gold was recovered into the combined gravity-flotation concentrate, and leaching this combined concentrate dissolved 95.5% of the contained gold, giving an overall gold recovery of approximately 92.1%. Results for the high-grade master composites were similar, with 96.9% of the gold recovered into the combined gravity-flotation concentrate, and leaching this combined concentrate dissolving 95.0% of the contained gold, for an overall gold recovery of approximately 92.1%.

In completing the initial mineral resource estimation and the metallurgical testwork, several recommendations for further work were identified. Specifically, it is recommended that the path forward for this project and the Handeni property should include:

- Development of an improved understanding of the geological model, through the analysis and interpretation of existing drill data, particularly through the acquisition of additional geochemical information from existing drill sample material using handheld XRF equipment.
- Conducting a 15 hole reverse circulation drill program to test key nearby stratigraphy for Magambazi-type gold mineralisation.
- If warranted, additional reverse circulation and diamond drilling should be undertaken in a work second program to follow-up on results from the reverse circulation drilling program.
- Further metallurgical testwork should be undertaken to investigate opportunities for reduction of cyanide consumption, incorporation of flotation in the process flowsheet and improved understanding of differences observed between composite grades predicted by drill core assays and those back-calculated from metallurgical results.
- Updating the resource estimation incorporating the outstanding 44 diamond drillholes.
- An Engineering and Project Assessment that involves the continuation of initial trade-off studies, evaluation and development of a program to address grade discrepancies, possible bulk sampling, and expanding land permit.

Expected costs for the recommended path forward are estimated at $381,000 for Phase I (points 1-2) work, $1,078,000 for Phase II (points 3-5), for an approximate total of $1,459,000.

2 INTRODUCTION

2.1 Terms of Reference, Scope & Purpose of Report

In February 2013, East Africa Metals Inc. (EAM), retained Advantage Geoservices Limited, Jim King Consultants, and Aurum Exploration Services to prepare an updated summary report on the Handeni gold exploration licence owned by Canaco Resources Inc. On April 4, 2013, Canaco, by way of a Plan of Arrangement, transferred all of its assets and liabilities to EAM, except for $60M cash. As a result of the Plan of Arrangement, EAM has ownership of the Handeni gold exploration license and this report is to support EAM's application to list on the TSX Venture Exchange.

The initial Magambazi mineral resource estimate, the main subject of this technical report, was successfully completed in the second quarter of 2012 with the assistance of a variety of organizations forming the Magambazi project team. The organizations who contributed to this work and their scope of responsibility are summarized in Table 2.1.

Table 2.1: General Areas of Responsibility

Organization	Main Scope of Responsibility
Aurum Exploration Services	Site physical inspection, drilling QA/QC program auditing, drilling database validation, including assessment of QA/QC program, assay results, standard/blank use, assay certificates, laboratory and procedures, overall assembly of this technical report
Advantage Geoservices Limited	Site physical inspection, collecting umpire samples, mineral resource statistical analysis, block modeling, data validation, estimation and mineral resource classification
Jim King Consulting Inc.	Metallurgical testwork design, analysis and evaluation, including program management
SGS Minerals Services	Sample receipt, sample preparation and laboratory testing
ACME Labs, ACME Analitik Laboratuar Hizmetleri Limited Sirketi and ACME Analytical Laboratories (Vancouver) Ltd.	Sample receipt, sample preparation and laboratory testing
G&T Metallurgical Services Ltd.	Metallurgical sample receipt, sample preparation, metallurgical testwork and related laboratory analyses
Rescan Environmental Services Ltd.	Environmental baseline studies and study team support for atmospheric, vegetation, wildlife, aquatics, hydrology, hydrogeology, socio-economic and environmental permitting considerations.
Canaco Resources Inc. and/or Canaco Tanzania Ltd.	Overall project management, general study coordination, topography, land ownership, mineral and metallurgical sampling, geologic interpretation

The reader is directed to the attached Qualified Person Certificates for a detailed list of the individual report section responsibilities for each of the Qualified Persons.

The primary objectives of this report are to:

- consolidate and review all available past and present work
- review all available drilling, sampling and analytical procedures used at site, in the laboratories and in record retention
- collect field samples for independent testing and verification
- review and validate all drilling data collected for this report, including assessment and validation of associated QA/QC programs and assay results
- estimate and classify mineral resources within the Magambazi area of Canaco's Handeni property
- determine the metallurgical response of mineralised material to potential processing methods
- identify risks and opportunities for the project
- make recommendations for a path forward and for further work.

This study has been prepared in accordance with the requirements and standards for disclosure of the stock exchanges overseen by the Canadian Securities Administrators, namely, NI 43-101, Companion Policy 43-101CP, Form 43-101F and the Canadian Institute of Mining, Metallurgy and Petroleum ("CIM") Standards on Mineral Resource and Reserves – Definition and Guidelines.

2.2 Sources of Information & Data

The authors have prepared this report using information from the following sources:

- drilling and assay data obtained from Canaco through a program of field sampling and analytical laboratory processing of field samples
- visits to the project site
- information from previous technical reports prepared in accordance with NI 43-101 requirements
- site physical inspection, observation and database validation activities, including but not limited to:
  - Review and observation of drilling, sampling, logging and core retention procedures and practices at site
  - sampling, shipping and assaying of independently collected and processed material samples, including use of an independent assay laboratory
  - review and examination of drill core material from selected holes
  - Drilling database validation, including assessment of QA/QC program, assay certificates, laboratories and procedures
- first principle estimation and statistical analysis, including but not limited to:

- estimation of statistics and geostatistics for the mineral resource model, including variography and continuity checking
- mineral resource block model creation
- detailed density assessment and statistics for the block model, including density variation by domain, lithology, mineralisation, alteration and oxidation
- mineral resource grade estimation
- mineral resource classification
- mineral resource model validation and benchmarking

- metallurgical testwork and laboratory analytical results derived from quarter core sample material provided by Canaco
- where applicable, the authors' experience at numerous mineral resource development projects and with mining/mineral processing operations
- information supplied by other experts as listed in Section 3 of this report.

2.3 Visits to the Property by Qualified Persons

Table 2.2 lists the dates the various Qualified Persons, for this report, visited the site.

Table 2.2: Qualified Persons Site Visits

Qualified Person	Company	Visit Date(s)
Dr. Sandy Archibald, P.Geo.	Aurum Exploration Services	Feb 12-17, 2012 Dec 14-16, 2010
Mr. Ian Farrelly, P.Geo.	Aurum Exploration Services	Sep 25-28, 2011 Aug 2-7, 2011
Mr. James N. Gray, P.Geo.	Advantage Geoservices Limited	Feb 12-17, 2012
Dr. Jim King, P.Eng.	Jim King Consulting Inc.	Feb 12-17, 2012

Since drilling on the property was completed on March 28th, 2012, and the only work performed was a handheld XRF study in May 2012, it was concluded that an additional site visit for EAM was not necessary.

3 RELIANCE ON OTHER EXPERTS

The authors of this report have relied upon the following documents and experts (who are not qualified persons), and in this regard the authors disclaim responsibility for information provided in the following:

- Legal audit and opinion with regard to the title, mining concessions, and registration issues provided by LawFields Consulting in a letter dated 4 May 2012. This information pertains to Item 4.2.2.
- Geological and topographic mapping data and information from Mr. Cris Carman of CEC Geology LLC.
- Geological mapping data and interpretation from Mr. Iain Groves of Insight Geology PTY.
- Handheld XRF study and interpretation by Mr. Eoin McGrath of Aurum Exploration Services and Prof. David Groves.
- Metallurgical test and analytical results provided by G&T Metallurgical Services Ltd.
- Initial environmental and socio-economic baseline fieldwork and study team support for atmospheric, vegetation, wildlife, aquatics, hydrology, hydrogeology, socio-economic and environmental permitting considerations, provided Rescan Environmental Services Ltd.
- Petrology and structural interpretation prepared by Mr. Josef Klominsky of the Czech Geological Survey, Praha, Czech Republic.
- Petrographic study of Magambazi prepared by Vancouver Petrographics Ltd.
- Sample preparation and laboratory assay results provided by SGS Minerals Services.
- Sample preparation and laboratory assay results provided by ACME Labs, ACME Analitik Laboratuar Hizmetleri Limited Sirketi and ACME Analytical Laboratories (Vancouver) Ltd.
- Sample preparation and laboratory assay results provided by ALS.
- Sample preparation and laboratory assay results provided by G&T Metallurgical Services Ltd.
- Preliminary Leapfrog modeling of mineralised areas provided by SRK Consulting (Australasia) Pty Ltd.

4 PROPERTY DESCRIPTION & LOCATION

4.1 Size & Location

The Handeni property covers an area of 97.38 km^2 and is located in northeastern Tanzania, in the Handeni District of the Tanga Region, approximately 30 km south of the town of Handeni as shown in Figure 4-1. The United Republic of Tanzania comprises a total area of 945,087 km^2 and is located between longitudes 29°E to 41°E and latitudes 1°S to 12°S. The country is bounded by Kenya and Uganda to the north, the Indian Ocean to the east, Mozambique, Malawi and Zambia to the south, with Burundi, Rwanda and the Democratic Republic of Congo to the west.

Figure 4-1: Property Location

Source: Archibald, 2011

4.2 Mineral Tenure

4.2.1 General Tenure Rights

The first effort to regulate the mineral industry in Tanzania was recorded in the Mineral Policy of Tanzania, October 1997. This was subsequently followed by the *Mining Act of Tanzania* (1998) with a further revision taking place in April 2010, and passed by an act of Parliament. The 2010 legislation imposes higher royalties (increasing from 3% to 4% for precious- and base- metals; 5% for diamonds, gemstones and uranium), allows the Minister, in consultation with holders of a special mining licence, to make regulations prescribing the minimum shareholding requirement and procedure for selling shares to Tanzanian nationals offering shares to the public through listing with the stock exchange.

Licences are granted on a first come, first served basis except in a situation where licences are subjected to a competitive bidding process. The types of licences which may be granted under the Mining Act include a prospecting licence, a retention licence, a special mining licence, a mining licence, a gemstone mining licence, a primary mining licence and a primary prospecting licence. Primary mining licences (PMLs) are restricted to Tanzanian citizens or corporate entities whose membership is composed exclusively of Tanzanian citizens. None of the other categories of mineral rights (see below) are subjected to this restriction. Licences to mine gemstones are only granted to Tanzanians, regardless of the size of the extraction operation. It is understood that agreements/licences currently in force with non-Tanzanian controlled mining companies remain unchanged.

In terms of mineral tenure requirements, the holder of a prospecting licence must:

- commence prospecting operations within three months, or such further period as the licensing authority may allow, from the date of the grant of the licence or such other date as is stated in the licence on commencement period
- give notice to the licensing authority of discovery of any mineral deposit with potential commercial value
- expend on prospecting operations not less than the amount prescribed.

The holder of a mining licence or a special mining licence must:

- develop the mining area and carry on mining operations in substantial compliance with the program of mining operations and their environmental management plan, and commence production in accordance with the program of mining operations
- employ and train citizens of Tanzania in accordance with their proposals as appended to the licence
- demarcate the mining area and keep it demarcated in the prescribed manner.

Whenever required by the minister, after consultation with the Mining Advisory Committee, licence holders must post a bond to finance the costs of rehabilitating and making safe the mining area upon termination of mining operations in the event that the holders of the special mining licence have failed to meet their obligations.

Aboriginal or previously disadvantaged people do not maintain preferential rights to mining rights; however, occupiers of land are entitled to compensation from holders of a mining right if there is any disturbance to the rights of a lawful occupier of land (Nguluma, 2009).

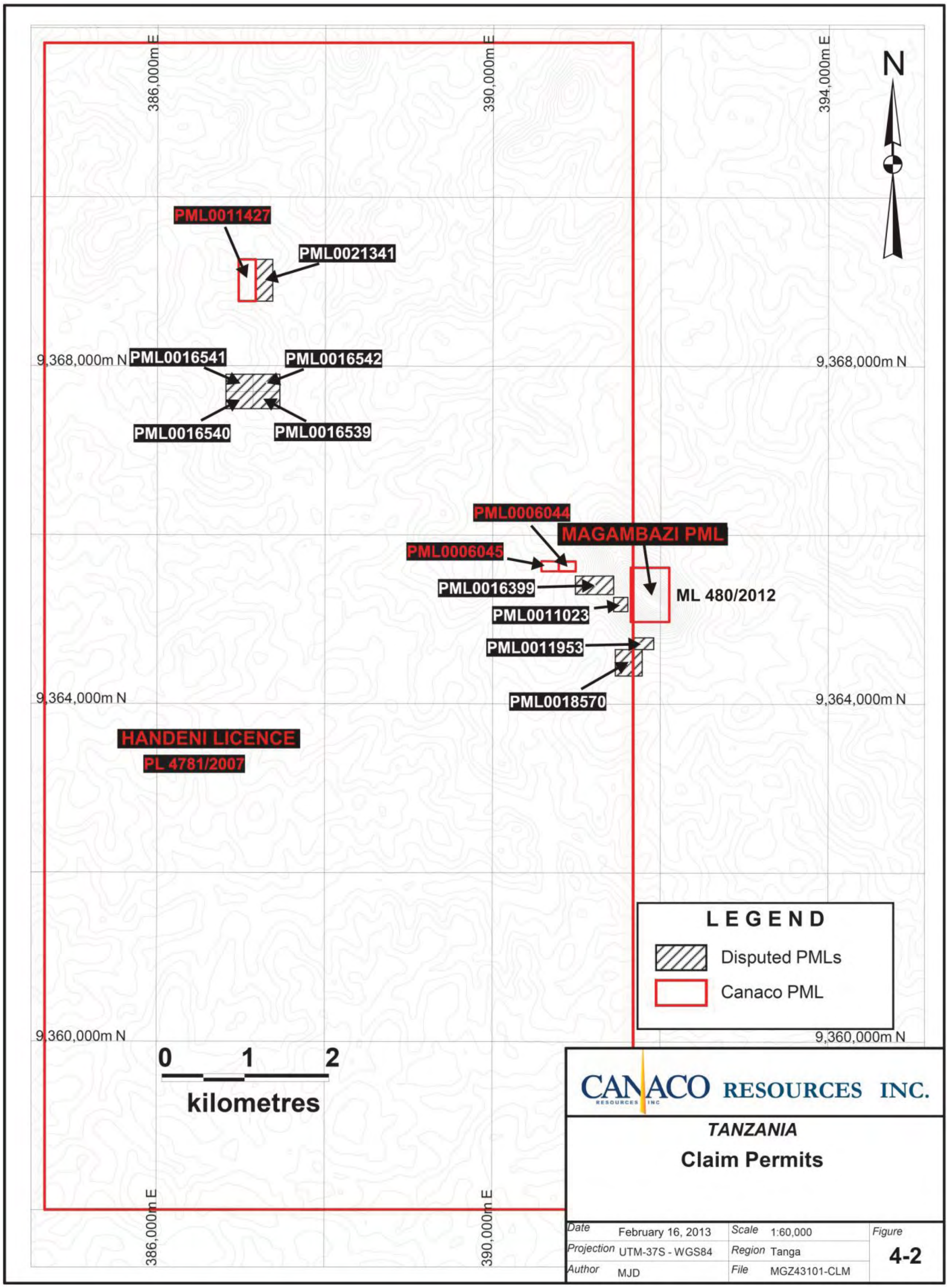
To summarize, in terms of land holdings and cost, a Prospecting Licence grants exclusive exploration rights over an area not exceeding 200 km² for a period of three years, after which time the licence may be renewed for two-year periods with a 50% reduction in area for each extension. Required work expenditures and land fees per square kilometre increase with each renewal. Minimum annual work expenditures are set at US$300/km² for the initial three-year period, increasing to US$1,000/km² andUS$3,000/km² for each successive two-year period. Annual land rents are US$20/km² for the initial three-year period, increasing to US$30/km² and US$50/km² for each successive two-year period. A Mining Licence can be granted for a period not exceeding ten years, renewable for a period of up to ten years, on presentation of a suitable feasibility study, environmental impact study and employment plan (Taylor, 2009).

4.2.2 Handeni Property Tenure Rights

The property consists of two key tenured blocks known as Handeni and Magambazi. These areas are outlined in Figure 4-2 and Table 4-1. The Handeni Prospecting Licence (PL 4781/2007; covering an area of 96.92 km^2 in May 2012) is 100% owned by Canaco, having been acquired from Midlands Minerals Tanzania Limited with official transfer approved on August 16, 2008. This Prospecting Licence covers artisanal workings identified as Majiri Bomba, Kwadijava South, Kwadijava, Magambazi North and Magambazi Central. The adjoining Magambazi tenure is a combined contiguous group of four Primary Mining Licences (PMLs 7811 to 7814), presently held by Denwill Mining Services Limited (“Denwill”). One of the shareholders of Denwill is also the President and a director of Canaco Tanzania Limited. The other shareholder of Denwill is also a director of Canaco Tanzania Limited. On March 1, 2012, the four PMLs were amalgamated into one PML 007EZ. On December 17, 2012 the Magambazi PMLs were converted to Mining License ML 480/2012. Canaco has an option to acquire all of the outstanding shares of Denwill for US$40,000 (which has not yet been exercised). On May 14, 2010, Denwill granted Magambazi Mines Company Limited (“MML“; a Tanzanian company formed by the local miners), a 2% royalty over mineral products that may be produced from the Magambazi property. An initial advance royalty payment of US$140,000 was paid to MML in January 2010, and to date an aggregate of US$1,040,000 advance royalties payment have been made to MML. Canaco has agreed to grant Abdallah Omary Kigoda a 2.0% net smelter royalty for minerals recovered from the 0.07 square kilometre area of the former PML 0010145 held by Kigoda.

Twelve Primary Mining Licences (PMLs 6044, 6045, 11023, 11427, 11953, 16399, 16539, 16540, 16541, 16542, 18570 and 21341) exist within the Handeni Prospecting Licence, and are owned by other parties (Figure 4-2). Six PMLs exist on alluvial workings west and south of Magambazi, and four exist on Kwadijava South while two others exist at the Kwadijava surface workings area.

Figure 4-2: Property Tenure Map



Source: Canaco, 2013.

As noted in a letter from Lawfields Attorneys-at-Law (Tanzania) on May 10, 2012, two of the licences have technically expired (6044 and 6045; however, Canaco understands at this writing that they have been renewed. In total, nine PMLs were issued after Canaco's PL 4781/2007 was granted in November 22, 2007. In their title opinion, Lawfields note that these nine PMLs are illegal and their ownership is currently being addressed by the Commissioner for Minerals in accordance with the Mining Regulations 2010. They are bound for revocation. Canaco has an option to acquire the three PMLs that were issued before PL 4781/2007 was granted in November 22, 2007. None of these PMLs coincide with the mineralised area of the estimated mineral resource that is the subject of this report.

The Prospecting Licence corners, shown in Table 4.1, for PL 4781/2007 and ML 480/2012 were established by GIS coordinate points, and have not been surveyed or marked on the ground. Both Licence types have required rentals, other associated obligations, as well as payments that require fulfilment in order to maintain and renew tenure. Title information was provided by Canaco and a copy of a recent title opinion was provided by Lawfields. A formal title search was not completed by the author. Complete title information and details of the terms of any property agreements can be obtained from Canaco or its solicitor. The claim information provided by Canaco was confirmed by Lawfields, following Lawfields' searches at the Ministry of Energy and Minerals and review of records maintained by the Tanzanian Commissioner for Minerals. The Handeni and Magambazi licences were reported by Canaco to be in good standing as of May 10, 2012, and in the intervening time the only change is the conversion of the provisional PML 007EZ licence number to the official ML 480/2012.

Table 4.1: Property Tenure Location and Status

Tenure	Owner	Tenure type	Status	Area	Corner	Corner Coordinates	
						Latitude S	Longitude E
PL 4781/2007	CTL	Prospecting Licence	Start 22/11/2007	96.92 km^2	A	5° 40' 48.00"	37° 57' 27.00"
			Exp. 21/11/2013		B	5° 40' 48.00"	38° 01' 15.00"
			(First renewal)		C	5° 48 18.00"	38° 01' 15.00"
					D	5° 48 18.00"	37° 57' 27.00"
ML 480/2012	Denwill	Mining Licence	Start 17/12/2012	29.722 Ha	A	5° 44' 10.50"	38° 01' 29.00"
			Exp. 16/12/2022		B	5° 44' 31.50"	38° 01' 29.00"
			(First renewal)		C	5° 44' 31.50"	38° 01' 14.08"
					D	5° 44' 10.50"	38° 01' 14.08"

Note: The tenure positions noted above refer to those shown in current title documents. The prospecting licence is issued for three years and the mining licence for five years.

4.2.3 Environmental Liabilities

Canaco is not aware of any current or past environmental liabilities on the Handeni property.

The Magambazi area of the Handeni property occurs within the 7,500 ha Magambazi Forest Reserve, which is administered under the *2002 Forestry Act*. Proposed mining development in a forest reserve in Tanzania requires the preparation and submission of a Tanzanian Environmental Impact Assessment ("EIA") in accordance with national regulations. The EIA was submitted in February 2012 to the National Environmental Management Council of Tanzania. On August 27, 2012, Canaco received an EIA certificate from the Tanzanian government for the entire Handeni Property, including the Magambazi Project. Pursuant to receipt of the EIA certificate, four primary mining licenses related to the Magambazi Project on the Handeni Property were converted into a mining license covering 0.30 square kilometres. Canaco is now required to produce an Environmental Management Plan that will then be incorporated into the Forest Reserve Management Plan, prior to commencement of development activities.

Canaco has also initiated a program of environmental baseline and field studies such that it can complete a full Environmental Impact Assessment for the project at a future date, in concert with engineering development work and in accordance with international standards. This program is outlined in more detail under Section 20, Environmental, Social & Community Issues.

4.2.4 Exploration Permits and Significant Risk Factors

Handeni Property exploration work described in this report and conducted under Canaco's supervision has been completed in accordance with Tanzanian Mining Law through the granting of the Prospecting Licence.

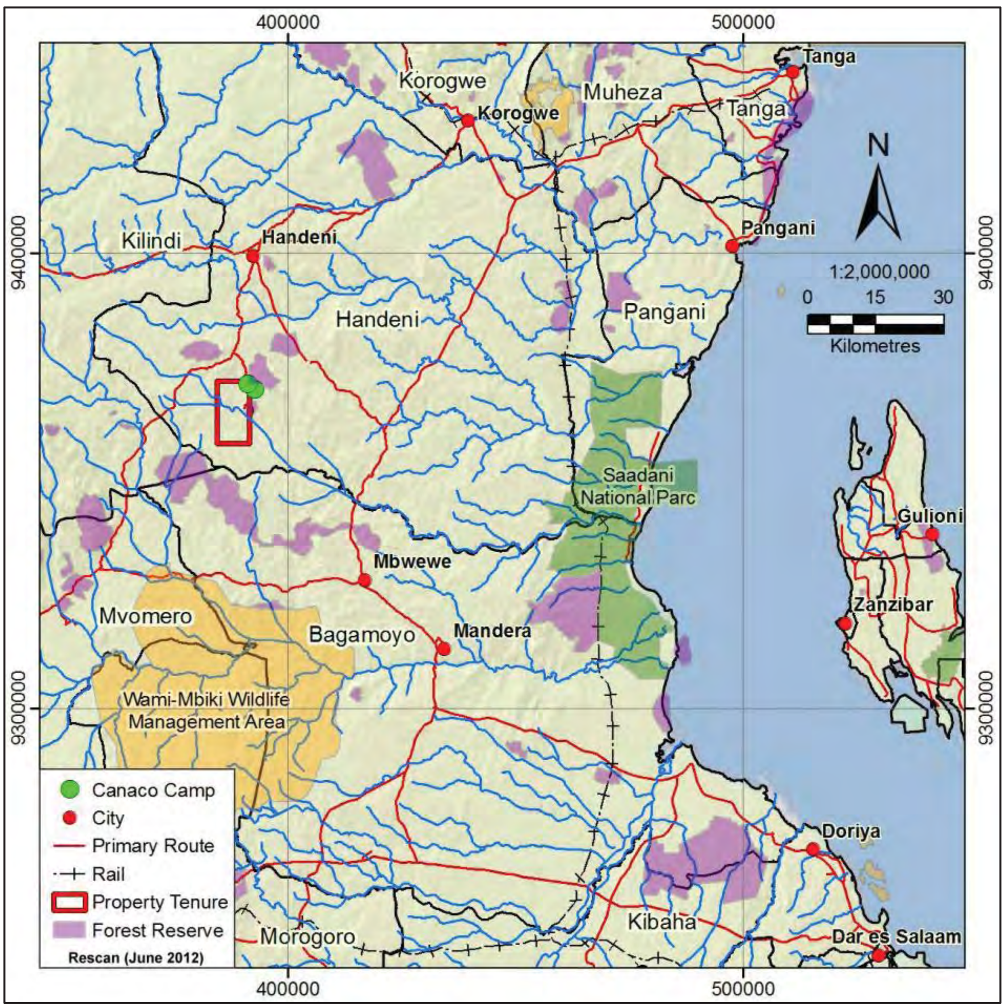
No risk factors are known that may affect access, title, or the right or ability to perform work on the property. A discussion of potential risks and opportunities that may be related to this project is presented in Section 25.2 to provide further clarification for the reader.

5 ACCESSIBILITY, CLIMATE, LOCAL RESOURCES, INFRASTRUCTURE & PHYSIOGRAPHY

5.1 Accessibility

The Handeni project is located in the province of Tanga, Tanzania, approximately 95 km inland from the coast as shown in Figure 5-1. This project consists of five mineral concessions covering an area of 97.6873 km^2 centred at longitude 37.9900°E, latitude -5.7447°S, WGS84 datum, or 388,000mE and 9,365,000mN (UTM37S, WGS84).

Figure 5-1: Property Location & Access Routes



The property lies in the east central coastal area of Tanzania, approximately 160 km northwest of Dar es Salaam and 110 kilometers west-southwest of the port city of Tanga. The project site is rural and sparsely populated, with less than one thousand inhabitants in each of the two nearest towns (Madebe and Nyasa), and a population of approximately 400,000 in the town of Handeni 35 km to the north. Larger population centres near the project site include Dar es Salaam and Tanga with populations of approximately 2.5 million and 245,000 inhabitants, respectively. Each of these population centres could be a source of labour and services required to support development of a mineral resource project.

The rural and isolated project site is accessible through a network of public roadways in the area. Road access to the site is available from two unpaved public roads, with paved highways extending to within approximately 20 km of the site. A paved roadway extends from Dar es Salaam via Highway A7 for 105 km to the west, then north along the Arusha/Moshi Highway for approximately 110 km to the town of Mkata. Access here changes to an all-weather unpaved road heading WNW 50 km to Handeni, and southward 30 km from the town of Handeni to the property camp location at the northeast end of the property. From the camp, various unpaved roads provide access to areas of interest on the property. A vehicle trip from Dar es Salaam to the property takes approximately five hours, with the Dar es Salaam portion slowed by urban traffic congestion, and the Handeni section slowed by variably maintained dirt roads.

From the city of Tanga, the partially paved A14 roadway (portions of which are still under construction) is used in conjunction with unpaved roadways through the towns of Muheza, Korogwe and Handeni to access the project site. The vehicle trip between Tanga and the site takes approximately 3 hours.

Indirect air access to the site is available via scheduled or chartered fixed wing flights to the paved runway at Tanga. The scheduled flights operate between the more populated centres of Dar es Salaam, Arusha, Zanzibar and Tanga. Helicopter charters are also available from Dar es Salaam to a prepared landing area at the village of Madebe, with the flight taking 45 minutes.

5.2 Climate

There are four main climatic zones in Tanzania: a tropical coastal area; a hot and dry central plateau; semi-temperate highland areas; and high, moist lake regions. The Handeni property is located in the coastal and central plateau zones. There are two rainy seasons in the area from November to December and from March through May. In the Tanga Region, most areas get at least 750 mm of rain per year, which increases to approximately 1,100 mm - 1,400 mm along the coast and can exceed 2,000 mm in the Usambara Mountains. For dry areas of the region, such as Korogwe, rainfall is below 600 mm. Maximum rainfall typically occurs in April and May except in the mountains where it tends to peak in November and December.

Due to the moderating influence of the Indian Ocean, temperature variations in the region are relatively minor. In hot months (December to March) the average temperature ranges from 30°C to 32°C and in cooler months it ranges between 23°C to 28°C. The region also has high relative humidity, often reaching 100% (lows are 65% to 70%).

The two meteorology stations closest to the Project are in the towns of Handeni and Morogoro, and are operated by the Tanzanian Meteorological Agency (TMA). The Handeni field data was procured through the TMA and the Morogoro data were procured from the National Climate Data Center (NCDC), operated by the US National Oceanic and Atmospheric Administration (NOAA).

During March 2012, Canaco installed an automated meteorological station at the Handeni camp to record site-specific data. This automated station was installed to specifications set by the World Meteorological Organization. The station uploads data via satellite daily and at this writing its data correlates well with the regional data provided from the TMA station in the town of Handeni located approximately 35 km to the north of the site. The regional historic data from Handeni and Morogoro was used to produce the long-term averages displayed in Table 5.1.

Table 5.1: Typical Local Historical Meteorological Data

	Units	Handeni	Morogoro
Station Information			
Latitude	-	5° 26' 1.200" S	6° 49' 59.880" S,
Longitude	-	38° 1' 58.800" E	37° 38' 60.000" E
Elevation	masl	756	526
Distance from Project Location	-	35 km North	130 km South
Operation Period	-	1980-current for precipitation; 2005-current for all other parameters	1957-current
Data Period Summarized	-	1980-2010 for precipitation 2005-2010 for all parameters other than precipitation	2005-2011
Temperature			
Mean Monthly Maximum	°C	n/a	28[a] (Feb 2006)
Mean Monthly Minimum	°C	n/a	22[a] (Jun 2010)
Mean Daily Maximum Temp	°C	33 (Feb 2005)	34 (Jan 2009)
Mean Daily Minimum Temp	°C	16 (Jul 2006)	16 (July 2011)
Maximum Twice Daily Wet Bulb Temp	°C	27 (Nov 2005)	n/a
Minimum Twice Daily Wet Bulb Temp	°C	14 (Jul 2009)	n/a
Relative Humidity			
Relative Humidity	%	72	n/a
Precipitation			
Average Annual Total Precipitation	mm	767[b]	654
Maximum Annual Total Precipitation	mm	1257[b] (2006)	998 (2006)
Minimum Annual Total Precipitation	mm	530[b] (1983)	334 (2005)
Evaporation (Piche)			
Average Annual Evaporation	mm	1691.6	n/a
Maximum Monthly Total Evaporation	mm	197 (Jan 2009)	n/a
Minimum Monthly Total Evaporation	mm	57 (April 2008)	n/a
Wind			
Maximum Wind Speed	m/s	6[c] (July 2010)	9 (Jan 2006)

Notes: a. 2008 monthly data missing; b. data missing from April 1997 to December 2002; c. twice daily wind speed; d. Data shown is derived from Tanzanian Meteorological Agency historical records at the towns of Handeni and Morogoro. Information for this table was provided by Rescan Engineering in May 2012.

The mean daily minimum and maximum temperatures ranged from 16°C to 34°C with an average relative humidity of 72%. The average annual total precipitation was 767 mm at Handeni station

(756 masl) from 1980 to 2010 and 654 mm at the Morogoro station (526 masl) from 2005 to 2011. The annual average evaporation was 1692 mm at the Handeni station. Maximum wind speed was measured to be 6 m/s at the Handeni station from twice-daily measurements and it was measured to be 9 m/s at Morogoro station from hourly measurements.

Project activity can be conducted year round at the Handeni property.

5.3 Local Resources

5.3.1 Tanzania

Tanzania is one of the poorest countries in the world. The economy depends heavily on agriculture, which accounts for almost half of GDP, provides 85% of exports, and employs 80% of the work force as seen in Table 5.2. Topography and climatic conditions limit cultivated crops to only 4% of the land area. Industry traditionally features the processing of agricultural products and light consumer goods. The World Bank, the International Monetary Fund, and bilateral donors have provided funds to rehabilitate Tanzania's out-of-date economic infrastructure and to alleviate poverty. Long-term growth through 2008 featured an increase in industrial production and a substantial increase in the output of minerals, lead by gold. During the period between 2006 and 2010, World Bank data reflected in Figure 5-2 shows that Tanzanian GDP has grown at an average rate of 6.9 % per year.

The United Republic of Tanzania comprises Mainland Tanzania and the Zanzibar archipelago. Although they form one country, there are two presidents. Zanzibar also has its own parliament and exercises some autonomy. The elections in 2000 were considered to be free and fair in Tanzania. Constitutional restrictions prevented Tanzanian President Benjamin Mkapa from running in the October 2005 election and he was succeeded by Jakaya Kwete who captured 80% of the popular vote. On October 31, 2010, Kwete won the presidential vote for a second term with 62.8% of the popular vote over his nearest rival, Willibrod Slaa, who captured 27.1% of the popular vote.

The historically state-lead economy is becoming more market-based, but remains hindered by poor infrastructure, and a high incidence of HIV/AIDS. Tanzania still hosts greater than 500,000 refugees, more than any other African country. These refugees are predominantly from Burundi and the Democratic Republic of the Congo. There has been progress in privatizing state-owned enterprises. The government generally supports economic reform and has largely followed through on commitments to donors, but interests opposed to liberalization have hindered implementation. Agriculture is the dominant economic sector, employing over 80% of the labour force and accounting for more than 44% of GDP.

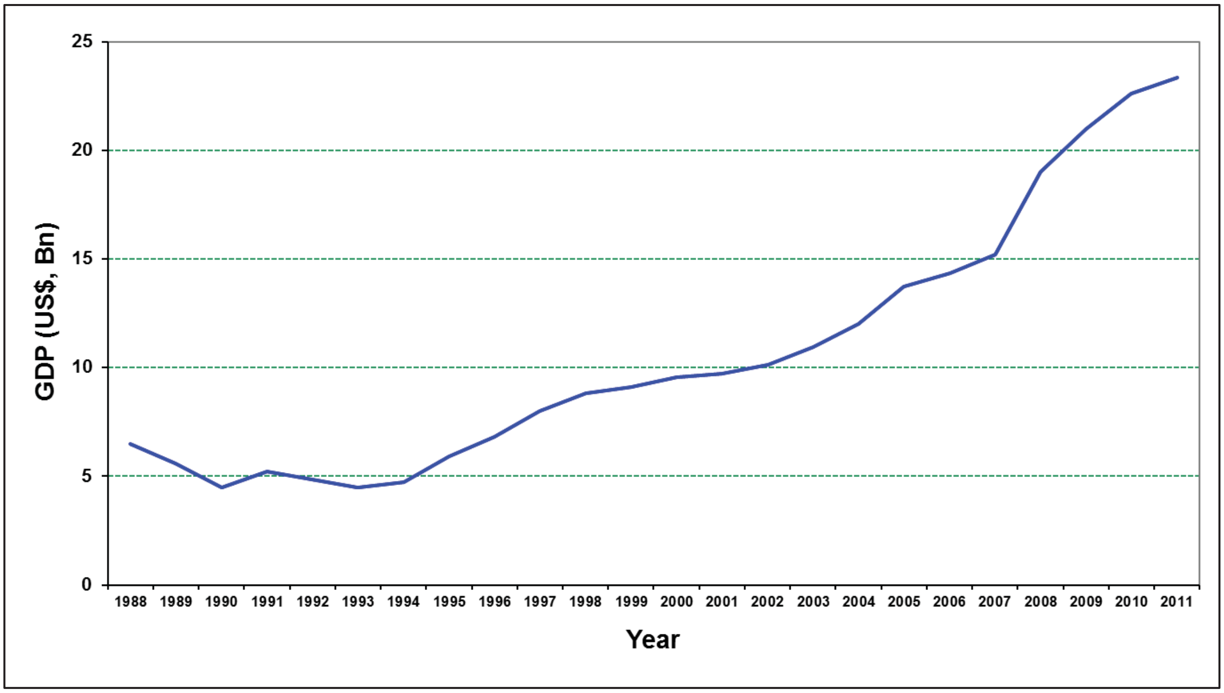
Table 5.2: Tanzanian Economic Information

Population	41,050,000
Total area	945,087 km^2
GDP	$23.33 billion
GDP growth rate	6.1%

GDP per capita	$1,500
Major exports	Gold, manufactured goods, cashew nuts, tobacco, coffee
Exports of goods and services	$5.659 billion
Major export trading partners	China 15.6%, India 11%, Japan 6.1%, UAE 5.0%, Germany 4% (2010)
Major imports	Consumer goods, machinery and transportation equipment, raw materials, crude oil
Imports of goods and services	$8.65 billion
Major import trading partners	China 17.3%, India 15.4%, South Africa 7.9%, Kenya 7%, UAE 4.8%, Japan (2010)
Debt	$9.114 billion

Note: All figures are approximate for 2011 unless otherwise stated and taken from CIA World Fact Book.

Figure 5-2: Tanzanian GDP



Note: All figures are approximate for 2012 and taken from World Bank (http://web.worldbank.org).

The *1997 Tanzania Investment Act* established the Tanzania Investment Centre that identified investment priorities and overhauled the company registration process while also establishing investor rights and incentives in an effort to attract foreign investment. Levels of foreign ownership or control are unlimited, though land ownership remains restricted.

HIV/AIDS is one of the greatest development challenges facing Tanzania today. As at 2007, HIV prevalence in the 15 to 49 age group is estimated at 5.4%, with about 940,000 people estimated to be living with HIV/AIDS. Further, the country has as many as 1.2 M AIDS-related orphans (Avert, 2010).

5.3.2 Tanga Region

The Tanga region is one of the 20 regions in the Tanzanian mainland. The Tanga region lies between latitude 4° and 6° to the south of the equator, and longitude 37° and 39°10" east. The region is relatively small, occupying only 3% (27,348 km^2) of the total landmass of Tanzania. It is bordered by five other regions: Morogoro and Pwani to the south; Kilimanjaro to the west; and Arusha to the north and west. Kenya is located to the north of Tanga.

The main ethnic groups in the region in terms of numbers are Sambaa, Zigua, Bondei, and Digo. The economy of the Region is dominated by agriculture, fishing along the coastal regions and allied activities. Beekeeping is also prevalent in the Handeni area. Some mining is carried out at Magambazi village and in alluvial areas to the west and north.

The region has minor production of three types of minerals: gemstones (including turquoise, kornurupine, ruby and tourmaline), construction minerals (such as sand, gravel and crushed aggregate), and industrial minerals (including limestone, bauxite, zircon and garnet).

A total road network of 3,907 km is present in the Tanga Region. Paved all weather roads account for 352 km, whereas regional and district gravel roads total 939 km, and 2,716 km are feeder roads. The Handeni region is served by two airstrips: one in the city of Tanga (commercial flights daily; paved 1,268 m) and one in Mombo (unpaved, 1,280 m). The Mombo strip is capable of supporting small planes only.

The Tanga region is relatively well supplied with water resources and is a source of hydroelectric power for the national grid system. A total of 97 MW of hydroelectric power are provided by the Pangani Falls and Hale Hydroelectric Power Stations.

5.4 Infrastructure

Figure 5-3 illustrates the major transportation infrastructure including roadways, railways and ports.

Figure 5-3: Tanzanian Transportation Infrastructure

Source: United Nations, Department of Peacekeeping Operations, Map No. 3667, Rev 6.

Tanzania is crossed by a system of generally poorly maintained paved roads (approximately 6800 km), many unpaved roads (approximately 72,000 km), and a small rail system (approximately 3,689 km), including wide and narrow gauges. There are no navigable rivers for large-scale transport of goods.

The country also has three major ports on the Indian Ocean at Dar es Salaam, Mtwara, and Tanga. There are nine airports with paved runways in the country, one of which is at Tanga, and 116 with unpaved runways.

Petrochemical pipelines are limited to approximately 250 km of natural gas pipeline, and 900 km of oil pipeline (as of 2009). The country produces more electricity than it uses, but it also relies on some imported power. High voltage lines are routed generally along the alignment of the Arusha/Moshi highway and some lower voltage branch lines serve some communities near the area for the project.

The closest high-tension electricity power line is located 30 km to the north of the property close to the town of Handeni. It is unlikely that this line will have enough capacity to run the infrastructure for any extraction operation. It is therefore likely that any plant on the Handeni Property will be powered by diesel fuel as a self-sufficient generating station. The exact power demand is presently unknown

Domestic and international telephone and facsimile services are provided by the Tanzania Telecommunications Company Limited. A competitive cell phone network has been established in the country, (including more than ten licensed providers) and it primarily serves the major populations and main transportation routes.

The Canaco field camp consists of a combination of temporary and semi-permanent structures. These include tented modular sleeping quarters, a fully equipped field office; a canteen, several open sided sheds for sample processing (e.g., core sawing); and two sealed containers for storage of unused assay pulps returned from the assay laboratories. Power to the camp is provided by a diesel generator and communication links are provided by mobile phone and a satellite-based broadband connection.

Local labour is plentiful in the area. Most of the technically qualified staff is sourced from the universities of Dodoma, Dar es Salaam and Mwanza. Contract staff from North America, Europe, and Australia is frequently brought to the project to provide further assistance.

If the Handeni Project proves to be economic, significant space exists on the Handeni licence to accommodate mineral processing facilities including a process facility as well as impoundment of tailings and waste materials if required. A hydrogeological program is currently underway to identify a suitable water supply source with the goal of using it to support commercial activities if they prove to be practical.

5.5 Physiography

The Handeni region is slightly elevated and inland from the relatively flat topography of the coastal area. Topography is characterized by gently rolling plateaus, with an average elevation of

600 m, cut by minor seasonal dendritic drainages. Locally, steep knolls a few hundred metres high rise above the plateaus, and generally represent a more resistive underlying geological assemblage. At Magambazi Hill (850 m), artisanal workings are found to be on or near such knolls as seen in Figure 5-4. Vegetation consists of moderate to loosely spaced indigenous tropical trees, with sufficient light penetration to provide for full grass cover. Saprolitic/lateritic soil cover is extensive, with well-drained cover.

Figure 5-4: Magambazi Hill Looking Northwest

Note: Magambazi North is present on the right, the central hill is Magambazi Central and the main Magambazi mineralised zone is present to the left. Artisanal bedrock workings are present to the left of centre and the processing area is seen in the bottom right. Source: Archibald, 2012.

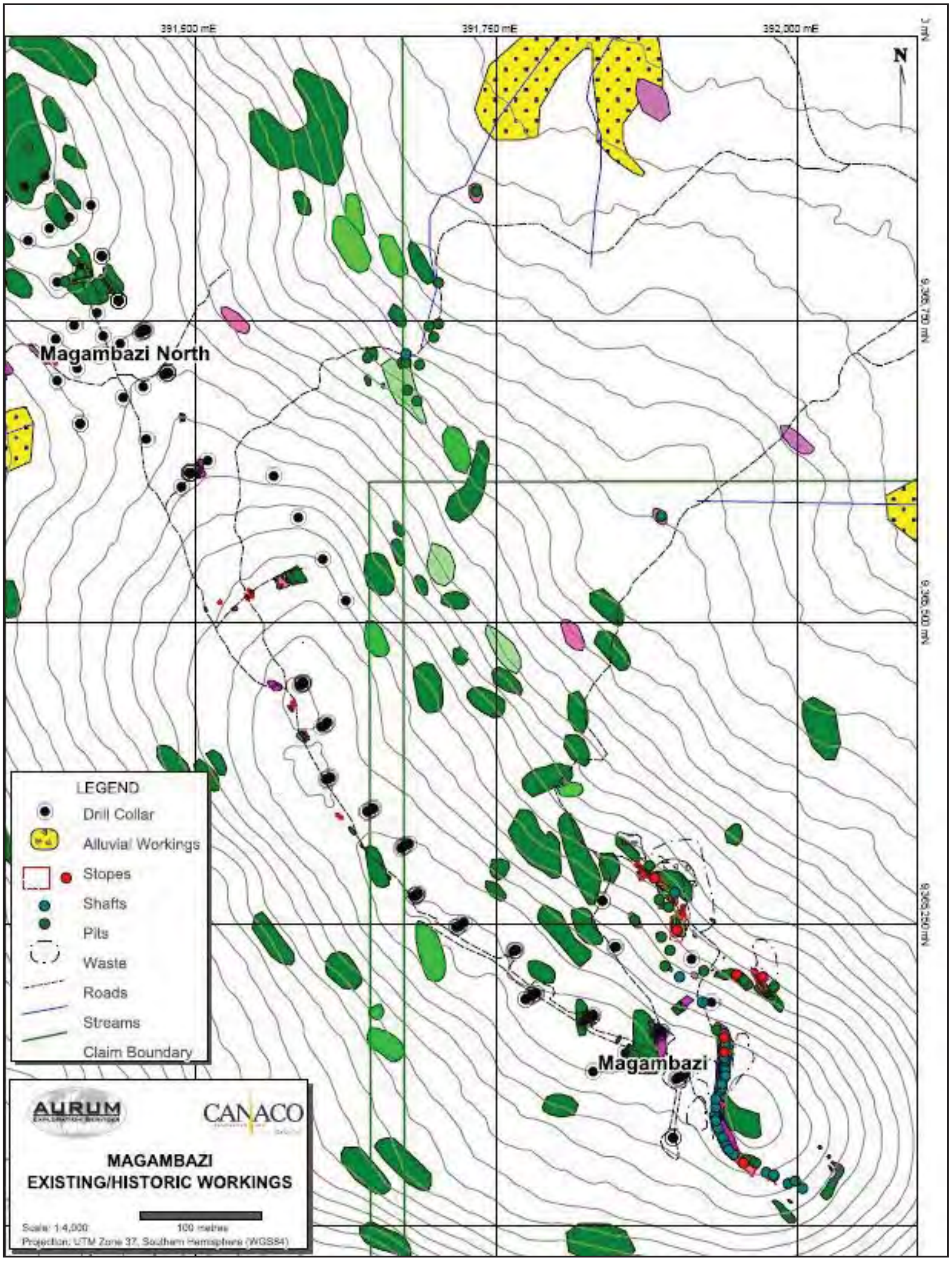
6 HISTORY

Gold was discovered by locals in the Magambazi area in 2003, spurring a gold rush with intense alluvial and hard rock mining (Figure 6-1). This activity was still underway during each of the Qualified Person property visits for this project, and a number of the artisanal areas have been identified on the property as current mineral exploration prospects, namely at Magambazi, Semwaliko (now known as Kwadijava), and Majiri (Figures 6-1 and 6-2). An active artisanal mining village is present at Magambazi, the principal focus of Canaco's mineral exploration efforts in the area and the subject of this report. Production figures are not available from the artisanal work. The main historical and present workings for the property at Magambazi and Kwadijava are illustrated in Figures 6-2 and 6-3.

Figure 6-1: Native Gold Recovered from Bedrock Workings at Magambazi

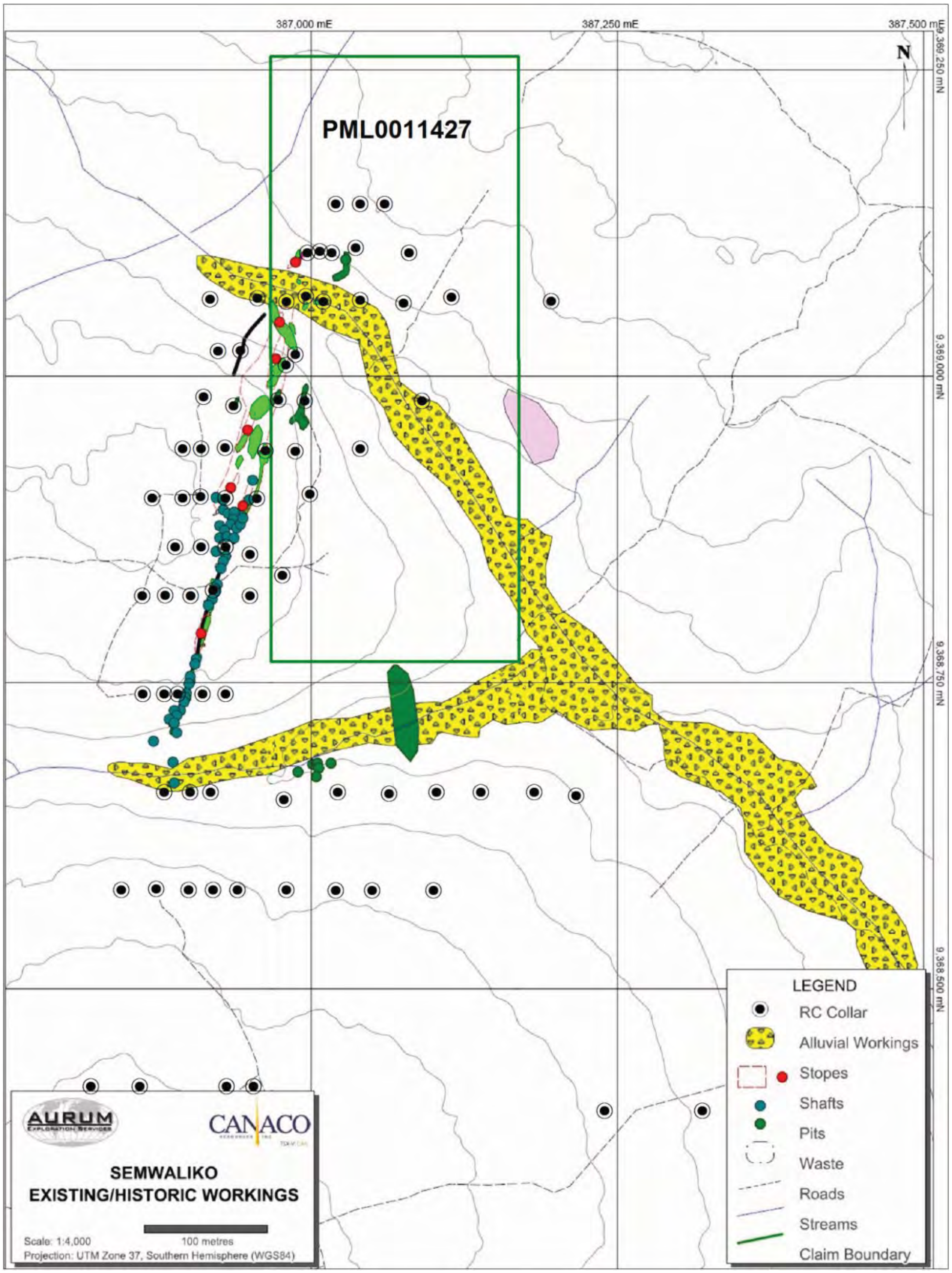
Source: Archibald, 2012.

Figure 6-2: Artisanal Workings in the Magambazi Area



Note: The large polygons represent outcrop/subcrop: greens are amphibole gneisses and pinks are feldspathic gneisses. Source: Modified from Archibald, 2011.

Figure 6-3: Kwadijava Area Artisanal Workings



Note: The location of PML0011427 relative to the Handeni Property can been seen in Figure 4-2.
Source: Modified from Archibald, 2011.

Midlands Minerals Corp. was granted a preliminary prospecting licence over the Handeni Project area on July 14, 2005. No statement by Midlands Minerals Corp. has been found in the public record regarding execution of mineral exploration at the Handeni property prior to optioning the property to Canaco in 2007. The author and Canaco are unaware of any company owning mineral rights or the licence area prior to 2005.

On March 13, 2007, Canaco entered an option agreement to acquire a 60% interest in the 2,700 km^2 New Kilindi Prospecting Licence from Midlands Minerals Corp. To earn the interest, Canaco was required to spend $2.5 million in work programs, including 5,000 m of drilling over a six year period and make a cash payment of $100,000 over two years and issue 200,000 common shares of Canaco were also included in the terms of the agreement. An additional 15% could be earned by completion of a feasibility study.

Subsequently, in April 2008, Canaco renegotiated the Kilindi licence agreement that resulted in a reconfiguration of Canaco's landholdings in the Handeni area and the acquisition of a 100% interest in a 196-square-kilometre prospecting licence that now forms part of the Handeni Project, the core of Canaco's exploration program in the region. In exchange, Canaco relinquished its interest in the non-core peripheral properties. A finder's fee of 75,000 common shares was to be paid, of which 25,000 common shares were issued at the time of entering into the agreement, and the final 50,000 common shares were issued in December 2010 on receipt of regulatory approval by the TSX Venture Exchange. In 2010 on renewal of the licence, non-core peripheral properties were relinquished and the licence consists of 100 km^2.

On July 26, 2007, Canaco entered into an Option Agreement (the "Magambazi Agreement") to acquire a 100% interest in the Magambazi primary mining licences (the "Magambazi PMLs"). Magambazi was adjacent to the eastern boundary of Kilindi. The agreement was signed with the local miners working the area. Magambazi hosts both active artisanal alluvial and hard rock deposits. Terms of the option required a cash payment of $136,000 over two years for the right to explore. At any time prior to the second anniversary of the agreement, Canaco had the right to purchase a 100% interest in Magambazi for US$1.8 M, subject to a 2% NSR. On February 12, 2008, the local miners transferred the Magambazi PMLs to Magambazi Mines Company Limited ("MML") and transferred the Magambazi Agreement to MML. Canaco paid a total of US$256,000 for the right to explore the Magambazi properties over the three-year period ended July 26, 2010. In January 2010, Canaco paid MML an additional US$140,000 to extend the right to explore the Magambazi properties to July 26, 2011. On April 22, 2010, MML entered into a Transfer Deed with Denwill Mining Services Limited ("Denwill"), a Tanzanian company formed by two local Tanzanians, whereby MML agreed to transfer the Magambazi PMLs to Denwill for US$1.8 million, subject to a 2% NSR. MML may request for an advance on the royalties for an amount up to US$900,000 at any time before commercial production commences on the property. If the US$1.8 million payment to acquire the Magambazi PMLs is made before July 26, 2011, then the US$140,000 paid.

On February 11, 2011, as directed by the Tanzanian Ministry of Energy and Minerals, Canaco entered into an agreement with Abdallah Omary Kigoda ("Kigoda"). Canaco agreed to pay Kigoda US$2.0 million in cash (paid in February 2011) and a 2.0% net smelter royalty for minerals recovered from the 0.07 km^2 area of the former PML 0010145 held by Kigoda. These payments are compensation for the cancellation of the former PML and an acknowledgement that substantial development work on the conflicted mineral right had already been undertaken by Kigoda.

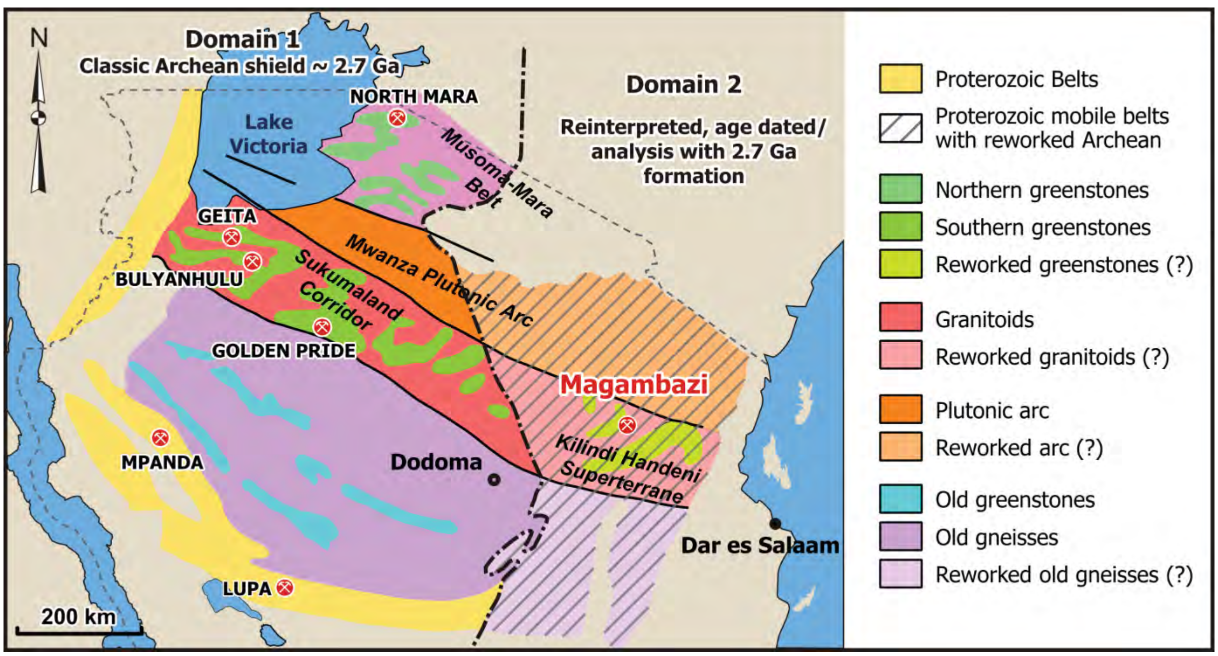
The Option Agreement will expire on April 28, 2020. Denwill also agreed to convert the Magambazi PMLs into a mining license. On December 17, 2012, the Magambazi PMLs were converted into a mining licence covering 0.30 square kilometres pursuant to receipt of the EIA certificate.

7 GEOLOGICAL SETTING & MINERALISATION

7.1 Regional Geology

The Handeni property is located in what has traditionally been classified as part of the Proterozoic Usugaran-Ubendian System (Pinna et al., 2004). This assemblage of rocks occurs south and east of the Lake Victoria Archean craton, hosting orogenic gold deposits such as Geita and Bulyanhulu (Figure 7-1). The Usugaran system is north-south trending, and the geology of this region represents a non-traditional exploration environment dominated by high-grade metamorphic (granulite to amphibolite facies) rocks. Granulites and biotite gneisses of pelitic to volcaniclastic origin make up a larger portion of the Usugaran System, with lesser volumes of amphibolite, metamorphosed mafic volcanics, gabbro and dolerite and minor ultramafic rocks. Metamorphic grades are typically upper amphibolite with lesser granulite. Major structural trends are dominantly southwest. Traditionally, rocks of granulite facies in the Usugaran System are rich in a variety of coloured gemstones, and these have been mined for decades.

Figure 7-1: Schematic Map of Tanzanian Craton



Source: D. Groves, 2010.

Recent academic studies, e.g., Kabete (2008), highlighted the area as prospective for metamorphosed Archean orogenic gold deposits within the Sukumaland Corridor. The Sukumaland Corridor is the host to major gold deposits in the Lake Victoria Goldfields, e.g., Bulyanhulu, 16.46 Moz Au; Geita, 17.0 Moz Au; and Golden Pride, 1.94 Moz Au (all data is taken from company annual reports for combined resource and reserves as of December 31, 2009). The Handeni property lies in this proposed prospective area, approximately 500 km along strike from the nearest major mine (see Figure 7-1).

The following is an excerpt from an extended abstract discussing new ideas on the provenance of the Handeni area and implications for gold mineralisation (Groves et al., 2008).

"Traditionally, exploration for Precambrian orogenic gold deposits (Groves et al., 1998) has been concentrated towards the centre of cratons away from cratonic margins in sub-greenschist to greenschist-amphibolite transition domains (Goldfarb et al., 2005) where most giant gold deposits have been found; for example Timmins in Canada, Kalgoorlie in Western Australia, Geita in Tanzania, and Ashanti in Ghana. However, recent exploration has increasingly uncovered orogenic-style gold deposits in amphibolite to lower-granulite facies terranes external to accepted craton margins. An important example is the World-class Plutonic deposit (>10 Moz Au) of Western Australia in Archean rocks reworked in the Paleoproterozoic by tectonism related to the Capricorn Orogeny, but on strike to the north of the major gold producing Eastern Goldfields Province. A more recent discovery is the Tropicana prospect (>4 Moz Au) to the south of the Eastern Goldfields in Archean rocks tectonically reworked in the Neoproterozoic Albany-Fraser Mobile Belt. It is debated whether these are Archean gold deposits overprinted by Proterozoic orogeny (e.g. Vielreicher et al., 2002) or Proterozoic gold deposits, because deposit-scale evidence is often equivocal. However, it is noticeable that these examples, as well as several in Proterozoic mobile belts of Africa, are sited almost exclusively in domains adjacent to well-endowed Archean cratons. These regional relationships strongly suggest that the deposits are metamorphosed or reworked Archean orogenic gold deposits rather than epigenetic deposits of Proterozoic age formed in largely reworked continental crust.

Recent studies in the Archean Tanzania Craton by Kabete (2008) and Kabete et al. (2008) reinterpret its tectonic framework in terms of eight superterranes.

In the north, the generally low metamorphic-grade granitoid-greenstone belts are divided into three superterranes of which the southernmost, Lake Nyanza Superterrane, contains most of the World-class orogenic gold deposits including Geita, Bulyanhulu and Golden Pride. Geochronological studies (Kabete et al., 2008) strongly suggest that the higher metamorphic-grade Kilindi-Handeni Superterrane on strike to the ESE represents Archean belts overprinted by Neoproterozoic orogeny related to the East African Orogen further east, forming what is informally referred to here as the "Sukumaland Corridor". This is confirmed from available regional aeromagnetic data that show curvilinear magnetic signatures in the Kilindi-Handeni Superterrane more similar to the Archean terranes than to Proterozoic mobile belts. Interestingly, a number of newly recognised gold prospects, exploited on a small scale by artisanal miners, are sited at several locations in the overprinted south-southeastern extent of the Sukumaland Corridor. Although poorly exposed, the terrane comprises curvilinear metamorphosed supracrustal sequences, including amphibolites, within granitic gneisses which are transected by broadly ENE-trending shear zones, very similar geological settings to those of the world-class gold deposits in the lower metamorphic-grade terranes to the west-northwest. The gold mineralisation of the Handeni

Project, including Magambazi, thus demonstrates the potential for discovery of World-class, overprinted, Archean orogenic gold deposits in non-traditional exploration terranes in Tanzania, just as has occurred in recent years in Western Australia."

A more detailed and recent explanation of the tectonic and temporal framework of the Tanzanian Shield and the contained gold mineralisation is presented by Ketebe et al (2012). In this study, the Kilindi-Handeni Superterrane is subdivided into three newly characterized terranes; Mkurumu-Magamba, Songe, and Ukaguru. The Mkurumu-Magamba Terrane, and to a lesser extent the Songe Terrane, contain restricted zones of greenstone and quartzofeldspathic rocks that exhibit overgrowths of amphibolite, kyanite and garnet on early-formed metamorphic fabrics. These overgrowths are interpreted to be spatially associated with gold mineralisation in the Mkurumu-Magamba Terrane (e.g., Mkurumu, Negero and Magambazi prospects).

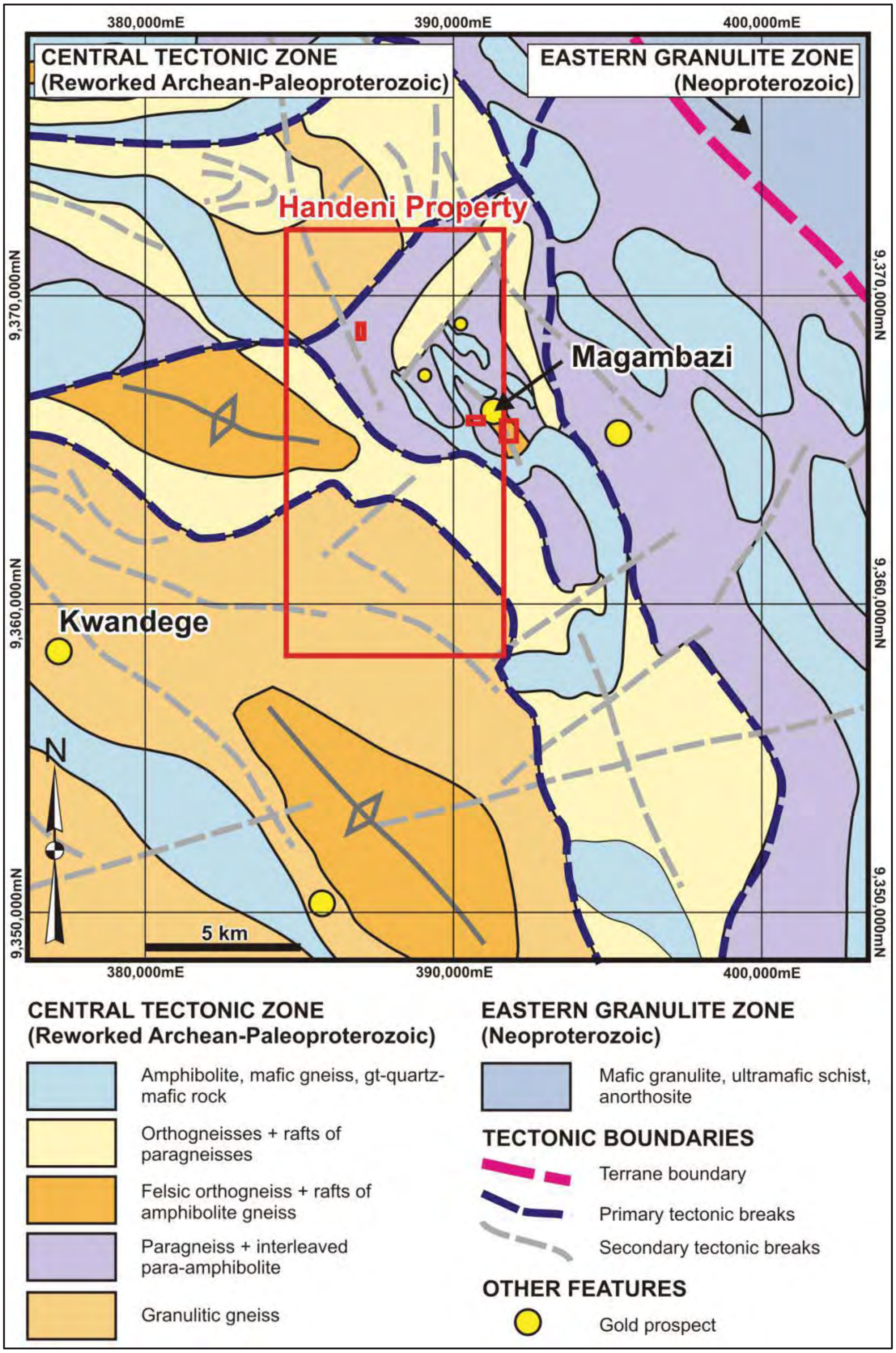
The Handeni region now, and over the last few years, is only beginning to receive the attention of mineral exploration companies and very little is known of the local geology as it specifically relates to the potential to host mineralisation. The geology and location of known gold discoveries, occurring in both alluvial and in bedrock settings, does suggest the primary mineralisation is controlled by regional structures in dominantly mafic host rocks.

7.2 Property Geology

The property geology is a reasonable representation of the local geology in the Kilindi and Handeni districts as illustrated in Figure 7-2. Lower resolution mapping by the Geological Survey of Tanzania supplemented by Canaco geologists indicates the area is covered by a thin veneer of lateritic/saprolitic that covers much of the property, and contains isolated outcrops in lowland areas and significant outcrops on the tops and sides of the hills in the property. When the regional mapping performed by the Geological Survey of Tanzania is combined with the regional airborne geophysics (Kebete et al., 2012) the resulting geological compilation appears to be correspond closely (Figure 7-2). Foliations mapped across the property are quite varied, typical of highly deformed gneissic terrains, and indicative of assemblages that are highly folded and faulted.

The majority of known geological information was compiled from the Magambazi area of the project during exploration conducted by Canaco geologists and contractors, where topographic relief and existing workings (Figure 7-3) have allowed a detailed examination of outcrops (Figure 7-4). This area is structurally complex, and comprises a sequence of garnetiferous amphibolite with localized composition up to garnerite and variably characterized gneiss, including localized biotite, amphibole-biotite, and sillimanite±graphite bearing rocks (Figure 7-5). The presence of sillimanite was identified in thin section by Colombo (2011), whereas field identification and an earlier petrographic study by Klominsky (2010) suggested the mineral was kyanite. Until further mineralogical tests (X-ray diffraction) are performed, it is recommended that the aluminosilicate Al_2SiO_5 is named sillimanite. Partial migmatization is widespread and augen and porphyroblastic textures give rise to granite-like gneisses (Klominsky, 2010).

Figure 7-2: Property Regional Geology

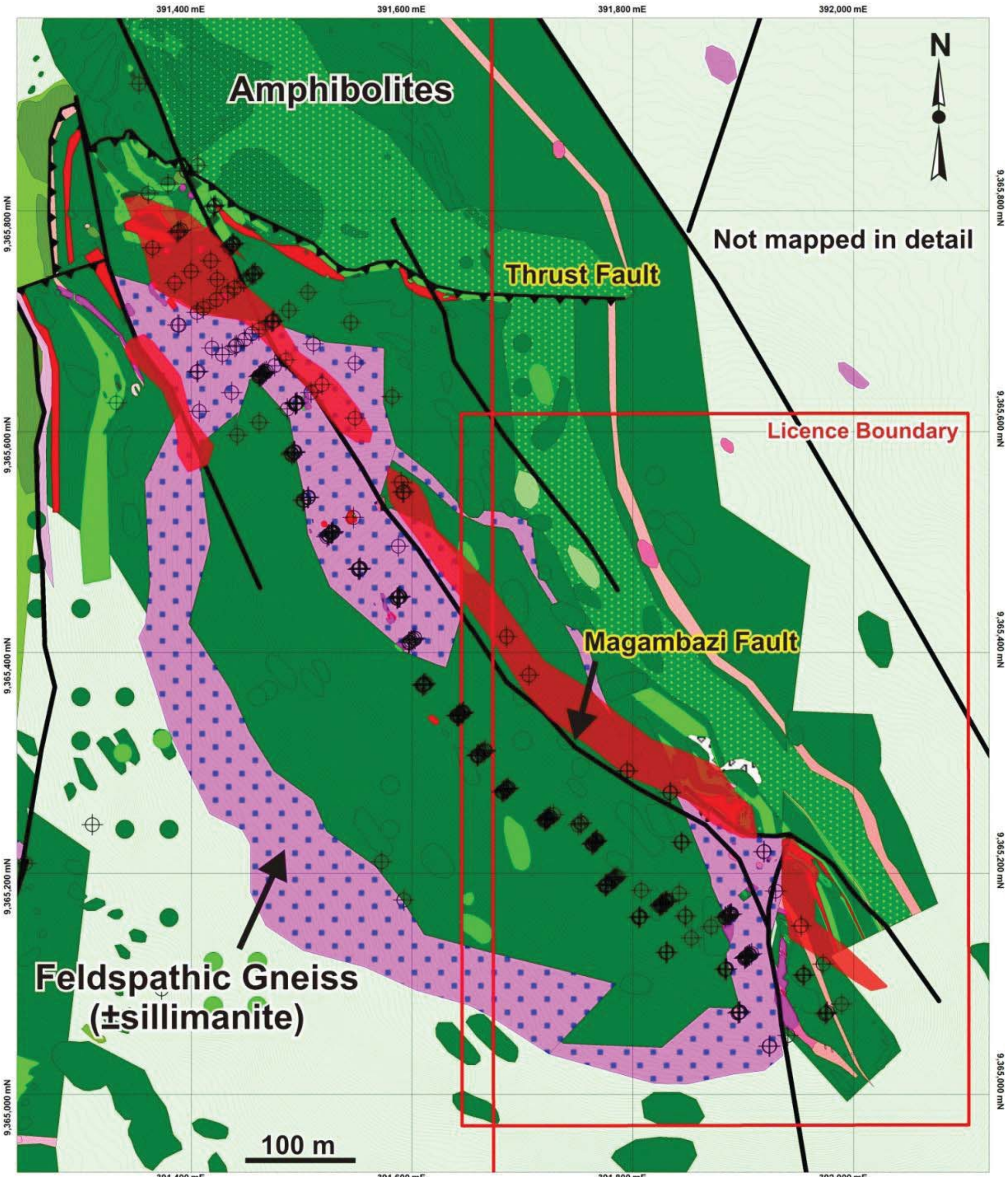


Source: After Kabete et al., 2012.

Figure 7-3: Artisanal Workings at Magambazi with Local Miners Working the Magambazi Mineralisation Adjacent to the Northwest-Trending Magambazi Fault

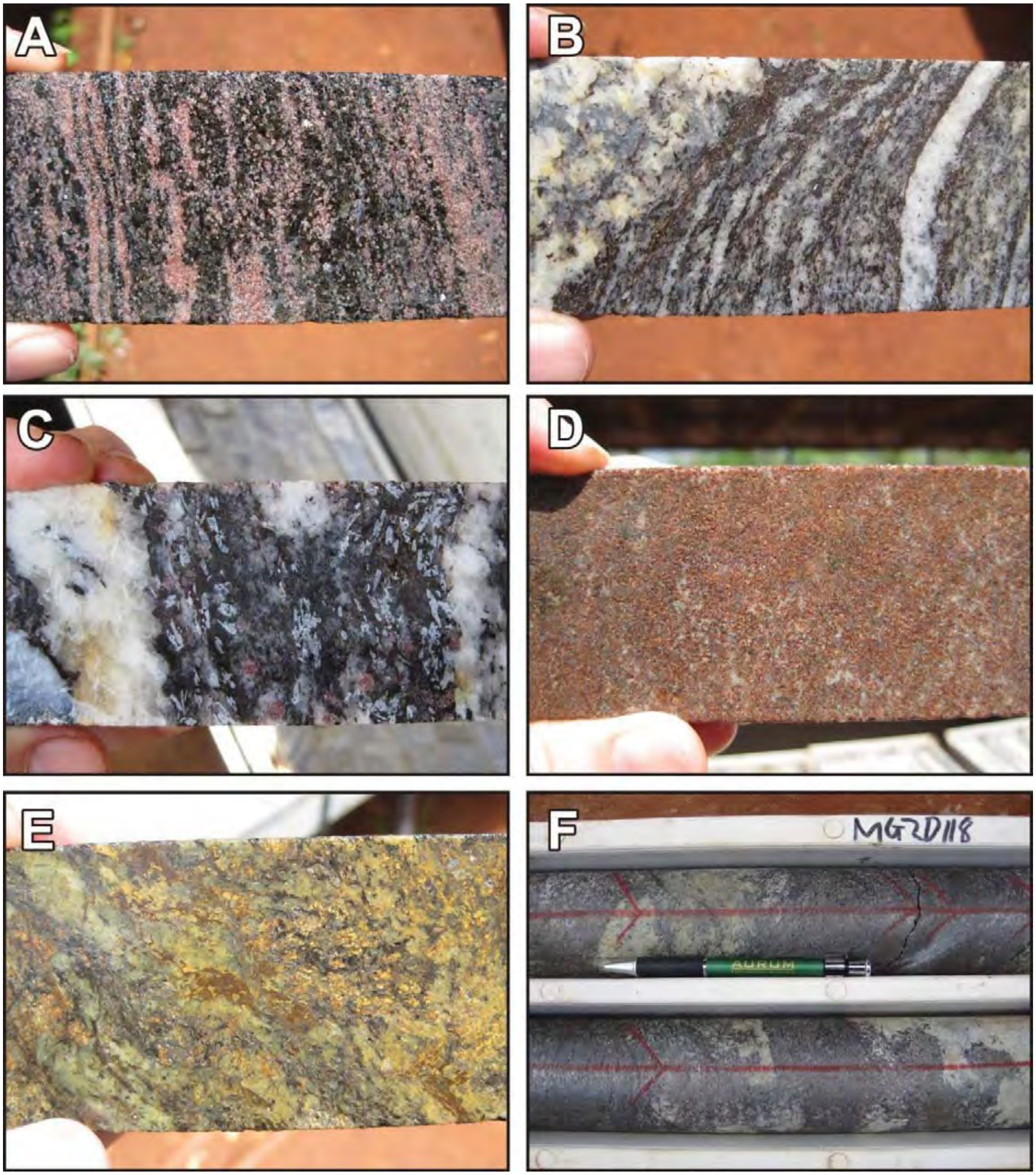
Note: Stretched foliation-parallel auriferous quartz veins are apparent within the bleached GASIL unit.
Source: Canaco, 2012.

Figure 7-4: Surface Geology of the Magambazi Hill



Note: Geological Interpretation by Canaco, with high-grade gold mineralisation (in red) by the author. Feldspathic gneisses (pinks) and variably composed amphibolites (greens). Diamond drill holes collars are also illustrated. Source: Canaco, 2012.

Figure 7-5: Typical Lithologies from the Handeni Property



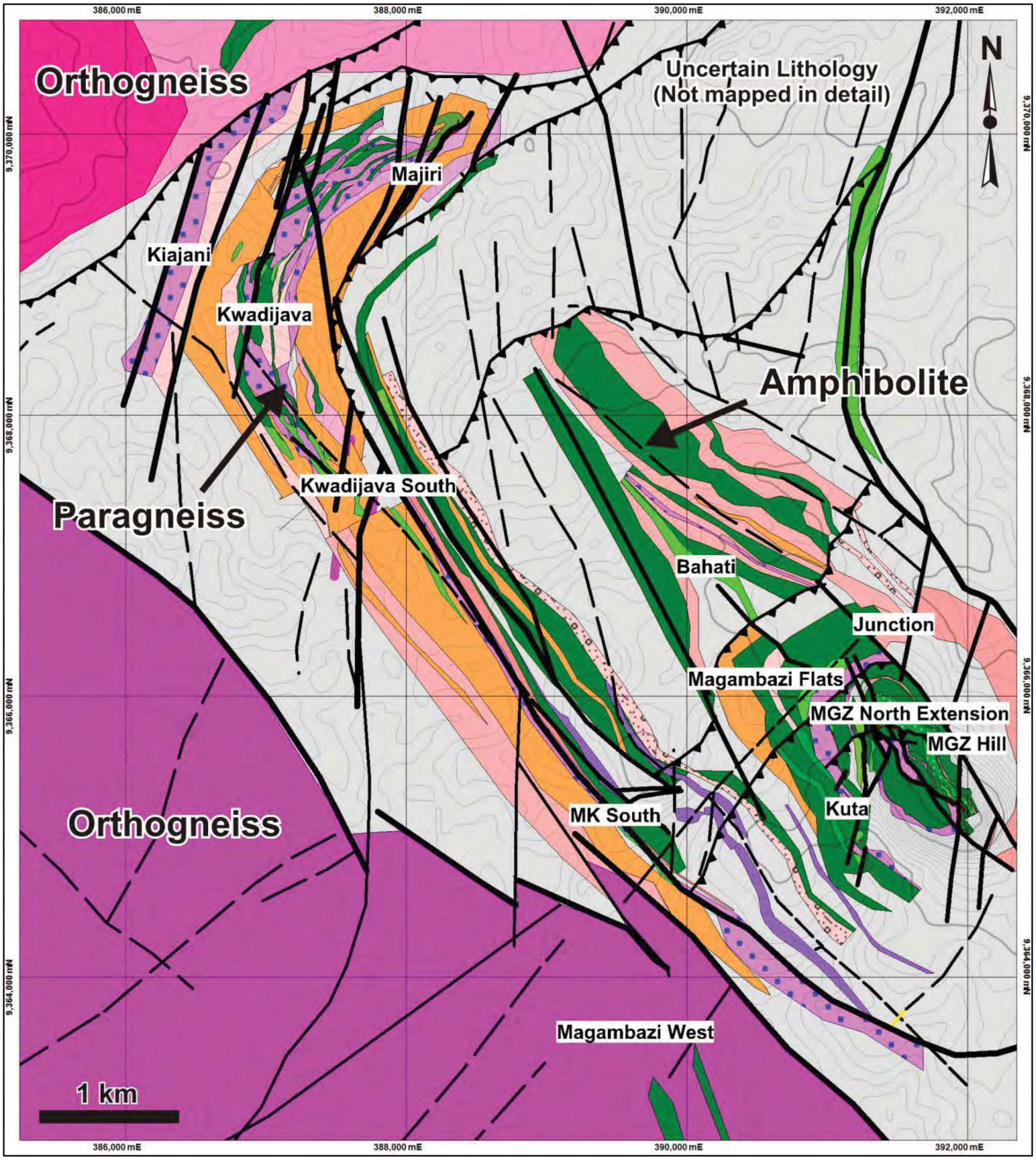
Note: A. Garnet-bearing amphibolite, B. Feldspathic gneiss, C. Garnet-Sillimanite-bearing feldspathic gneiss, D. Garnet-silica rock (GASIL), E. weathered sulphide zone containing graphite, F. Massive graphite with feldspathic gneiss. Source: Archibald, 2011.

Areas of altered amphibolite are notably less foliated, and exhibit less pronounced compositional banding compared to adjacent gneisses, which display extensive ductile deformation. This character variation between the gneisses and altered amphibolite suggests a fundamental difference in the origin and/or history of the parent rocks. The gneisses represent a volcano-sedimentary protolith, whereas the garnet amphibolite probably represents mafic volcanic rocks. A petrographic study by Klominsky (2010) concluded that the metamorphic assemblage present at Magambazi likely formed at amphibolite facies with a pressure of ~0.8 GPa and at a temperature ~650°C, but if the kyanite he identified is sillimanite the pressure would be lower (~0.5 GPa) and the temperature would be unchanged.

The discovery of gold at Kilindi and Magambazi is indicative of a new and emerging exploration environment that appears capable of hosting primary gold mineralisation. Research conducted by Kabete (2008) and Kabete et al. (2012) suggests that the highly endowed Sukumaland Superterrane, the geological host to Tanzania's most significant gold deposits, has been overprinted on its interpreted east-southeastern extension by Proterozoic orogeny. Other newly-recognized gold prospects, exploited on a small scale by artisanal miners, are sited at several locations in this overprinted Archean terrane. Of current interest on the property is the well-exposed Magambazi prospect. Here, high gold-grade sulphide-bearing quartz veins are enclosed in up to 80 m thick alteration zones with lower-grade, sulphide-associated gold mineralisation over a drill delineated strike of 960 m. The host rocks and alteration zones are high metamorphic grade gneisses and unaltered amphibolite.

In the northern part of the property, large hills (monoliths) of granite gneiss trend in an east-northeast direction and are interpreted to be located north of a major regional east-northeast trending structure (Majiri Fault). To the south of this structure, the stratigraphy generally strikes northwest with moderate dips east although dip reversals are common, indicating tight to isoclinal folding along a northwest trending axis. In the Majiri area, south of, but proximal to, the Majiri Fault, the stratigraphy trends east-northeast and dips moderately south. The structure of the area is poorly defined by outcrop mapping, but drilling programs have helped to identify lithologies and controls on mineralisation. The regional magnetic dataset provides comparative analogies to magnetic patterns noted in the greenstone terranes of the Lake Victoria area. However, recent airborne geophysics (magnetic and radiometric) over the northern part of the Handeni property has helped to define the local geological structure (Figure 7-6). The dominant structure in the Magambazi area is a doubly plunging synclinorium with a primary northwest-long axis. A series of isoclinal anticlines and synclines follow similar north or northwest-trends to the Magambazi structure. East-trending, low angle, south-dipping thrust faults have been interpreted at Majiri, and from drilling at Magambazi North. North-northwest trending graphitic shears and east-northeast trending graphitic faults have also been mapped and identified by drilling in the Magambazi area.

Figure 7-6: Simplified Geology Map of the Handeni Property



Note: Significant geological units have been labelled (magenta = orthogneiss; light pink/flesh = paragneiss; green = amphibolite; grey = uncertain lithologies or not mapped in detail). Showings are labelled and in white boxes.
Source: After I. Groves, 2012.

7.3 Mineralisation

The gold mineralisation exposed at Magambazi, through mapping and drilling, has significance with respect to establishing a deposit model that can be applied to exploration in the region and potentially as a deposit with extensions that project onto the Handeni property. Field observations indicate the Magambazi prospect contains numerous significant bedrock artisanal workings that are located on the western flank of an 11 kilometre long geochemical anomaly. Local miners are exploiting gold mineralisation within steeply dipping, north-northwesterly-trending occurrences of sulphide and quartz veins.

From surface, mineralised occurrences are being mined by artisans over widths up to 10 m (Figure 7-3) and these define a north-northwesterly trend with a total strike length of 350 m. Drilling has confirmed that this mineralisation continues at depth, and is traceable laterally beyond the known surface extents of mineralised showings for a distance of 960 m. Mineralisation is characterized as vein-related structurally controlled orogenic gold associated with pyrrhotite, arsenopyrite (löllingite), trace amounts of galena and chalcopyrite, and locally graphite. The immediate host rocks are garnet-silica altered amphibolite, enclosed within a sequence of interbedded paragneiss and amphibolite. Multiple mineralised intercepts have been encountered, and two main types of gold mineralisation are observed from diamond drilling at Magambazi: high-grade gold associated with pervasive silicification on the postulated footwall of the main Magambazi Fault, termed the Magambazi Lode (D. Groves, 2012); and low-grade gold in an apparent stratabound relationship occurring to the west of this fault, which is interpreted to represent the tops of differentiated basalt flows (D. Groves, pers comm., 2012).

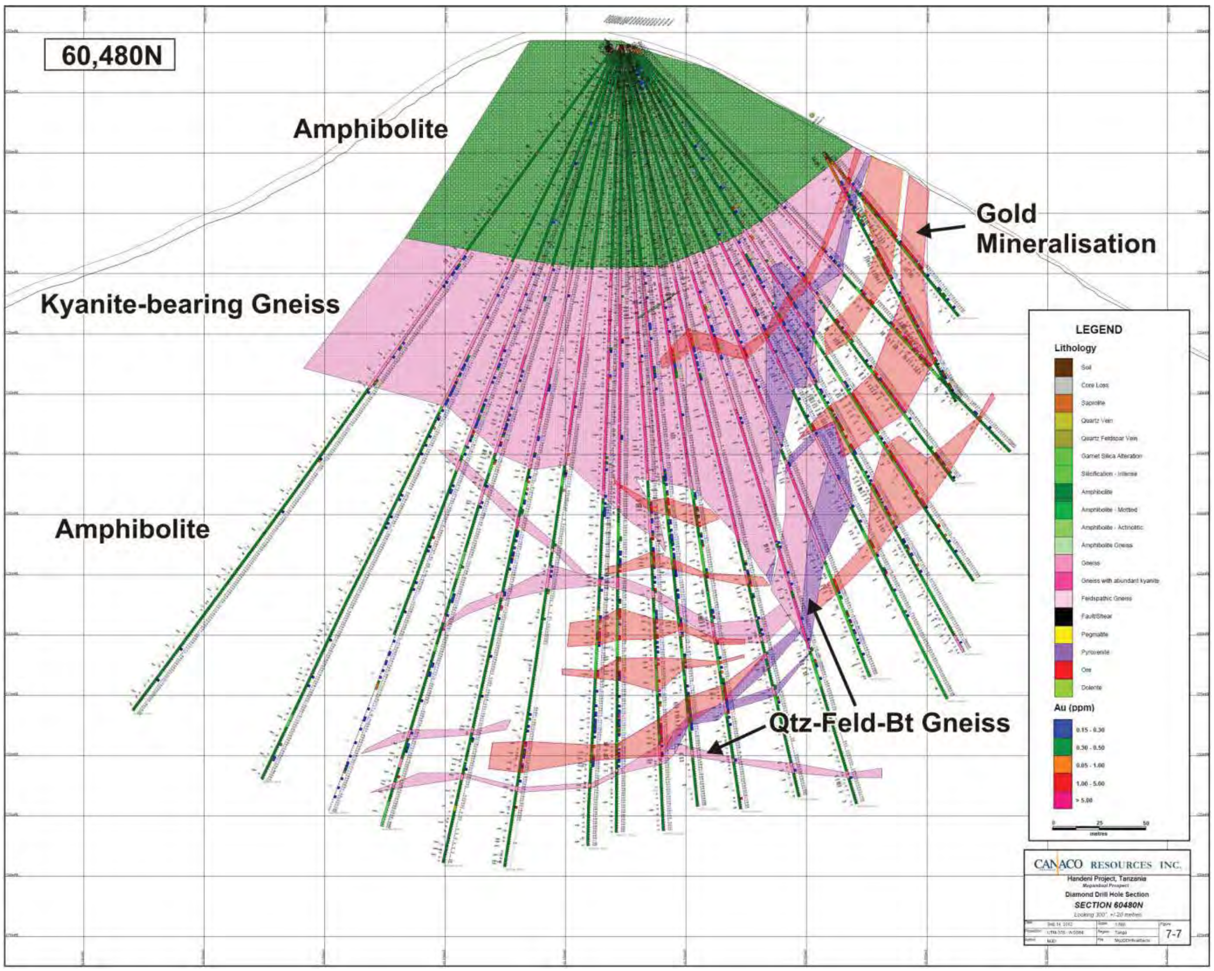
Structurally, two major steep faults trend northwest along the orientation of the mineralised system, although the nature of the rock in the main mineralised zones is competent their actual fault plane is difficult to definitively identify. The alteration and later metamorphism appear to have annealed the areas of significant mineralisation. This, and the decrease in pronounced compositional banding, suggests a high-grade metamorphic overprint of an originally lower metamorphic-grade orogenic gold deposit.

At depth, mineralisation trends at Magambazi and Magambazi North are similar in a northwest orientation, but vary in dip and plunge direction. At Magambazi, mineralisation dips steeply to moderately west, and plunges northwest. In contrast, mineralisation at Magambazi North dips moderately to gently east, and plunges southeast. The fact that the Magambazi North mineralised zone dips in a direction opposite to that of the interpreted main foliation, while also paralleling the trend, suggests the primary depositional environment hosting gold mineralisation likely predated the last major compressive tectonic event.

The planar nature of the early mineralisation could represent a thrust plane, or a primary lithological feature. Initial geological work indicated that diabase sills could have formed the locus for mineralisation, through a competency contrast during brittle deformation. However, additional XRF geochemical interpretation of several profiles at Magambazi suggest that the GASIL horizons might represent the tops of differentiated mafic flows, which underwent seafloor hydrothermal alteration prior to the deposition of the overlying sediments. This interpretation also provides a brittle host rock and impermeable cap for potential mineralisation, but does not preclude the contact acting as a later decollement plane during thrust faulting.

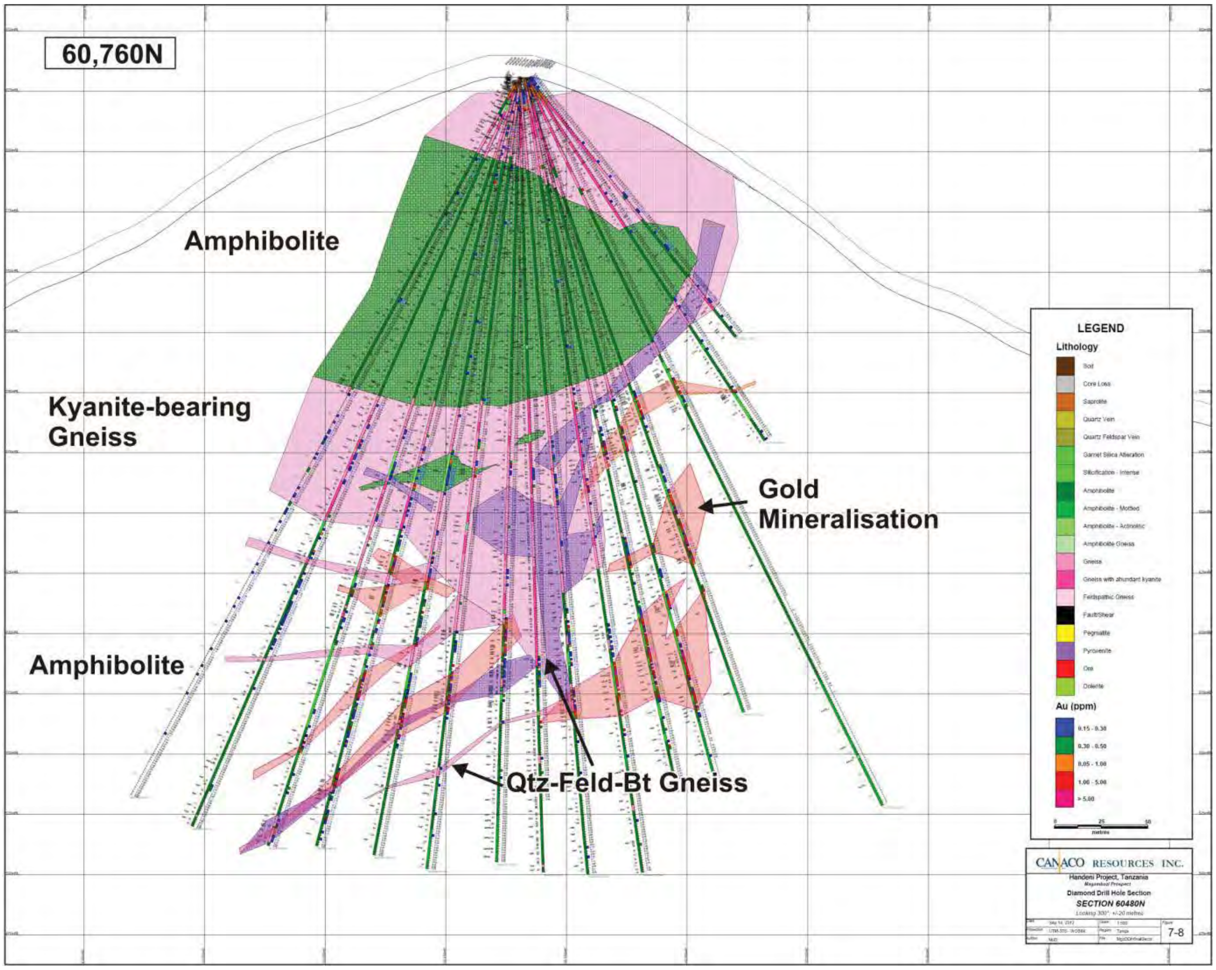
Drill section results through Magambazi, Magambazi Central and Magambazi North are shown in Figures 7-7, 7-8 and 7-9, respectively, which display reasonable overall continuity in mineralisation between most drill holes.

Figure 7-7: Drill Section 60,480N through Magambazi



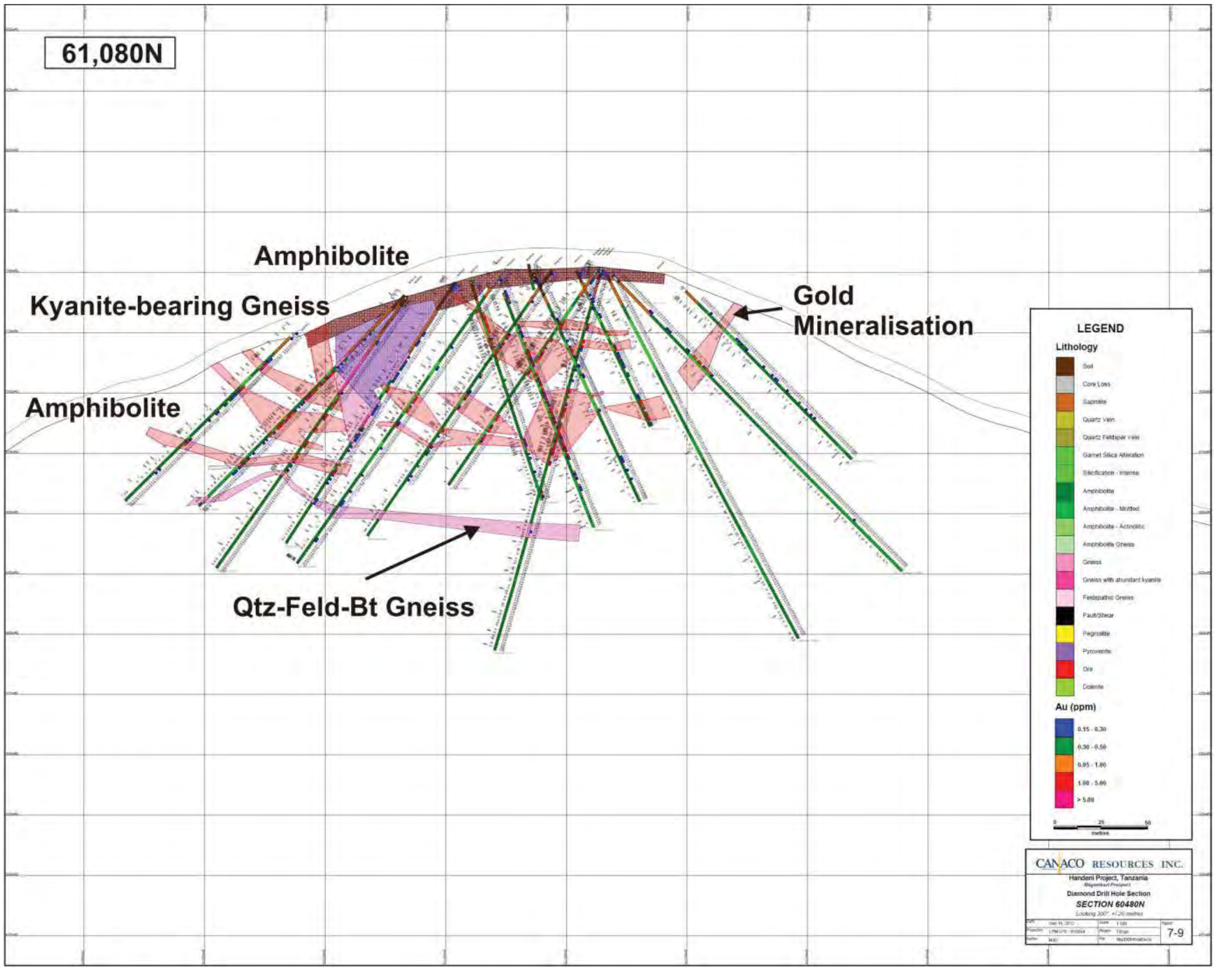
Note: The synformal nature of the country rock is evident, as are the thickness and geometries of the ore outlines. Each grid square is 50 x 50 m. Source: Canaco, 2012.

Figure 7-8: Drill Section 60,760N through Magambazi Central



Note: Mineralisation is steeper than sections in Magambazi North and the main Magambazi zone to the south.
Source: Canaco, 2012.

Figure 7-9: Drill Section 61,080N through Magambazi North



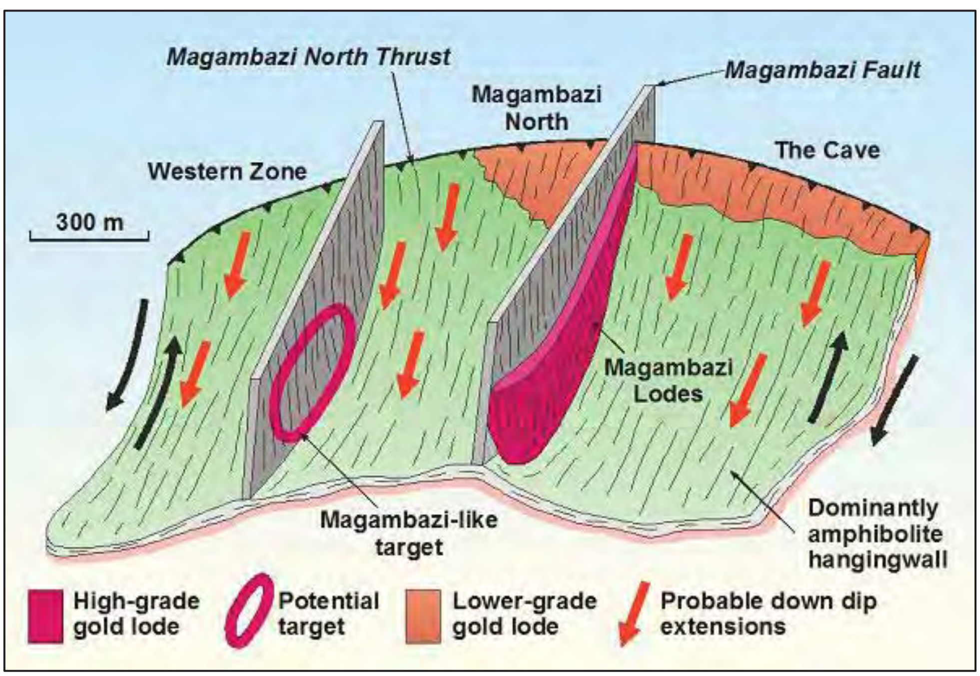
Note: Drilling to the west reveals the synformal nature of the mineralised structure and the presence of faults.
Source: Canaco, 2012.

The presence of significant visible free gold within the drill core of the alteration envelope and gold-hosted zones suggests that gold has been released from refractory arsenopyrite (FeAsS) by recrystallization at high temperature during metamorphism and lead to the production of löllingite ($FeAs_2$). The same process would result in pyrite forming pyrrhotite with trace constituents of copper and lead forming chalcopyrite and galena (D. Groves, personal communication).

The mineralised zones encountered at Magambazi are not typical of major deposits commonly discovered in known orogenic greenstone belts. A number of analogies may however be drawn with the high metamorphic grade at the Southern Cross belt of Western Australia (I. Groves, personal communication). The presence of the mineral resource at Magambazi suggests that other areas within the Handeni property might be prospective for the same style of mineralisation. This is based on similar structural features and lithologies.

In summary, the northwest-trending Magambazi gold mineralisation is in the hanging wall of the metamorphically annealed northwest-trending Magambazi fault, which in turn is in the hanging wall of a roughly east-west trending thrust fault (probably corresponding to the top of a hydrothermally altered mafic flow) that dips at approximately 20° to the south, and is exposed on the Magambazi saddle at North Magambazi (D. Groves, 2012). This thrust is mineralised over several hundred metres of strike length at North Magambazi. Recent drill testing beneath this thrust to the north indicates that all known mineralisation at Magambazi is in the hanging wall of this thrust as shown in Figure 7-10. Potential exists for discovery of additional high-grade gold targets where high-angle fault zones cut the thrust fault plane, either in structures parallel to the Magambazi fault, or along strike of the fault northwards towards Kwadijava.

Figure 7-10: Schematic Model for Magambazi



Source: D Groves, 2011.

8 DEPOSIT TYPES

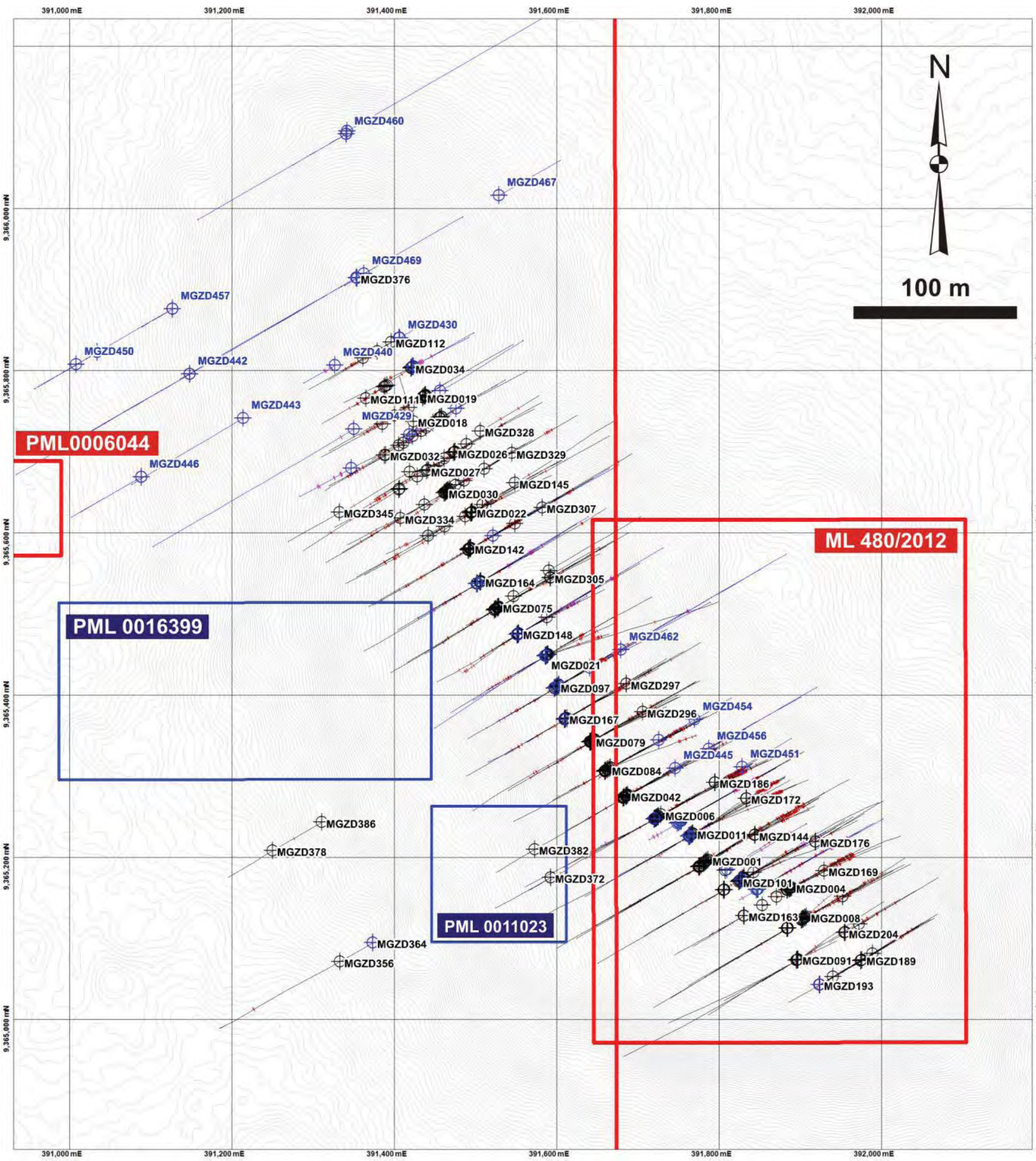
Gold deposits in the Handeni property consist of artisanal placer deposits and orogenic vein-related mineralisation in altered amphibolite gneiss. The host assemblage is interpreted to represent an original metamorphosed Archean lode-gold terrane (predominately mafic volcanic and mafic volcaniclastic rocks) that has been entrained within the Proterozoic Usugaran belt, and undergone further alteration/metamorphism during the Proterozoic Eon. A prominent east-northeast trending thrust cuts across the northern portion of the property. Thrusts of this nature are identified as a locus of major mineralisation in the Lake Victoria greenstones (Groves, 2010). Additionally, mineralisation in Lake Victoria is also concentrated along northwest-trending faults. Both of these features are present in the Magambazi area. Many of the significant gold deposits of the Lake Victoria area are spatially associated with iron formation; however, this relationship has not currently been noted in the Handeni area.

At Handeni, artisanal alluvial placer deposits are located at Magambazi, Magambazi North, Kwadijava South, Kwadijava, and Majiri. At Magambazi, Magambazi North, and Kwadijava. Artisanal workings occur in quartz-vein-related gold, with mineralisation located within silica and garnet altered amphibolite gneiss. Garnet in these altered sections is generally fine grained (<2 mm) and the altered zones typically display only a vague banding texture as compared to associated gneisses. The depth extent of these mineralised systems has been confirmed by the recent diamond drilling.

Diamond drilling in the Magambazi area has revealed the character of a gold mineralised system extending well over 1000 m longitudinally, 350 m laterally while also displaying continuity. This character is illustrated in the area drill hole plan that displays the surface projection of the gold mineralised system shown in Figure 8-1. As anticipated in a highly metamorphosed system, the continuous mineralised trend has a tendency to pinch and swell along strike. Late structures appear to have caused small-scale displacement, making correlation between zones difficult at times.

The exploration model applied to the Handeni property is orgenic gold mineralisation (Groves et al., 1998; Hagemann and Cassidy, 2000), subsequently structurally deformed and metamorphosed.

Figure 8-1: Location of Diamond Drillholes at Magambazi



Note: Gold intercepts >2 g/t are illustrated by red lines on the drillhole trace for drilling included in the 2012 resource, and magenta for holes excluded. Canaco owned licences are in red and contentious licences are in blue. Source: Archibald, 2013.

9 EXPLORATION

All mineral exploration to date has been conducted by Canaco, except for Niton portable XRF soil analyses and geological mapping by C. Carman and I. Groves of CEC Geology LLC and Insight Geology Pty. respectively; petrographic work conducted by Josef Klomínský and F. Colombo of the Czech Geological Survey and Vancouver Petrographics Ltd., respectively; and airborne geophysics by New Resolution Geophysics.

9.1 Historical

In 2007 and 2008, Canaco conducted initial reconnaissance geological assessment and rock sampling in the areas of known artisanal mining, and encountered encouraging results. These areas include Magambazi, Semwaliko (renamed Kwadijava in 2011), and Majiri Bomba (renamed Majiri) which are located as shown in Figure 7-6 and in Figure 9-1). Aeromagnetic data and Landsat IKONOS satellite data were assessed to establish a general structural/geological interpretation of the property. A key major ENE-trending linear feature was established across the Majiri area, and key major NW linear features were also identified, associated with the well exposed topographic high area of the Magambazi hill. Systematic soil sampling was conducted across the key regions of interest, and in-filled as appropriate for improved anomaly definition. A pronounced 11 km long soil anomaly was defined by this program, and is seen to generally connect the known areas of artisanal working between Magambazi, Kwadijava, and Majiri. Further assessment was conducted to determine if additional trace elements in the soils were directly related to gold mineralisation. A Niton X-ray fluorescence (XRF) instrument was used on a set of grid soil pulps in the Magambazi area, and a correlative arsenic-gold anomaly was discovered in addition to a potential flanking copper anomaly (Carman and Groves, 2008). Channel, chip and trench sampling was conducted at Magambazi, Kwadijava, and Majiri, in areas interpreted to host potential near surface mineralisation. The longest and highest grade intercepts were identified at Magambazi. Full details of the procedures and parameters in the historic surveys are presented in Archibald (2011).

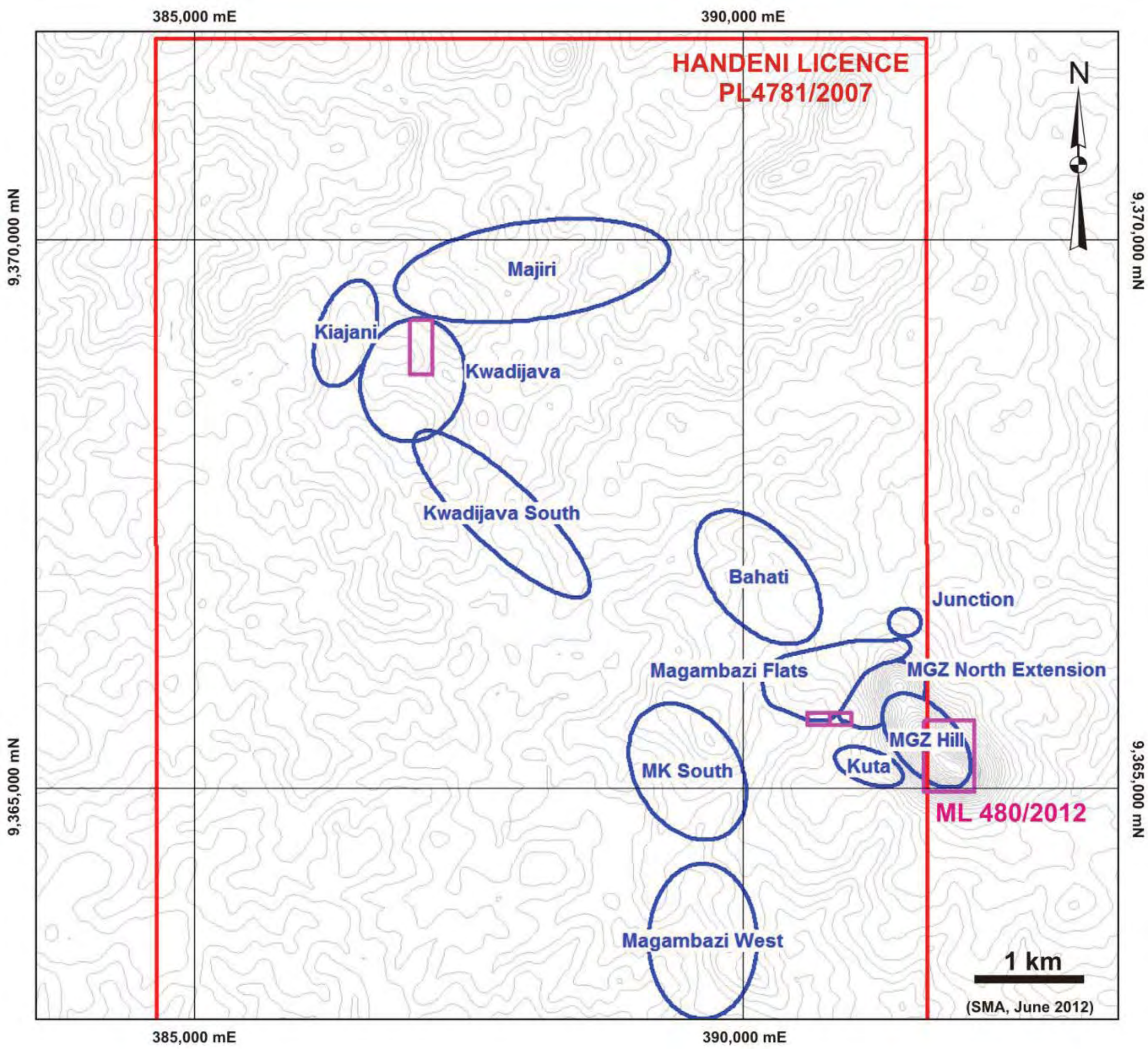
In August 2008, a program of reverse circulation drilling was conducted to test the potential down dip extension of mineralisation mined at the artisanal rock workings at Kwadijava. A series of fence holes were drilled to test for this projected mineralisation, but failed to provide much encouragement in terms of alteration or mineralisation. The best intersection was 12 m grading 1.04 g/t Au.

In September of 2008, Canaco indicated that a new strong soil anomaly at the Majiri area of the property had been defined. Follow-up mapping identified a gentle dipping shear system containing sheeted quartz veins. Trenching and chip sampling were also conducted.

In late 2009, a program of diamond drilling was commenced in the Magambazi area and this program continued until March 28 2012. The results of this program are presented in Section 10 of this report.

In June 2012, a portable XRF trace element geochemistry study was carried out on twelve drillholes located on section line N60560 at Magambazi (McGrath, 2012). Interpretation of the results was performed by D. Groves.

Figure 9-1: Prospect Locations within the Magambazi Licence



Source: Archibald, 2012.

9.2 Soil Sampling

A total of 19,852 soil samples (1,610 in 2007, 6462 in 2008, and 11,780 in 2010) were collected throughout the property and analyzed for gold, at the locations shown in Figure 9-2 on the following page. Initial sampling concentrated on systematic 800 m spaced lines covering areas and trends of interest from Canaco's compilation of geological information on the property. In-fill line sampling, up to 40 m spacing, was conducted in areas of prospective interest. From this work, an 11 km long gold anomaly in soil was identified, covering the Magambazi area in the southeast and connecting to the Kwadijava area in the northwest, and further following northward to the Majiri area. The average gold concentration of the soil samples was 8.31 ppb, which was heavily influenced by the weighting of 10,365 samples containing gold less than the analytical limit of detection. From the 19,852 samples collected only 150 had gold concentrations greater than 150 ppb, of which samples from or adjacent to the Magambazi area accounted for 79%, samples from the Kwadijava –Kwadijava-Majiri trend accounted for 15%, and the remaining samples from outside these two areas. The maximum concentration recorded was 6,836 ppb Au from Magambazi South.

In 2008, samples previously sent to the laboratory for assay were subjected to Niton XRF analysis to determine a suite of potential gold-related trace elements. The survey examined three wide spaced lines covering the central, southeastern, and northwestern portion of Magambazi Hill, in addition to a central 40 m x 40 m grid situated near known mineralisation in the central Magambazi Hill area. A total of 338 samples were analysed in the study. From the suite of elements analysed (including As, Co, Cu, Fe, Hg, Mn, Mo, Ni, Pb, Rb, Se, Sr, Th, U, W, Zn and Zr), two elements (As and Co) define distinctive trends related to known gold mineralisation. Silver content is directly related to gold content, whereas Cu content increases in areas immediately peripheral to known gold mineralisation.

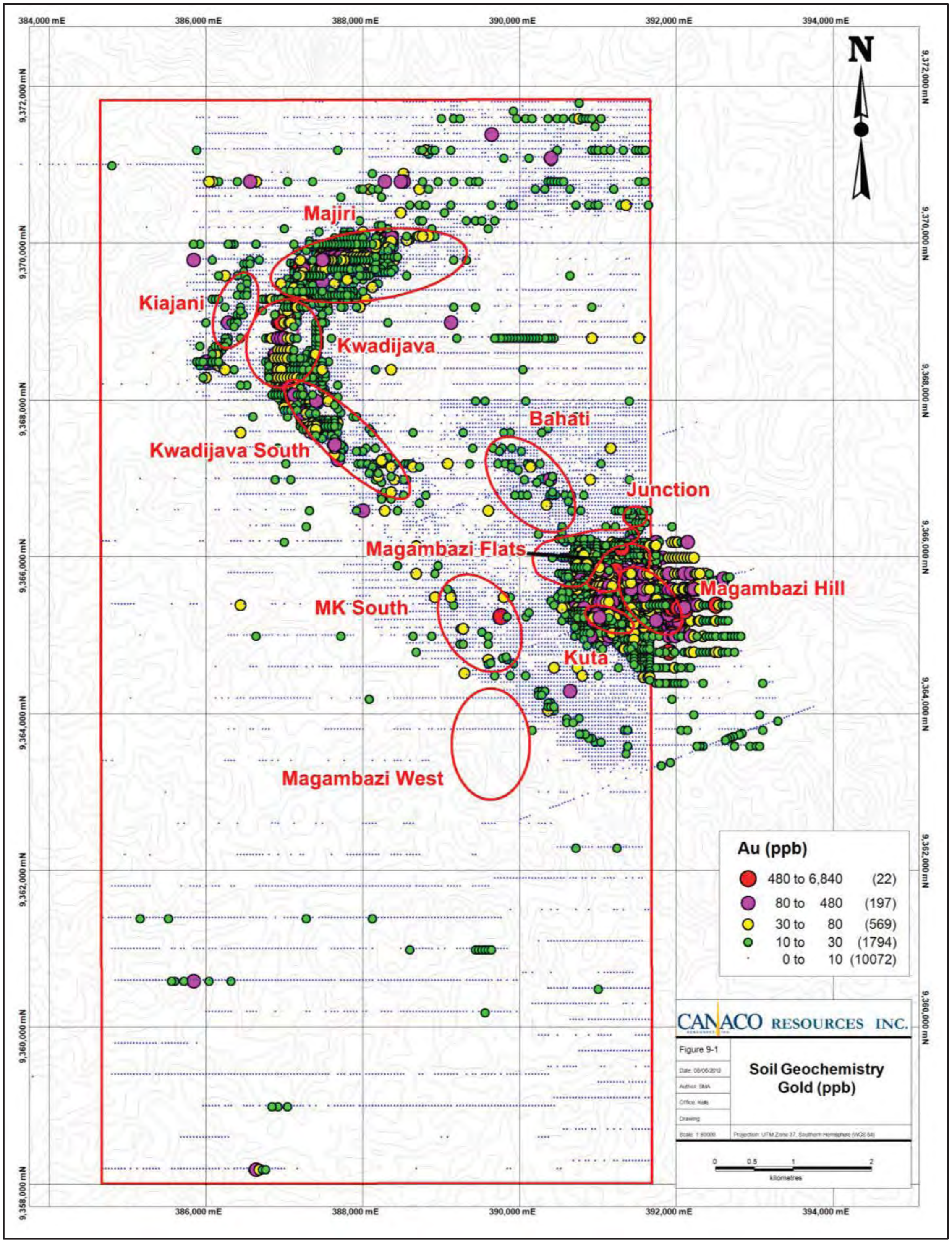
9.3 Lithogeochemical Sampling

A total of 126 channel samples were collected at Magambazi and Magambazi Central during early exploration in 2008. The most significant result was seven metres of 5.6 g/t gold, including 3 m of 10.15 g/t gold in a 10 m wide (approximate 6.5 m true thickness) artisanal working at Magambazi (Archibald, 2011).

At Kwadijava 10 channel samples were collected, with the best mineralised intervals containing 2.54 g/t gold over 10 m, and a 2 m interval containing 14.3 g/t gold from shallow workings. The true thicknesses of these intervals are unknown.

In 2011 a total of 185 samples were taken from outcrops at Majiri. A single trench hosted two 1 m samples, 4 m apart, assaying 3.29 and 3.30 g/t, respectively.

Figure 9-2: Soil Sample Locations



Source: Redrawn from Archibald, 2011.

9.4 Airborne Geophysics

A high-resolution XPlorer magnetic and radiometric airborne survey was carried out over part of the Handeni Property (Figure 9-3) from September 1-2, 2010, by New Resolution Geophysics (NRG), Pretoria, South Africa. Using a Eurocopter AS350B2 helicopter, 935 line kilometres were surveyed. The survey was flown at an elevation of 25 m with a 90° (east-west) orientation, and a line spacing of 100 m. The spacing was reduced to 50 m over the Magambazi hill to provide extra detail on the current resource definition area. Measurements collected were total magnetic field, potassium-, uranium- and thorium-gamma ray counts, and radar altimetry data (Figure 9-4).

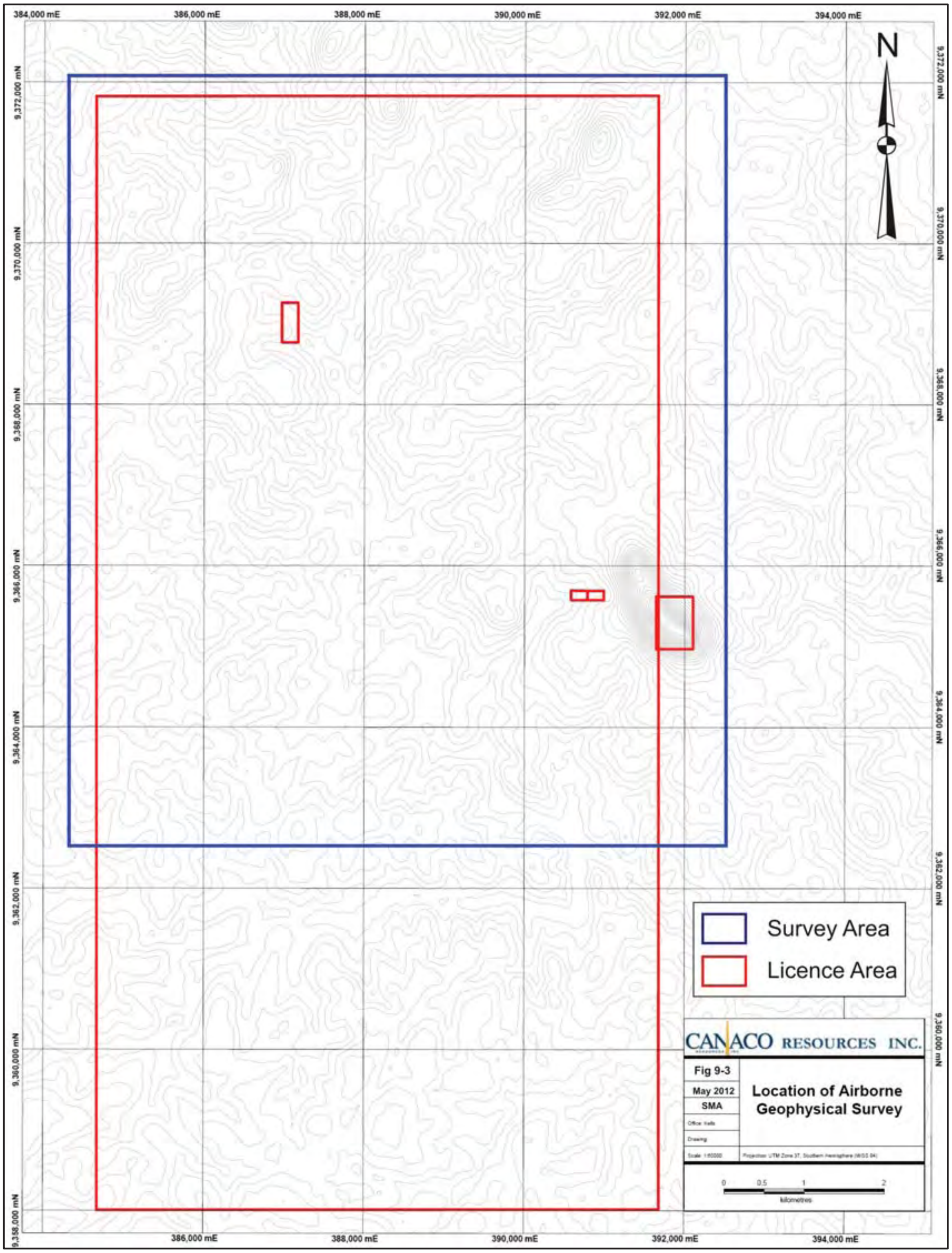
The data was processed by a NRG and the following products were delivered to Canaco: total magnetic intensity, reduced to magnetic pole, first vertical derivative, analytic signal, digital terrain model (DTM), total count radiometrics, and ternary radiometrics. The data was interpreted by Canaco and used to refine the geology of the property. Additional exploration targets were identified when the interpreted geophysical data was integrated with the results of soil sampling, RAB, RC and diamond drilling.

9.5 XRF Trace Element Geochemistry

In June 2012 a XRF trace element geochemistry study was conducted on twelve drillholes on section line N60560 by McGrath (2012). A total of 1,834 pulps were analysed using a Niton portable XRF instrument set for “soil mode”. Complete XRF analysis of the pulps was only possible on two of the holes, since many of the samples had not been returned from the assay laboratory, or unmineralised sections had not been sampled, in the remaining ten holes. A spectrum of trace and major elements were analysed during the study to help discriminate between local lithologies (gneiss, amphibolite and garnet-silica alteration) and determine if a correlation existed between gold and other elements. The study indicated that the garnet-silica (GASIL) unit that is most closely associated with the gold mineralisation can be identified using a distinctive Ca, Zr, Mn, Cr and Y signature. Due to the highly localised nature of the gold mineralisation, there were no elements that showed any predictable linear variation with gold concentration. High gold concentrations (determined by fire assay) were frequently shown to be concurrent with high arsenic concentrations, however there are significant occurrences of high arsenic values that do not contain associated high gold values.

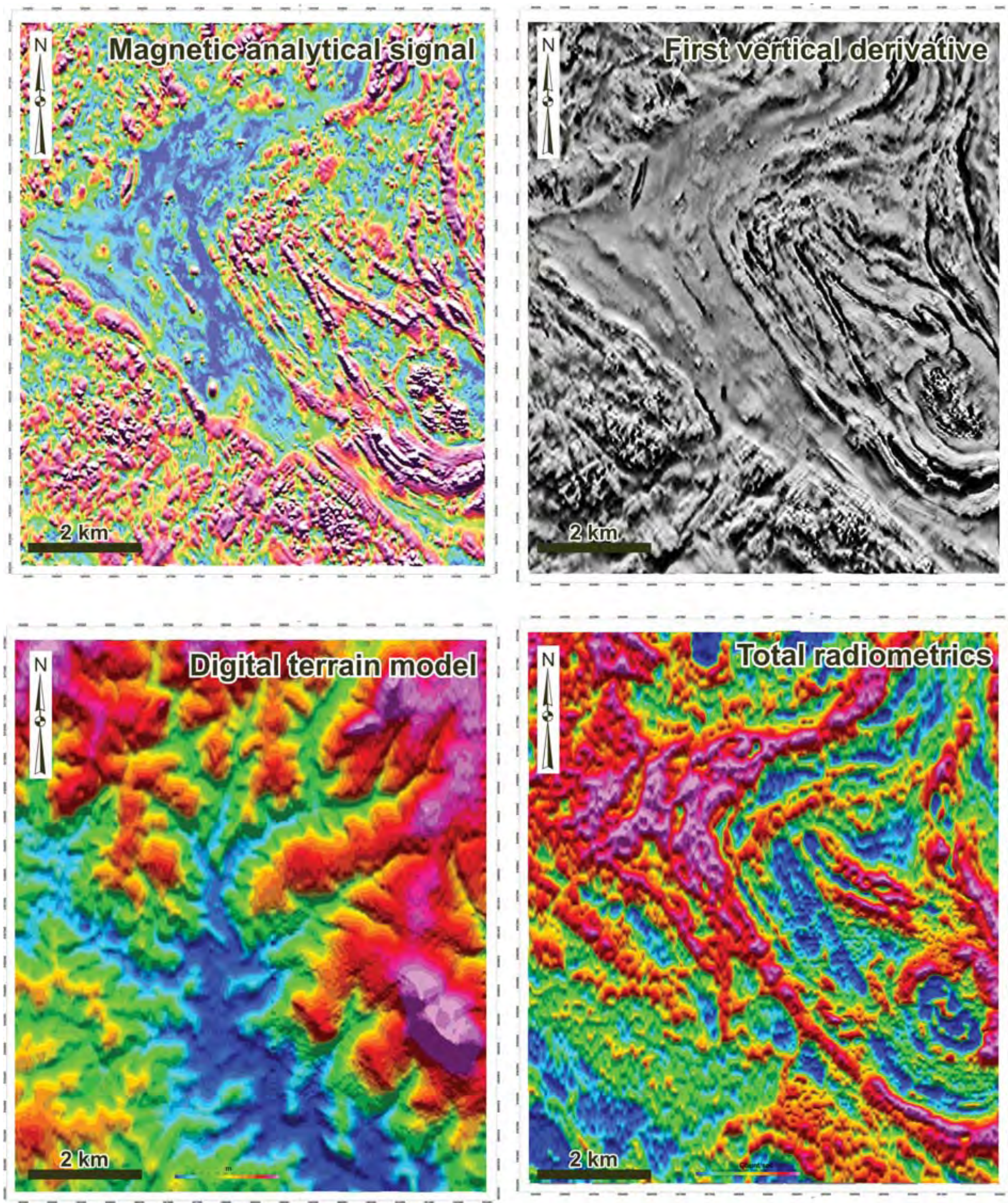
Addition work on the XRF geochemical dataset was conducted by D. Groves (June 2012). Initial interpretation of drillcore at Magambazi indicated that diabase sills (now amphibolites) may have formed the locus for tabular mineralisation, caused by the competency contrast during brittle deformation within the sill. Using the geochemical data of McGrath (2012), D. Groves concluded that the signatures now indicate that the targeted GASIL horizons likely represent the tops of differentiated basalt flows, which formed during seafloor hydrothermal alteration prior to the deposition of the precursor to the overlying sediments (now paragneiss). Low-grade gold mineralisation was thus controlled by a brittle host rock (GASIL) which was overlain by an impermeable sedimentary cap rock.

Figure 9-3: Location of Airborne Geophysical Survey (blue) Relative to Handeni Property and the Magambazi Resource Area



Source: Canaco, 2012.

Figure 9-4: Examples of Airborne Geophysical Survey Data



Source: Canaco, 2011.

10 DRILLING

10.1 General

Prior to Canaco's involvement on the project no drill holes are known to have been drilled on the property. The exploration drill hole collars, including test holes for water source determination, are illustrated in Figure 10-1 on the following page. The complete drilling, that has served as a basis for this report and the mineral resource estimate, is summarized in Table 10.1 below. The main areas shown in Figure 10-1, where this drilling was conducted, are referred to in the following text as Kiajani, Majiri, Kwadijava, Kwadijava South, Bahati, Junction, Magambazi Flats, Magambazi North Extension, Magambazi Hill, Kuta, MK South and Magambazi West. The collar locations and total depths for all drill holes are listed in Table A-1 of Appendix A. The mineral resource estimate was estimated on 397 diamond drill holes representing 102,646 m in the Magambazi area.

Table 10.1: Summary of Drilling on the Handeni Project

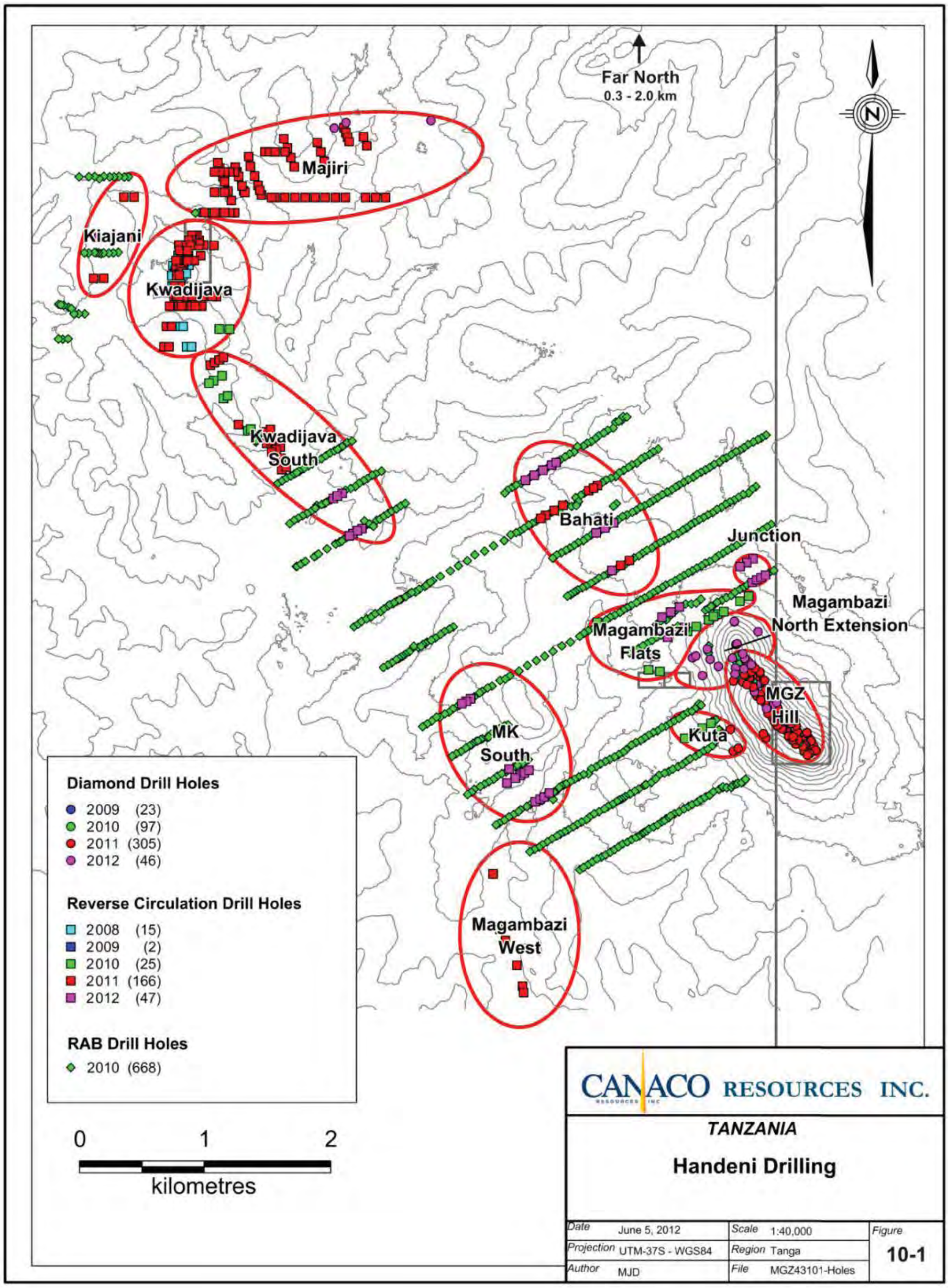
Year	RAB		RC		Diamond	
	Holes	Metres	Holes	Metres	Holes	Metres
2008	-	-	15	1,807	-	-
2009	-	-	2	194	23	5,572
2010	668	10,402	25	3,723	97	21,497
2011	-	-	166	15,920	303	83,351
2012	-	-	47	6,636	48	11,425
Total	**668**	**10,402**	**255**	**28,280**	**471**	**121,846**

10.2 Reverse Circulation Drilling

A total of 28,280 m of reverse circulation (RC) drilling was conducted in 255 holes between March 24, 2008 and May 17, 2012 with truck-mounted RC rigs and this work is also summarized in Table A.1 of Appendix A. The first ten-hole drill program was completed between March 24 and May 31, 2008 and was designed to test the depth extension of a known artisanal placer and hard rock mine workings at Kwadijava. A further five RC holes tested a gold soil anomaly, as shown in Figure 10-1. The most significant gold mineralised intercepts at Kwadijava included 12.0 m grading 1.04 g/t Au, located in altered amphibolite gneiss (drill hole MGZC001). Only two RC holes were drilled in 2009, both in the Magambazi area for a total length of 194 m.

In 2010, an additional nine RC drill hole program, totalling 1,376 m was drilled between July 25 and August 7, 2010. This program targeted the southern extension of soil anomalies and artisanal workings at Kwadijava and Kwadijava South. The highest gold assays reported from this program included a 12 m interval grading 1.11 g/t Au, including a 1 m section grading 8.44 g/t Au (drill hole MGZC040). Also in July 2010, four holes were drilled in the Kuta area for a total length of 646 m, with a maximum intercept of 0.09 g/t Au recorded over 1 m (drill hole MGZC030). At Magambazi 1,578 m of exploration drilling was conducted in 13 holes (in addition to one water bore hole) on Magambazi Flats and on the Magambazi Hill.

Figure 10-1: Summary Drill Plan of the Handeni Property



Source: Canaco, 2012.

Exploration drilling in 2011 was conducted in five areas: Kwadijava, Kwadijava South, Majiri, Kiajani, and Bahati. Figure 10-2 illustrates a typical RC drilling operation in these areas. The greatest concentration of drilling in 2011 occurred at Majiri where 5,685 m was drilled in 61 holes. Drilling results were variable, but the highest gold concentration recorded was 3.53 g/t over 1 m in hole MGZC076. A total of 65 RC holes (5,183 m) were drilled at Kwadijava and analysed for gold. The maximum 1 m interval recorded from the area was 18.80 g/t Au from a 1 m long interval in hole MGZC161. At Kwadijava South 17 RC holes were drilled for a total length of 1,974 m, and the highest gold grade was 1.82 g/t over 1 m long interval in hole MGZ140. Results from the 6 holes drilled at Kiajani were disappointing with the highest concentration of gold being 0.78 g/t over a 1 m long interval in hole MGZC167. The total length drilled at Kiajani in 2011 was 900 m with no significant gold results. Drilling at Bahati was undertaken to determine if Magambazi-style mineralisation is present 1 km to the NW of the hill. Results from the nine hole, 1,304 m program at Bahati are pending and they are not material for the mineral resource estimate.

Figure 10-2: Reverse Circulation Drilling, Kwadijava Area

Source: Canaco, 2010.

RC drilling was focused on six areas of the Handeni property during 2012, and a total of 6,636 m was drilled up to May 17, 2012, when the campaign was completed. The greatest amount of drilling took place at MK South where 14 holes have recovered 2,104 m of rock. At Behati nine holes were drilled for a total of 1,377 m, seven holes drilled for a total of 1,055 m at the Junction Prospect, and an additional eight holes at Magambazi Flats for a total of 1,018 m there. Drilling at Kwadijava South included seven holes for a total of 832 m and two holes Kiajani for a total of 250 m. Assay results for RC drilling conducted in 2012, in these areas, are pending and are not material to the mineral resource estimate.

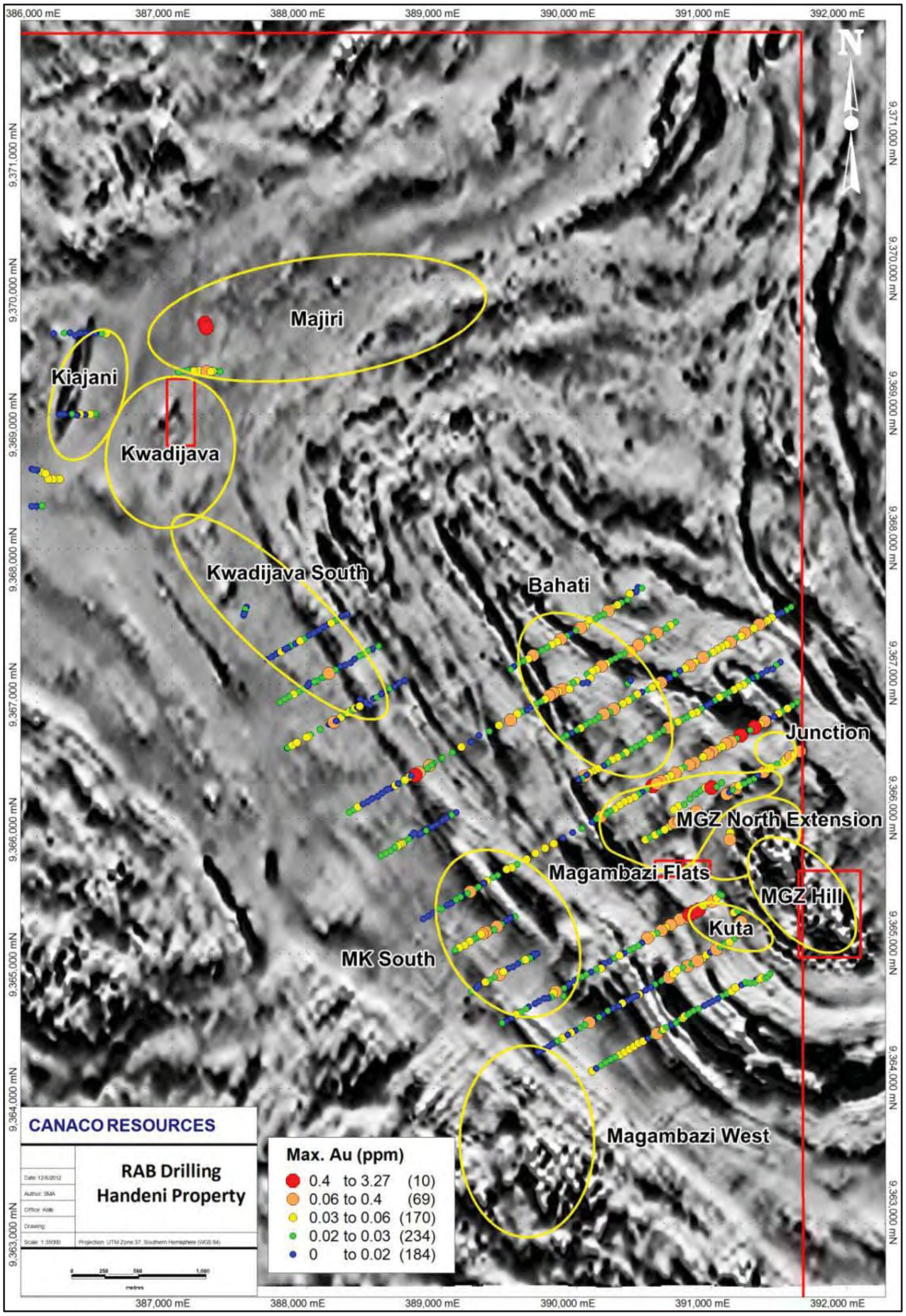
Industry best practices were followed during the RC program. The core material was pulverized into chips and delivered to surface using compressed air through the inner tube of the rod string, providing a 30-40 kg sample per metre. Much of the geotechnical and structural information derived from diamond (core) drilling is lost through the RC method. Samples were collected in meter long intervals, were split through a three-tier riffle split on the cyclone of the RC drill rig, bagged into polyethylene sample bags, double tagged, and stapled closed. The larger sample fraction not sent to the laboratory was collected in a large polyethylene plastic bag and stored at the project camp for future reference. The RC drilling and sampling technique may introduce a minor potential sample bias, but this can be qualified through effective recovery documentation and comparative twin diamond drill work. The relationship between RC sample length and true thickness of mineralisation is difficult to quantify since accurate core axis information cannot be obtained.

10.3 Rotary Air Blast Drilling

To quickly assess the regional potential of bedrock mineralisation on the Handeni Property a 10,402 m Rotary Air Blast (RAB) drilling program was undertaken by Stanley Mining Services Tanzania between July 29 and September 10, 2010. RAB is a quick and effective way to core poorly consolidated material and collect a sample at relatively shallow depths (typically less than 50 m). This program was conducted in the areas shown in Figure 10-3. A total of 668 1.5" diameter, predominantly vertical holes were drilled to depths not exceeding 48 m and 3,457 samples were collected. These samples were typically taken as splits at 4 m intervals, however some samples were smaller if the hole was terminated prior to completing a whole drill rod.

Gold results from the RAB drilling program appear to show isolated gold samples with only ten samples displaying gold concentrations from 0.40 to 3.27 g/t (typically over 4 m). However, when the RAB drilling locations are plotted with the maximum gold concentrations on the recently flown airborne magnetic data, it is apparent that the anomalous gold samples are associated with magnetic highs, faults cross-cutting the regional foliation, or close to minor fold hinges. It is also interesting to note that some of the tight fold closures, which might be prospective for saddle reef gold, have not been drilled.

Figure 10-3: Handeni Property RAB Drilling Locations



Note: Drill plan shows the maximum gold intercepts recorded over 4 m intervals. The background image is the first vertical derivative of the magnetic geophysical survey. Source: Archibald, 2011.

10.4 Diamond Drilling

Diamond drilling at the property was conducted by Layne Drilling Tanzania Ltd (formerly Stanley Mining Services of Tanzania) from September 7, 2009 to January 1, 2012, Simba Drilling Company Ltd from February 25 2011 to March 29, 2012, and Kluane Drilling Tanzania Ltd from February 17, 2011 to March 28, 2012. Early drilling was conducted by truck-mounted drilling rigs, with later work performed by track mounted and modular units. Rigs travel between sites via cleared dirt roads. A typical diamond drilling operation is illustrated in Figure 10-4 below. Drill holes were commenced using HQ size drilling, and typically reduced to NQ or NTW at depths of approximately 10 to 15 m. Only four holes at Magambazi were drilled exclusively at HQ size (MGZD116, 118, 120 and 127) all others were drilled at NQ and NTW size core. Exploration diamond drilling outside the main Magambazi area of was focused on three peripheral areas on the property: Magambazi North Extension, Kuta and Majiri. A total of 22 holes (6,764 m) have been drilled at Magambazi North Extension, four holes at Kuta (883 m) and three holes (506 m) at Majiri, with the locations tabulated in Table 10.2.

Figure 10-4: Drilling of an Inclined Diamond Hole (MDGZ449), Magambazi North Extension

Table 10.2: Mineral Exploration Diamond Drill Holes at Kuta, Majiri & Magambazi North Extension

Hole ID	Easting	Northing	Azimuth (°)	Dip (°)	Total Depth (m)	Prospect
MGZD356	391333	9365071	240	-46	249.78	Kuta
MGZD364	391373	9365094	240	-53	347.81	Kuta
MGZD378	391250	9365208	240	-59	97.74	Kuta
MGZD386	391311	9365243	240	-70	187.9	Kuta
MGZD437	388921	9370053	73	-45	198.76	Majiri
MGZD444	388151	9369992	73	-45	107.25	Majiri
MGZD447	388243	9370035	73	-45	200.02	Majiri
MGZD376	391353	9365914	240	-80	447.88	MGBZ NE
MGZD408	391353	9365914	240	-60	501.06	MGBZ NE
MGZD439	391353	9365914	240	-45	390.53	MGBZ NE
MGZD442	391148	9365796	240	-45	349.52	MGBZ NE
MGZD443	391213	9365741	240	-50	250.27	MGBZ NE
MGZD446	391088	9365669	240	-70	249.85	MGBZ NE
MGZD448	391088	9365669	240	-50	153.64	MGBZ NE
MGZD449	391353	9365914	240	-75	498.44	MGBZ NE
MGZD450	391008	9365807	240	-50	91.6	MGBZ NE
MGZD452	391148	9365796	240	-60	302.61	MGBZ NE
MGZD453	391034	9365822	240	-70	198.74	MGBZ NE
MGZD455	391034	9365822	240	-50	129.6	MGBZ NE
MGZD457	391127	9365876	240	-80	251.66	MGBZ NE
MGZD459	391148	9365796	240	-75	350.52	MGBZ NE
MGZD460	391340	9366092	240	-45	298.25	MGBZ NE
MGZD463	391354	9365914	240	-88	499.73	MGBZ NE
MGZD464	391127	9365876	240	-50	240.36	MGBZ NE
MGZD465	391340	9366092	240	-75	295.6	MGBZ NE
MGZD466	391340	9366092	240	-90	449.45	MGBZ NE
MGZD467	391529	9366016	60	-45	124.12	MGBZ NE
MGZD468	391341	9366095	60	-46	409.11	MGBZ NE
MGZD469	391362	9365920	60	-60	281.73	MGBZ NE

Mineral resource related diamond drilling was exclusively focused at Magambazi where 441 holes (not including two abandoned holes) were drilled for a total of 113,863 m, of which 397 holes totalling 102,646 m are used in the mineral resource estimation. The remaining 44 holes either have not passed the QA/QC protocols or assays were pending, and they were not incorporated in the mineral resource estimation.

Exploration diamond drill holes were selected and drilled based on one or more of the following; favourable host rocks, geochemical and/or geophysical anomalies and/or the presence of *in situ* gold mineralisation. Diamond drill holes were drilled systematically in a series of northeast-trending, 40 m spaced sections along strike and down-dip of known mineralisation previously identified by prospecting, mapping and earlier drilling. Mineral resource drilling was planned to ensure that sufficient coverage at depth was obtained, for determination of the grade and continuity of the auriferous system.

During exploration, Canaco and their drilling contractors conducted the drilling program according to industry best practices. Drill hole collar coordinates were surveyed and at completion the holes were capped with concrete monuments as shown in Figure 10-5. These coordinates were surveyed prior to drilling and again after drilling, by a qualified Canaco surveyor using a DGPS Epoch 25 with a measurement accuracy of ±1 cm. Azimuth and dip information was collected downhole using a Reflex EZ-Shot orientation instrument at roughly 30 m intervals. Core orientation information was initially taken at approximately 30 m intervals, and reduced to 6 m intervals in areas of mineralisation to determine the orientation of mineralisation and structures (e.g., foliation) within the rock. Core orientation measurements were collected every 6 m during drilling in 2012 to increase the confidence and reliability of the measurements. All holes were capped upon completion, with the collar points surveyed and denoted by cement markers.

Figure 10-5: Cement Marker Denoting the Location of Drill Hole Collars

Source: Archibald et al., 2011.

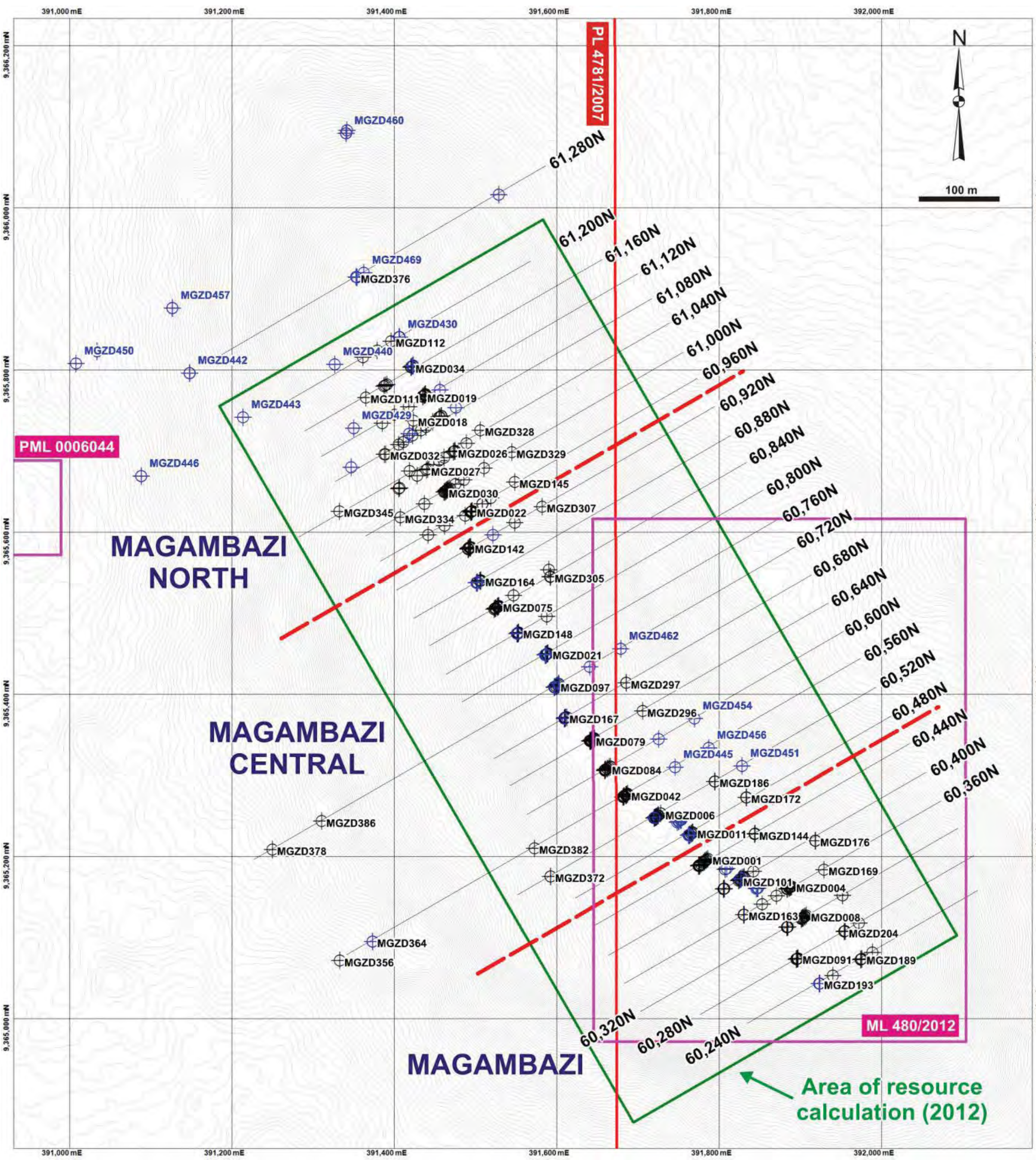
Drill core recoveries for the project were acceptable, and the samples collected were representative of the observed mineralisation. Determining the exact true thickness from individual drill holes is difficult in this case, since the foliation present within the core does not necessarily correlate with the orientation of the veins. This is because there appear to be at least two phases of deformation that have affected the veins subsequent to formation. Considering that thicknesses are best calculated by drawing grade envelope sections and estimating the true thickness from interpreted sections (and correlating between sections), the intervals reported in Appendix A likely represent 60% to 90% of the true thickness.

10.5 Magambazi

At Magambazi, 26 sections were drilled with 40 m spacing between sections that allowed for systematic follow-up of the discovery hole, MGZD001. A plan of all of the drill holes is presented in Figure 10-6. Table 10.3 is included to identify drill hole collar labels obscured in Figure 10-6.

Individual zones are presented in Figures 10-7, 10-8 and 10-9, which display the vertical projection of key drill hole intercepts with gold concentrations greater than 2.0 g/t. A significant number of other intervals included in the mineral resource estimate have not been plotted for clarity. The drilling was targeted at the depth extension of existing artisanal workings, where channel sampling encountered encouraging gold grades.

Figure 10-6: Magambazi Drill Hole Plan showing Collar Locations, Section Numbers & Zone Names



Note: The blue dashed lines represent the divisions for Magambazi, Magambazi Central and Magambazi North operational areas. Source: Canaco, 2012.

Table 10.3: Magambazi Diamond Drill Holes (holes in blue drilled subsequent to resource)

Section	Diamond Drill Holes
61,280N	MGZD376
61,200N	MGZD 112, 113, 114, 115 [430, 433, 436, 440, 443]
61,160N	MGZD034, 052, 057, 058, 110, 111 [424, 431, 435]
61,120N	MGZD019, 020, 023, 033, 051, 054, 055, 137, 139, 141 [429, 438]
61,100N	MGZD018
61,080N	MGZD024, 025, 032, 105, 106, 108, 109, 116, 118, 120, 140 [428, 432, 441]
61,040N	MGZD026, 027, 031, 059, 060, 061, 067, 068, 069, 070, 104, 138, 326, 328, 342, 345
61,000N	MGZD030, 117, 119, 121, 122, 124, 125, 127, 310, 314, 321, 329, 334, 337, 341
60,960N	MGZD022, 028, 029, 047, 048, 049, 050, 062, 063, 071, 072, 145, 312, 317, 320, 323, 347
60,920N	MGZD142, 147, 158, 162, 166, 302, 307, 308, 313, 318, 322, 325, 331, 333, 339, 343 [425]
60,880N	MGZD164, 168, 171, 179, 362, 370, 381, 391, 399 [407, 417, 427, 434]
60,840N	MGZD075, 076, 077, 146, 150, 153, 156, 161, 165, 170, 291, 298, 301, 304, 305, 311, 319, 327
60,800N	MGZD148, 151, 154, 157, 160, 300, 324, 336, 346, 353, 387, 397 [402, 411, 419]
60,760N	MGZD021, 043, 045, 046, 073, 074, 143, 275, 278, 283, 288. 295, 303, 383 [416, 423]
60,720N	MGZD097, 182, 191, 196, 203, 208, 244, 248, 253, 264, 268, 386, 378, 389 [412, 426, 461, 462]
60,680N	MGZD167, 173, 178, 183, 212, 218, 257, 259, 262, 266, 272, 280, 286, 297, 309, 316, 388 [405]
60,640N	MGZD079, 080, 081, 177, 181, 188, 192, 246, 250, 258, 269, 276, 279, 287, 293, 296, 315, 373
60,600N	MGZD084, 088, 090, 093, 095, 185, 187, 194, 249, 256, 267, 277, 284, 294, 306, 396 [454, 458]
60,560N	MGZD042, 044, 064, 065, 066, 099, 133, 135, 219, 224, 232, 237, 369, 374, 377, 382, 385 [445, 456]
60,520N	MGZD006, 035, 036, 037, 082, 098, 107, 134, 136, 184, 186, 220, 225, 231, 234, 265, 338, 349, 357, 367, 372, 379 [242, 451]
60,500N	MGZD392, 393, 398, 401 [404, 414, 418, 420]
60,480N	MGZD011, 012, 013, 096, 103, 128, 131, 172, 174, 205, 211, 216, 222, 230, 238, 243, 360, 375, 384 [413, 422]
60,440N	MGZD001, 002, 003, 085, 086, 129, 132, 144, 149, 152, 197, 201, 226, 233, 236, 241, 245, 251, 348, 354, 359, 363, 365
60,420N	MGZD395 [410]
60,400N	MGZD010, 038, 039, 041, 087, 089, 101, 176, 227, 240, 254, 260, 274, 332, 340, 351, 371, 380, 390 [406]
60,380N	MGZD394, 400 [403, 409, 415, 421]
60,360N	MGZD004, 005, 007, 015, 016, 040, 078, 163, 169, 190, 202, 207, 210, 215, 330, 350, 355, 361, 368
60,320N	MGZD008, 009, 014, 017, 083, 123, 126, 209, 252, 261, 271, 273, 290, 299, 335, 344, 352, 358, 366
60,280N	MGZD091, 092, 094, 100, 102, 130, 155, 159, 200, 204, 206, 213, 217, 223, 229, 235, 282, 285
60,240N	MGZD189, 193, 195, 198, 199, 214, 221, 228, 239, 247, 255, 270, 289, 292 [263, 281]

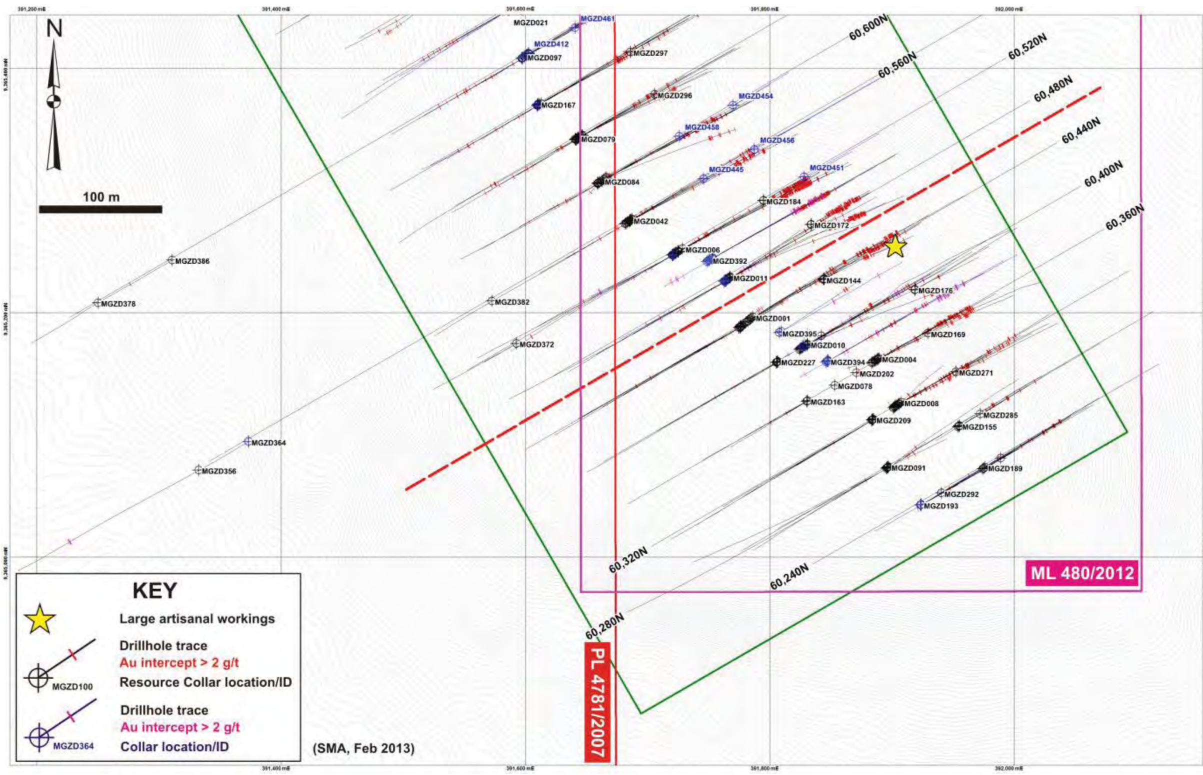
A summary of each drill hole is given in Table A.2 of Appendix A, and this includes several holes which were not used in the mineral resource estimate (specifically, drill holes MGZD242, MGZD263, MGZD281, MGZD364, and MGZD402 to MGZD469). Most of the holes were drilled at an azimuth of either 60° or 240°, with several holes drilled from the same collar point using dips varying from 41° to 90° (vertical). The lowest grade intercept reported was 13.0 m long containing 0.47 g/t Au from hole MGZD072 (Section 60,960N), and the highest grade was 8.40 m long containing 80.90 g/t Au from hole MGZD096 (Section 60,480N). The longest intercept recorded was from Magambazi North (Section 61,040N) where a 68.3 m long interval contained 1.90 g/t Au. From the 434 holes where assays have been reported by Canaco (see Table A.2 of Appendix

A) a total of 298 holes contained gold mineralisation. Information in Table A.2 of Appendix A was supplied by Canaco and incorporates several minor changes to previously released grades and intervals. These minor adjustments and corrections have been included in the mineral resource estimation and their impact is included in the published mineral resource estimate data.

Mineralisation at Magambazi has been divided into three areas: Magambazi South; Magambazi Central; and Magambazi North. The nomenclature is employed for operational terms since the lithologies and the interpreted mineralisation is continuous through the three areas, albeit with slight variations in gold grade, thickness and mineralogy.

Plans illustrating the gold grades greater than 2 g/t in drill holes, projected to surface, from Magambazi South, Magambazi Central and Magambazi North are shown in Figures 10-7, 10-8 and 10-9, respectively. Drill holes used in the 2012 resource estimation are denoted at black collar symbols (and red grade intervals), whereas drillholes not incorporated in the resource calculation are illustrated as blue collar symbols (and magenta grade intervals). Figure 10-7 shows that the highest concentration of the gold mineralisation in Magambazi South is located on the east-northeast side of the hill where gold intensity decreases to the south. Only a few isolated gold intercepts were recorded from the western side of the hill.

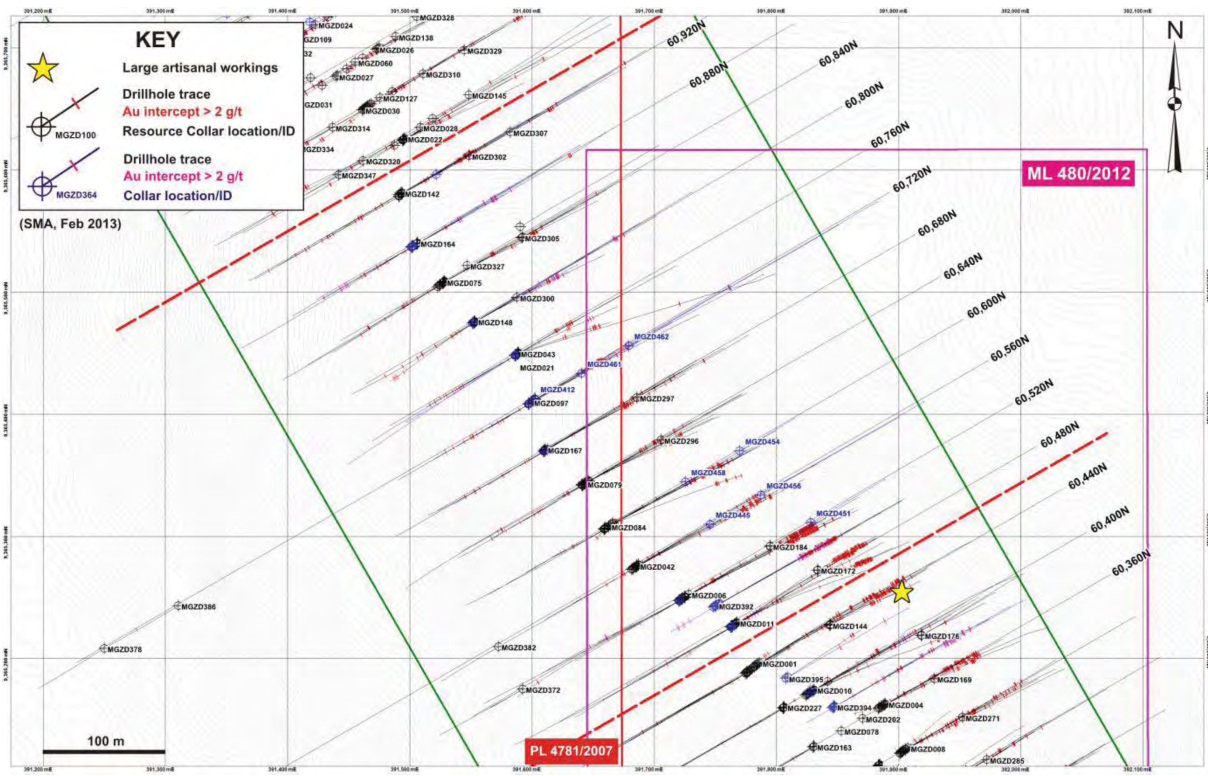
Figure 10-7: Magambazi South Drill Hole Plan (>2.0 g/t Au Vertical Projections)



Note: The yellow star denotes the location of the large artisanal bedrock gold pit in Figure 7-4. Source: Canaco, 2013.

Figure 10-8 is a northern continuation of Figure 10-7 and it reveals that gold mineralisation in Magambazi Central is concentrated beneath the southeastern side of the hill in an area of bedrock artisanal workings (denoted by the star in Figure 10-8), and trends northwestwards for approximately 200 m. The projection of the gold grades greater than 2 g/t on the eastern side of the hill appear to show that the density of values decreases in a northwestwardly direction. Similarly, projections of the gold grades greater than 2 g/t on the western side of the hill appear to show that the number of gold intercepts increase in a northwestwardly direction.

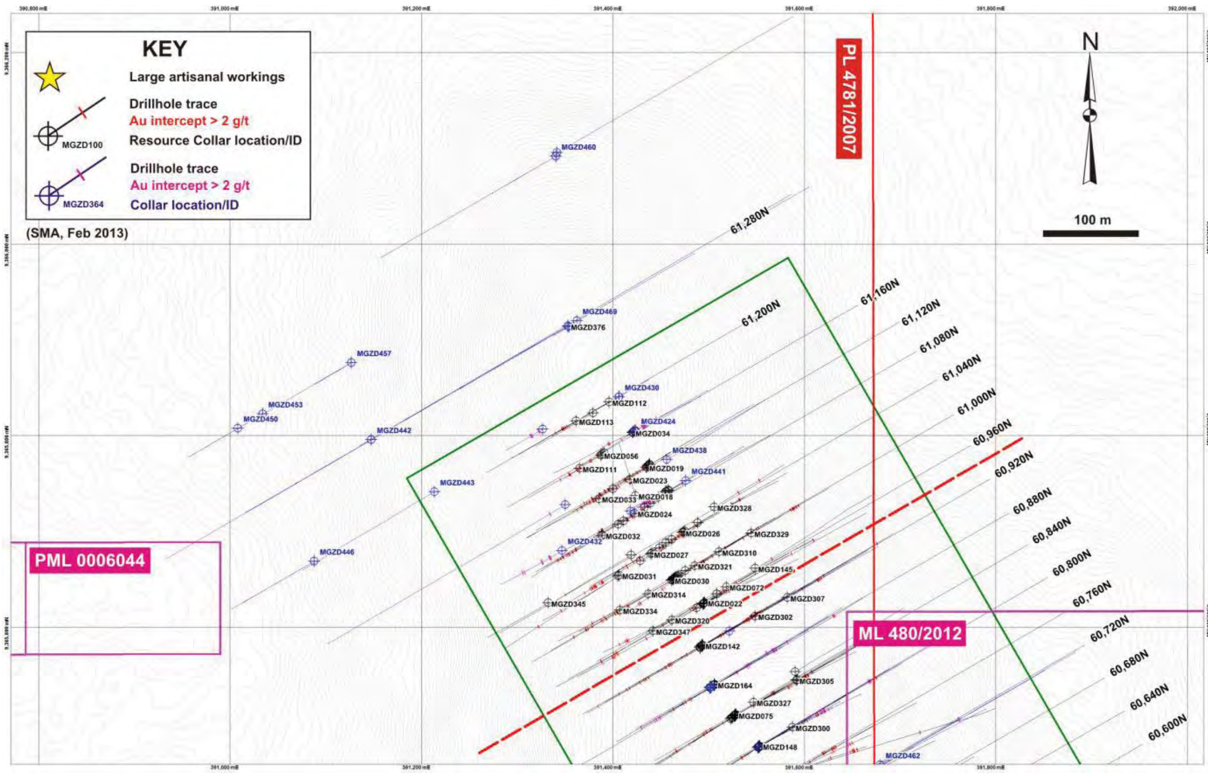
Figure 10-8: Magambazi Central Drill Hole Plan (>2.0 g/t Au Vertical Projections)



Source: Canaco, 2013.

Figure 10-9 is a northern continuation of Figure 10-8 and it shows a reduced incidence of intervals with gold grades greater than 2 g/t on either side of the hill in Magambazi North, This suggests that the mineralised structure (possibly a folded thrust fault plane or tabular body) is closing at this point. Exploration drilling at the Magambazi North Extension tested the possibility of mineralisation to the northwest and indicated that mineralisation was absent (Figure 10-8 and Appendix A2).

Figure 10-9: Magambazi North Drill Hole Plan (>2.0 g/t Au Vertical Projections)



Source: Canaco, 2013.

11 SAMPLE PREPARATION, ANALYSES & SECURITY

The following sections summarize the extent of the author's knowledge regarding the sample preparation, analysis, security and Quality Assurance/Quality Control ("QA/QC") protocols used in the drilling programs at Magambazi.

This includes an independent review of QA/QC information relating to those assay results available to February 29th, 2012 and used to support the initial mineral resource at Magambazi (Archibald *et al*, 2012). Subsequent to this time, an additional 69 drill holes have been completed at the project (see Table A2.2 Appendix A2). The section author has not undertaken QA/QC reviews on samples derived from these later drill holes.

11.1 Sampling Method & Approach

Geotechnical logging was performed on the core samples at the drill site to avoid unnecessary breaks that might affect the RQD of the core (Figure 11-1A). Core orientation marks were taken every 6 m using a spear and the core was oriented and marked. At the end of every shift the core was transported by pick-up truck to the core logging facilities at Magambazi camp. The core logging process involved an initial cleaning of the core and checking of the core tags, and mark-ups on the individual boxes. Any discrepancies noted were addressed with the driller who was responsible for the core. At the camp all core was photographed prior to being logged by the geologist with an emphasis on structure, lithology, alteration and mineralisation (Figure 11-1B).

Sample intervals were marked-up by the geologist logging the core and were based on sample intervals of either 0.7 m for mineralised core or 1 m for unmineralised core (Figure 11-1C). Sample intervals were not based on the geological contacts. The physical sampling of the core was done with a diamond blade core cutting saw. The core was sawn in half along the line marked by the geologist to ensure a representative sample is taken (Figure 11-1D).

Sample bags were pre-numbered by a technician and the split core was moved to the sampling area for final preparation. Individual samples were then bagged and the ticket book filled out with tickets added to the sample and to the core box (Figure 11-1E). The "side" of the split core was chosen systematically by reference to the orientation line and foliation in order to prevent any bias in sample selection. The samples from each drill hole were laid out in succession within the sampling area and QC samples were inserted at pre-determined points within the sampling stream. Once bagged, the samples were taped securely to prevent any disturbance during transit (Figure 11-1F). Typically, all bags were sealed at the end of each shift, but it was noted on some occasions that unsealed bags were left overnight. All sample preparation, and in particular the selection and insertion of QC samples, was undertaken under the direct supervision of the logging/project geologist. The remaining core was retained in the core trays and specific gravity and magnetic susceptibility measurements were taken before being placed in storage. The individual sealed sample bags were placed in polypropylene bags and sealed with a hand-tied knot in preparation for shipment to the preparation laboratories.

Figure 11-1: Core Handling & Sampling Photographs

Note: See text for a description of the sampling procedures illustrated. Source: Archibald, 2012.

Based on recommendations by Archibald (2011), certified reference materials are now stored in the main administration building in clearly marked plastic containers (Figure 11-2A). The containers hold individual 100 g standards in clear plastic bags with removable identification labels to minimise the insertion of an incorrect standard (Figure 11-2B). Certified blanks are stored in sealed plastic buckets in a covered shed outside, and further covered by a heavy tarpaulin to reduce exposure to dust and moisture (Figure 11-2C). Once these buckets are opened material is transferred to the sample bag using a plastic scoop, and at the end of the process any unused material is discarded. Coarse reject and pulverized rock samples analysed at SGS Mwanza are stored at their secure facility in Mwanza (Figure 11-2D) before being transferred to the camp to be stored in the open (Figure 11-2E). When analytical pulps are returned from the assay laboratory they are stored in locked shipping containers with purpose built A-frame roofs to minimize the risk of water damage (Figure 11-2F).

In the author's opinion, industry best practices have been employed during the sampling of the drill core, the storage of the reference materials and storage of returned samples.

Reverse circulation (RC) drilling has also been undertaken within the property. The associated sampling methodology is summarized as follows (after Archibald, 2011). The core material was pulverized into chips and delivered to surface using compressed air through the inner tube of the rod string, providing a 30-40 kg sample per metre. Samples were collected in metre sized intervals. At Handeni, RC drill samples were split through a three tier riffle split on the cyclone of the Stanley RC drill rig, bagged into polyethylene sample bags, double tagged and stapled closed before dispatch to the laboratory. Standards, blanks and duplicates were included as quality control samples. RC samples were analyzed using SGS Laboratories' FAA505 analysis protocol, requiring a 25 gram sample subject to fire assay, and AA finish. The larger sample fraction not sent to the laboratory was collected into a large polyethylene plastic bag and stored at the project base camp for future reference.

The initial mineral resource estimation did not include any RC drilling data. As such, QA/QC information associated with these samples were not reviewed as part of this report.

Channel samples were collected at various locations within the property. The sampling methodology is described in Archibald (2011) and is summarised as follows. Channel rock chip samples were collected to represent continuous samples across outcrops or mining faces. Samples were measured using a standard tape measure, marked on the rock face using spray marker paint, and collected using the pick of the hammer, or chisel where required, in order to obtain as representative a sample as possible over 1 m or less. Samples were collected in polyethylene plastic bags, labelled and sealed with staples. Locations were taken by GPS stating ±10.0 m accuracy. Standards were inserted at 50 sample intervals in addition to random duplicate samples. All rock samples were analyzed using SGS Laboratories' FAA505 analysis protocol, requiring a 25 gram sample subject to fire assay, and AA finish.

Figure 11-2: Security & Chain of Custody Related Photographs

Note: See text for a description of the security of samples, standards, blanks illustrated.
Source: All Archibald, 2012, except D (Farrelly, 2012).

Soil samples collected on the property were processed using the sampling procedure outlined in the report of Archibald, 2011. In summary, 3 kg samples were collected in clear plastics bags and a sample tag was inserted prior to sealing. Sample standards and duplicate samples were inserted at 50 sample intervals. The samples were transported to the assay laboratory (SGS in Mwanza), and upon arrival they were dried, sieved using a 2 mm screen, split to produce a 25 to 50 g aliquot, which was digested in *aqua regia* and diisobutyl ketone (DIBK), prior to atomic absorption (AA) gold analysis.

QA/QC information associated with the channel and soil samples were not reviewed as part of this report.

11.2 Laboratory Procedures

All drill core samples were collected and provided to independent laboratories by Canaco. This report presents an independent review and validation of the procedures and data for results that have been analysed to the date of February 29th, 2012.

In order to expedite sample processing for the large number of samples produced, in a short time from the Magambazi drill program, several laboratories and locations have been involved in the preparation and processing of assay results. In particular, SGS Mineral Services Laboratory (African Assay Laboratories Tanzania Ltd.) in Mwanza, Tanzania served as the primary laboratory for sample preparation and assaying. To this end, approximately 89% of all samples tested were prepared and assayed in the SGS Mwanza laboratory. In addition to SGS' laboratory, ALS and ACME laboratories were used to process and analyse a smaller proportion of samples. ALS Chemex Laboratories Mwanza were used to prepare core samples with subsequent assay work being completed at their Johannesburg, South Africa laboratory. Approximately 3.8% of all samples were processed and assayed through ALS' laboratories. Further, ACME Laboratories Ankara were used to prepare core samples with subsequent assay work being completed at their Vancouver, Canada laboratory. Approximately 7.2% of all samples were processed and assayed through ACME's laboratories. In each case, all samples were assayed using appropriate gold fire assay techniques (SGS FAA505; ALS Au-AA24; and ACME G601 + G610 protocols).

To address delays that arose at the primary assay laboratory when site drilling increased from approximately 1,000 m/mo to approximately 9,000 m/mo, in mid-2011, generally:

- samples from mineralised zones were analyzed at SGS
- samples from logged alteration zones were assayed at ALS
- remaining samples were dispatched to ACME.

Initial sampling of early drill holes was limited to high priority zones where mineralisation and/or alteration were recorded during the core logging procedure. Later in the exploration program, retrospective sampling was conducted on lower priority sections of these drill holes and in some cases that material was processed in a different laboratory from the higher priority portion of the same hole. Consequently, the situation exists where sample suites from individual drill holes were sampled, prepared and assayed in different laboratories at different times. Approximately 47 holes or 11.7% of all holes drilled, at this writing, fall into this category.

The SGS Mineral Services facility in Mwanza was awarded ISO/IEC 17025:2005 accreditation during November 2011. The ALS Chemex assay laboratory in Johannesburg has held ISO/IEC 17025:2005 accreditation since April 2008. Check sample analyses were sent to the ALS Laboratory Group in Vancouver for analysis. The ALS Laboratory Group in Vancouver carries current ISO 9001:2008 and ISO/IEC 17025:2005 accreditation. Additional core samples were processed in the ACME Analitik Laboratuar Ankara with subsequent fire assay at ACME

Analytical Laboratories (Vancouver) Ltd. ACME Analytical Laboratories (Vancouver) Ltd., carries current ISO 9001:2008 accreditation for the provision of assays and geochemical analyses

In order to verify laboratory practices and procedures, the author visited the laboratories of ACME Eurasia in Ankara, Turkey as well as those of SGS and ALS in Mwanza, Tanzania between September 19 and 30, 2011.

During this visit, the author found the ACME, SGS and ALS laboratories to be well run operations. The ACME laboratory is a new facility, and as would be expected, the machinery, layout and procedures used in the preparation sections are considered appropriate and fit for purpose. The SGS and ALS laboratories are more established operations and a number of general issues were noted at these laboratories, but nothing was noted during the visit to suggest that the quality of sample preparation or assay has been compromised. The SGS and ALS laboratories in Mwanza are well organised and maintained facilities and each is considered suitable for the preparation and analysis of samples from the Magambazi project.

A summary of the preparation and analytical procedures at each laboratory is detailed in Table 11.1.

Table 11.1: Preparation & Assay Methods Used During Analysis of Drill Core Samples at SGS, ACME & ALS Chemex

Laboratory	Preparation Code	Description	Assay Code	Description	Lower Detection Limit	Upper Detection Limit
SGS	PRP87	Dry, crush, split, pulverise to a nominal 75µm (<1.2kg)	FAA505, FAG505	50g Fire Assay, AAS Finish; 50g, Fire Assay, Gravimetric Finish	0.01 ppm	100 ppm
Acme	R200-100	Crush 1kg passing 10 mesh, split 1000g and pulverize to 200mesh	G601+G610 (+G612)	Fire Assay 50g - AA finish (Automatic Grav Overlimits G612)	0.005 ppm	10 ppm
ALS	Cru-21, SPL-21, Pul-31	Fine crushing to 70% -2mm or better, Split sample using a riffle splitter, Pulverise a split or total sample of up to 250g to 85% passing 75 micron or better	Au-AA24; Au-GRA22	Au by fire assay and AAS (50g); Au by fire assay and gravimetric finish.	0.005 ppm	10 ppm

The sample preparation and assay methodologies used at each of the laboratories, employed by Canaco, are largely comparable. At ALS and ACME, a gravimetric finish is applied to any samples which fall above the upper detection threshold of 10 ppm gold. In contrast, at SGS, the upper detection limit for the FAA505 assay technique is significantly higher at 100 ppm Au, above which a gravimetric finish is undertaken. Dilutions are used at SGS at the instrumentation stage for high-grade or over-range samples which do not breach the upper detection limit threshold.

In the author's opinion, all drill core samples were prepared and assayed using appropriate techniques at the laboratories.

11.3 Sample Security & Chain of Custody Procedures

The chain of custody procedure from the extraction of the core from the core barrel, through logging and sampling up to the point of dispatch to the laboratory is described in Section 11-2. Through all of these stages the responsibility for security lies with Canaco and their on-site personnel. Samples are transported from Magambazi to the Mwanza laboratories by Canaco personnel or by international courier companies in the case of overseas laboratories. The security of the sample during transit cannot be guaranteed as tamper proof seals are not used on the sample bags. Upon receipt at the laboratory, the chain of custody passes to the assayer. Following assay, the remaining material is stored under secure conditions at the laboratory facilities. The chain of custody reverts to Canaco when the samples leave the assay laboratory.

During various site visits, certain lapses in best practice were observed. These include: wearing of rings while handling core and sample bags containing core being left open overnight. These were brought to the attention of Canaco personnel and they are understood to be isolated occurrences.

In general, industry best practices with respect to chain of custody procedures are followed on site. However, the weakest point in any chain of custody is during transport. The absence of tamper proof fastenings on the samples has been noted and their introduction would greatly improve the chain of custody between the site and laboratory.

11.4 Drill Program QA/QC

Diamond drilling at Magambazi was supervised by Canaco geologists who also directed and managed the preparation, logging and sampling of core as well as bulk density measurements. During sampling, quality control standards and blanks were inserted at pre-determined intervals to confidentially monitor laboratory performance. The progressive introduction and refinement of QA/QC procedures at Magambazi included the implementation of field, reject and pulp duplicates, as well as specific programs of re-assaying and umpire laboratory assaying; all consistent with industry best practice.

Throughout the drilling programs at Magambazi, Canaco have refined and improved their QA/QC procedures. Initially, certified reference material (CRMs) and blank samples were inserted within the sampling stream at a rate of 1 CRM per 15 samples and 1 blank per 25 samples. From June 2011, when drilling activity increased significantly, field duplicates were inserted at a rate of 1 per 75 samples.

Following a review of on-site procedures during August 2011, a revised QA/QC protocol was introduced. The rate at which CRMs and blanks was amended to 1 per 20 samples and the insertion of field duplicates was modified to similar levels (i.e. 5%). This was accompanied by the inclusion of pulp and reject duplicates into the sampling stream as additional control samples. These amendments to QA/QC procedures were implemented on a phased basis from August to October 2011.

The individual QA/QC control samples are discussed in the following sections.

11.4.1 Certified Reference Materials or Standards

Canaco has used a variety of CRMs derived from Certified Laboratories in Australia and Canada. Specifically, certified laboratory standards were obtained from Gannet Holdings Pty, Ltd., Western Mineral Standards and Geostats Pty for incorporation into the sampling sequence. Some additional CRMs, sourced from Ore Research and Exploration (OREAS) and CDN Resource Laboratories, were also used as supplementary standards for insertion in non-drill core samples such as pulp duplicates. Since March 2008, all standards have been stored in a secure location within the locked field office.

A summary of the CRMs used routinely by Canaco as part of their drill core QA/QC program is presented in Table 11.2.

With respect to drill core assessment, Canaco has utilized a well-designed suite of standard samples, in terms of gold tenor and representative sample geology.

Monitoring of CRM performance was undertaken by Canaco personnel throughout the drilling and labwork program. Canaco has indicated that it employed a percentage difference from recommended value threshold for CRM failure, from program outset to April 22, 2010, using the following criteria:

- CRM measurements within ±10% from the recommended value for the standard were considered acceptable (a pass);
- CRM measurements higher than ±10% but within ±30% from the recommended value for the standard were considered acceptable (a pass) unless definitive trends were noted across other standards within an individual batch;
- Any CRM measurement in excess of ±30% of the recommended value for the standard was considered acceptable (a pass) if it occurred in a single standard provided that all other standards within an individual batch were acceptable as per the above criteria.

Table 11.2: CRMs Used by Canaco as Part of Drilling QA/QC

Standards								
CRM ID	Value Au ppm	Std. Dev. Au ppm	2 Low[1] Au ppm	2 High[1] Au ppm	3 Low[2] Au ppm	3 High[2] Au ppm	Source	Times Used
AUOE-3	0.6525	0.0352	0.5821	0.7229	0.5469	0.7581	Western Mineral Standards	31
AUOE-4	0.7079	0.0208	0.6663	0.7495	0.6455	0.7703	Western Mineral Standards	53
AUOI-2	1.9904	0.0599	1.8706	2.1102	1.8107	2.1701	Western Mineral Standards	75
AUOI-3	2.1281	0.0459	2.0363	2.2199	1.9904	2.2658	Western Mineral Standards	29
AUOJ-3	2.0707	0.0618	1.9471	2.1943	1.8853	2.2561	Western Mineral Standards	84
AUOL-2	3.8546	0.1047	3.6452	4.064	3.5405	4.1687	Western Mineral Standards	28
G302-10	0.18	0.02	0.14	0.22	0.12	0.24	Geostats PTY	188
G302-7	2.14	0.09	1.96	2.32	1.87	2.41	Geostats PTY	5
G305-7	9.59	0.33	8.93	10.25	8.6	10.58	Geostats PTY	47
G307-3	0.24	0.02	0.2	0.28	0.18	0.3	Geostats PTY	29
G307-6	1.07	0.05	0.97	1.17	0.92	1.22	Geostats PTY	44
G308-1	0.23	0.02	0.19	0.27	0.17	0.29	Geostats PTY	49
G310-6	0.65	0.04	0.57	0.73	0.53	0.77	Geostats PTY	167
G901-7	1.52	0.06	1.4	1.64	1.34	1.7	Geostats PTY	1151
G904-1	12.66	0.51	11.64	13.68	11.13	14.19	Geostats PTY	82
G907-4	3.84	0.16	3.52	4.16	3.36	4.32	Geostats PTY	2
G907-6	7.25	0.29	6.67	7.83	6.38	8.12	Geostats PTY	275
G908-1	0.06	0.01	0.04	0.08	0.03	0.09	Geostats PTY	60
G909-6	0.57	0.03	0.51	0.63	0.48	0.66	Geostats PTY	805
G909-8	34.18	1.39	31.4	36.96	30.01	38.35	Geostats PTY	30
G995-1	2.75	0.18	2.39	3.11	2.21	3.29	Geostats PTY	1037
G998-4	4.36	0.22	3.92	4.8	3.7	5.02	Geostats PTY	1
G999-4	3.02	0.17	2.68	3.36	2.51	3.53	Geostats PTY	857
ST92/1364	8.59	0.37	7.85	9.33	7.48	9.7	Gannet Holdings PTY	19

Note: [1] Lower and upper caution thresholds (± 2 standard deviations). [2] Lower and upper fail thresholds (± 3 standard deviations).

These criteria were not considered to be within acceptable industry standards for disclosure. This was recognized by Canaco personnel and a change to Standard Deviation based thresholds was enacted from April 22, 2010 onward, according to the following criteria:

- any CRM measurement in excess of ± 2 standard deviations from the recommended value was considered a “caution”
- any CRM measurement in excess of ± 3 standard deviations from the recommended value was considered a “fail”
- any assay for a blank sample in excess of 10 times the laboratory detection limit of the technique is considered a “fail.”

The performance of each of the various CRMs is discussed in the following sub-sections.

11.4.1.1 Western Mineral Standards CRMs

Six CRMs sourced from Western Mineral Standards were used as control samples at Magambazi from September 2009 to December 2010 and include AUOE-3, AUOE-4, AUOI-2, AUOI-3, AUOJ-3 and AUOL-2. Control charts illustrating the performance of each of these CRMs are presented in Figures 11-3 to 11-8 on the following pages.

The overall performance of the Western Mineral Standard CRMs is summarized in Table 11.3 below. High fail rates were recorded for AUOE-4, AUOI-3, AUOJ-3 and AUOL-2. It should be noted that these standards were used primarily within early drill holes up to MGZD058 and sporadically thereafter (within holes MGZD80, 84 and 101), before being phased out in December 2010.

These CRMs were sourced in screw cap jars from which the material for the standards was dispensed when required. Based on the results, Canaco considered it likely that inhomogeneity through settling or contamination of the jars may have been an influence on performance of these standards. For this reason, subsequent CRM material was sourced within individually wrapped sachets.

Table 11.3: Summary of Western Mineral Standards CRM Performance

CRM ID	Fail Low	Fail High	Fail Rate	Caution Low	Caution High	Caution Rate
AUOE-3	1	1	6.5%	0	0	0.0%
AUOE-4	7	4	20.8%	4	3	13.2%
AUOI-2	2	3	6.7%	5	3	10.7%
AUOI-3	4	4	27.6%	4	2	20.7%
AUOJ-3	13	2	17.9%	7	1	9.5%
AUOL-2	2	1	10.7%	1	1	7.1%

Figure 11-3: Control Chart for Western Mineral Standard AUOE-3

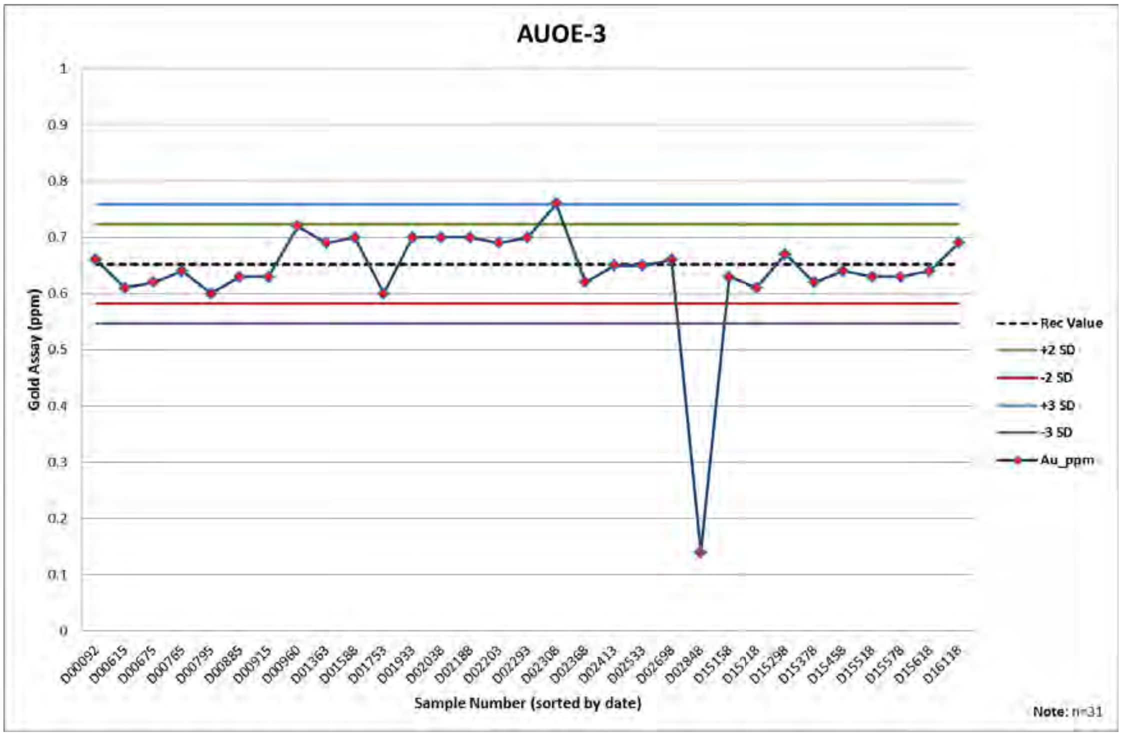


Figure 11-4: Control Chart for Western Mineral Standard AUOE-4

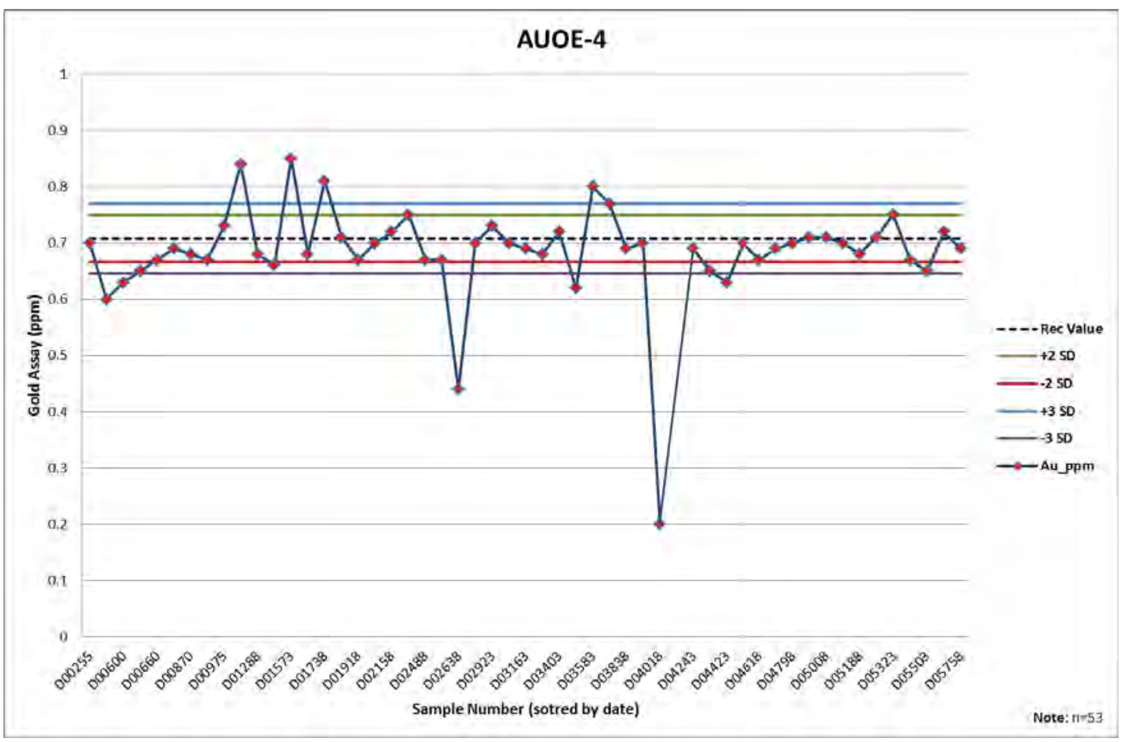


Figure 11-5: Control Chart for Western Mineral Standard AUOI-2

Figure 11-6: Control Chart for Western Mineral Standard AUOI-3

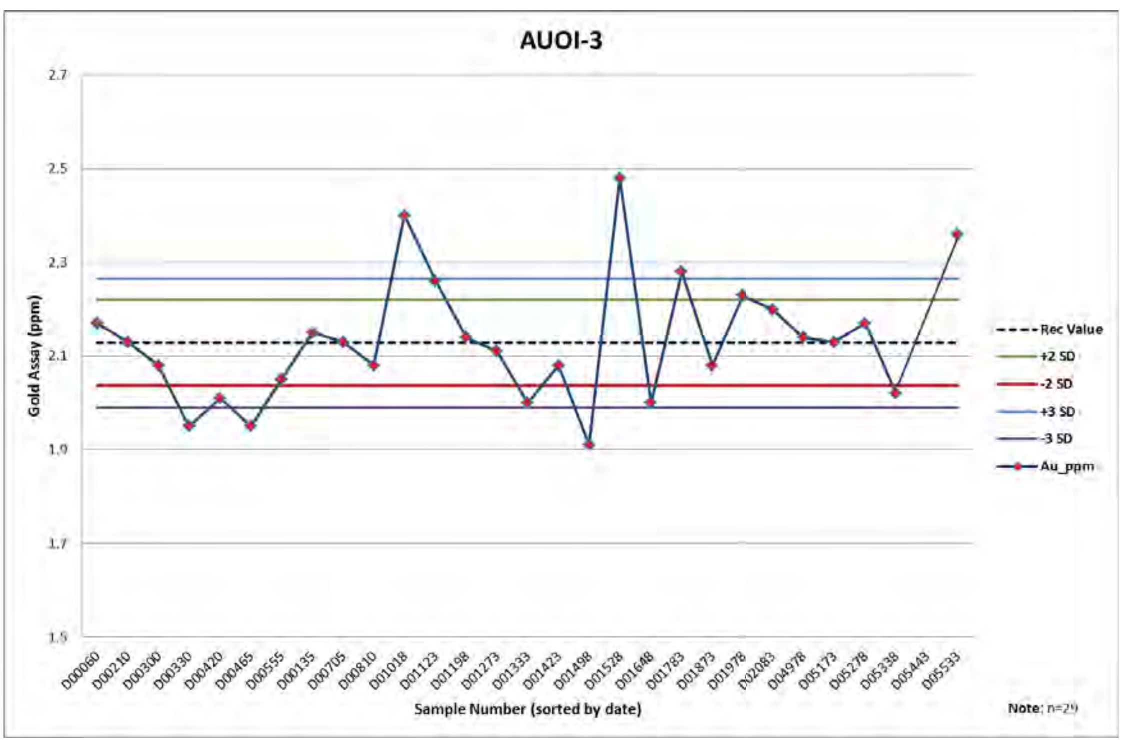


Figure 11-7: Control Chart for Western Mineral Standard AUOJ-3

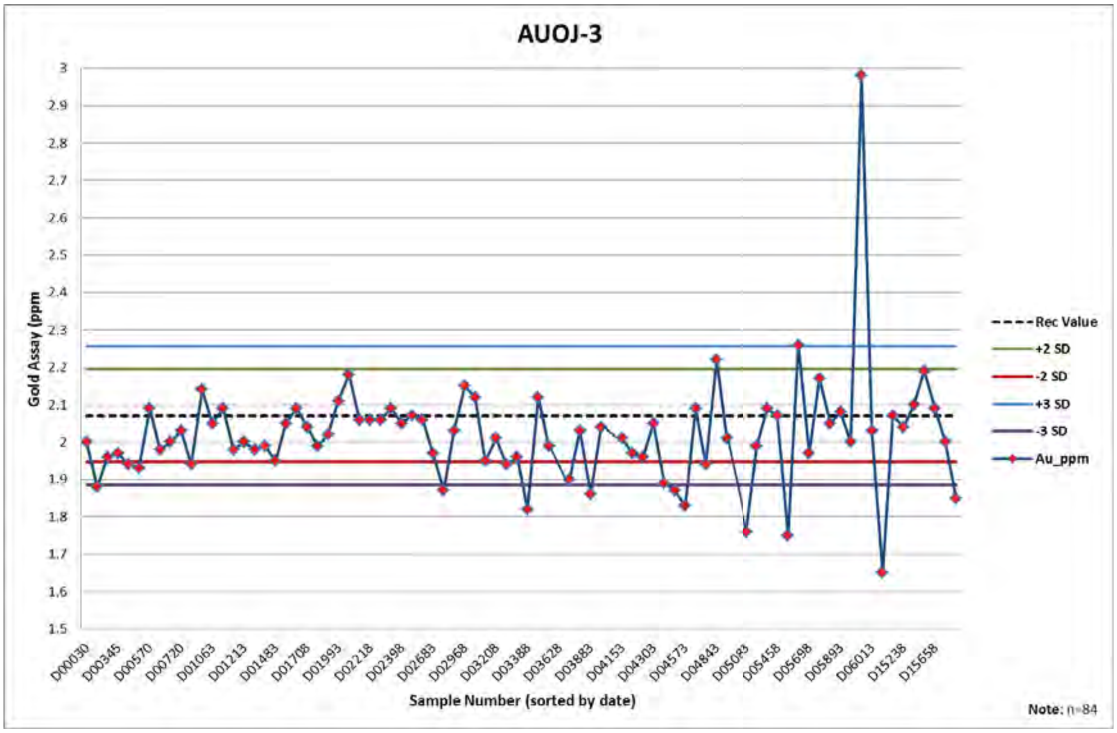
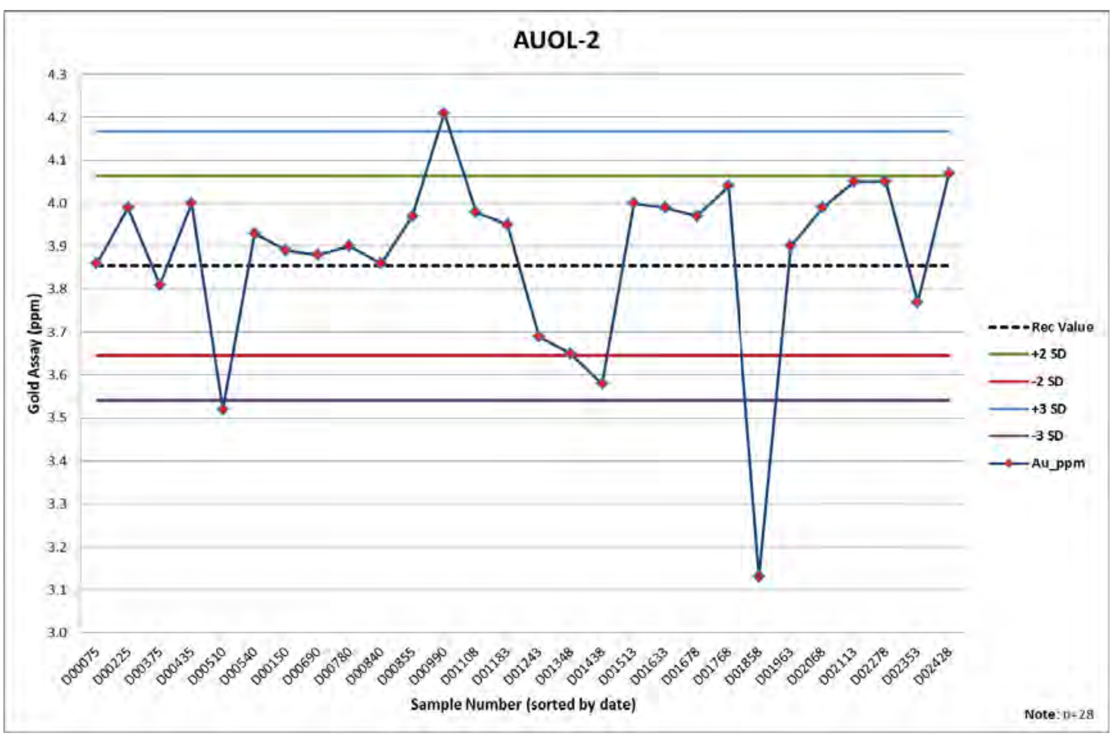


Figure 11-8: Control Chart for Western Mineral Standard AOUL-2



11.4.1.2 Geostats PTY CRMs

From February 2010 onwards, a suite of 17 Geostats Pty CRMs were introduced as control standards on a phased basis. Table 11.2 (above) and Table 11.4 (below) show the specific CRM standards that were used, when they were used and their expected performance characteristics. Of these, G901-7, G995-1, G999-4, G909-6 and G907-6 have been used most frequently and these represent a relatively wide distribution of grades ranging from 0.57 to 7.26 ppm gold.

Table 11.4: Introduction Dates for Geostats PTY CRMs

CRM ID	Start Date	Finish Date
G302-10	07/07/2010	29/08/2011
G302-7	13/02/2012	Present
G305-7	25/02/2010	22/12/2010
G307-3	23/11/2010	29/12/2010
G307-6	25/02/2010	20/12/2010
G308-1	27/03/2011	29/09/2011
G310-6	19/12/2011	Present
G901-7	07/07/2010	Present
G904-1	08/07/2010	Present
G907-4	13/02/2012	Present
G907-6	07/07/2010	Present
G908-1	27/03/2011	31/08/2011
G909-6	07/07/2010	Present
G909-8	08/07/2010	Present
G995-1	07/07/2010	Present
G998-4	13/02/2012	Present
G999-4	25/02/2010	Present

Control charts for a selection of these CRMs are presented in Figures 11-9 to 11-21. The introduction of the Geostats PTY standards coincides with a relative improvement in CRM performance. This is understood to reflect the change to individually wrapped sachets from dispensing jars.

It is clear from the control charts that significant outlier values are present for a number of the Geostats PTY standards (e.g., G302-10, G901-7, G909-6 etc.). Field error is suspected as the primary contributor to CRM failure in the majority of these cases (e.g. sample mix-up: G908-1 inserted instead of G907-1 in batch 205). This was recognised by Canaco personnel and tighter controls were introduced with respect to the handling and recording of information related to CRMs. This has resulted in an overall improvement in the Geostats PTY CRM performance for analytical batches from October 2011 onwards; although continued vigilance is warranted if further drilling/assaying is conducted.

Figure 11-9: Control Chart for Geostats PTY Standard G302-10

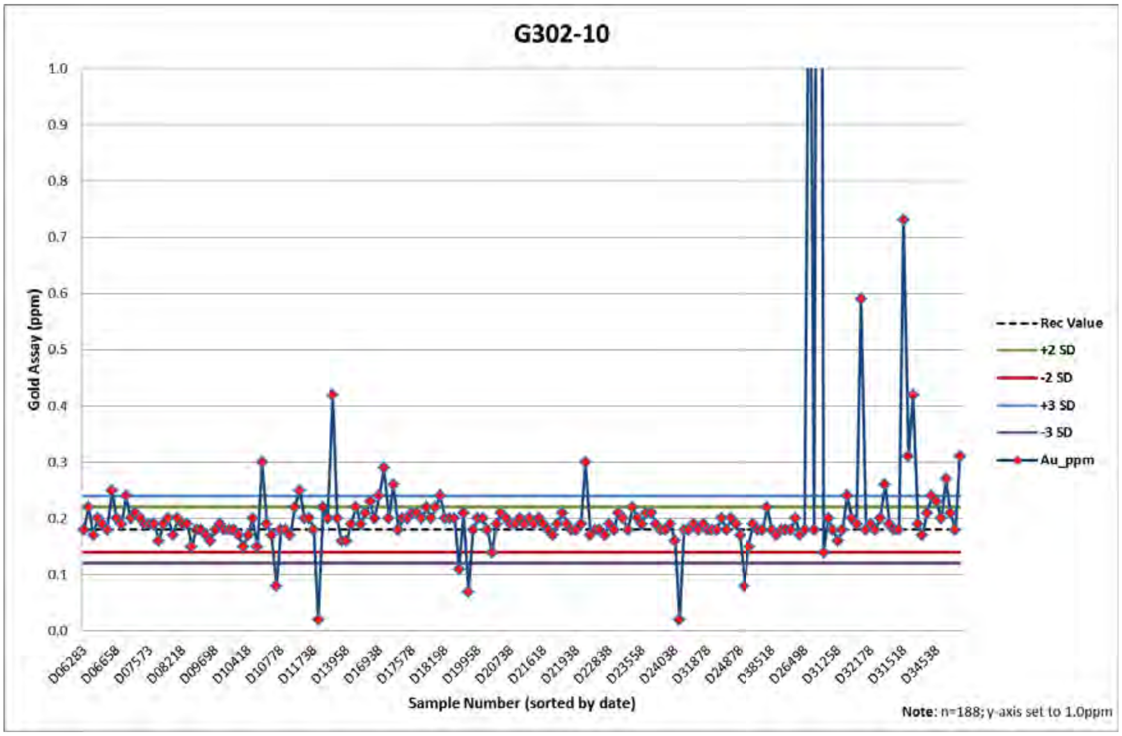


Figure 11-10: Control Chart for Geostats PTY Standard G305-7

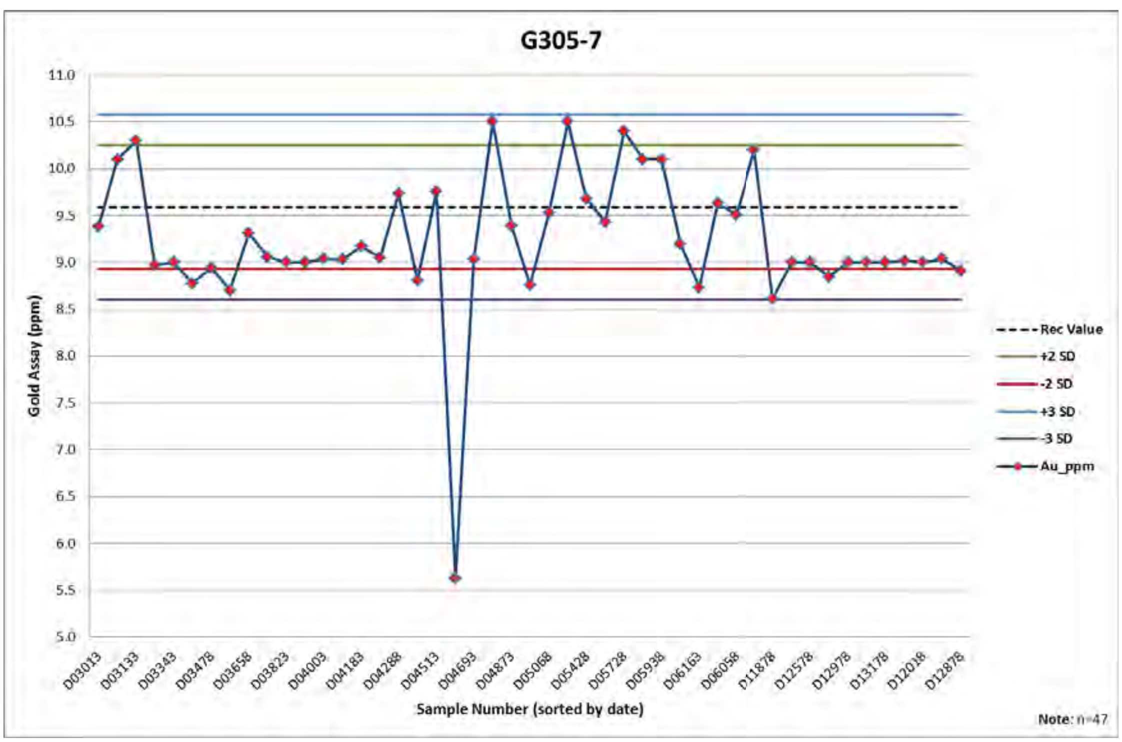


Figure 11-11: Control Chart for Geostats PTY Standard G307-3

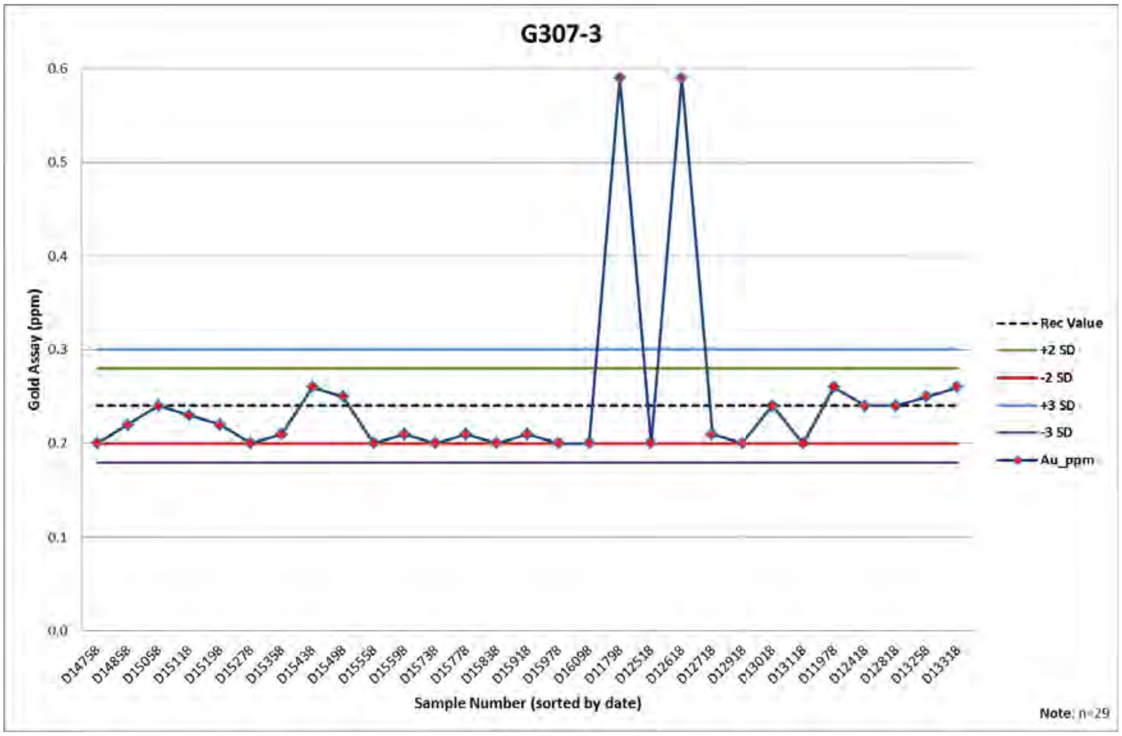


Figure 11-12: Control Chart for Geostats PTY Standard G307-6

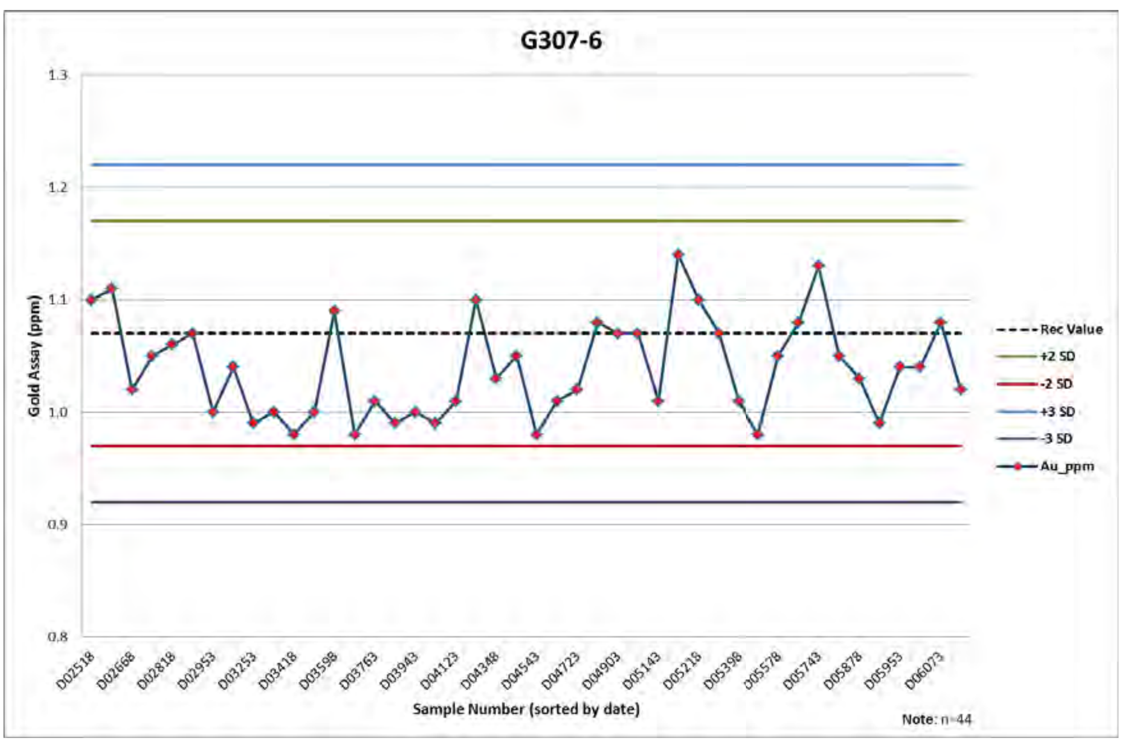


Figure 11-13: Control Chart for Geostats PTY Standard G308-1

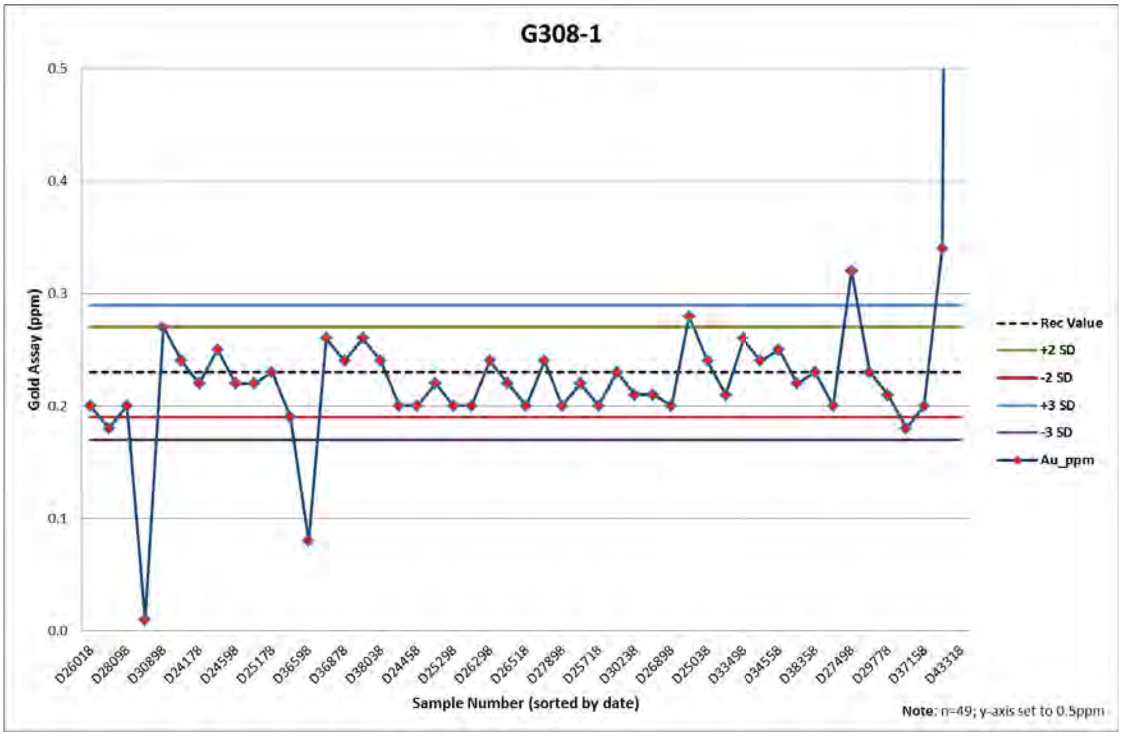


Figure 11-14: Control Chart for Geostats PTY Standard G310-6

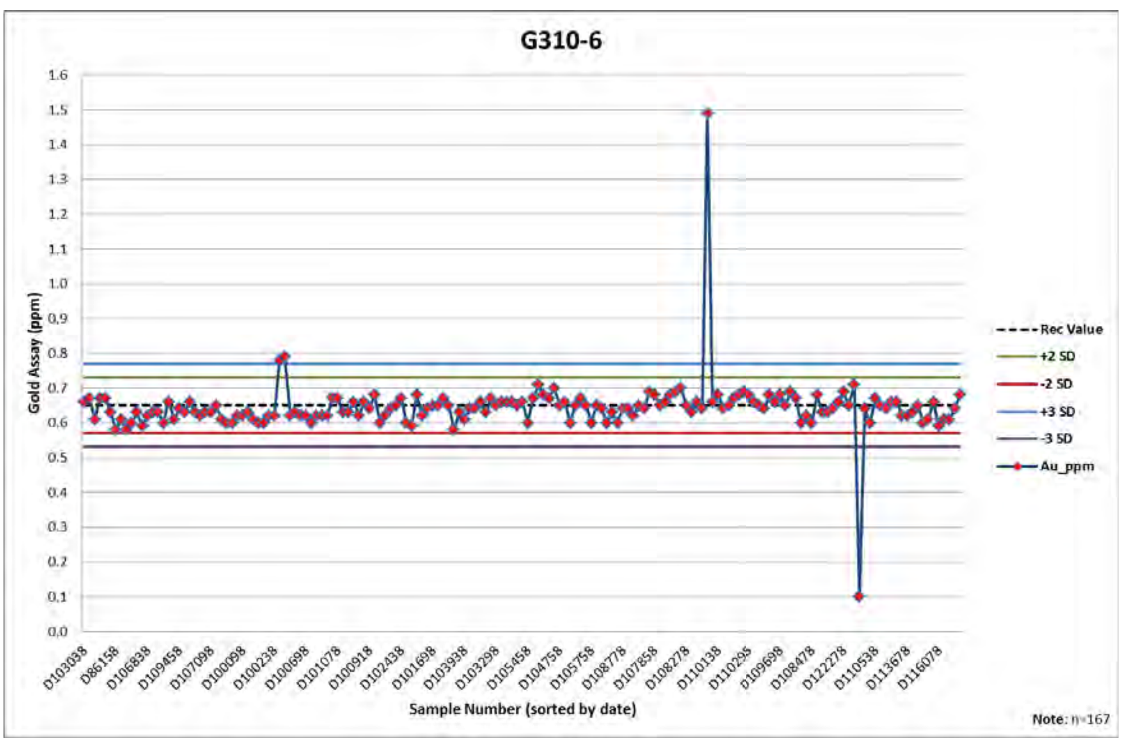


Figure 11-15: Control Chart for Geostats PTY Standard G901-7

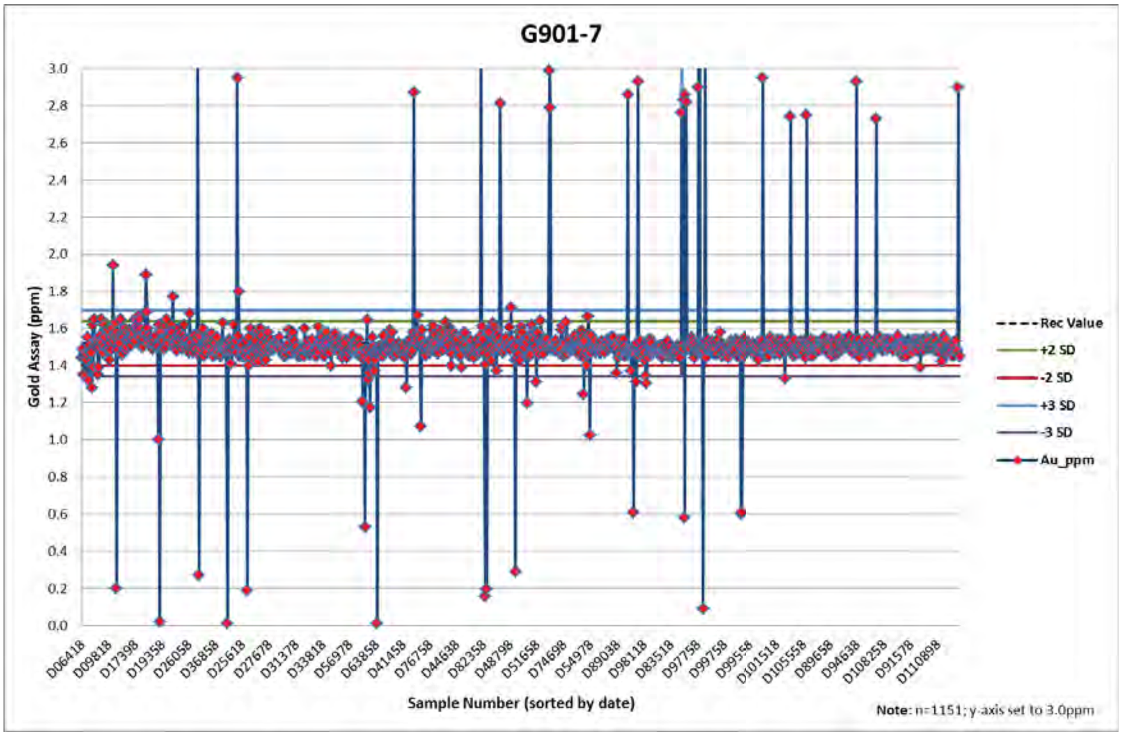


Figure 11-16: Control Chart for Geostats PTY Standard G904-1

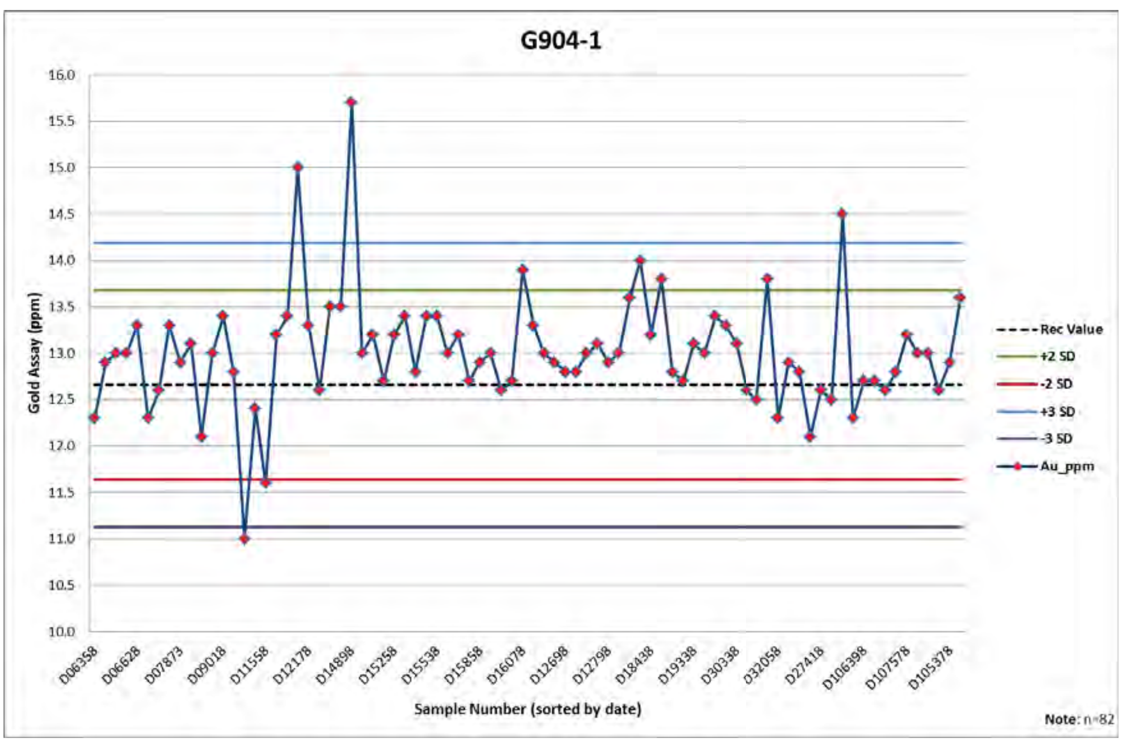


Figure 11-17: Control Chart for Geostats PTY Standard G908-1

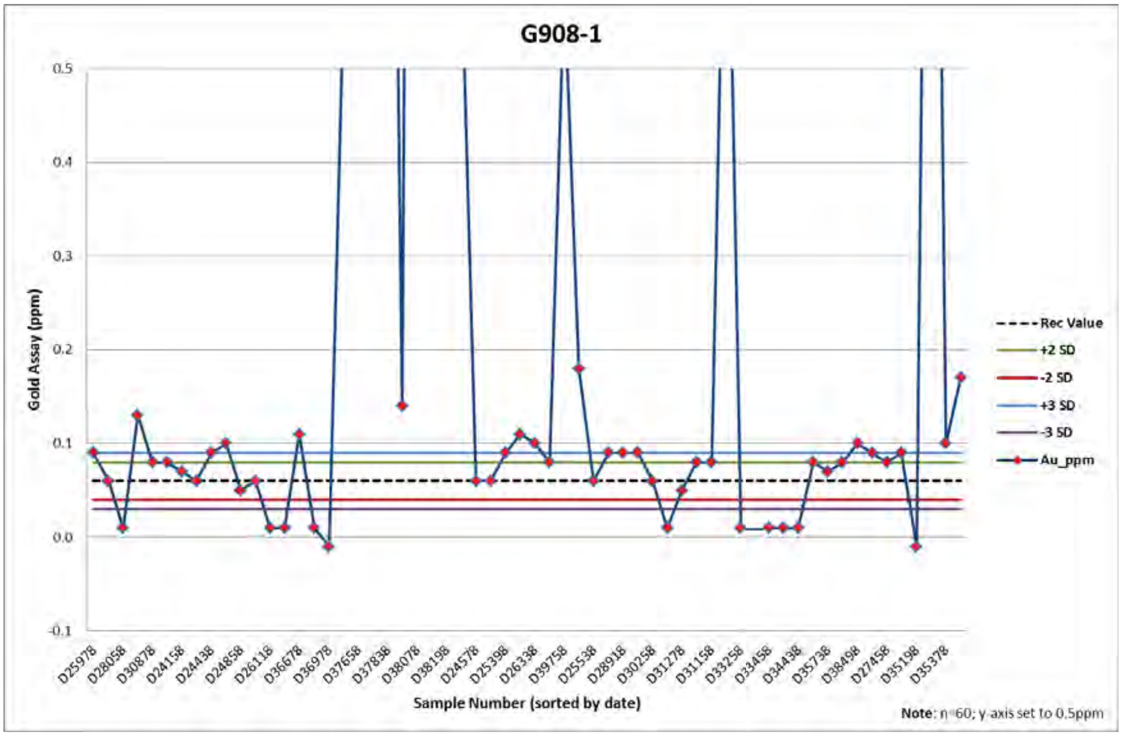


Figure 11-18: Control Chart for Geostats PTY Standard G909-6

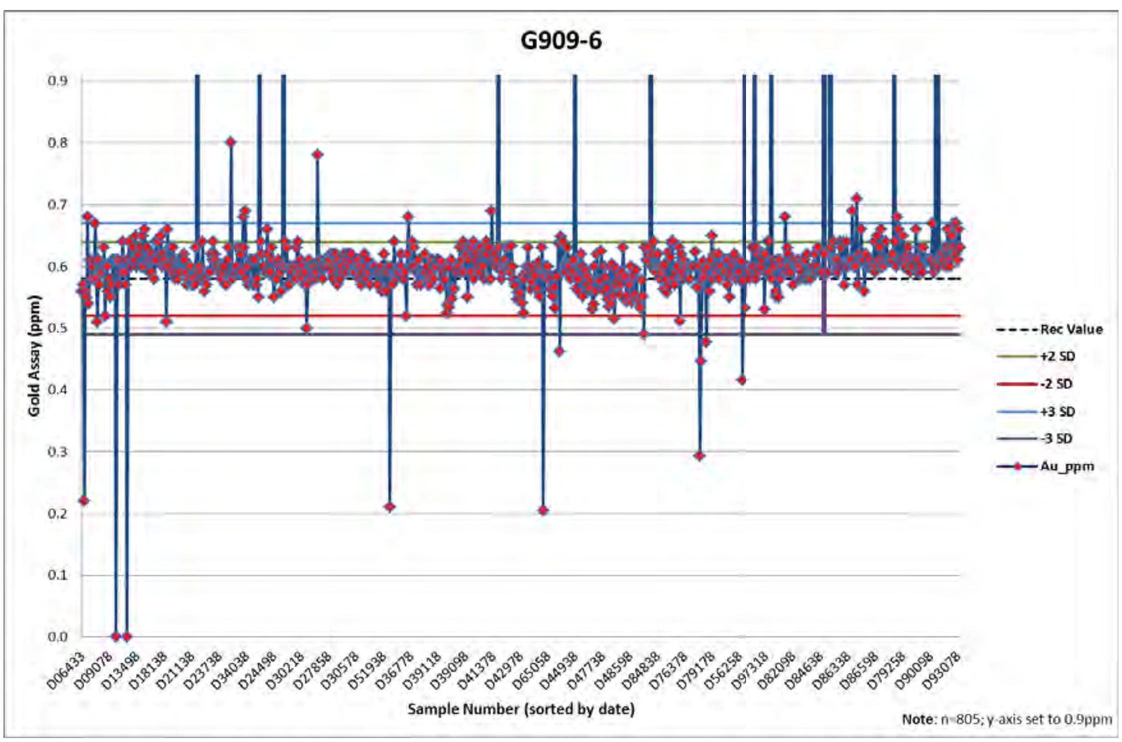


Figure 11-19: Control Chart for Geostats PTY Standard G995-1

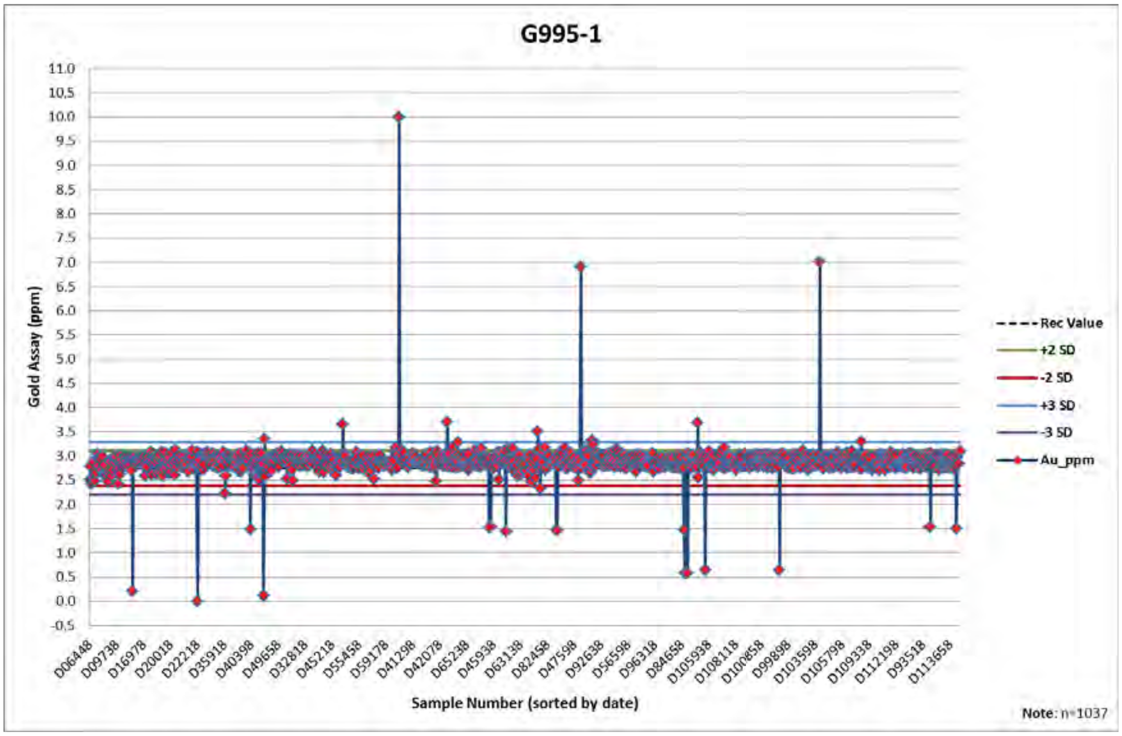


Figure 11-20: Control Chart for Geostats PTY Standard G999-4

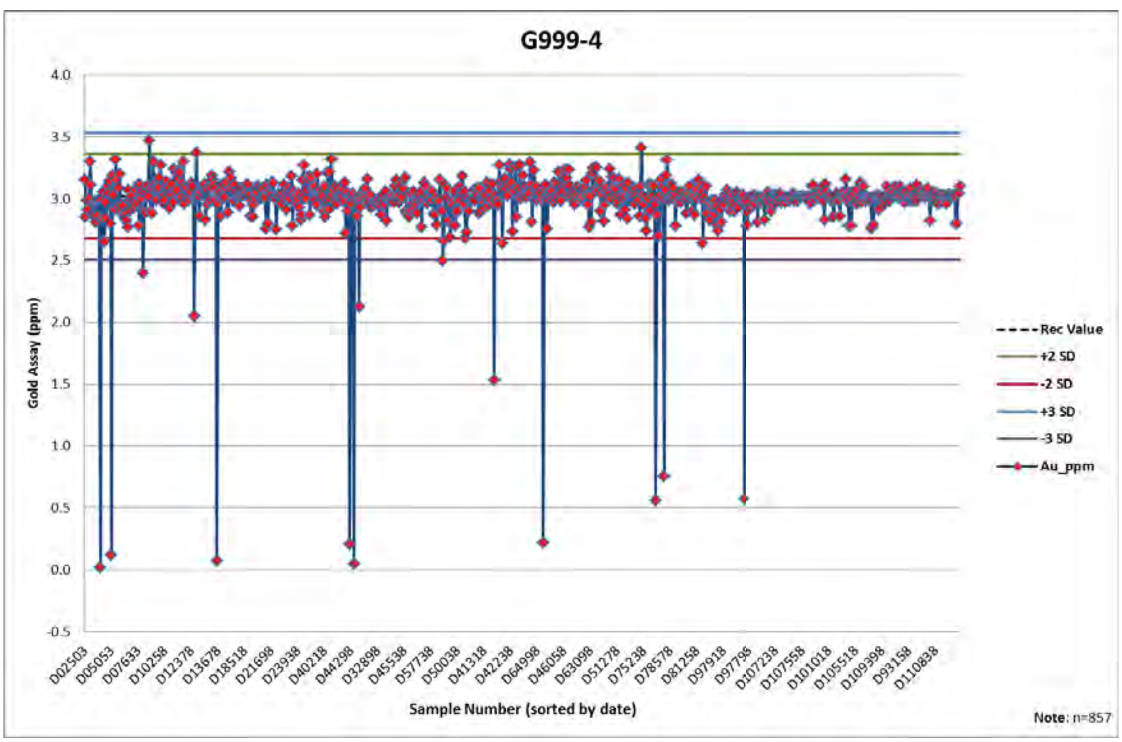
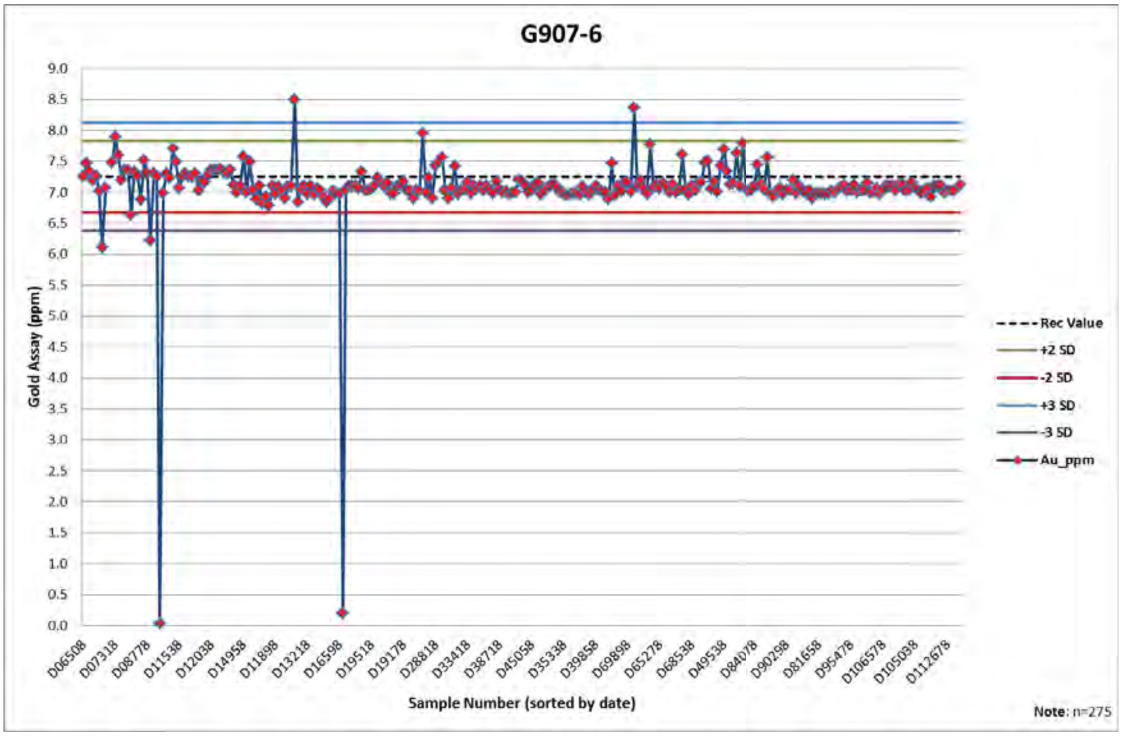


Figure 11-21: Control Chart for Geostats PTY Standard G907-6



The overall performance of the Geostats PTY CRMs is summarized in Table 11.5. Relatively high failure rates, in excess of 5%, were recorded for G302-10, G307-3, G308-1, G901-7, G907-4, and G908-1. The influence of suspected field error is evident for a number of CRMs. Examples include G302-10 (Figure 11-9) where two outlier values of 1.46 and 3.0 ppm Au potentially represent G999-4 and G901-7 respectively; G307-3 (Figure 11-11) in which two outlier values of 0.59 ppm Au possibly represent an incorrectly inserted CRM G909-6; and G901-7 (Figure 11-15) where a number of outlier values occur within the 2.74-2.95 ppm Au range and potentially represent G995-1. Although incorrect recording of the inserted standard is the most likely source of these outlier values, these are still considered to be QA/QC fails for current purposes.

In general, lower grade standards (<0.25 ppm Au) have a poorer overall performance relative to higher grades (e.g. G302-10, 0.18ppm Au; G307-3, 0.24 ppm Au; G308-1, 0.23 ppm Au and G908-1, 0.06 ppm Au). In particular, G908-1 is exceptionally low grade, shows weak behaviour throughout (53.3% fail rate) and is most likely at the sensitivity limit for the SGS FA505 technique. The use of this standard has been discontinued.

Table 11.5: Summary of Geostats PTY CRM performance

CRM ID	Fail Low	Fail High	Fail Rate	Caution Low	Caution High	Caution Rate
G302-10	6	16	11.7%	0	7	3.7%
G302-7	0	0	0.0%	0	0	0.0%
G305-7	1	0	2.1%	8	4	25.5%
G307-3	0	2	6.9%	0	0	0.0%
G307-6	0	0	0.0%	0	0	0.0%
G308-1	2	3	10.2%	2	1	6.1%
G310-6	1	4	2.4%	0	0	0.0%
G901-7	33	26	5.1%	13	12	2.1%
G904-1	1	3	4.9%	1	4	6.0%
G907-4	0	1	50.0%	0	0	0.0%
G907-6	6	2	2.9%	1	2	1.1%
G908-1	11	21	53.3%	0	8	13.3%
G909-6	12	27	4.8%	6	22	3.5%
G909-8	0	1	3.3%	2	1	10.0%
G995-1	18	10	2.7%	2	20	2.1%
G998-4	0	0	0.0%	0	0	0.0%
G999-4	15	0	1.8%	4	3	0.8%

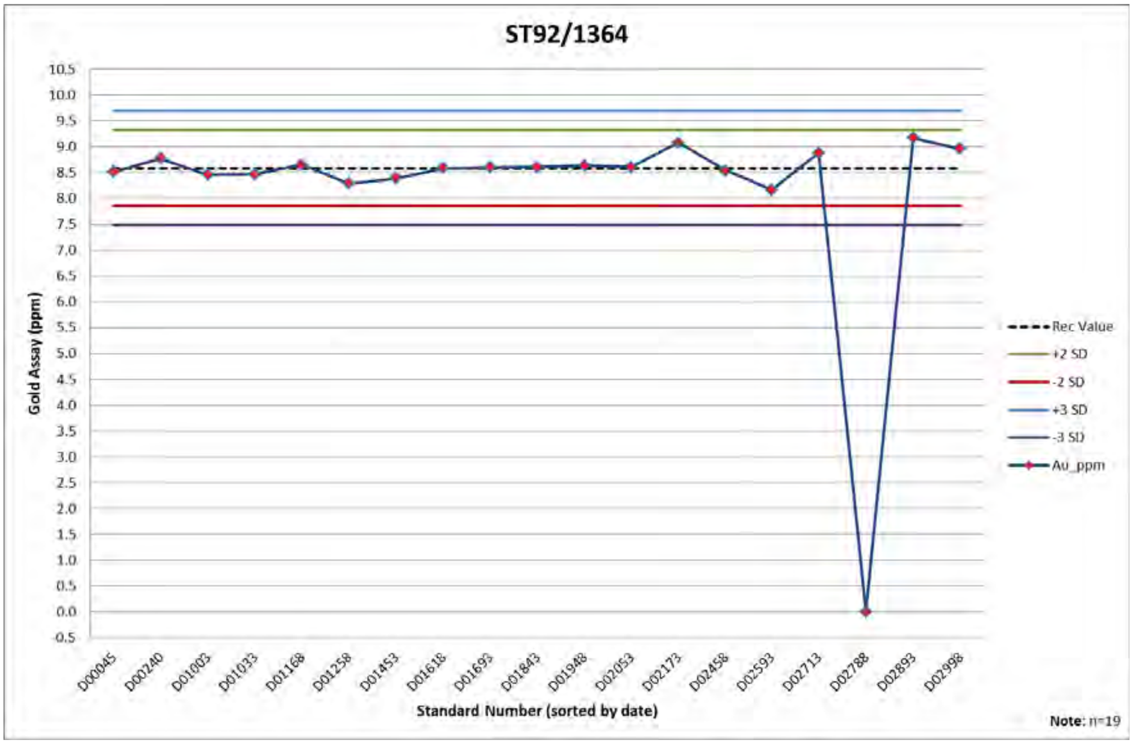
The control chart for CRM G907-6 (Figure 11-21) shows a marked change in behaviour from November 2010 onwards (corresponding to sample D14698). Earlier standards appear to lie at or above the recommended value whereas the subsequent samples tend to fall below the recommended value. The source of this behaviour is unclear but may represent a change in the tenor of the standard or alternatively a change in the laboratory analytical procedure. Further investigation will be required to determine the source of this observed trend.

11.4.1.3 Gannet Holdings PTY CRM

A single high grade CRM, ST92/1364 sourced from Gannet Holdings PTY was used as a control sample at Magambazi from September 2009 to February 2010. The CRM has a recommended value of 8.59 ppm Au and was used sporadically in 18 early drill holes up to and including MGZD035. A performance chart for this CRM is presented in Figure 11-22.

The overall performance of ST92/1364 is generally within acceptable limits with the exception of sample D02788 from MGZD032. In this case, it is suspected that a blank sample was inserted erroneously and that field error is the most likely source of the fail.

Figure 11-22: Control Chart for Geostats PTY Standard ST92/1364



11.4.2 Blank Samples

Three different types of blank sample have been used as a QA/QC control sample during drilling programs at Magambazi. Quartz blanks were sourced from unmineralised quartz veins from the Handeni area and these were used as blank control samples throughout the initial drilling phases. These quartz blanks are considered to be uncontrolled blanks since their grade and quality is not certified in advance.

From December 2010 onwards, certified blank material has been sourced from HUMAC Laboratories in Mwanza. This material consists of granite chips derived from the Mwanza area from which a sub-set is analyzed by HUMAC using their Ultra Trace Geochem technique to demonstrate its suitability for use as a blank sample. The use of the certified blank was introduced on a phased basis largely determined by the availability of certified and uncertified blank material on site.

Low grade CRMs were also used as a “pseudo-blank” control sample at Magambazi. The purpose of a blank sample from a QA/QC perspective is to test for potential contamination within the sample preparation stage of the laboratory procedure. As the CRM material is essentially a pulp, it by-passes the coarse crush and pulverization stages within a laboratory. For this reason, the use of low grade CRMs is not considered an appropriate surrogate to barren rock samples as a monitor for potential contamination. From December 2010 to September 2011, Canaco used

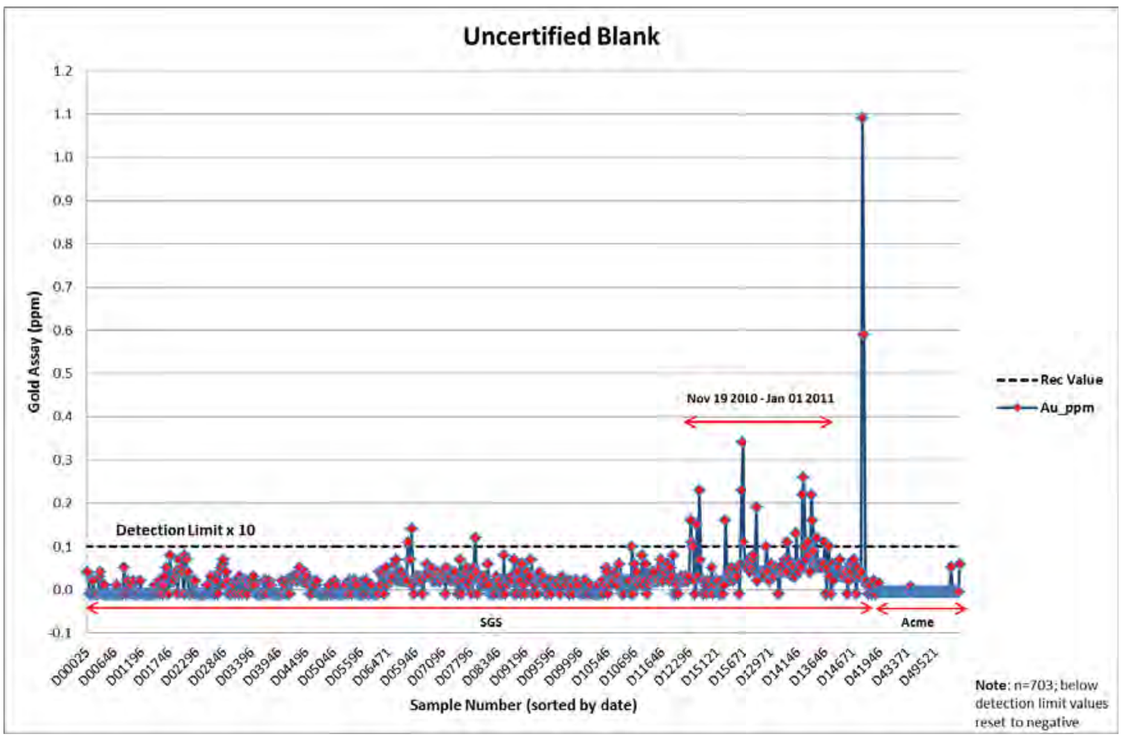
Geostats PTY CRM GLG307-1 sporadically as a blank sample for QA/QC purposes. From a QA/QC perspective, the associated batches are essentially uncontrolled for potential contamination.

11.4.2.1 Uncertified Blank Samples

Canaco has indicated that material for uncertified blank samples is derived from barren quartz veins sourced from the general Handeni area and is considered suitably independent of the Magambazi area.

A control chart to illustrate the performance of the uncertified blank material is presented in Figure 11-23.

Figure 11-23: Control Chart for Uncertified Blank Samples



Note: n=703, BDL values reset to negative.

In general, the majority of the uncertified blank samples are within acceptable limits. A noticeable deterioration in performance is evident between November 2010 and January 2011, during which time the proportion of fails increased. In the majority of cases, no discernible contamination trails are evident within the samples bounding these fails. As such, systematic laboratory contamination is not suspected. It is therefore considered likely that the source of the gold in these samples may relate to elevated levels of gold within the blank material itself. The two high outlier values subsequent to these samples are considered to be the result of field error (i.e. blank sample inserted into an incorrect sample bag). The apparent improvement in later samples is related to the assaying laboratory (ACME) at which the majority of samples were below the detection limit of 0.05 ppm Au. These ACME blank samples were assayed from September – October 2011 after a hiatus in the use of the uncertified blank material. It is considered likely that this improvement reflects replenishment in the supply of uncertified blank material from that used previously, and not from differences in laboratory procedure between ACME and SGS. The overall fail rate for the uncertified blank sample is in the order of 3%.

11.4.2.2 Certified Blank Sample

Material for the certified blank samples was derived from unmineralised granite sourced from the general Mwanza area and is considered suitably independent of the Magambazi area. It is supplied by HUMAC Laboratories in Mwanza, Tanzania who independently assay and certify the material for use as a blank. The certified blank material consists of granite chips of approximately 1cm diameter which are supplied in sealed plastic containers.

Control charts for the performance of the certified blank samples at SGS, ALS and ACME are presented in Figures 11-24 to 11-26.

Figure 11-24: Control Chart for Certified Blank Samples Assayed at SGS

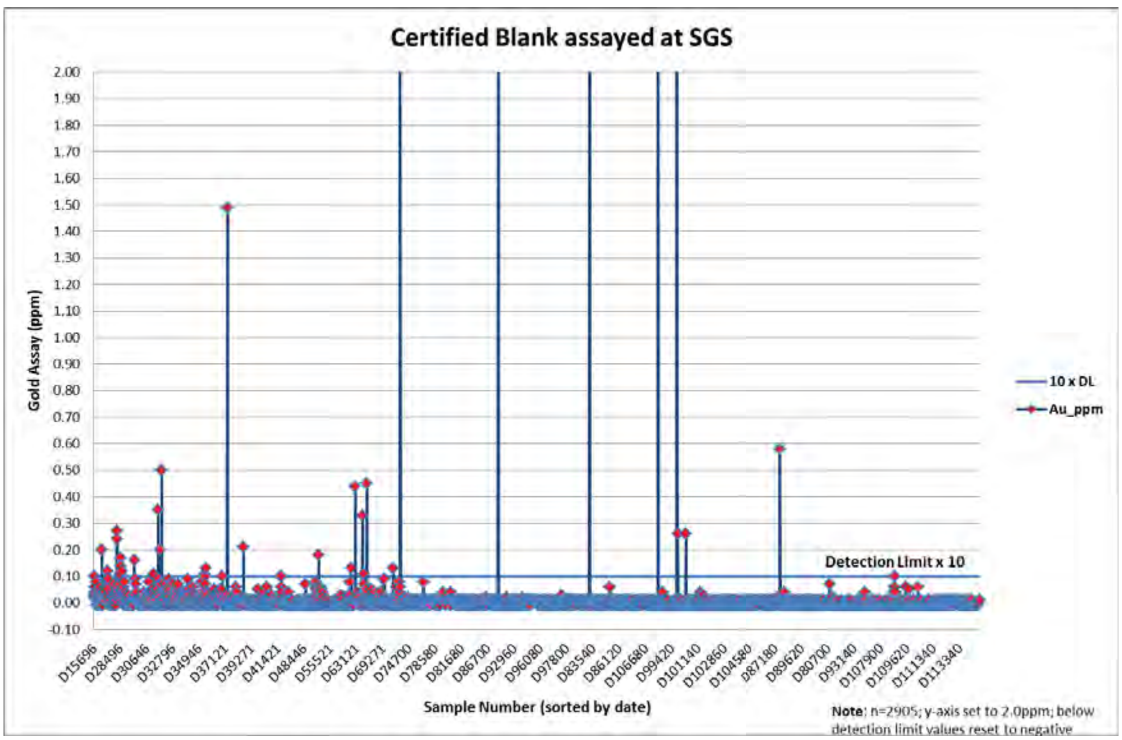


Figure 11-25: Control Chart for Certified Blank Sample Assayed at ALS

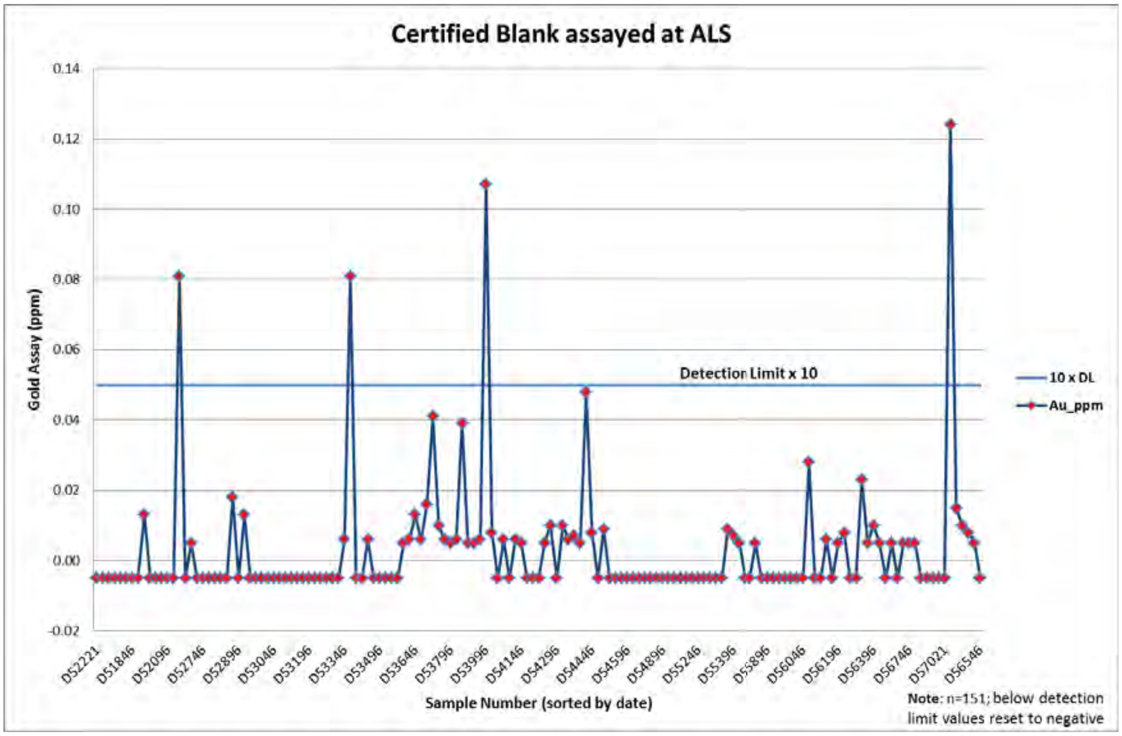
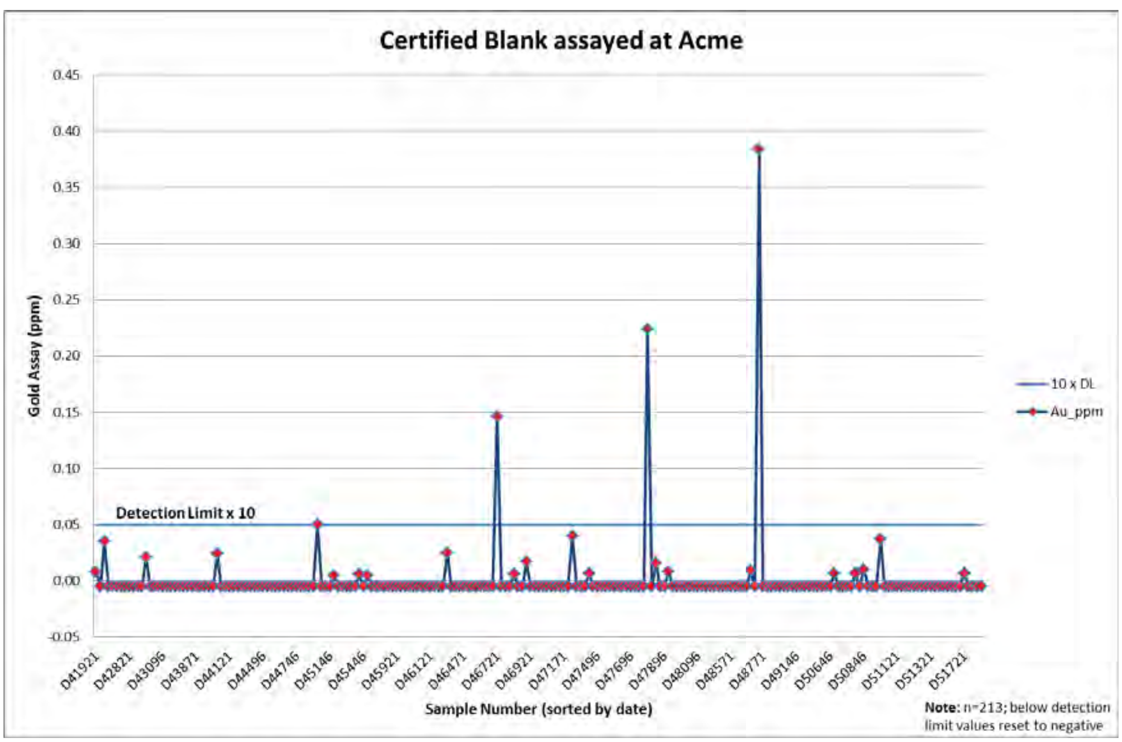


Figure 11-26: Control Chart for Certified Blank Sample Assayed at ACME



In general, the vast majority of certified blank samples are within acceptable limits. The failure rates at each lab are 1.10% for SGS, 2.64% for ALS and 1.41% for ACME. The overall average for the data set is 1.16%, which represents a clear improvement relative to the uncertified blank sample material.

A number of outlier values exist within the SGS certified blank dataset (>0.5ppm). In each case, there is little evidence of contamination trails within the surrounding samples. As such, field error is suspected as the most likely source of these elevated values (i.e. insertion of a CRM in the place of a blank). A noticeable improvement in certified blank performance is evident from September 2011 onwards (MGZD285 and later holes) and may reflect changes to preparation procedures at the laboratory. There are no significant outlier values within the ACME and ALS datasets. Overall performance at both laboratories is generally considered to be good apart from a small number of failing samples.

11.4.2.3 Low Grade CRM GLG307-1

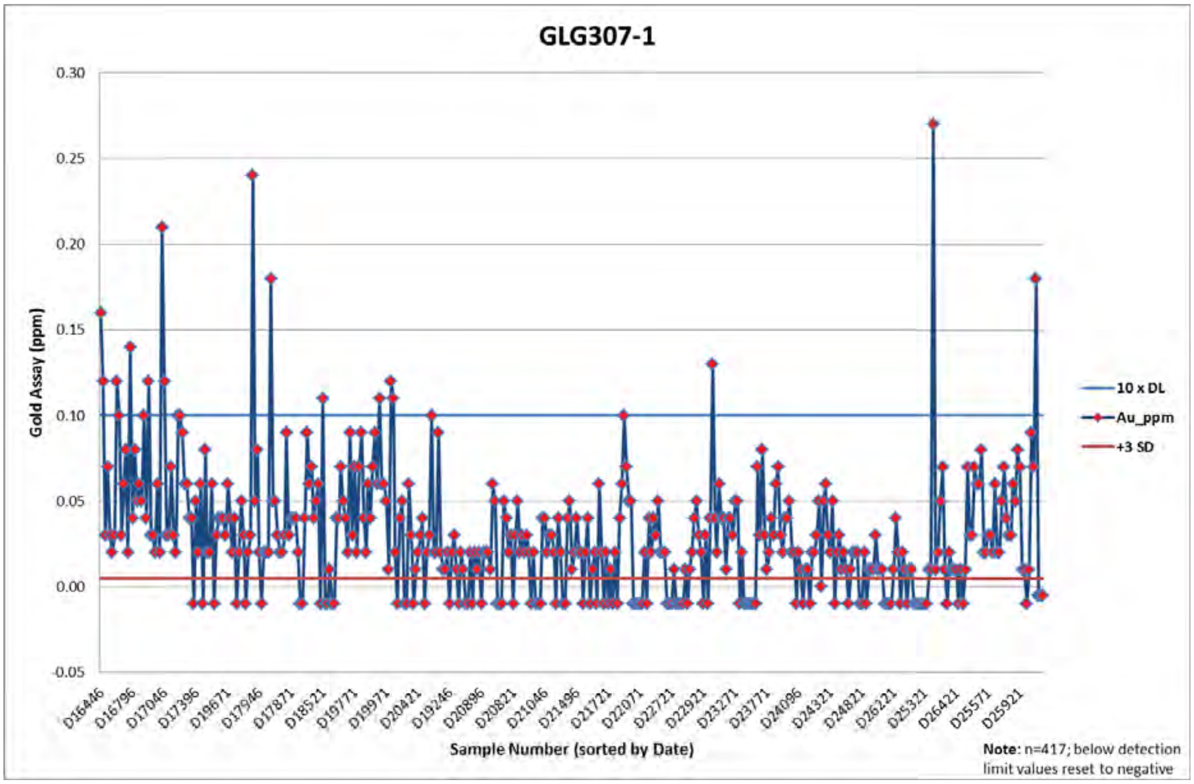
From December 2010 to September 2011, staff at Magambazi used Geostats CRM “GLG307-1” sporadically as a blank sample for QA/QC purposes. This CRM is an exceptionally low grade gold standard (recommended value 2.86 ppb Au; standard deviation 1.70 ppb Au) which is significantly below the lower detection limits for the fire assay techniques used at SGS and ACME (limit of detection 10 ppb and 5 ppb gold, respectively). The primary objective of inserting blank samples as part of a QA/QC program is to monitor for potential contamination within the coarse crush and pulverization stages of the laboratory preparation procedures. For this reason, it is essential that the blank material is similar in tenor to the other samples within a batch, such that it passes through the same preparation routine at the laboratory. GLG307-1 is a pre-pulverized pulp that is supplied as individually wrapped sachets which proceeds to the assaying section of the laboratory without any preparation. The use of GLG307-1 is therefore considered unsuitable as a monitor for contamination within the preparation section of a laboratory.

A control chart for the performance of GLG307-1 is presented in Figure 11-27.

Application of a standard deviation based threshold to GLG307-1 yields an upper limit of 0.0051ppm Au. This level is significantly lower than the lower detection limit for the SGS FA505 technique (L.D.L. = 0.01ppm Au) and close to the lower detection limit for the ACME G601 technique (L.D.L = 0.005 ppm Au). As such, the CRM is at the limits of the lower sensitivity ranges for each of these assay techniques. An upper threshold of 0.1 ppm has been applied within the control chart which corresponds to 10 times the detection limit at SGS; the laboratory at which the majority (99%) of the samples were assayed. Using this discriminator, 16 fails are evident within the dataset corresponding to a fail rate of 3.8%.

The reason for the relatively high fail rate is unclear but may be related to the sensitivity of the assay technique at low grades or alternatively to potential residual contamination from the use recycled fusion pots. Given that the pattern of fails within the GLG307-1 data does not suggest a systematic error and that similar trends are not evident within the other blank datasets (uncertified and certified blanks); the former interpretation is favoured.

Figure 11-27: Control Chart for Blank Sample GLG307-1 assayed at SGS & ACME



It should be stressed that the use of GLG307-1 is not considered an appropriate monitor for preparation stage contamination and its use has been discontinued since October 2011. GLG307-1 was used systematically as a blank sample at Magambazi for a ten-month period from December 2010 and was included in 73 batches relating to samples from 67 individual drill holes. These are summarized in Table 11.6 on the following page. From a QA/QC perspective, these batches are uncontrolled for potential contamination.

11.4.3 Duplicate Samples

A number of duplicate sample types have been included as part of routine QA/QC procedures at Magambazi from June 2011 onwards, when drilling activity increased significantly at site. Subsequently, reject and pulp duplicate samples were introduced and the insertion rate for all duplicate samples was increased to 1 per 20 samples. The various duplicate sample types are discussed in the following sections.

Table 11.6: Listing of Drill Holes & Batches in Which GLG307-1 Was Used as a Blank Sample

Hole_ID	StandardID	Au_Job_No
MGZD002	GLG307-1	MW103522
MGZD002	GLG307-1	MW110237
MGZD002	GLG307-1	MW110236
MGZD003	GLG307-1	MW103518
MGZD003	GLG307-1	MW103519
MGZD003	GLG307-1	MW110237
MGZD003	GLG307-1	MW110238
MGZD006	GLG307-1	MW103520
MGZD006	GLG307-1	MW110238
MGZD006	GLG307-1	MW110239
MGZD007	GLG307-1	MW110239
MGZD010	GLG307-1	MW110239
MGZD010	GLG307-1	MW110240
MGZD011	GLG307-1	MW103519
MGZD011	GLG307-1	MW111063
MGZD013	GLG307-1	MW103519
MGZD013	GLG307-1	MW111064
MGZD014	GLG307-1	MW111065
MGZD015	GLG307-1	MW103436
MGZD016	GLG307-1	MW103436
MGZD016	GLG307-1	MW103437
MGZD018	GLG307-1	MW111065
MGZD019	GLG307-1	MW111066
MGZD019	GLG307-1	MW111065
MGZD021	GLG307-1	MW111066
MGZD021	GLG307-1	MW111067
MGZD022	GLG307-1	MW111067
MGZD022	GLG307-1	MW111068
MGZD025	GLG307-1	MW111068
MGZD026	GLG307-1	MW111069
MGZD026	GLG307-1	MW111068
MGZD028	GLG307-1	MW111069
MGZD028	GLG307-1	MW111070
MGZD029	GLG307-1	MW111071
MGZD029	GLG307-1	MW111072
MGZD030	GLG307-1	MW110109
MGZD030	GLG307-1	MW111072
MGZD036	GLG307-1	MW110108
MGZD039	GLG307-1	MW103439
MGZD039	GLG307-1	MW103440
MGZD039	GLG307-1	MW103441
MGZD041	GLG307-1	MW103441
MGZD041	GLG307-1	MW103442
MGZD042	GLG307-1	MW110232
MGZD044	GLG307-1	MW110109
MGZD044	GLG307-1	MW110108
MGZD060	GLG307-1	MW110111
MGZD064	GLG307-1	MW110111
MGZD064	GLG307-1	MW110110
MGZD065	GLG307-1	MW110111
MGZD065	GLG307-1	MW110112
MGZD069	GLG307-1	MW110235
MGZD073	GLG307-1	MW110230
MGZD074	GLG307-1	MW110231
MGZD074	GLG307-1	MW110232
MGZD078	GLG307-1	MW103437
MGZD078	GLG307-1	MW103438
MGZD082	GLG307-1	MW110232
MGZD083	GLG307-1	MW103436
MGZD083	GLG307-1	MW110242
MGZD089	GLG307-1	MW103442
MGZD095	GLG307-1	MW110233
MGZD098	GLG307-1	MW110234
MGZD100	GLG307-1	MW103520
MGZD100	GLG307-1	MW103521
MGZD100	GLG307-1	MW103522
MGZD101	GLG307-1	MW110233
MGZD101	GLG307-1	MW110234
MGZD102	GLG307-1	MW103517
MGZD102	GLG307-1	MW103518
MGZD103	GLG307-1	MW103522
MGZD103	GLG307-1	MW103523
MGZD103	GLG307-1	MW103524
MGZD104	GLG307-1	MW103438
MGZD104	GLG307-1	MW103439
MGZD105	GLG307-1	MW103527
MGZD105	GLG307-1	MW103527
MGZD106	GLG307-1	MW103525
MGZD106	GLG307-1	MW103526
MGZD107	GLG307-1	MW103524
MGZD107	GLG307-1	MW103525
MGZD108	GLG307-1	MW103528
MGZD109	GLG307-1	MW103617
MGZD110	GLG307-1	MW103526
MGZD110	GLG307-1	MW103527
MGZD111	GLG307-1	MW103618
MGZD111	GLG307-1	MW103617
MGZD112	GLG307-1	MW103618
MGZD112	GLG307-1	MW103619
MGZD113	GLG307-1	MW103619
MGZD113	GLG307-1	MW103620
MGZD114	GLG307-1	MW103528
MGZD114	GLG307-1	MW103529
MGZD115	GLG307-1	MW103620
MGZD115	GLG307-1	MW103621
MGZD116	GLG307-1	MW103622
MGZD116	GLG307-1	MW103623
MGZD117	GLG307-1	MW103621
MGZD117	GLG307-1	MW103622
MGZD118	GLG307-1	MW103624
MGZD118	GLG307-1	MW103625
MGZD118	GLG307-1	MW103623
MGZD119	GLG307-1	MW103625
MGZD119	GLG307-1	MW103626
MGZD120	GLG307-1	MW110112
MGZD120	GLG307-1	MW110113
MGZD121	GLG307-1	MW110114
MGZD121	GLG307-1	MW110115
MGZD122	GLG307-1	MW110226
MGZD122	GLG307-1	MW110227
MGZD123	GLG307-1	MW110227
MGZD123	GLG307-1	MW110228
MGZD123	GLG307-1	MW110229
MGZD124	GLG307-1	MW110230
MGZD124	GLG307-1	MW110229
MGZD125	GLG307-1	MW110235
MGZD125	GLG307-1	MW110236
MGZD125	GLG307-1	MW110236
MGZD126	GLG307-1	MW110240
MGZD126	GLG307-1	MW110241
MGZD126	GLG307-1	MW110241
MGZD127	GLG307-1	MW111070
MGZD127	GLG307-1	MW111071
MGZD128	GLG307-1	MW111075
MGZD128	GLG307-1	MW111073
MGZD128	GLG307-1	MW111074
MGZD129	GLG307-1	MW111080
MGZD129	GLG307-1	MW111077
MGZD129	GLG307-1	MW111078
MGZD129	GLG307-1	MW111079
MGZD130	GLG307-1	MW111075
MGZD130	GLG307-1	MW111076
MGZD130	GLG307-1	MW111077

11.4.3.1 Field Duplicates

Field duplicates are secondary splits of drill samples which are used to assess geological variability and combined sampling/analytical variance. Field duplicates at Magambazi consist of quartered splits of the core from the selected sample. This sample type was introduced during June 2011 with an initial insertion rate of 1 per 75 samples. From September 2011 onwards, the insertion rate for field duplicates was increased to 1 per 20 samples. A total of 2,099 field duplicates have been taken to date and dominantly from drill holes MGZD200 onwards. The majority of these samples were assayed at SGS (94.6%) with lower proportions assayed at ALS (2.3%) and ACME (3.1%).

Scatterplots of the original vs duplicate values for the entire field duplicate dataset and for assays from individual laboratories are presented in Figures 11-28 to 11-32 on the following pages.

The scatterplots in Figures 11-28 and 11-29 for the entire dataset show a poor overall correlation with marked variation at lower grades below 3 ppm Au. There is a slight tendency towards higher original assay results within the data, although a number of duplicate values within the 5.5-14.6 ppm Au range correspond with low grade original assay results generally less than 0.5 ppm Au, as seen in Figure 11-29.

Separate scatterplots were prepared for assays conducted at individual laboratories and are presented in Figures 11-30 to 11-32. As expected, the SGS data shows a similar overall trend to the dataset as a whole. The ALS and ACME field duplicate datasets are generally low grade (<2.5 ppm Au). Both show a moderate correlation up to 0.2 ppm Au and 0.3 ppm Au respectively, with a slight tendency towards higher original assay results in both cases.

In spite of the variability between individual sample pairs, the average values for the original and duplicate samples are similar as seen in Table 11.7 below.

Table 11.7: Average Values for Field Duplicate Pairs

	Original Assay Gold ppm	Duplicate Assay Gold ppm
SGS Average	0.336	0.322
ALS Average	0.029	0.097
ACME Average	0.037	0.357
Overall Average	0.32	0.316

In general the correlation between field duplicates is poor. This suggests that there is significant heterogeneity between sample pairs and supports the observation that gold mineralisation at Magambazi has a strong nugget effect.

Figure 11-28: Scatterplot for the Entire Field Duplicate Dataset

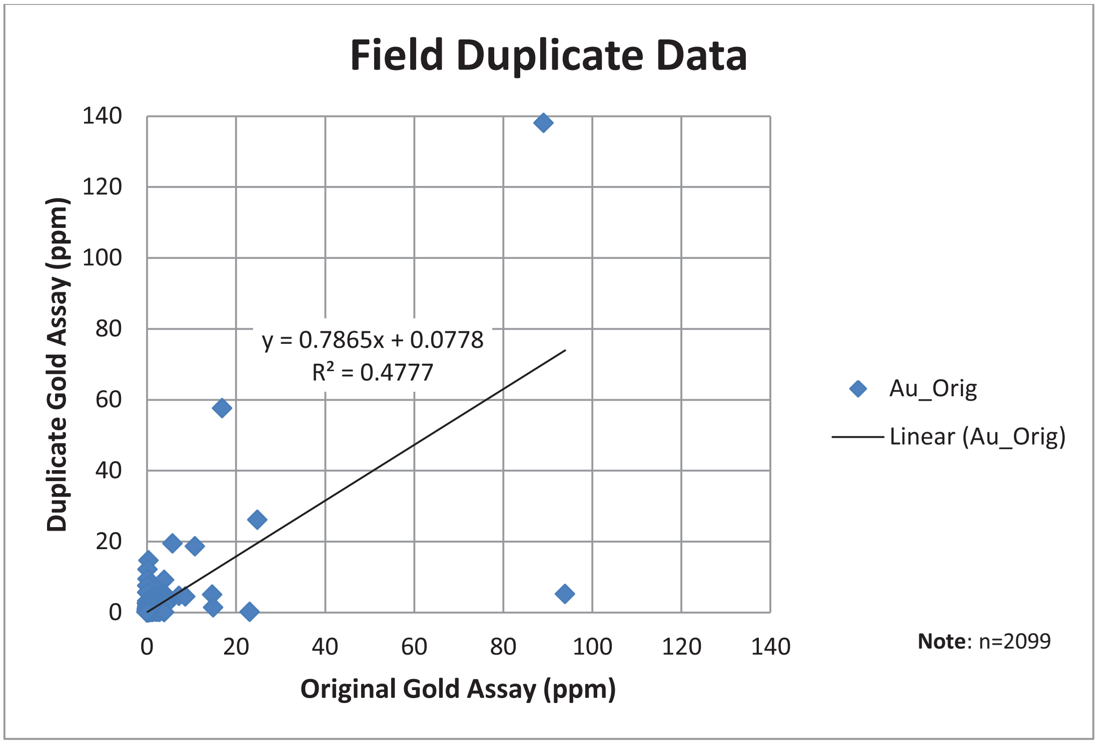


Figure 11-29: Scatterplot for Field Duplicate Data Ranging from 0 to 20 ppm Au

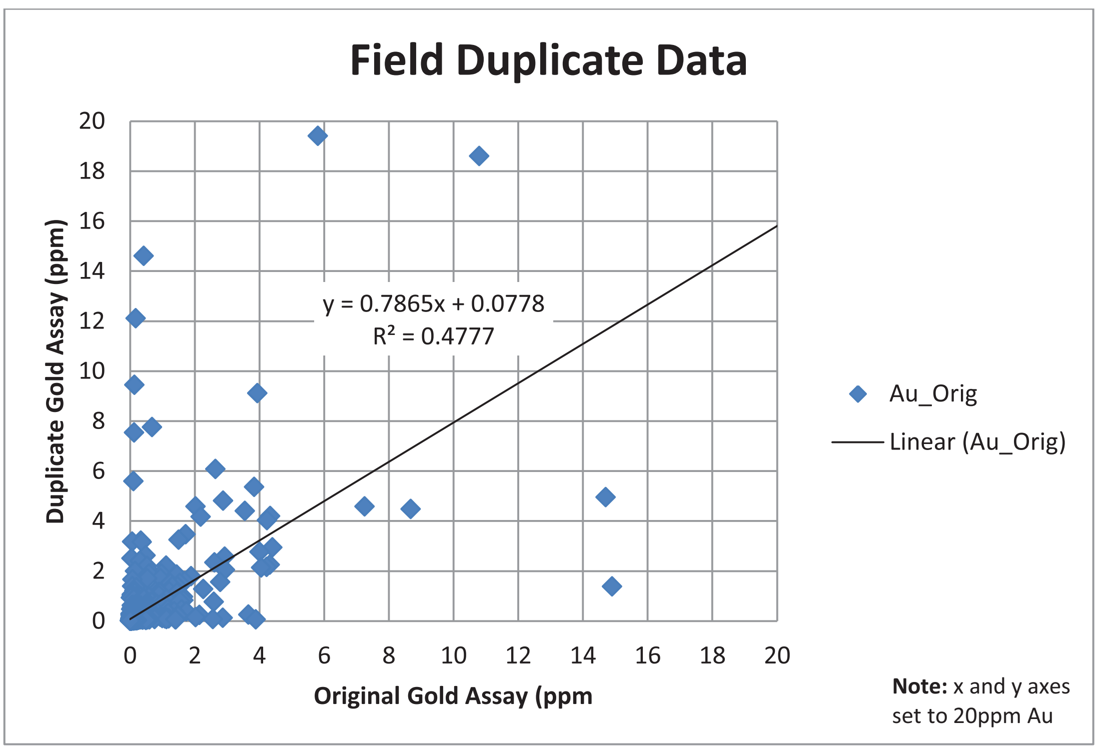


Figure 11-30: Scatterplot for Field Duplicates Assayed at SGS

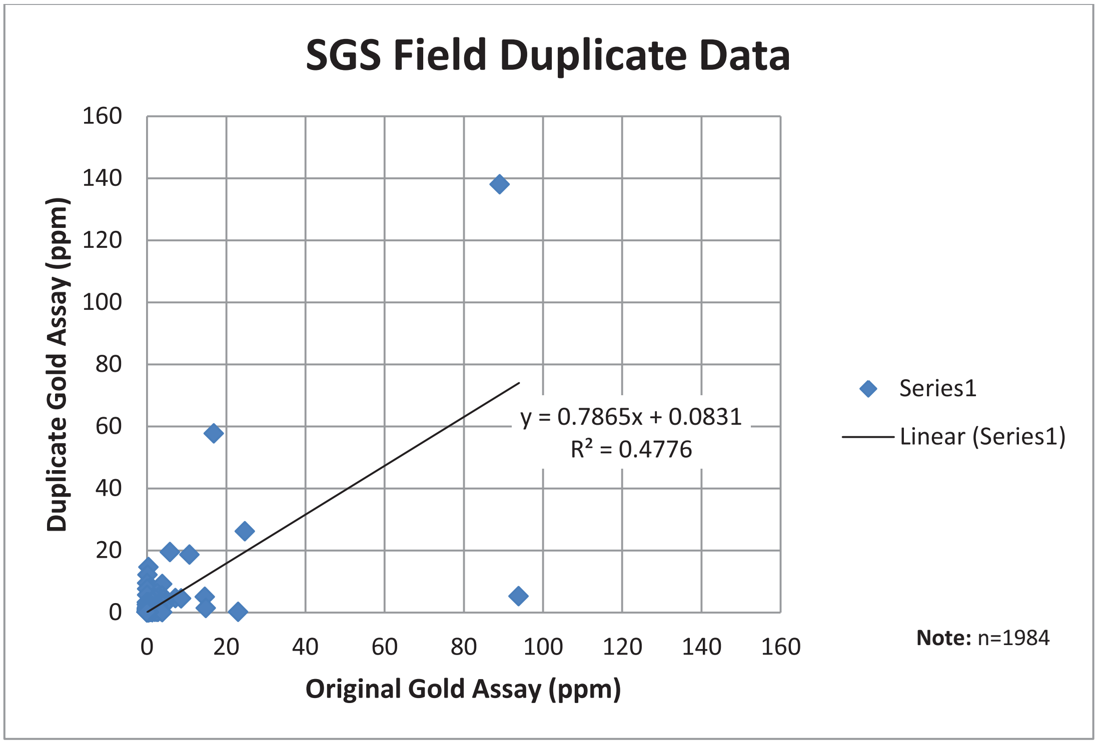


Figure 11-31: Scatterplot for Field Duplicates Assayed at ALS

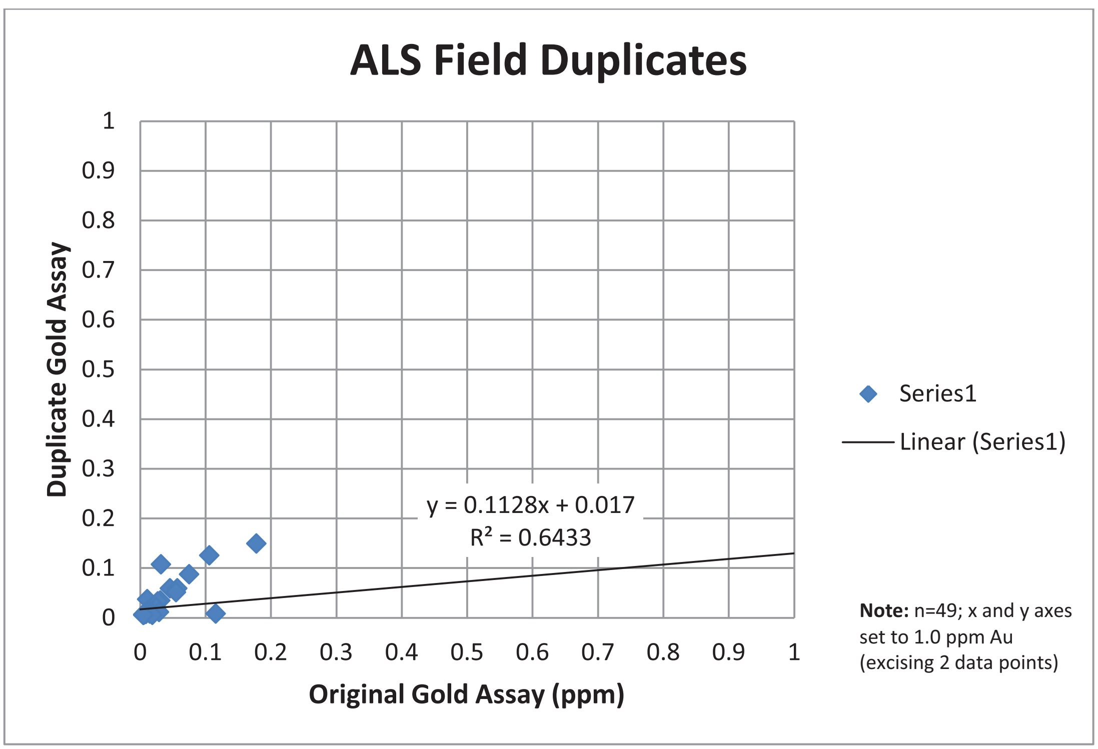
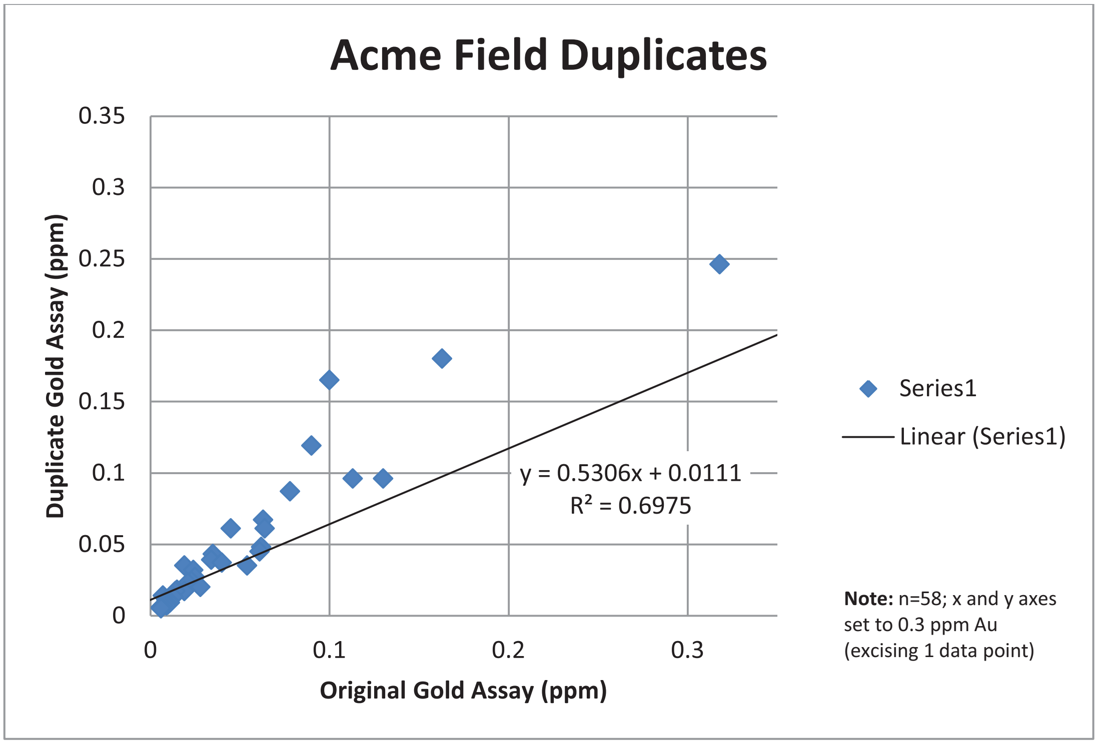


Figure 11-32: Scatterplot for Field Duplicates Assayed at ACME



11.4.3.2 Reject Duplicates

Coarse reject duplicates are splits of a sample taken after the coarse crush but before pulverizing and then assayed as a separate, duplicate sample. These are routinely performed by the sample preparation laboratory as part of their internal quality control but it is best practice that additional coarse reject duplicates are also requested by the submitting company. Coarse reject duplicates measure the homogeneity of the sample at the coarse reject stage and assesses combined preparation and analytical precision.

From September 2011 onwards, Canaco requested that additional coarse reject duplicates be prepared and assayed at SGS Mwanza. To date, a total of 685 coarse reject duplicates have been assayed in addition to those prepared routinely by the laboratory. Results for the Canaco reject duplicates and those undertaken as part of internal QC procedures by SGS and ACME are presented in Figures 11-33 to 11-35.

Figure 11-33: Scatterplot for Canaco Coarse Reject Duplicates Assayed at SGS

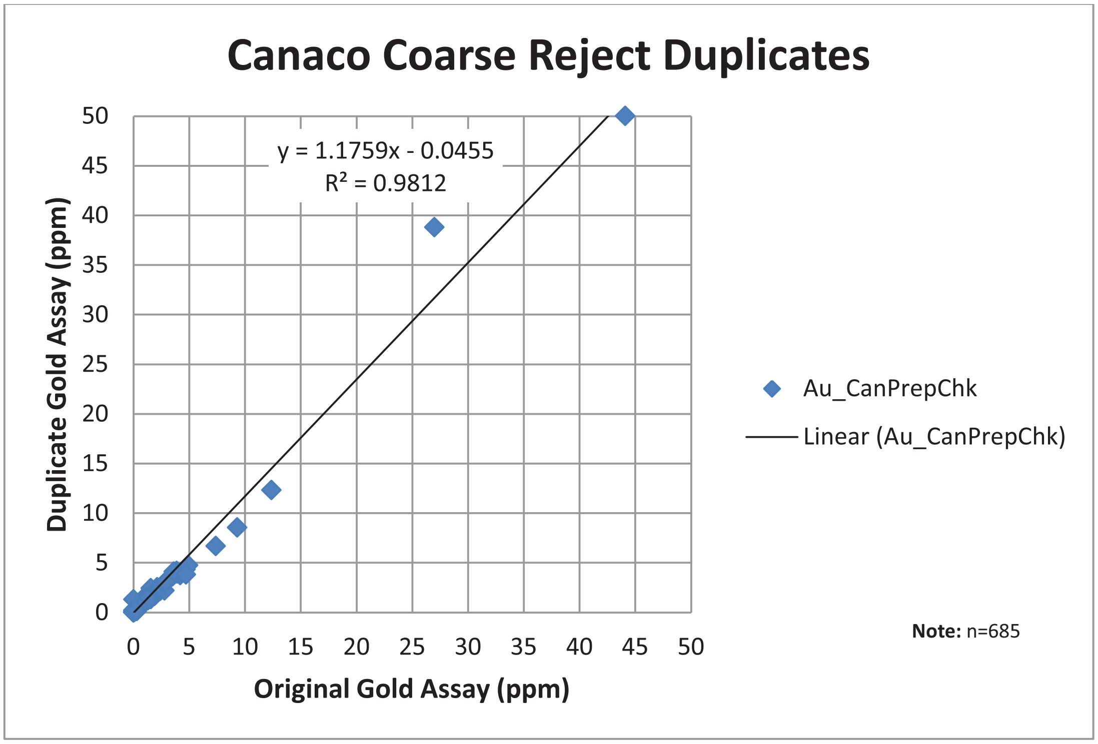


Figure 11-34: Scatterplot for SGS Internal QA/QC Coarse Reject Duplicates

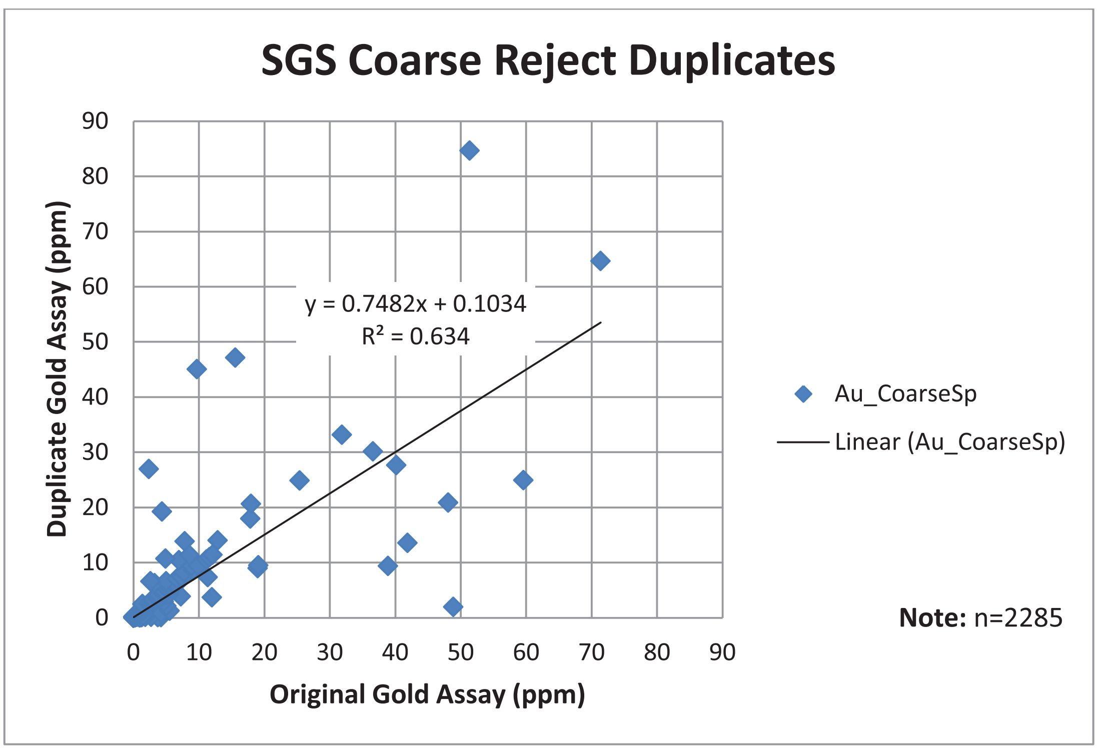
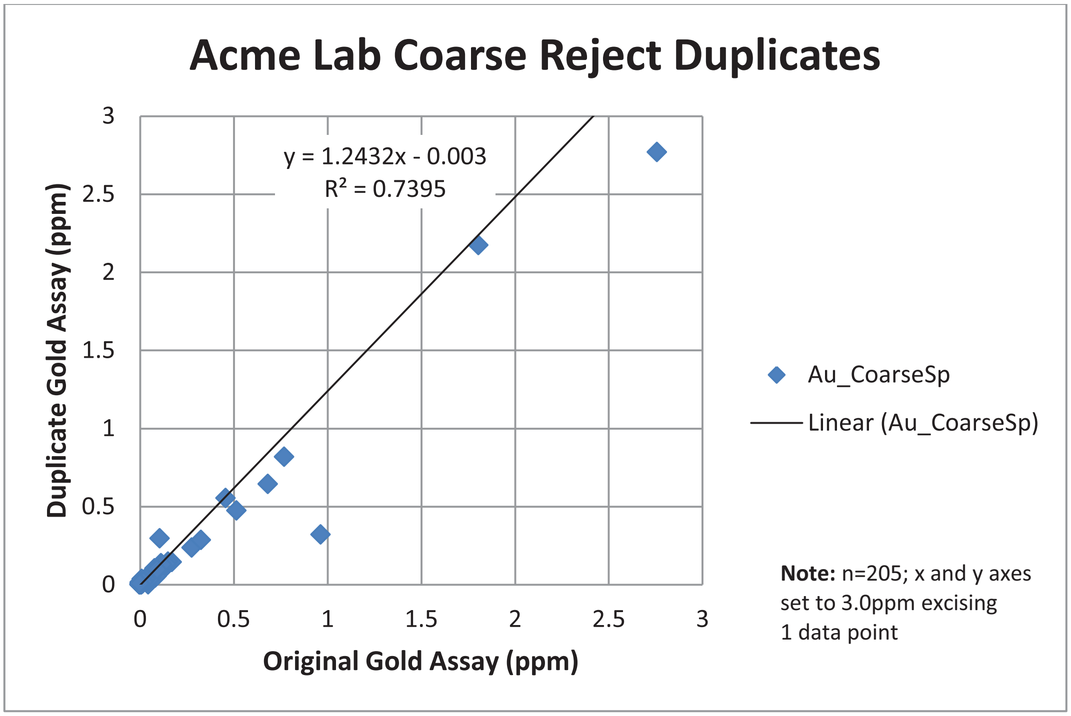


Figure 11-35: Scatterplot for ACME Internal QA/QC Coarse Reject Duplicates



The Canaco coarse reject data set shows an excellent correlation between initial and duplicate material up to a concentration of 12.5 ppm Au and is reflected in the high correlation, R^2 value of 0.98. Similarly, the ACME data set shows a strong correlation between the sample pairs, although variability is noted for a small subset of samples resulting in a lower R^2 value of 0.73. A moderate (R^2 = 0.63) correlation is also evident for SGS sample pairs up to gold grades of approximately 12 ppm Au above which a greater variability is noted.

Overall, the coarse reject data demonstrates that homogeneity of the samples at the coarse crush stage is good and that no significant bias is being introduced by this phase of the laboratory preparation procedure at the SGS or ACME laboratories.

11.4.3.3 Pulp Duplicates

Pulp duplicate samples are regularly taken from the unused analytical pulp returned from the primary laboratory and these duplicates are inserted into a subsequent batch of samples for analysis by the same laboratory. The objectives of pulp duplicate samples are twofold: to provide an extra degree of confidence in the reliability of the initial result and to provide an assessment of between-batch precision (i.e., analytical variation).

From September 2011 onwards, pulp duplicates were introduced as a supplementary QA/QC sample for the Magambazi assays, all of which were assayed at SGS Mwanza. Scatterplots of the resultant data are presented in Figures 11-36 to 11-37.

Figure 11-36: Scatterplot of Pulp Supplicate Sample Pairs

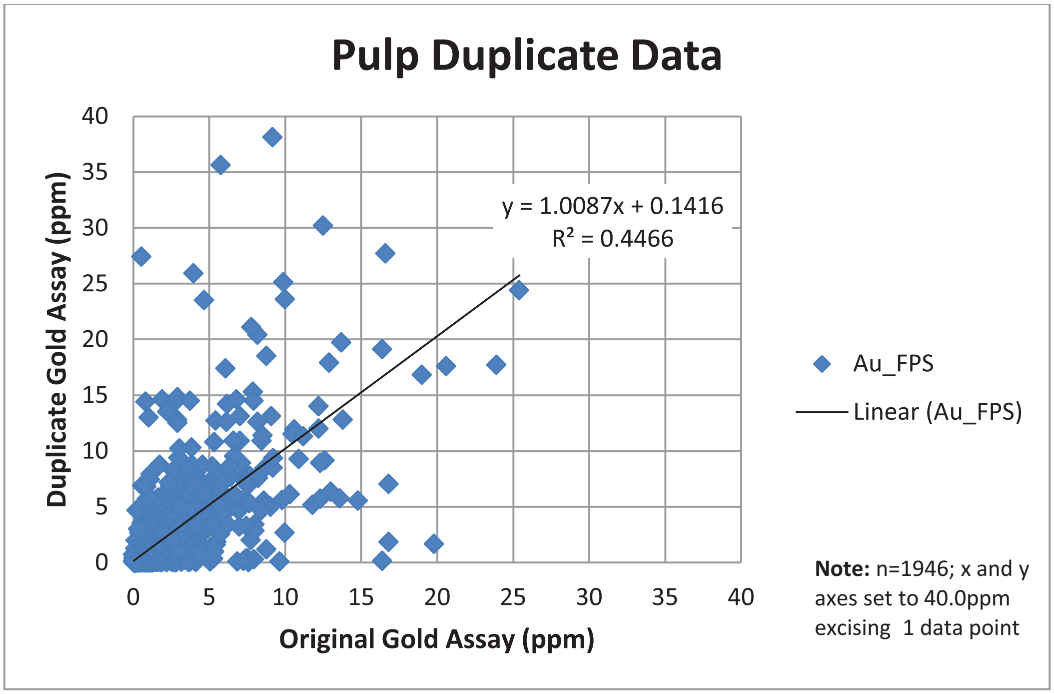
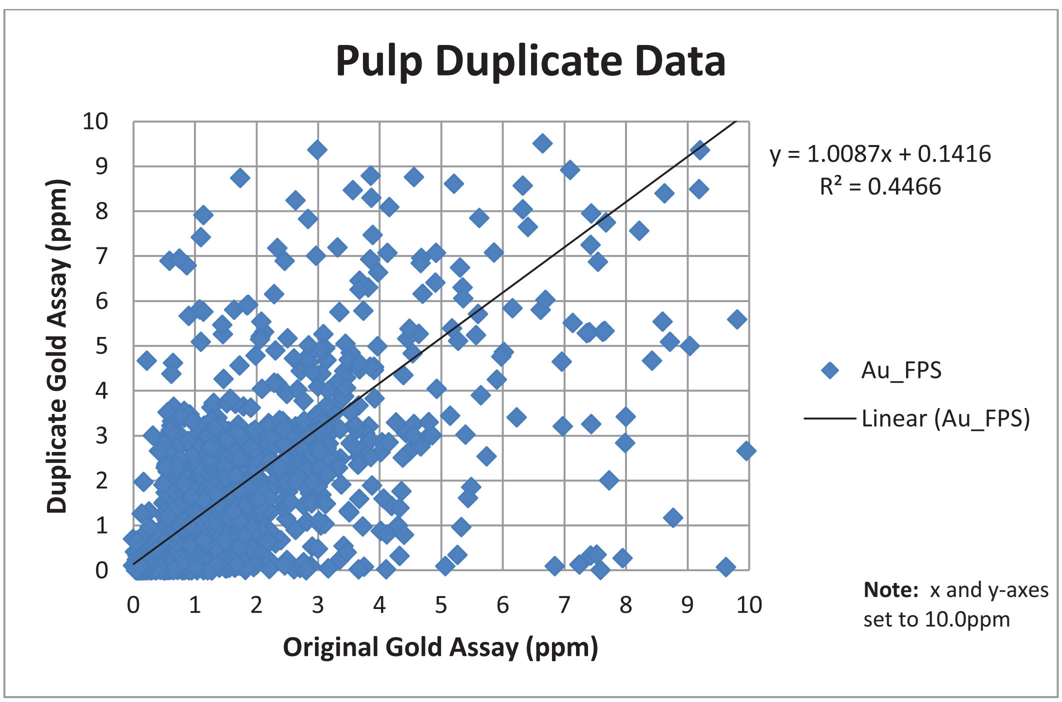


Figure 11-37: Scatterplot of Pulp Duplicate Sample Pairs up to the 10 ppm Gold Range



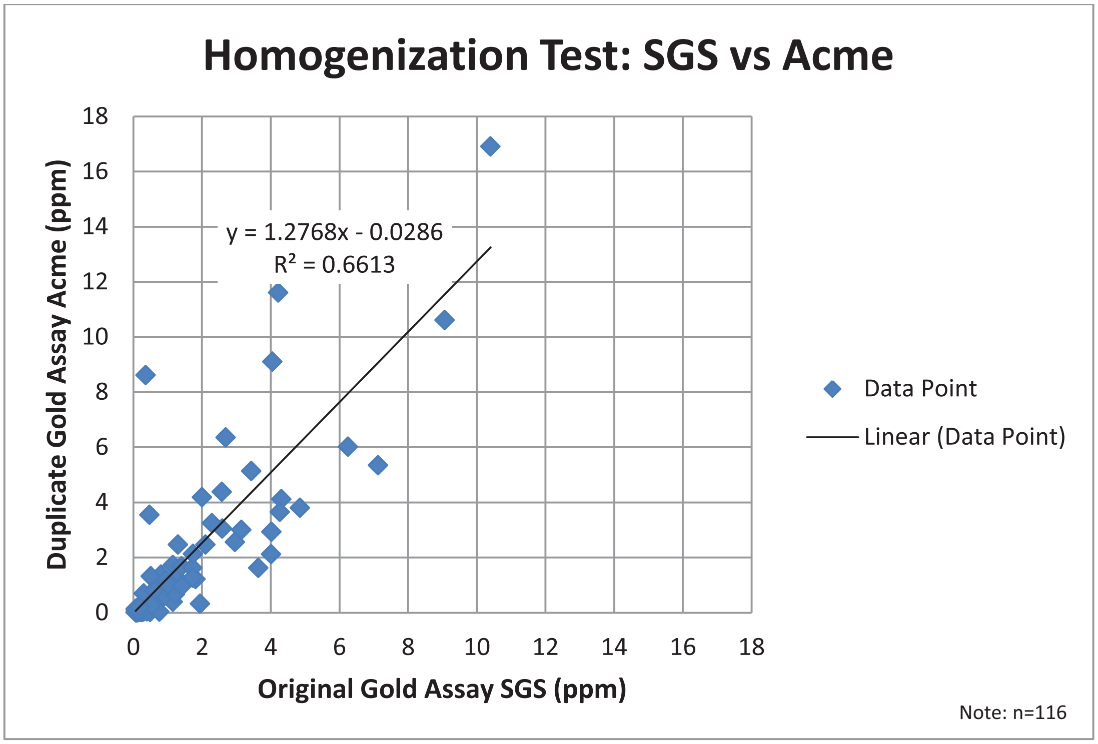
The pulp duplicate data show a poor correlation between original and duplicate analyses; with a lower R^2 value of 0.44 relative to the coarse reject duplicates (minimum R^2 value of 0.63). Given the samples are repeat assays of analytical pulps, a stronger correlation between the sample pairs would be expected. The strong variation is in contrast with the correlations noted above for the coarse reject samples. Theoretically, the level of variation should decrease as a sample passes through preparation stages of a laboratory (i.e. increasing correlation is expected as samples are taken at various points in their processing from field duplicates to coarse reject duplicates with the strongest correlation expected for pulp duplicates).

The pulp duplicate data from Magambazi shown in Figures 11-36 and 11-37 indicates high variability throughout all samples, particularly at lower grades. These results raise concerns about the repeatability of assays. The apparent dissimilarity between pulp duplicate pairs is, however, at variance with other comparable duplicate datasets. Assaying laboratories routinely undertake repeat assays (i.e. duplicate assays from the same pulp) as part of their internal QA/QC procedures. The corresponding data for SGS, ALS and ACME was reviewed and found to show moderate to good correlations. Similarly, duplicate data from the Canaco re-assay program was also reviewed and again displayed better correlations than seen within the pulp duplicate data. Lastly, data from a series of analytical pulps originally processed at SGS but later re-assayed at ALS Vancouver was examined and found to have a moderate correlation. The apparent absence of correlation within the pulp duplicate dataset is inconsistent with these datasets.

Further investigation of this issue has revealed that SGS Mwanza do not routinely homogenize pulp samples. Samples which have been stored and then transported are subject to stratification (including CRMs). When combined with the weight of evidence from other duplicate data sets, it was considered that stratification of the material during transport could be an influence on the variation noted within the pulp duplicate dataset. In order to test this hypothesis, a suite of pulp samples from drill holes MGZD341, MGZD370 and MGZD393 was selected for re-assay. These samples were homogenised prior to assay at ACME Vancouver and the results are plotted against the original gold assay values in Figure 11-38.

The results show an improved correlation between the original assay and duplicate values (R^2 = 0.66) and supports the interpretation that homogenization of the pulp prior to analysis has an influence on the repeatability of the assay. It is therefore considered likely that the absence of homogenization for the pulp duplicate samples assayed at SGS Mwanza has contributed to the variability illustrated in Figure 11-35.

Figure 11-38: Scatterplot of Homogenized Pulp Duplicates Assayed at ACME vs. Original SGS Assay



11.5 Discussion of QA/QC Results

11.5.1 Re-Assay Data / Assay Selection for Mineral Resource Database

Canaco has implemented a policy of re-assaying analytical pulps where QA/QC issues have been identified within the initial assay data received from the laboratories. To date, some 6,394 re-assays have been completed on problematic sample suites from a total sample population of 86,754 samples. These re-assays have been necessitated primarily where QA/QC CRM failures have occurred. From March 2011 onwards, efforts have been made to re-assay samples affected by failing QA/QC CRMs as soon as the issue has been identified.

Logistical issues, however, have impeded execution of the re-assay program and it is not complete at this writing. In many cases, not enough CRM pulp has remained after the initial assay to support a second assay. For this reason, in some cases, fresh CRMs are being inserted into the sample stream to ensure that re-assay data can be monitored effectively for QA/QC compliance. Additionally, delays in the repatriation of analytical pulps from the laboratory to the Magambazi site have also hampered progress of the re-assay program.

It should also be noted that a change in the thresholds for monitoring of CRM performance (from percentage difference from recommended value to standard deviation based thresholds) was enacted from April 22, 2010 (refer to section 11.4.1). Prior to this time, the discriminator for

QA/QC fails used at Magambazi was less restrictive. As such, certain sample suites that were originally perceived to be QA/QC compliant are now considered fails. Canaco has made every effort to retrospectively correct these issues as part of the re-assay program.

For the purposes of providing a database upon which an initial mineral resource estimate could be based, it was recognised that provisions would have to be made for samples that were influenced by unresolved QA/QC issues. To this end, all samples within the project database were screened for QA/QC issues and a sphere of influence placed around any failing control sample. The sphere of influence in each case covered samples in sequence above and below a CRM fail to the halfway point with surrounding CRM passes. In cases where re-assay data was available and deemed to be QA/QC compliant, the re-assay values were preferentially selected as the representative assay for all samples within the sphere of influence.

All samples that remained within the influence of unresolved QA/QC fails were assigned a lower level of confidence in the assay value. A total of 3567 samples relating to sample intervals within 190 drill holes were assigned to the category of lower confidence. It was decided that excising these samples from the mineral resource database would significantly bias the dataset and adversely affect the derived geological interpretation. For this reason, these samples were permitted to remain within the mineral resource database but with the proviso any calculated composite or interpolated block using these values would remain within the inferred mineral resource category.

The re-assay program described above is ongoing. Once completed, it is envisaged that the majority of remaining QA/QC fails can be qualified and their influence removed from any future mineral resource updates.

Outside of routine QA/QC issues, a number of problem drill holes were identified by Canaco personnel. In each case, higher than expected assay results were recorded for drilling intervals which were considered by Canaco geologists to be outside of interpreted mineralised zones. This was first noticed in MGZD167 and later in MGZD201 and MGZD318.

The results from drill hole MGZD167 were examined in detail. This hole contained a sequence of samples (D37202 - D37214) which returned higher grades than anticipated in addition to a failed Canaco CRM (D37198). The retained core was inspected and no evidence of mineralisation was noted. Additionally, a portable Niton XRF instrument was used to conduct an analysis of the analytical pulp from Canaco CRM D37198, confirming that the correct standard was inserted. Subsequently, the analytical pulps from samples D37196 – D37252 were re-assayed. All CRMs in the re-assay dataset were passes, the values recorded for samples D37202 - D37214 were significantly lower than the originals and these values were consistent with the observation that these represent unmineralised core. Therefore, significant doubt was raised relating to the initial assay results for drill hole MGZD167 that clearly did not relate either to the core or the analytical pulps.

The interpretation discussed above was presented to the SGS laboratory manager and the results from Batch 378 relating to this drill hole were reviewed. The insertion point for the internal laboratory QC samples was examined and it was noted that 3 QA/QC samples were included between samples D37193 – D37214 (an analytical blank after D37194, a CRM after D37196 and an analytical repeat after sample D37211). Therefore, the sample range from D37193 – D37214 represents an individual laboratory rack of 25 samples. This includes the majority of samples where the original assay value is in doubt. For this reason, it is considered probable that the source of the issue relates to a mix-up within the laboratory and most likely to the analysis of a different rack at the atomic absorption spectroscopy stage.

A similar pattern was evident for drill holes MGZD201 and MGZD318. In MGZD201 a suite of samples between 287m to 308.7 m returned anomalously high assay results. The analytical pulps from these samples were re-assayed and returned uniformly low results. Similarly, exceptionally high assay results were recorded for a suite of samples between 207-223 m in MGZD318. As previously noted, this was inconsistent with the geological interpretation of the drill hole. The analytical pulps were re-assayed and returned low-grade values. Subsequently, quarter core samples were taken across a significant portion of MGZD318 (130-230 m) and were sent to ACME Vancouver for assay. The quarter core sample results support the re-assay values and demonstrate that the initial result set for 207 to 233 m in MGZD318 was suspect.

Based on the number of samples affected and the assumed distribution of internal laboratory control samples, it is considered probable that rack mix-ups at the laboratory affecting approximately 25 samples per hole is the most likely cause of the issues highlighted. In each case the re-assay value has been preferentially selected as the representative assay for these samples. It should be noted that the questionable results within MGZD167, 201 and 318 were only recognised through the attention of Canaco staff and largely because anomalous results were recorded in zones considered to be barren. The drilling database has been reviewed by the author and by Canaco personnel. Although similar issues have not been identified, the recognition of issues such as potential rack mix-ups, particularly within mineralised zones, is problematic. Continued vigilance in the review and interpretation of assay results by all those involved in the Magambazi project is warranted.

11.5.2 Assessment - Diamond Drill Samples

Drill core handling and sampling has been observed to be conducted in a professional manner by Canaco personnel at Magambazi. Following sampling, the split core is placed into an individual sample bag and tape sealed. QA/QC samples are placed into the sample stream under the supervision of the project/logging geologist. The individual sealed sample bags are then placed in polypropylene bags and sealed with a hand tied knot in preparation for shipment to the preparation laboratories. The samples are transported by Canaco personnel in vehicles to the preparation laboratories in Mwanza (Archibald, 2011) or alternatively shipped to the ACME Laboratory in Turkey. Chain of custody procedures on site generally conform to industry best practice. The absence of tamper proof fastenings on the samples has been noted and their introduction would greatly improve the chain of custody during transit of samples between the site and laboratory.

Throughout the drilling programs at Magambazi, Canaco has progressively improved and refined the on-site QA/QC procedures. Following a detailed review by the author during August 2011, a revised QA/QC protocol was introduced. The rate of CRM and blank insertion was revised to 1 per 20 samples and the insertion of field duplicates was amended to similar levels (i.e. 5%). This was accompanied by the inclusion of pulp and reject duplicates into the sampling stream as additional control samples. These amendments to QA/QC procedures were implemented on a phased basis from August to October 2011 and are consistent with industry best practice.

Canaco has used a variety of CRMs throughout the drilling programs at Magambazi. An initial suite of CRMs sourced from Western Mineral Standards recorded a high proportion of QA/QC fails. Several key intersections from holes containing these failed standards were re-assayed at ALS Vancouver and are discussed in Archibald (2011). The author concurs with the observation therein that the ALS results are “comparable and correlative with that of the initial SGS results”. The Western Mineral Standards CRMs were sourced in screw cap jars from which the material for the standards was dispensed when required. Based on the results, it is considered likely that inhomogeneity through settling or contamination of the jars may have been an influence on the poor performance of these standards. Subsequent CRM suites were sourced from Geostats PTY and supplied within individually wrapped sachets. The introduction of these standards coincided with an overall improvement in CRM performance. However, high fail rates, in excess of 5%, are evident for G302-10, G307-3, G308-1, G901-7, G907-4, and G908-1. The influence of suspected field error is apparent for a number of CRMs. Consequently, revised procedures have been established at Magambazi to improve CRM handling and the recording of information pertaining to inserted standards.

A noticeable change in the behavior over time with respect to G907-6 has been observed. An initial suite of assays for this CRM fall above the recommended value whereas the subsequent samples tend to return values which lie below the recommended value. The source of this behaviour is unclear but may represent a change in the tenor of the standard or alternatively a change in the laboratory analytical procedure and/or laboratory drift. Further investigation is required to determine the source of this observed shift in trend.

In general, lower grade standards have a poorer performance relative to higher grades (e.g. G302-10 and G307-3). In particular, G908-1 and GLG307-1 are exceptionally low grade and both display high fail rates. This may reflect a sensitivity issue for the SGS FA505 technique at low grades.

Three different blank samples have been used at Magambazi: an uncontrolled and uncertified blank sourced from unmineralised quartz veins in the Handeni area, a certified blank supplied from HUMAC Laboratories in Mwanza and a low grade CRM (GLG307-1) which was used as a “pseudo-blank” control sample. With the exception of high outlier values, ascribed to field error, the performance of the certified blank is generally good. A higher than average fail rate for the uncontrolled blank over the period between November 2010 to January 2011 is considered likely to represent elevated gold in the source material as opposed to systematic contamination at the laboratory. Otherwise, the uncontrolled blank performance is generally within acceptable limits. Of more concern is the use of Geostats PTY standard GLG-307-1 as a blank sample over the period from December 2010 to September 2011. A CRM pulp is not considered to be a suitable substitute for blank rock material. GLG307-1 was used exclusively as a blank sample in 73 batches relating to samples from 67 individual drill holes. These sample batches are therefore considered to be uncontrolled for potential contamination.

The progressive introduction of revised QA/QC procedures at Magambazi included the implementation of field, reject and pulp duplicates. The correlation between field duplicates is poor but moderate correlations are observed for lower grade samples assayed at SGS and ALS. In general, there is significant heterogeneity between sample pairs and this is consistent with the observation that gold mineralisation at Magambazi has an exceptionally strong nugget effect. The data from coarse reject duplicate data requested by Canaco and also internal laboratory QA/QC coarse reject duplicates from SGS and ACME has been reviewed. The Canaco and ACME reject data shows a strong correlation whereas increased variability is noted between the SGS sample pairs. Overall, the coarse reject data demonstrates that homogeneity of the samples at the coarse crush stage is good and that no significant bias is being introduced within this phase of the laboratory preparation procedure at both laboratories.

In contrast to the coarse reject samples, the pulp duplicate data shows a poor correlation with elevated variation amongst sample pairs. These results raise concerns about the repeatability of assays. The variability within the pulp duplicate dataset is inconsistent with other datasets from Magambazi and suggests that a laboratory procedural issue is influencing these samples. As noted previously, SGS Mwanza does not routinely homogenize pulp samples. Therefore, the pulp duplicate sample material is subject to stratification during transport over multiple journeys between the laboratory and Magambazi site (approximately 1,800 km over a variety of ground conditions). A test was undertaken on a suite of pulp samples which were homogenized prior to assay at ACME Vancouver. The resultant data shows an improved correlation between sample pairs (Figure 11-37) and supports the interpretation that homogenization of the pulp has an influence on the repeatability of the assay. It is considered likely that variability observed in the pulp duplicate data reflects the settling of the sample material during transport, the lack of homogenization prior to analysis and natural heterogeneity within the sample (i.e. nugget effect). The natural variability in gold at Magambazi is presented and discussed in Section 13.3.4.4 (Head Grade Reconciliation).

Significant issues relating to the veracity of assay results for certain samples from three drill holes (MGZD167, 201 and 318) have been identified by Canaco geologists. In all three cases, rack mix-up at the SGS assaying laboratory is suspected to be the likely cause of the error. Canaco has resolved these issues through proactive re-assaying of analytical pulps and supplementary quarter core sampling of the remaining drill core. Continued vigilance in the review and interpretation of assay results by all those involved in the Magambazi project is advised.

Canaco has committed to a significant re-assay program of analytical pulps where QA/QC issues are identified within the original assay data. The re-assay program is ongoing with the objective of resolving all historical and current QA/QC fails within a reasonable timeframe. At present, 3567 samples lie within the sphere of influence of unreconciled QA/QC sample fails. For the purposes of providing a database upon which an initial mineral resource estimate could be based, provisions have been made to deal with these samples in the manner described in section 11.7. Logistically, it is far more difficult to deal with QA/QC fails retrospectively and, as such, it is recommended that the re-assay program is pursued to conclusion and that the current practice of resolving QA/QC fails as they arise is continued.

The author is satisfied that the quality of gold analytical data is sufficiently reliable to support the initial mineral resource estimation (Archibald *et al*, 2012) and that sample preparation, analysis and security are generally performed in accordance with exploration best practices and industry standards.

12 DATA VERIFICATION

In consideration of the data summarized below, as well as information provided elsewhere in this report, the author of this section believes the current Canaco project data are acceptable for the purposes used in this report.

12.1 Electronic Database

Initially, an Access database was provided by Canaco to Independent Qualified Persons as a universal project dataset along with a full set of assay certificates. On review of this data, a number of issues were identified in relation to the database structure and extraction of the contained information. Subsequent efforts to repair the initial database were unsuccessful. A decision was taken by Canaco to fully rebuild the project database using a more suitable software platform.

Information recorded from diamond drill core logging and assaying was integrated using industry standard data management software (Maxwell DataShed). The author was personally involved in the construction of the project database and is satisfied that acceptable procedure was followed throughout. The resultant data was reviewed, including validation of a random selection of data against the source information, and it is considered acceptable for use in support of the initial mineral resource estimation.

Since disclosure of the initial Magambazi resource, an additional 69 drill holes have been completed on the project. This new information has been integrated into the project database but has not been independently reviewed or validated by the section author.

12.2 Drill Hole Collar Checks

The section author did not conduct drill hole collar checks on the property. Five drill hole collar checks were undertaken previously using a hand held GPS as part of a previous independent technical report on the property (Archibald, 2011). As part of the site visit from February 13 to 15, 2012, Dr. Archibald surveyed an additional 20 collar locations using a handheld GPS unit. The average deviation was 1.89 m for the easting and 0.63 m for the northing, with the largest deviation recorded being 3.3 m in the easting component. It was noted that several concrete slabs used to mark the location of some of the holes checked in 2011 had been removed, probably due to damage, and had not been replaced. Monuments for those drill hole collars should be replaced for future reference.

12.3 Independent Verification of Mineralisation

12.3.1 Core Samples

Mr. Jim Gray of Advantage Geoservices visited Magambazi from February 12 to 17, 2012. As part of the review of mineralised intervals within the Canaco drill core, Mr. Gray collected four independent samples for assaying. The samples consisted of quartered core from selected intervals from drill holes MGZD082, MGZD342 and MGZD027. A CRM and blank sample was included with the core samples which were then submitted to ACME Analytical Laboratories (Vancouver) Ltd. in Vancouver for fire assay, using the G601 technique.

The results of the independent samples analyzed at ACME are presented alongside the original SGS assay results for the selected intervals in Table 12.1, and the original assay certificates are presented in Appendix B.

Table 12.1: Independent Quartered Core Sample Assay Results

Hole ID	Sample Number	From (m)	To (m)	SGS Au (ppm)	New ID	ACME Au (ppm)
MGZD082	D09411	263.1	264	1.11	JNG_1	3.279
MGZD342	D95484	135	135.7	4.43	JNG_2	0.122
MGZD342	D95485	135.7	136.4	0.32	JNG_3	0.546
MGZD027	D02432	102.8	103.5	0.71	JNG_4	0.442

Given the strong nugget effect observed within the QA/QC field duplicate data, the variation between the original SGS assay and the ACME results is not unexpected. The ACME results however confirm the presence of gold mineralisation within these sample intervals.

No samples were collected as part of the current report, since drilling stopped approximately 6 weeks after the QP site visit. It is assumed that all drilling procedures and protocols would not have changed in the intervening period.

12.3.2 Umpire Samples

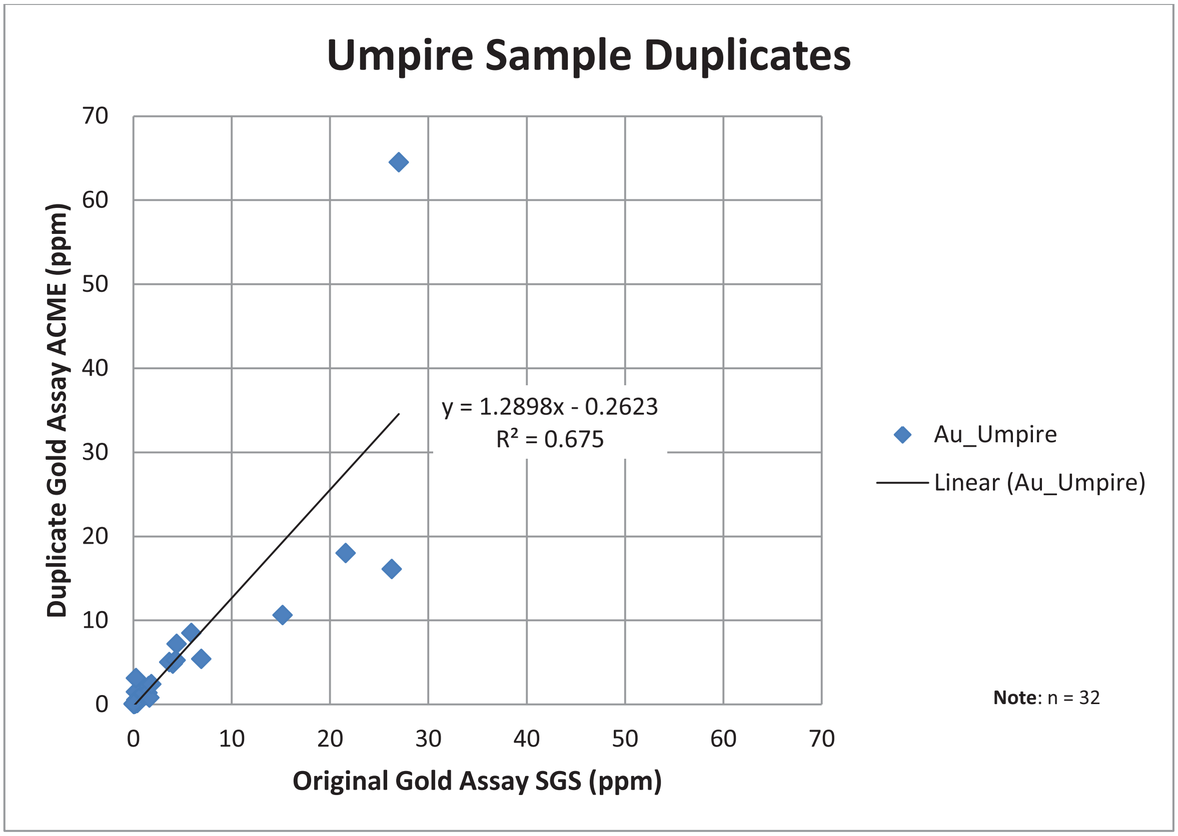
A suite of Umpire Samples were collected from SGS Mwanza and submitted to ACME Analytical Laboratories (Vancouver) Ltd. for assay. These samples represent coarse crush duplicates which are prepared at the primary laboratory and then set aside for later submission to a second laboratory for pulverization and assay. This approach provides a test of sample preparation and splitting procedure in the laboratory in addition to analytical variation. A total of 32 Umpire Samples were selected from 19 drill holes ranging from MGZD303 to MGZD348. The selection process was designed to cover a range of assay grades.

A scatterplot of the Umpire Sample results plotted against the original SGS assays is presented in Figure 12-1.

The Umpire Sample results show a moderate to good correlation with the SGS assay results up to the 10 ppm Au level. Above this concentration a tendency towards higher grades for the original SGS assay is observed with the exception of sample D92625 from MGZD336 (64.5 ppm Au at ACME and 27 ppm Au at SGS).

The ACME results for the Umpire Samples confirm the presence of gold within the samples and the levels of correlation are consistent with other coarse crush duplicate datasets.

Figure 12-1 Scatterplot of Pulp Supplicate Sample Pairs



13 MINERAL PROCESSING & METALLURGICAL TESTING

The metallurgy of the Magambazi deposit has been examined in a comprehensive test program carried out at the G&T laboratories in Kamloops, British Columbia, under the direction of Dr. Jim King, of JKCI.

The objectives of the program were to:

- confirm the free milling nature of the Magambazi gold mineralisation
- investigate the variability of the metallurgical response within the deposit
- define an operable flowsheet for processing material from the Magambazi deposit, along with all related metallurgical parameters including Bond Work Index hardness and abrasivity, primary grind size, and cyanide leach conditions including reagent requirements and leach residence times
- produce algorithms that relate gold recovery to the head grade of the mineralised material.

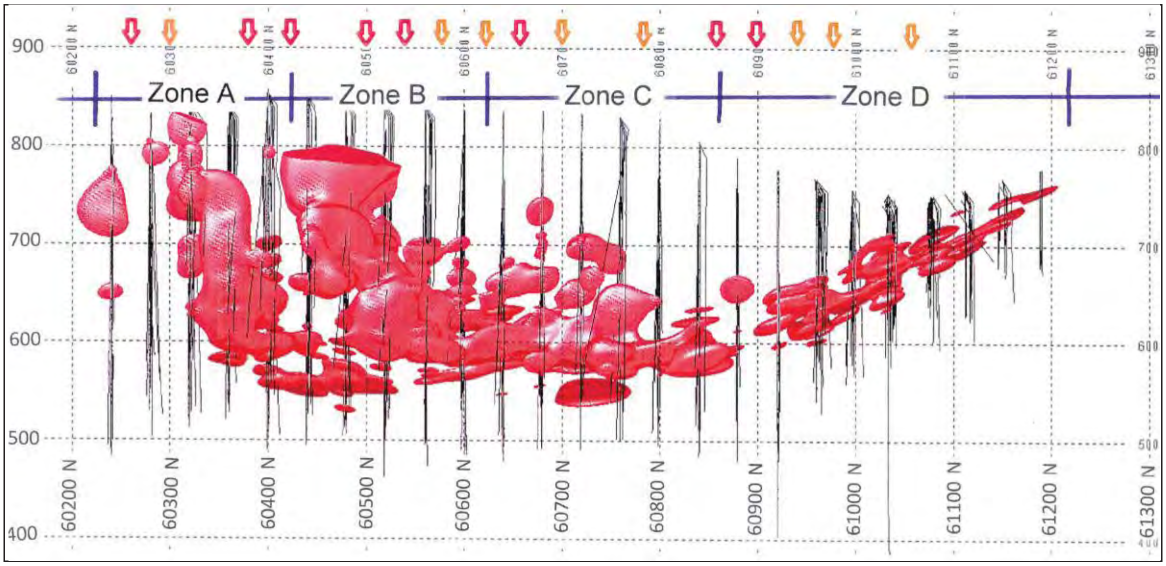
13.1 Sample Description & Preparation

To obtain a comprehensive and detailed picture of the metallurgy in the Magambazi deposit, an extensive sampling program was undertaken to generate composites that would be thoroughly representative of the entire mineralisation in the Magambazi deposit. To this end, some 2935 individual drill core intervals were selected as constituents for making up the metallurgical testwork composites, representing 2325 m of drill core and weighing 2.77 tonnes. To maintain security and sample integrity, each drill core intercept was shipped as quarter core in individual sample bags. It was shipped directly from the mine site to the G&T laboratory in Kamloops, British Columbia.

The drill core taken from the Magambazi deposit was sawn in half, with one-half of the drill core used for assaying by external certified laboratories. The other half core was kept in core boxes on-site. To generate the metallurgical samples, the selected intervals of the one half core on-site was sawn again to provide one quarter core for metallurgical testing with the remaining quarter core retained in the core boxes on-site.

The Magambazi mineralisation is contained within a long hill, approximately 200 m high and 1200 m long, situated in a northwest-southeast direction. Mineralisation outcrops close to the top of the hill and is also encountered at depths of up to 300 m from the crest of the hill. The deposit has been fan drilled on 40 m centres along strike, with the majority of the mineralisation contained within Sections 60,240N through 61,200N. Zones of high intensity mineralisation generally coincide with interpreted structural controls. However, some uncertainty exists regarding the correlation between structure and mineralisation. This is evident from the simplified pictorial of mineralisation along strike, in Figure 13-1, looking from the East side of the deposit, generated by SRK using the program Leapfrog.

Figure 13-1: Simplified Leapfrog Model of the Mineralisation, Looking West



To examine the variability of the deposit from a metallurgical point of view, the deposit was divided into four zones, A Zone through D Zone, which corresponds to the Sections in Table 13.1.

Table 13.1: Deposit Zones by Section

	From	To
Zone A	60240	60400
Zone B	60440	60600
Zone C	60640	60840
Zone D	60880	61200

The potential methods of mining the Magambazi deposit were being considered coincidentally with the start of the metallurgical test program. Two composites were therefore made up from each of the four zones A through D, a low-grade composite representing material that might potentially be included in the process feed if the deposit were to be mined by open pit methods, and a high-grade composite representing material that might potentially be mined by underground mining methods. The low-grade composites were made up using drill core intervals that had a grade range between 0.2 and 3 grams of gold per tonne. The high-grade composites were made up using drill core intervals grading over 3 g of gold per tonne. The complete listing of all the intercepts used in preparing the high and low grade zone composites A through D are given in Appendix C. Composite details are summarised in Tables 13.2 and 13.3 below, including element assays of the head grade samples that were split out during the preparation of the composites.

Table 13.2: Composite Details

	No of metres	Weight, kg	Au Grade, g Au/t
Zone A LG Composite	227.4	317.2	1.57
Zone A HG Composite	190.6	240.5	8.26
Zone B LG Composite	183.0	216.4	1.94
Zone B HG Composite	500.3	589.2	8.01
C Zone LG Composite	221.0	247.2	1.58
C Zone HG Composite	314.2	355.2	6.66
D Zone LG Composite	511.7	598.7	1.51
D Zone HG Composite	176.7	203.0	5.34
Total Drill Core	2,325.0	2,767.4	

Table 13.3: Zonal Composites

COMPOSITE	Total Meters	Weight kg	Predicted Au Grade (1) g Au/t	Assay of Head Samples (2)	Element Assays, % except g/t for Au, Ag and Hg (2)											
					Fe(t)	Fe	Au	Ag	S	C	CO3	TOC	S(s)	Sb	As	Hg
A ZONE LG	227.4	317	1.57	Zone A LG Head 1	10.20	4.84	0.84	1.00	1.36	0.24	0.77	0.09	1.29	<0.002	0.13	<1
				Zone A LG Head 2	10.00	4.93	0.75	1.00	1.27	0.21	0.75	0.06	1.22	<0.002	0.13	<1
				Arithmetic Mean	10.10	4.89	0.80	1.00	1.32	0.22	0.76	0.07	1.26	<0.002	0.13	<1
A ZONE HG	190.6	240	8.26	Zone A HG Head 1	9.40	5.21	2.33	1.00	1.61	0.19	0.63	0.06	1.58	<0.002	0.83	<1
				Zone A HG Head 2	9.00	5.10	6.10	<1	1.58	0.19	0.59	0.07	1.53	<0.002	0.74	<1
				Arithmetic Mean	9.20	5.16	4.22	1.00	1.60	0.19	0.61	0.06	1.56	<0.002	0.79	<1
B ZONE LG	183	216	1.94	Zone B LG Head 1	8.60	4.60	1.48	1.00	1.34	0.29	0.59	0.17	1.31	<0.002	0.19	<1
				Zone B LG Head 2	8.70	4.55	1.97	1.00	1.25	0.30	0.69	0.16	1.13	<0.002	0.17	<1
				Arithmetic Mean	8.65	4.58	1.73	1.00	1.30	0.29	0.64	0.17	1.22	<0.002	0.18	<1
B ZONE HG	500.3	589	8.01	Zone B HG Head 1	7.90	4.94	2.13	1.00	1.67	0.64	1.46	0.35	1.62	<0.002	0.91	<1
				Zone B HG Head 2	7.80	4.74	3.70	1.00	1.54	0.57	1.44	0.28	1.47	<0.002	0.72	<1
				Arithmetic Mean	7.85	4.84	2.92	1.00	1.61	0.60	1.45	0.31	1.55	<0.002	0.82	<1
C ZONE LG	221	247	1.58	Zone C LG Head 1	9.00	5.12	0.53	1.00	1.70	0.50	0.93	0.32	1.57	<0.002	0.21	<1
				Zone C LG Head 2	9.30	4.74	0.85	<1	1.74	0.48	0.96	0.39	1.66	<0.002	0.21	<1
				Arithmetic Mean	9.15	4.93	0.69	1.00	1.72	0.49	0.94	0.35	1.62	<0.002	0.21	<1
C ZONE HG	314	355	6.66	Zone C HG Head 1	9.10	5.10	6.71	1.00	1.64	0.53	1.40	0.25	1.55	<0.002	0.77	<1
				Zone C HG Head 2	9.20	5.33	8.35	1.00	1.61	0.52	1.22	0.27	1.49	<0.002	0.76	<1
				Arithmetic Mean	9.15	5.22	7.53	1.00	1.63	0.52	1.31	0.26	1.52	<0.002	0.77	<1
D ZONE LG	511.7	599	1.51	Zone D LG Head 1	8.30	4.19	2.33	1.00	1.13	0.41	1.18	0.17	1.07	<0.002	0.22	<1
				Zone D LG Head 2	8.70	4.09	1.52	<1	1.15	0.43	1.38	0.16	1.11	<0.002	0.24	<1
				Arithmetic Mean	8.50	4.14	1.93	1.00	1.14	0.42	1.28	0.16	1.09	<0.002	0.23	<1
D ZONE HG	176.7	203	5.34	Zone D HG Head 1	8.30	4.27	3.90	1.00	1.66	0.69	1.90	0.30	1.55	<0.002	0.57	<1
				Zone D HG Head 2	8.10	3.99	5.29	1.00	1.51	0.64	1.69	0.30	1.48	<0.002	0.45	<1
				Arithmetic Mean	8.20	4.13	4.60	1.00	1.59	0.66	1.80	0.30	1.52	<0.002	0.51	<1

(1) Predicted grade of composite calculated using as-received 1/4 core weights and drill core assays

(2) Element assays done on head samples split out from composites during composite preparation

An important aspect of the metallurgical testwork was to generate the gold recovery-head grade algorithms that could be used to assign value to the various mineralised blocks in the block model. To produce these algorithms, composites of varying head grade were also made using the same constituents selected for the Zone A through D composites. The detailed listing of intercept constituents used to construct the Grade Composites is given in Appendix D and summarised in Table 13.4 below.

Table 13.4: Grade Composites

	Au Grade Range of Constituents		Weight, kg	Predicted Au Grade (1)	Assays, % except g/t for Au, Ag and Hg										
	From	To		g Au/t	Fe	Au	Ag	S	C	CO3	TOC	S(s)	Sb	As	Hg
Grade Composite A1	0.20	0.50	26.85	0.28	2.98	0.17	1	0.814	0.21	0.63	0.08	0.78	<0.002	0.02	<1
Grade Composite A2	0.50	0.80	28.50	0.65	4.25	0.45	<1	1.54	0.22	0.66	0.09	1.52	<0.002	0.04	<1
Grade Composite A3	0.80	1.20	30.68	1.00	4.68	6.59	1	1.49	0.27	0.87	0.10	1.46	<0.002	0.05	<1
Grade Composite A4	1.20	1.60	27.67	1.39	3.96	0.63	1	1.17	0.16	0.57	0.05	1.22	<0.002	0.08	<1
Grade Composite A5	1.60	2.00	28.43	1.78	4.62	1.27	1	1.26	0.27	1.08	0.06	1.28	<0.002	0.19	<1
Grade Composite A6	2.00	2.40	24.29	2.20	4.48	1.73	1	1.18	0.20	0.73	0.05	1.17	<0.002	0.16	<1
Grade Composite A7	2.40	3.00	19.49	2.71	4.69	1.54	1	1.52	0.24	1.08	0.03	1.47	<0.002	0.44	<1
Grade Composite A8	3.00	4.00	30.02	3.42	4.74	2.80	1	1.57	0.34	1.49	0.04	1.52	<0.002	0.50	<1
Grade Composite A9	4.00	6.00	19.52	5.04	4.71	3.70	1	1.66	0.46	2.03	0.05	1.69	<0.002	0.47	<1
Grade Composite A10	6.00	8.00	9.81	6.98	4.82	4.07	1	1.89	0.21	0.60	0.09	1.75	<0.002	0.83	<1
Grade Composite A11	8.00	12.00	12.76	9.33	4.49	9.29	1	1.62	0.24	0.99	0.04	1.57	<0.002	0.66	<1
Grade Composite A12	12.00	25.00	11.91	17.71	6.3	8.70	1	2.33	0.23	0.97	0.04	2.29	<0.002	1.14	<1
Grade Composite A13	25.00	>25.00	8.96	43.63	6.3	15.44	1	2.61	0.31	1.39	0.03	2.45	<0.002	1.75	<1
Grade Composite B21	0.00	0.40	30.64	0.21	3.63	0.45	1	0.79	0.24	0.90	0.06	0.76	<0.002	0.19	<1
Grade Composite B22	0.40	1.00	42.03	0.66	4.03	1.14	1	2.71	0.78	3.17	0.15	1.12	<0.002	0.11	<1
Grade Composite B23	1.00	2.00	57.51	1.48	3.76	1.15	1	1.41	0.46	1.12	0.24	1.29	0.00227	0.17	<1
Grade Composite B24	2.00	2.50	40.49	2.23	4.08	1.74	<1	1.4	0.49	1.30	0.23	1.36	<0.002	0.35	<1
Grade Composite B25	2.50	3.00	31.98	2.77	4.43	2.73	1	1.4	0.57	1.51	0.27	1.33	<0.002	0.31	<1
Grade Composite B26	3.00	4.00	43.41	3.43	4.7	2.48	1	1.43	0.64	1.96	0.25	1.48	<0.002	0.40	<1
Grade Composite B27	4.00	5.00	23.08	4.45	5.26	10.54	1	1.53	0.57	0.95	0.38	1.48	<0.002	0.57	<1
Grade Composite B28	5.00	7.00	34.19	5.84	3.92	3.75	1	1.68	1.03	1.94	0.64	1.63	<0.002	0.78	<1
Grade Composite B29	7.00	10.00	36.92	8.22	4.63	3.24	1	1.81	0.76	1.53	0.46	1.79	<0.002	0.69	<1
Grade Composite B30	10.00	15.00	24.02	12.40	5.02	5.18	1	1.89	0.58	1.45	0.29	1.78	<0.002	0.89	<1
Grade Composite B31	15.00	30.00	27.34	20.72	5.22	10.01	1	1.96	0.97	1.82	0.60	1.84	<0.002	1.44	<1
Grade Composite B32	30.00	>30.00	11.20	58.23	5.38	17.06	1	1.93	0.60	1.43	0.31	1.86	<0.002	1.29	<1
Grade Composite C41	0.00	0.25	39.39	0.13	3.45	0.23	1	0.714	0.38	1.05	0.17	0.67	<0.002	0.02	<1
Grade Composite C42	0.25	0.40	30.98	0.33	3.6	0.61	<1	1.19	0.34	0.78	0.19	1.06	<0.002	0.12	<1
Grade Composite C43	0.40	0.80	37.38	0.58	4.72	0.39	1	1.81	0.63	1.10	0.41	1.69	<0.002	0.06	<1
Grade Composite C44	0.80	1.30	30.37	1.04	4.79	1.94	1	1.58	0.46	1.33	0.20	1.34	<0.002	0.15	<1
Grade Composite C45	1.30	2.40	46.79	1.82	4.7	1.79	1	1.86	0.56	1.56	0.25	1.70	<0.002	0.33	1
Grade Composite C46	2.40	4.00	42.03	3.07	4.02	2.95	1	1.63	0.66	1.77	0.31	1.62	<0.002	0.51	<1
Grade Composite C47	4.00	6.00	20.25	4.87	4.21	1.52	<1	1.66	0.54	1.34	0.27	1.55	<0.002	0.44	<1
Grade Composite C48	6.00	10.00	23.47	7.89	5.76	7.17	1	2.41	0.99	1.61	0.67	2.29	<0.002	0.96	<1
Grade Composite C49	10.00	14.00	7.81	11.91	6.3	7.30	<1	2.68	0.89	1.57	0.57	2.51	<0.002	1.54	<1
Grade Composite C50	14.00	25.00	14.14	18.34	5.68	25.08	1	2.42	0.92	1.07	0.70	2.25	<0.002	2.02	<1
Grade Composite C51	25.00	>25.00	7.83	39.98	4.75	13.79	1	2.16	0.72	1.73	0.37	1.97	0.0028	1.41	<1
Grade Composite D61	0.00	0.25	51.16	0.13	3.48	0.17	<1	0.695	0.55	0.99	0.35	0.62	<0.002	0.04	<1
Grade Composite D62	0.25	0.50	43.04	0.39	3.46	0.24	<1	0.782	0.21	0.84	0.04	0.66	<0.002	0.03	<1
Grade Composite D63	0.50	0.75	46.69	0.63	3.86	0.72	<1	1	0.39	1.24	0.14	0.91	<0.002	0.09	<1
Grade Composite D64	0.75	1.00	36.01	0.87	4.18	1.19	<1	1.2	0.37	1.31	0.10	1.08	<0.002	0.13	<1
Grade Composite D65	1.00	1.30	34.92	1.13	3.87	0.42	<1	1.14	0.41	1.01	0.21	0.95	<0.002	0.18	<1
Grade Composite D66	1.30	1.75	44.39	1.51	4.48	0.70	1	1.38	0.43	1.39	0.15	1.27	<0.002	0.31	<1
Grade Composite D67	1.75	2.50	41.87	2.13	4.44	2.06	<1	1.56	0.52	1.96	0.13	1.40	<0.002	0.34	<1
Grade Composite D68	2.50	3.50	30.32	2.93	4.97	2.70	<1	1.89	0.64	1.76	0.29	1.60	<0.002	0.68	<1
Grade Composite D69	3.50	5.00	24.52	4.19	5.21	10.43	<1	2.13	0.69	1.65	0.36	1.78	<0.002	0.80	<1
Grade Composite D70	5.00	8.00	19.61	6.12	4.76	4.42	<1	2.04	0.66	1.73	0.32	1.83	<0.002	0.92	<1
Grade Composite D71	8.00	>8.00	28.38	14.20	4.45	5.57	<1	1.94	0.73	2.18	0.29	1.71	<0.002	0.83	<1

(1) Predicted grade of composite using as-received 1/4 core weights and drill core assays

The selected drill core intervals arrived at the G&T laboratory as quarter core. Each individual interval was crushed to an approximate size of 100% passing -15 mm and riffled to produce two equal sample halves. One half of each of the intercepts was used to make up the Zones A through D Low-Grade and High-Grade composites, the other half of each of the intercepts was used to make Grade Composites. To make the Grade Composites, every intercept within a given Zone was sorted according to its drill core assay, and then grouped into between 11 and 13 composites of increasing grade. Once they had been formulated, each of the composites described above was crushed to -6 mesh and then riffled into 2 kg charges for the metallurgical test program.

13.1.1 Mineralogy

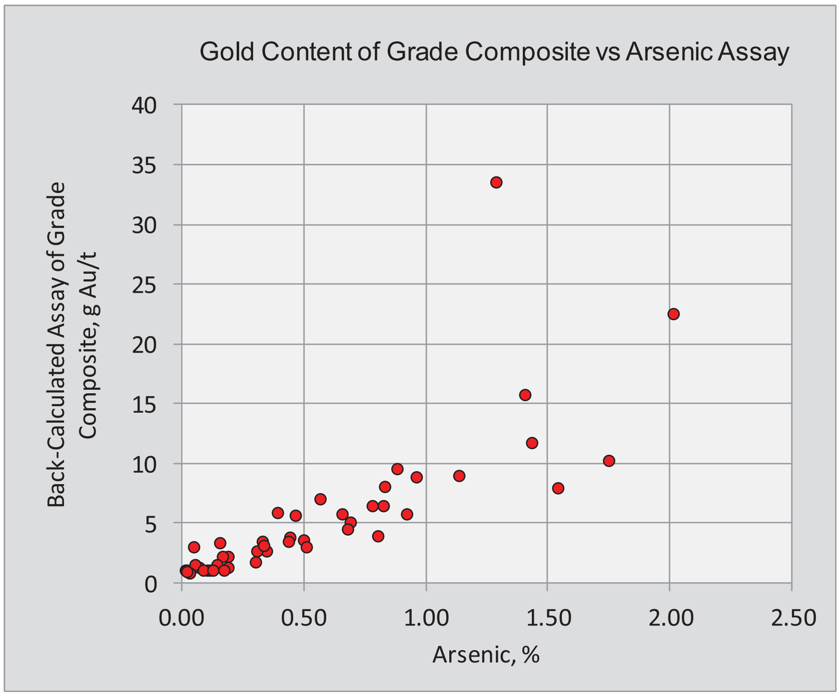
Samples of the high-grade and low-grade Zones A through D composites were each subjected to Qemscan analysis for mineral content. The results are tabulated in Table 13.5 and show that the principal minerals present were pyrrhotite, pyrite, arsenopyrite and lollingite, in decreasing order of abundance. Trace amounts of chalcopyrite were also observed to be present. The amount of pyrrhotite and pyrite was relatively consistent across all eight composites from Zones A through D, in both high-grade and low-grade composites.

Table 13.5: Mineralogy

Minerals	A Zone HG	A Zone LG	B Zone HG	B Zone LG	C Zone HG	C Zone LG	D Zone HG	D Zone LG
Chalcopyrite	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1
Pyrite	0.7	0.4	0.6	0.4	0.4	0.4	0.4	0.5
Pyrrhotite	3.6	2.9	3.5	2.6	3.6	3.3	3.1	2.4
Arsenopyrite	0.7	0.2	0.5	0.2	0.6	0.1	0.5	0.3
Lollingite	0.5	0.1	0.7	0.1	0.5	0.2	0.4	0.3
Iron Oxides	0.4	0.3	0.3	0.2	0.3	0.2	0.3	0.5
Quartz	21.2	16.3	30.7	22.2	24.6	22.6	24.7	22.4
Feldspars	28.2	20.1	31.9	25.3	29.5	28.3	34.1	29.8
Amphibole	28.4	40.7	20.9	32.2	28.4	30.9	22.8	30.1
Pyroxene	6.8	10.4	3.5	5.5	5.8	6.1	5.9	6.3
Biotite/Phlogopite	4.5	3.2	2.6	5.1	1.2	2.9	2.4	2.2
Calcite	0.9	0.8	1.3	0.8	1.2	1.0	2.0	1.3
Chlorite	0.5	0.9	0.2	0.3	0.3	0.6	0.3	0.4
Almandine	0.1	0.1	0.2	1.3	0.1	0.2	0.3	0.5
Ti Minerals	2.0	2.3	1.8	2.4	2.3	2.0	1.7	2.1
Apatite	0.5	0.6	0.4	0.4	0.5	0.4	0.5	0.4
Andalusite/Ky/Sill	0.2	0.1	0.2	0.6	0.0	<0.1	<0.1	<0.1
Others	0.7	0.6	0.8	0.4	0.7	0.6	0.6	0.5
Total	100	100	100	100	100	100	100	100

Testwork carried out on the Grade Composites demonstrated a very strong relationship between gold assay of the composite and its arsenic content. This relationship is shown in Figure 13-2. Detailed mineralogical work has not been carried out to delineate whether the gold is associated with either the arsenopyrite (FeAsS), or lollingite ($FeAs_2$), or both. As will be discussed in this Section 13 of the report, the recovery of gold from leaching gravity tailing is dependent on the head grade of the mineralisation from which the gravity leach tailing is produced. It is possible that the distribution of gold between the two arsenic minerals changes as the gold and arsenic content of the mineralisation increases. This should be evaluated in future testwork.

Figure 13-2: Gold – Arsenic Relationship



13.2 Summary

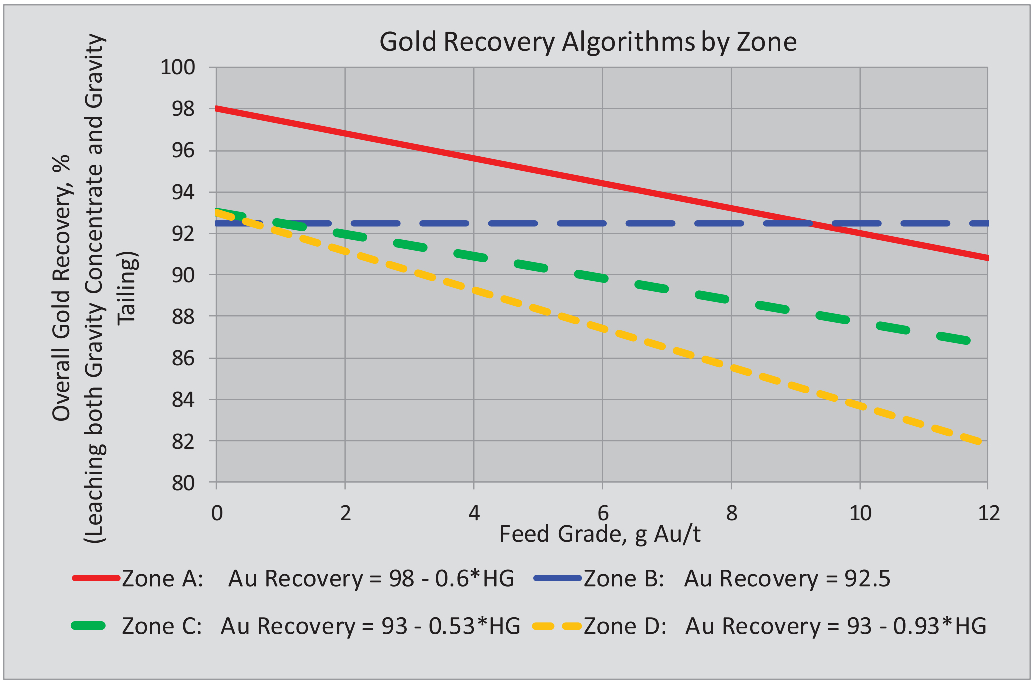
Mineralisation from the Magambazi deposit may be processed using conventional gravity concentration and cyanide leaching to recover the contained gold. The deposit has been divided into four zones, Zones A through D, along strike proceeding from South to North. Extensive composites representing a wide range of gold grade from each of these zones have been used to produce the gold recovery algorithms in Table 13.6 and shown graphically in Figure 13-3.

Table 13.6: Gold Recovery Algorithms by Zone

Zone A	Overall Gold Recovery =	98 - 0.6*HG
Zone B	Overall Gold Recovery =	92.5
Zone C	Overall Gold Recovery =	93 - 0.53*HG
Zone D	Overall Gold Recovery =	93 - 0.93*HG

Note. Calculated recoveries are expressed in percent.

Figure 13-3: Gold Recovery Algorithms by Zone



It should be noted that:

- Gold recovery is lower for mineralisation originating in the north of the deposit, represented by Zones C and D, than in the South represented by Zones A and B.
- Gold recovery is reduced as the feed grade mineralisation increases. Gold in the Magambazi deposit is closely associated with arsenic and two arsenic minerals have been identified, namely arsenopyrite and lollingite. It is likely that the reduction in gold recovery is due to a change of mineralogy and gold distribution between these two minerals as the gold content of the mineralisation increases. This aspect of the mineralogy should be investigated further.

The flowsheet suggested for processing the Magambazi deposit should comprise:

- Three stage crushing to a P80 of 6 mm.
- Single stage ball milling to a P80 product size of 180 to 200 µm, assuming the deposit might eventually be mined by open pit methods. Testwork has shown the Handeni deposit to contain medium-hard mineralised material with an average Bond Work Index of 16.6. It is considered medium abrasive with an average abrasion index of 0.30.
- Gravity concentration installed in the grinding circuit should be expected to recover approximately 70% of the gold in the plant feed into a gravity rougher concentrate representing approximately 2% of the mass feed. In this approach, the gravity concentrate

should be subjected to cyanide leaching using a cyanide concentration of 2000 ppm for a residence time of 48 hours.

- The ground process feed, after removal of the gravity concentrate, should be subjected to cyanide leaching using a cyanide concentration of 500 ppm for a residence time of 24 hours. The cyanide leaching should be carried out in a series of eight tanks, the first two tanks operated as straight leach tanks with the remaining six tanks operated as carbon in pulp tanks in a carousel arrangement.
- Cyanide consumption in the testwork averaged 2.5 kg NaCN per tonne of gravity concentrate, and 0.10 kg NaCN per tonne of gravity tailing. The overall cyanide consumption ranged from 0.10 to 0.30 kg NaCN per tonne of Grade Composite feed. It should be noted that these consumptions are the specific cyanide requirement to leach the gold and they do not include cyanide that will inevitably be left in solution at the end of the gravity concentrate and gravity tailing leaches. Whilst every effort will be made to recycle cyanide from leach solutions, the actual plant cyanide consumptions would be expected to be closer to 4 kg NaCN per tonne of gravity concentrate and 0.35 kg NaCN per tonne of gravity tailing. Based on the relative weights of gravity concentrate on gravity tailing, this calculates to an overall consumption of 0.43 kg NaCN per tonne of plant feed. A consumption of 0.50 kg NaCN per tonne feed is suggested for use in calculating operating costs.
- Lime consumption ranged from 1.5 to 5.0 kg CaO per tonne of gravity concentrate, with the highest consumption measured for Zone D material. Lime consumption ranged from 0.5 to 1.0 kg CaO per tonne of gravity tailing. The overall lime consumption ranged from 0.5 to 1.1 kg CaO per tonne of plant feed. A consumption of 1.00 kg CaO per tonne plant feed is suggested for use in calculating operating costs

13.2.1 Alternate Flowsheet Incorporating Flotation

To minimise the amount of material subjected to cyanide leaching, preliminary testwork has been carried out on low-grade and high-grade master composites of Zones A through D, to investigate whether satisfactory gold recoveries could be collected into a combined gravity concentrate and flotation concentrate that represented a small weight percentage of the plant feed.

For the low-grade master composite, 96.4% of the gold was recovered into the combined gravity-flotation concentrate, and leaching this combined concentrate dissolved 95.5% of the contained gold, giving an overall gold recovery of 92.1%. Results for the high-grade master composites were similar, with 96.9% of the gold recovered into the combined gravity-flotation concentrate, and leaching this combined concentrate dissolving 95.0% of the contained gold, for an overall gold recovery of 92.1%.

Although these results are preliminary and should be substantiated by further testwork on the high-grade and low-grade composites representing Zones A through D, they are encouraging. This gravity-flotation-leach flowsheet may offer significant advantages from an environmental and waste management standpoint if it is possible to cyanide leach less than 10% of the process plant fresh feed and achieve gold recoveries over 90%.

13.3 Testwork Results & Discussion

13.3.1 Bond Work Index & Abrasion Indices

During preparation of the zonal composites, a subset of samples was riffled out for measurement of the Bond work index and abrasion index across Zones A through D of the deposit. The results are summarised in Table 13.7. The Bond Work Index is expressed in kW.h per tonne.

Table 13.7: Bond Work Index & Abrasion Indices

		Bond Work Index kW.h/tonne	Bond Abrasion Index Ai
Zone A	Low Grade Composite	16.6	0.29
	High Grade Composite	16.8	0.34
Zone B	Low Grade Composite	16.2	0.32
	High Grade Composite	17.8	0.25
Zone C	Low Grade Composite	16.4	0.27
	High Grade Composite	16.7	0.27
Zone D	Low Grade Composite	16.6	0.29
	High Grade Composite	15.9	0.35
Arithmetic Mean		16.6	0.30

The Bond work index was consistent across Zones A through D, averaging 16.6, indicating the material in the Handeni deposit can be classified as medium hard. The abrasion index was also consistent, averaging 0.30, indicating medium abrasivity.

13.3.2 Preliminary Gravity + Leach Tests on Zonal Composites

A single gravity plus leach test was performed on each of the high-grade and low-grade zonal composites to confirm that the Magambazi deposit is free milling and contains gold that can be recovered by gravity and cyanidation methods. The tests would also provide an initial picture of variability across the deposit, the percentage of gold recoverable by gravity separation, and the required leach residence time and reagent consumption. The results were carried out on 2 kg samples ground to a nominal P80 of 100 µ and then subjected to a gravity separation with a Knelson concentrator fitted with a 4 inch diameter bowl. The Knelson concentrate was cleaned using a Super Panner. The Knelson gravity tailing and super panner tailing were combined and subjected to a cyanide leach at 33% solids pulp density, using a cyanide concentration of 1000 ppm NaCN, and a leach residence time of 96 hours. The results are summarised in Table 13.8 below.

Table 13.8: Exploratory Tests on Zones A through D

	Low Grade Composites				High Grade Composites			
Gravity Separation	Zone A	Zone B	Zone C	Zone D	Zone A	Zone B	Zone C	Zone D
Gravity/Leach Test No.	G11/L17	G13/L19	G15/L21	G1/L9	G12/L18	G14/L20	G16/L22	G2/L10
Product Weights,g								
Gravity Concentrate	15.8	16.6	18.0	15.6	18.3	23.5	22.2	16.9
Gravity Cleaner Tail	41.7	48.9	37.9	46.2	56.3	48.7	45.0	47.7
Gravity Rougher Tail	1944.9	1936.9	1941.8	1942.8	1929.0	1929.5	1938.9	1928.3
Feed	2002.4	2002.4	1997.7	2004.6	2003.6	2001.7	2006.1	1992.9
Weight %								
Gravity Concentrate	37.89	33.95	47.49	33.77	32.50	48.25	49.33	35.43
Gravity Cleaner Tail	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00
Gravity Rougher Tail	4664.03	3960.94	5123.48	4205.19	3426.29	3962.01	4308.67	4042.56
Assay, g Au/t								
Gravity Concentrate	91.04	108.40	101.00	78.00	303	358	453.60	140
Gravity Cleaner Tail	6.54	7.89	11.00	12.60	23.2	18.8	19.70	18.4
Gravity Rougher Tail	0.34	0.51	0.53	0.32	0.79	1.18	1.82	0.86
Au Distribution, %								
Gravity Concentrate	0.0	0.0	0.0	0.0	0.1	0.2	0.3	0.1
Gravity Cleaner Tail	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Gravity Rougher Tail	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.0
Feed	0.1	0.1	0.1	0.1	0.2	0.3	0.4	0.1
Backcalculated Composite Assay using Gravity Results								
Gold Grade, g Au/t	56.89	64.89	86.12	52.39	148.76	238.30	321.89	102.77
Cyanide Leaching of Gravity Tailing								
Calculated Cyanide Leach Feed								
Weight Gravity Rougher Tail, g	1922.3	1914.3	1918.0	1919.9	1906.5	1903.9	1914.1	1905.7
Assay of Gravity Rougher Tail	0.34	0.51	0.53	0.32	0.79	1.18	1.82	0.86
Weight Gravity Cleaner Tail, g	28.93	35.53	25.00	34.16	43.86	36.78	33.39	36.51
Assay of Gravity Cleaner Tail	6.54	7.89	11.00	12.60	23.20	18.80	19.70	18.40
Weight Cyanide Leach Feed, g	1951.2	1949.8	1943.0	1954.1	1950.4	1940.7	1947.5	1942.2
Calculated Grade of Leach Feed	0.43	0.64	0.66	0.53	1.29	1.51	2.13	1.19
(based on gravity tail weights and assays)								
Leach Feed Pulp Density, %solids by wt	33	33	33	33	33	33	33	33
Leach Feed Cyanide Strength, mg NaCN/L	1000	1000	1000	1000	1000	1000	1000	1000
Leach Feed pH	11.0	11.0	11.0	11.0	11.0	11.0	11.0	11.0
Start Leach Feed Solution Volume, mL	3902.0	3900.0	3886.0	3908.2	3900.8	3882.0	1947.5	3884.0
Cyanide Solution Sample Assay, g Au/t								
8h 30mL sample removed	0.19	0.23	0.16	0.29	0.56	0.58	2.06	0.46
24h 30mL sample removed	0.20	0.25	0.19	0.29	0.56	0.60	2.22	0.49
48h 30mL sample removed	0.20	0.25	0.19	0.29	0.56	0.60	2.23	0.48
72h 30mL sample removed	0.20	0.25	0.19	0.29	0.56	0.60		0.49
96h	0.20	0.25	0.19	0.29	0.56	0.59	2.24	0.47
End of Leach Solution Volume, mL	3782	3780	3766	3788	3781	3762	1828	3764
Cyanide Leach Residue Weight,g	1951	1947	1942	1952	1950	1938	1948	1941
Cyanide Leach Residue Assay, g Au/t	0.070	0.060	0.080	0.080	0.185	0.310	0.150	0.180
Cyanide Leach Gold Dissolution, %	85.00	89.22	82.48	87.81	85.73	79.09	93.62	83.84
Backcalculated Leach Feed Grade, g Au/t	0.47	0.56	0.46	0.66	1.30	1.48	2.35	1.11
(based on leach solution and residue weights and assays)								
Cyanide Consumption, g NaCN	0.97	0.66	0.47	0.75	0.43	0.51	0.11	0.82
- kg NaCN/tonne solids in Leach Feed	0.497	0.338	0.242	0.384	0.220	0.263	0.056	0.422
Lime Consumption, g CaO	1.23	0.86	1.01	1.42	1.21	1.06	1.00	0.98
- kg CaO/tonne solids in Leach Feed	0.63	0.44	0.52	0.73	0.62	0.55	0.51	0.50
Backcalculated Composite Grade, g Au/t	1.21	1.49	1.43	1.32	4.17	5.75	7.41	2.37
(based on cleaned gravity concentrate wt and assay, backcalculated leach feed grade plus an allowance for gold in the portion of gravity cleaner tail used for assay)								
Predicted Grade of Composite from Drill Core Assays, g Au/t	1.57	1.94	1.58	1.51	8.26	8.01	6.66	5.34
(based on as received 1/4 core weights and drill core data base assays)								
Calculated Overall Gold Recovery, %	85.0	89.2	82.5	87.8	85.8	79.1	93.6	83.8
(Gravity gold recovery + leach recovery x gold recovery in gravity tail)								

The following observations can be made from the testwork results:

- The Magambazi mineralisation is considered to be free milling. The gold reporting to a cleaned gravity concentrate plus the gold dissolved by cyanide leach treatment of the gravity rougher and cleaner tailings was over 90% of all gold in the composites for each of the eight zonal composites tested. Gold recovery appears to be reasonably uniform along the strike length of the deposit.
- Gold recovery into a Knelson gravity rougher concentrate ranged from 70 to 80%. Cleaning the Knelson gravity rougher concentrate with a super panner upgraded the rougher concentrate by a concentration ratio of approximately 3.5 but resulted in significant gold reporting to the super panner cleaner tailing.
- Gold dissolved in the cyanide leach ranged from 79% to 94%, when processing gravity tailing that represented between 25 and 50% of the gold in the fresh process feed
- Based on the gold assay of kinetic samples of leach solution taken after 8, 24, 48, 72, and 96 hours, there was no significant increase in gold dissolution after a 24-hour leach residence time.
- Discounting one anomalous result, the cyanide consumed in the gold leach reaction ranged from 0.2 to 0.5 kg NaCN per tonne of fresh feed. Lime consumption ranged from 0.44 to 0.73 kg CaO per tonne of fresh feed.
- The back calculated head grades of the gravity-leach tests run on the low-grade composites were in reasonable agreement with the predicted grade of the low-grade composites calculated using the as received quarter core weights and the drill core assays from the drill core database, for each constituent interval in the composite. For the high-grade composites there was a significant deviation in the testwork back calculated head grade compared to the predicted composite head grade using the drill core assays. For the high-grade composites zones A, B, and D, the back calculated head grade from testwork was between 30 and 50% lower than that predicted for the composite head grade using the drill core assays.

13.3.3 Primary Grind Evaluation

The effect of primary grind size on gold recovery was evaluated on each of the low-grade and high-grade Magambazi composites representing Zones A through D.

Five representative 2 kg charges of each composite were ground to produce grind sizes representing the range of P80 from 225 to 74 µm. The ground slurry samples were processed using a similar flowsheet to that used in the preliminary gravity + leach tests described in Section 13.3.2, except that the cyanide leach pulp density was increased from 33% to 50% solids by weight, the cyanide leach concentration was increased to 2000 ppm NaCN and the leach residence time was reduced to 48h from 96h.

Ground slurry was subjected to a gravity concentration step using a Knelson concentrator. The Knelson concentrate was cleaned using a Super Panner to further upgrade the gravity rougher concentrate. All products from the gravity separation steps were assayed to calculate the gold distribution. Cyanide leach tests were then run on the combined Super Panner cleaner tailing and the Knelson rougher tailing for each of the different grind sizes being evaluated.

The results are summarised in the tables and graphs that follow in the discussion below. The following observations can be made:

- For the low-grade composites, there was a clear trend for the amount of gold reporting to the cleaned gravity concentrate to increase as the primary grind was made finer, as shown in the graph below. For the high-grade composites, the amount of gold reporting to the cleaned gravity concentrate was less influenced by the primary grind size as seen in Figures 13-4 and 13-5.
- The overall gold recovery will closely approximate to the sum of gold reporting to the cleaned gravity concentrate and gold dissolved by leaching the gravity rougher and cleaner tailings. The recovery is plotted against grind size in Figures 13-6 and 13-7. Despite some scatter in the results, it is apparent that the primary grind size does not have a strong influence on the gold recovery over the range of primary grind size evaluated. It should be noted that the gold recovery from the Zone D low-grade and high-grade composites are approximately 2% lower than for composites from the other three Zones A through C.
- The economic primary grind size is normally determined by balancing the metal losses in the final tailing for a given primary grind size against the grinding operating and capital costs required to achieve that grind size. The graphs of leach residue assay versus grind size for both the low-grade and high-grade composites are shown below in Figures 13-8 and 13-9. The scattering in the results does not allow for a detailed economic analysis, but it is clear that for the low-grade composites, the primary grind size has very little effect on the gold assay of leach residues generated from the low-grade composites. For the high-grade composites, there is a trend for the leach residue assay to decrease with increasing fineness of grind.

By taking the average leach residue assay for the low-grade and high-grade composites, at each of the five nominal grind sizes, the data can be smoothed considerably as shown in Figure 13-10.

The average results indicate that the gold assay of the leach residues produced from the low-grade composites are relatively insensitive to grind size, and the low-grade composites can therefore be processed at a coarse grind size, with a P80 size of 200 µm. For the high-grade composites, increasing the fineness of grind from 230 µm to 130 µm reduces the assay of the cyanide leach tail by approximately 0.05 g of gold per tonne, which is worth approximately $2.50 per tonne of feed at current gold prices. With prevailing unit grinding operating costs, expressed in dollars per kilowatt hour input for operating and capital right of components, it should be economic to grind the high-grade mineralised material to a P80 of 130 µm.

Figure 13-4: Gold Recovered into Cleaned Gravity Concentrate vs. Primary Grind Size – Low Grade Composites, Zones A-D

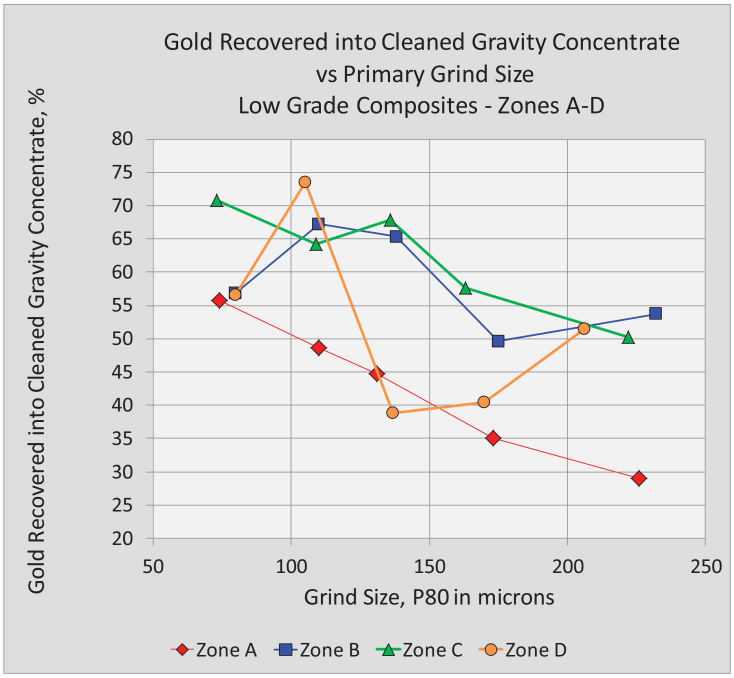


Figure 13-5: Gold Recovered into Cleaned Gravity Concentrate vs. Primary Grind Size – High Grade Composites, Zones A-D

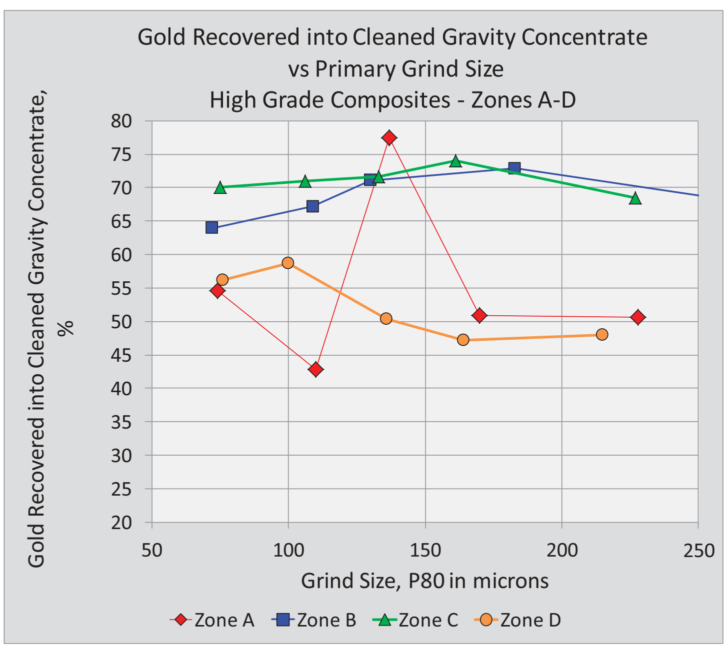


Figure 13-6: Gold Recovery vs. Grind Size – Low Grade Composites

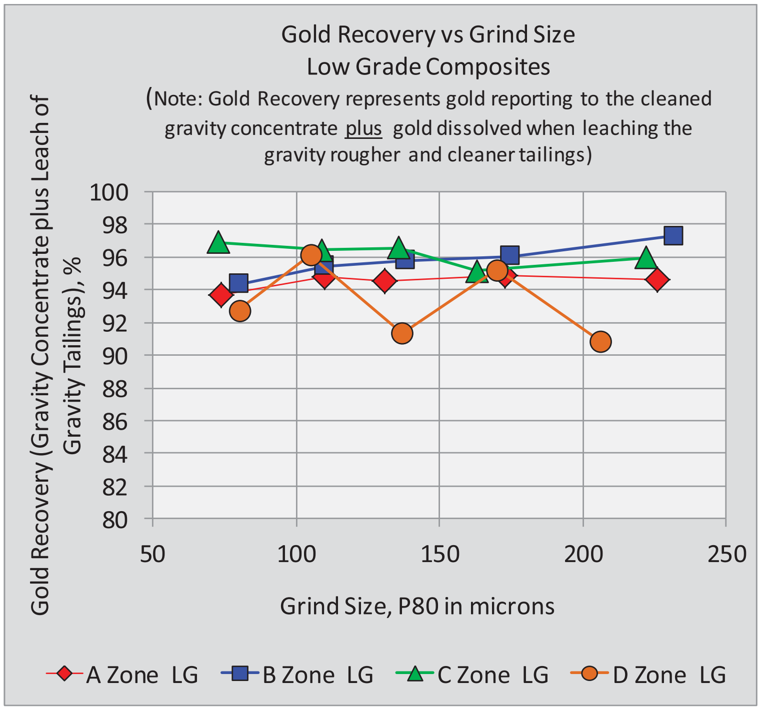


Figure 13-7: Gold Recovery vs. Grind Size – High Grade Composites

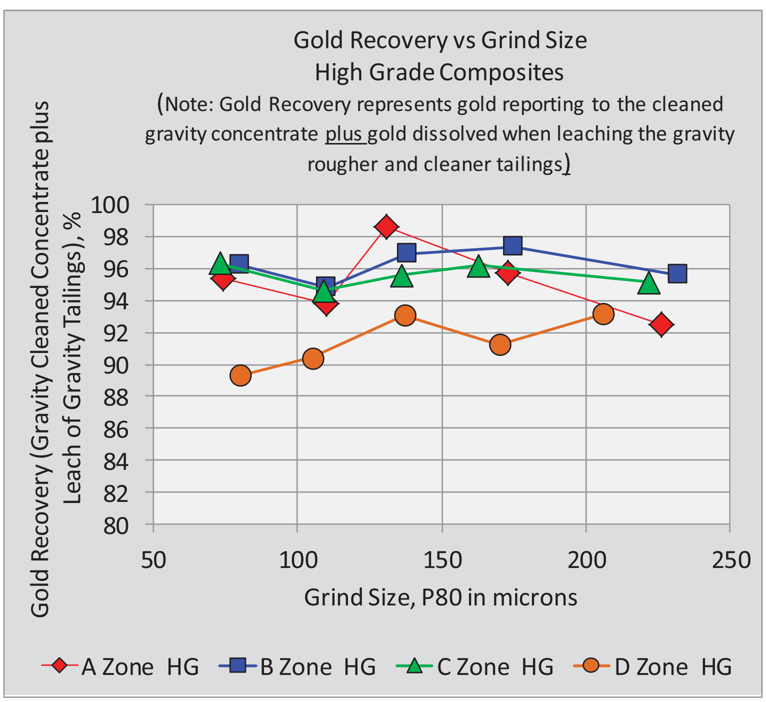


Figure 13-8: Leach Residue Assay vs. Grind Size – Low Grade Composites

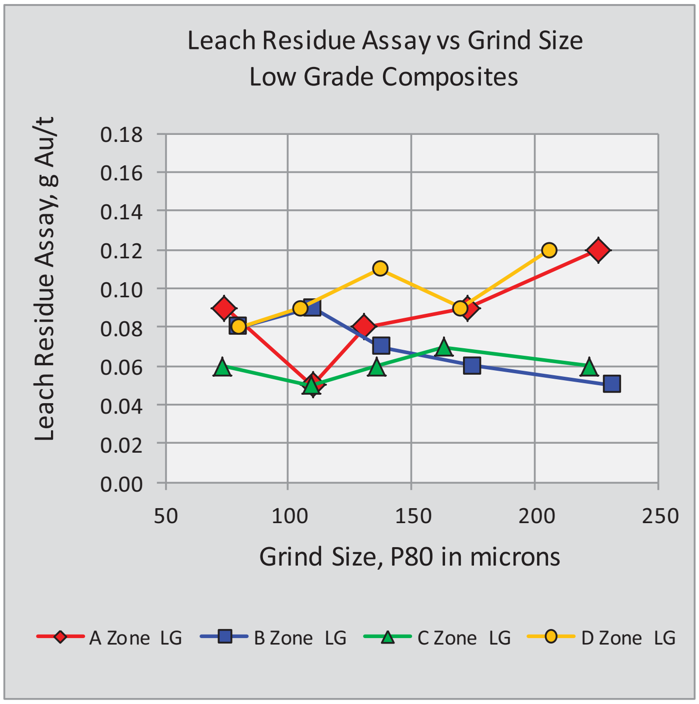


Figure 13-9: Leach Residue Assay vs. Grind Size – High Grade Composites

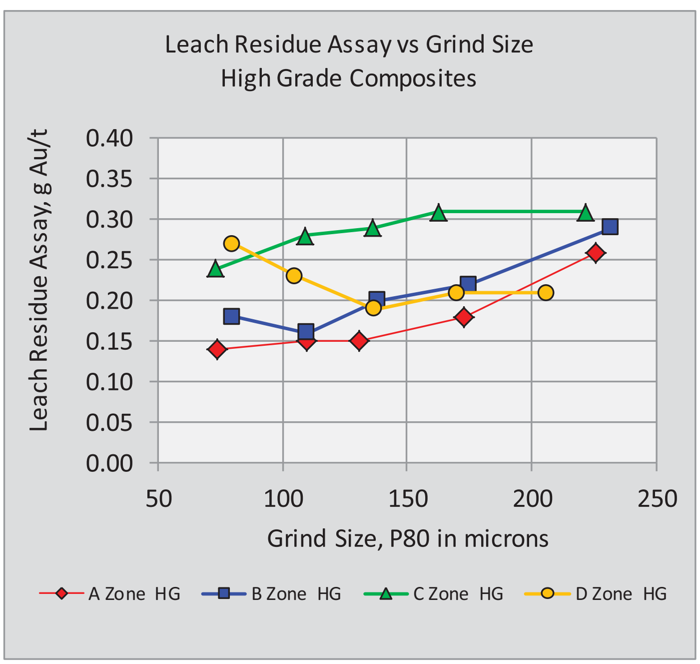
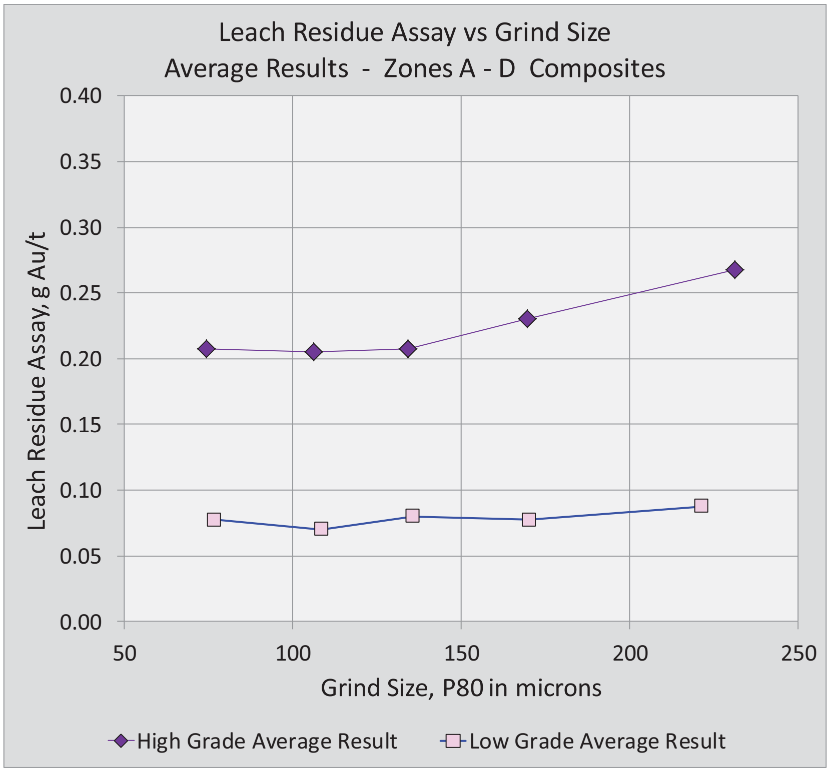


Figure 13-10: Leach Residue Assay vs. Grind Size – Average Results



If this deposit were to be mined by open pit methods, there would likely be significant dilution of the high-grade material component in the process plant feed, and it would not be justified to grind the entire process plant feed to 130 µm. Consequently, a significantly coarser grind size would be adopted and it is recommended that for the economic study on this deposit, a primary grind size of 200 µ is used if the deposit were to be mined by open pit methods.

Reagent consumption when leaching the gravity tailing was modest. Cyanide consumption ranged from 0.10 to 0.30 kg NaCN per tonne. Lime consumption ranged from 0.30 to 0.55 kilograms CaO per tonne. Reagent consumptions for both high-grade and low-grade composites were similar, and both showed a trend of reducing consumption with a coarser primary grind size.

The primary grind size test results are summarised in Tables 13.9 through 13.12 for each of the mineralised Zones and for each of the high and low grade composites tested.

Table 13.9: Zone A Primary Grind Results

Gravity Separation	ZONE A LG COMPOSITE					ZONE A HG COMPOSITE				
Gravity/Leach Test No.	G23/L49	G24/L50	G25/L51	G90/L98	G26/L52	G27/L53	G28/L54	G29/L55	G91/L99	G30/L56
Grind Size, K80	226	173	131	110	74	228	170	137	110	74
Product Weights,g										
Gravity Concentrate	15.1	22.3	23.3	19.6	21.3	24.6	24.6	23.9	21.9	22.4
Gravity Cleaner Tail	48.4	38.7	39.3	43.8	25.5	52.4	44.6	36.4	50.9	26.1
Gravity Rougher Tail	1925.3	1938.4	1925.9	1944.4	1965.9	1906.0	1923.8	1935.7	1933.6	1957.6
Feed	1988.8	1999.4	1988.5	2007.8	2012.7	1983.0	1993.0	1996.0	2006.4	2006.1
Weight %										
Gravity Concentrate	0.76	1.12	1.17	0.98	1.06	1.24	1.23	1.20	1.09	1.12
Gravity Cleaner Tail	2.43	1.94	1.98	2.18	1.27	2.64	2.24	1.82	2.54	1.30
Gravity Rougher Tail	96.81	96.95	96.85	96.84	97.67	96.12	96.53	96.98	96.37	97.58
Assay, g Au/t										
Gravity Concentrate	87.51	61.75	56.50	60	76.7	135	170	351.21	228	163
Gravity Cleaner Tail	47.82	35.87	15.51	7.1	21.5	29.4	48.4	6.01	11.6	49.2
Gravity Rougher Tail	0.48	0.60	0.53	0.48	0.38	0.90	0.98	1.15	3.14	0.89
Au Distribution, %										
Gravity Concentrate	28.98	35.05	44.68	48.59	55.76	50.60	50.91	77.44	42.84	54.60
Gravity Cleaner Tail	50.76	35.34	20.68	12.85	18.72	23.35	26.21	2.02	5.07	19.27
Gravity Rougher Tail	20.27	29.61	34.64	38.56	25.51	26.05	22.89	20.54	52.09	26.13
Feed	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00
Backcalculated Composite Assay using Gravity Results										
Gold Grade, g Au/t	2.29	1.96	1.48	1.21	1.45	3.32	4.13	5.43	5.81	3.32
Cyanide Leaching of Gravity Tailing										
Calculated Cyanide Leach Feed										
Weight Gravity Rougher Tail, g	1694.3	1718.1	1717.3	1896.0	1765.4	1627.5	1676.0	1717.8	1899.5	1745.5
Assay of Gravity Rougher Tail	0.48	0.60	0.53	0.48	0.38	0.90	0.98	1.15	3.14	0.89
Weight Gravity Cleaner Tail, g	36.94	28.31	24.61	22.80	14.81	41.26	33.75	25.36	30.60	14.87
Assay of Gravity Cleaner Tail	47.82	35.87	15.51	7.10	21.50	29.35	48.40	6.01	11.60	49.23
Weight Cyanide Leach Feed, g	1731.2	1746.4	1742.0	1918.8	1780.2	1668.8	1709.8	1743.1	1930.1	1760.3
Calculated Grade of Leach Feed	1.49	1.17	0.74	0.56	0.56	1.60	1.92	1.22	3.27	1.30
(based on gravity tail weights and assays)										
Leach Feed Pulp Density, %solids by wt	50	50	50	50	50	50	50	50	50	50
Leach Feed Cyanide Strength, mg NaCN/L	2000	2000	2000	2000	2000	2000	2000	2000	2000	2000
Leach Feed pH	11.0	11.0	11.0	11.0	11.0	11.0	11.0	11.0	11.0	11.0
Start Leach Feed Solution Volume, mL	1731.2	1746.4	1742.0	1918.8	1780.2	1668.8	1709.8	1743.1	1930.1	1760.3
Cyanide Solution Sample Assay, g Au/t										
8h 30mL sample removed	1.32	0.96	0.68	0.43	0.51	1.29	1.76	2.06	1.21	1.14
24h 30mL sample removed	1.42	1.03	0.71	0.44	0.52	1.45	1.96	2.22	1.22	1.22
32h 30mL sample removed	1.43	1.04	0.72	0.44	0.53	1.45	1.92	2.23	1.24	1.22
48h	1.46	1.05	0.73	0.44	0.54	1.45	1.90	2.24	1.23	1.23
End of Leach Solution Volume, mL	1641	1656	1652	1829	1690	1579	1620	1653	1840	1670
Cyanide Leach Residue Weight,g	1731	1746	1742	1919	1780	1669	1710	1743	1930	1760
Cyanide Leach Residue Assay, g Au/t	0.12	0.09	0.08	0.05	0.09	0.26	0.18	0.15	0.15	0.14
Cyanide Leach Gold Dissolution, %	92.39	92.09	90.11	89.79	85.69	84.77	91.34	93.71	89.13	89.77
Backcalculated Leach Feed Grade, g Au/t	1.58	1.14	0.81	0.49	0.63	1.71	2.08	2.39	1.38	1.37
(based on leach solution and residue weights and assays)										
Cyanide Consumption, g NaCN	0.04	0.06	0.21	0.52	0.07	0.24	0.10	0.11	0.49	0.32
- kg NaCN/tonne solids in Leach Feed	0.023	0.034	0.121	0.271	0.039	0.144	0.058	0.063	0.254	0.182
Lime Consumption, g CaO	0.65	0.64	1.01	1.20	1.02	0.47	0.60	1.00	0.96	1.11
- kg CaO/tonne solids in Leach Feed	0.38	0.37	0.58	0.63	0.57	0.28	0.35	0.57	0.50	0.63
Backcalculated Composite Grade, g Au/t	2.37	1.92	1.54	1.13	1.52	3.40	4.27	6.54	3.94	3.38
(based on cleaned gravity concentrate wt and assay, backcalculated leach feed grade plus an allowance for gold in the portion of gravity cleaner tail used for assay)										
Predicted Grade of Composite from Drill Core Assays, g Au/t	1.57	1.57	1.57	1.57	1.57	8.26	8.26	8.26	8.26	8.26
(based on as received 1/4 core weights and drill core data base assays)										
Calculated Overall Gold Recovery, %	94.6	94.9	94.5	94.8	93.7	92.5	95.7	98.6	93.8	95.4

Table 13.10: Zone B Primary Grind Results

Gravity Separation	ZONE B LG COMPOSITE					ZONE B HG COMPOSITE				
Gravity/Leach Test No.	G31/L57	G32/L58	G33/L59	G92/L100	G34/L60	G35/L61	G36/L62	G37/L63	G300/L301	G38/L64
Grind Size, K80	232	175	138	110	80	255	183	130	109	72
Product Weights,g										
Gravity Concentrate	20.1	20.4	22.3	24.2	19.0	23.4	24.0	19.0	19.4	16.5
Gravity Cleaner Tail	43.4	37.7	29.3	33.6	30.1	43.6	41.7	41.4	39.6	30.4
Gravity Rougher Tail	1930.6	1938.8	1945.3	1946.2	1963.2	1922.3	1925.7	1930.1	1940.9	1961.0
Feed	1994.1	1996.9	1996.9	2004.0	2012.3	1989.3	1991.4	1990.5	1999.9	2007.9
Weight %										
Gravity Concentrate	1.01	1.02	1.12	1.21	0.94	1.18	1.21	0.95	0.97	0.82
Gravity Cleaner Tail	2.18	1.89	1.47	1.68	1.50	2.19	2.09	2.08	1.98	1.51
Gravity Rougher Tail	96.82	97.09	97.42	97.12	97.56	96.63	96.70	96.97	97.05	97.66
Assay, g Au/t										
Gravity Concentrate	115	91.0	97.7	128	97.2	360	531	471	316	401
Gravity Cleaner Tail	16.0	9.90	9.61	17.7	13.9	17.0	46.0	39.0	32.4	33.2
Gravity Rougher Tail	0.67	0.78	0.45	0.47	0.50	1.63	1.47	1.05	0.88	1.39
Au Distribution, %										
Gravity Concentrate	53.70	49.60	65.31	67.24	56.87	68.52	72.86	71.07	67.18	63.93
Gravity Cleaner Tail	16.17	9.98	8.44	12.91	12.89	6.02	10.96	12.83	14.08	9.74
Gravity Rougher Tail	30.14	40.42	26.25	19.85	30.23	25.46	16.18	16.11	18.74	26.33
Feed	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00
Backcalculated Composite Assay using Gravity Results										
Gold Grade, g Au/t	2.15	1.87	1.67	2.30	1.61	6.19	8.79	6.32	4.56	5.16
Cyanide Leaching of Gravity Tailing										
Calculated Cyanide Leach Feed										
Weight Gravity Rougher Tail, g	1690.0	1734.0	1723.8	1911.1	1778.1	1662.1	1643.3	1645.3	1888.8	1702.4
Assay of Gravity Rougher Tail	0.67	0.78	0.45	0.47	0.50	1.63	1.47	1.05	0.88	1.39
Weight Gravity Cleaner Tail, g	23.88	27.23	18.55	13.20	19.28	31.53	30.15	29.80	11.20	19.41
Assay of Gravity Cleaner Tail	15.99	9.90	9.61	17.70	13.91	16.98	45.97	38.98	32.42	33.17
Weight Cyanide Leach Feed, g	1713.9	1761.3	1742.4	1924.3	1797.3	1693.6	1673.4	1675.1	1900.0	1721.8
Calculated Grade of Leach Feed	0.88	0.92	0.55	0.59	0.64	1.92	2.27	1.72	1.07	1.75
(based on gravity tail weights and assays)										
Leach Feed Pulp Density, %solids by wt	50	50	50	50	50	50	50	50	50	50
Leach Feed Cyanide Strength, mg NaCN/L	2000	2000	2000	2000	2000	2000	2000	2000	2000	2000
Leach Feed pH	11.0	11.0	11.0	11.0	11.0	11.0	11.0	11.0	11.0	11.0
Start Leach Feed Solution Volume, mL	1713.9	1761.3	1742.4	1924.3	1797.3	1693.6	1673.4	1675.1	1900.0	1721.8
Cyanide Solution Sample Assay, g Au/t										
8h 30mL sample removed	0.67	0.63	0.47	0.56	0.52	1.38	1.85	1.51	0.83	1.49
24h 30mL sample removed	0.80	0.70	0.51	0.56	0.55	1.70	2.00	1.68	0.84	1.55
32h 30mL sample removed	0.80	0.70	0.51	0.56	0.55	1.75	2.01	1.67	0.84	1.54
48h	0.80	0.71	0.51	0.56	0.53	1.79	2.02	1.67	0.85	1.53
End of Leach Solution Volume, mL	1624	1671	1652	1834	1707	1604	1583	1585	1810	1632
Cyanide Leach Residue Weight,g	1714	1761	1742	1924	1797	1694	1673	1675	1900	1722
Cyanide Leach Residue Assay, g Au/t	0.05	0.06	0.07	0.09	0.08	0.29	0.22	0.20	0.16	0.18
Cyanide Leach Gold Dissolution, %	94.10	92.19	87.92	86.15	86.90	85.99	90.16	89.29	84.15	89.47
Backcalculated Leach Feed Grade, g Au/t	0.85	0.77	0.58	0.65	0.61	2.07	2.24	1.87	1.01	1.71
(based on leach solution and residue weights and assays)										
Cyanide Consumption, g NaCN	0.32	0.80	0.22	0.43	0.36	0.47	0.50	0.38	0.65	0.20
- kg NaCN/tonne solids in Leach Feed	0.187	0.454	0.126	0.223	0.200	0.278	0.299	0.227	0.342	0.116
Lime Consumption, g CaO	0.49	0.53	0.52	0.92	0.69	0.46	0.35	0.58	0.87	0.92
- kg CaO/tonne solids in Leach Feed	0.29	0.30	0.30	0.48	0.38	0.27	0.21	0.35	0.46	0.53
Backcalculated Composite Grade, g Au/t	2.11	1.71	1.70	2.36	1.58	6.31	8.73	6.44	4.50	5.10
(based on cleaned gravity concentrate wt and assay, backcalculated leach feed grade plus an allowance for gold in the portion of gravity cleaner tail used for assay)										
Predicted Grade of Composite from Drill Core Assays, g Au/t	1.94	1.94	1.94	1.94	1.94	8.01	8.01	8.01	8.01	8.01
(based on as received 1/4 core weights and drill core data base assays)										
Calculated Overall Gold Recovery, %	97.3	96.1	95.8	95.5	94.3	95.6	97.3	96.9	94.8	96.2

Table 13.11: Zone C Primary Grind Results

Gravity Separation	ZONE C LG COMPOSITE					ZONE C HG COMPOSITE				
Gravity/Leach Test No.	G39/L65	G40/L66	G41/L67	G94/L102	G42/L68	G43/L69	G44/L70	G45/L71	G95/L103	G46/L72
Grind Size, K80	222	163	136	109	73	227	161	133	106	75
Product Weights,g										
Gravity Concentrate	19.9	17.6	20.3	22.1	15.8	25.7	20.7	23.4	24.7	18.8
Gravity Cleaner Tail	41.6	41.2	33.5	34.3	28.8	37.6	43.7	37.1	31.8	29.6
Gravity Rougher Tail	1916.8	1938.5	1943.1	1947.8	1966.1	1918.3	1927.2	1934.2	1943.6	1958.4
Feed	1978.3	1997.3	1996.9	2004.2	2010.7	1981.6	1991.6	1994.7	2000.1	2006.8
Weight %										
Gravity Concentrate	1.01	0.88	1.02	1.10	0.79	1.30	1.04	1.17	1.23	0.94
Gravity Cleaner Tail	2.10	2.06	1.68	1.71	1.43	1.90	2.19	1.86	1.59	1.47
Gravity Rougher Tail	96.89	97.06	97.31	97.19	97.78	96.81	96.77	96.97	97.18	97.59
Assay, g Au/t										
Gravity Concentrate	110	73.8	125	96	169	313	584	475	275	527
Gravity Cleaner Tail	8.50	10.9	9.40	12.9	9.58	20.0	23.4	33.8	19.5	25.1
Gravity Rougher Tail	0.94	0.26	0.46	0.38	0.42	1.54	1.67	1.63	1.11	1.78
Au Distribution, %										
Gravity Concentrate	50.29	57.68	67.81	64.21	70.75	68.47	74.04	71.63	70.98	70.09
Gravity Cleaner Tail	8.15	19.95	8.39	13.39	7.33	6.41	6.25	8.07	6.48	5.25
Gravity Rougher Tail	41.55	22.37	23.80	22.40	21.93	25.13	19.71	20.30	22.54	24.65
Feed	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00
Backcalculated Composite Assay using Gravity Results										
Gold Grade, g Au/t	2.19	1.13	1.88	1.65	1.87	5.93	8.20	7.78	4.78	7.05
Cyanide Leaching of Gravity Tailing										
Calculated Cyanide Leach Feed										
Weight Gravity Rougher Tail, g	1686.6	1688.8	1699.3	1910.2	1746.3	1684.6	1659.5	1724.6	1904.6	1726.3
Assay of Gravity Rougher Tail	0.94	0.26	0.46	0.38	0.42	1.54	1.67	1.63	1.11	1.78
Weight Gravity Cleaner Tail, g	29.92	29.73	21.63	13.90	17.70	25.55	32.06	26.02	11.10	18.23
Assay of Gravity Cleaner Tail	8.50	10.91	9.40	12.90	9.58	20.03	23.36	33.76	19.50	25.10
Weight Cyanide Leach Feed, g	1716.5	1718.5	1720.9	1924.1	1764.0	1710.1	1691.5	1750.6	1915.7	1744.6
Calculated Grade of Leach Feed	1.07	0.44	0.57	0.47	0.51	1.82	2.08	2.11	1.22	2.02
(based on gravity tail weights and assays)										
Leach Feed Pulp Density, %solids by wt	50	50	50	50	50	50	50	50	50	50
Leach Feed Cyanide Strength, mg NaCN/L	2000	2000	2000	2000	2000	2000	2000	2000	2000	2000
Leach Feed pH	11.0	11.0	11.0	11.0	11.0	11.0	11.0	11.0	11.0	11.0
Start Leach Feed Solution Volume, mL	1716.5	1718.5	1720.9	1924.0	1764.0	1710.1	1691.5	1750.6	1915.0	1744.6
Cyanide Solution Sample Assay, g Au/t										
8h 30mL sample removed	0.57	0.50	0.45	0.43	0.49	1.22	1.62	1.43	1.20	1.70
24h 30mL sample removed	0.67	0.54	0.49	0.44	0.51	1.61	1.78	1.57	1.23	1.72
32h 30mL sample removed	0.68	0.54	0.50	0.44	0.51	1.63	1.78	1.57	1.23	1.72
48h	0.68	0.54	0.50	0.45	0.51	1.70	1.80	1.57	1.23	1.70
End of Leach Solution Volume, mL	1627	1628	1631	1834	1674	1620	1602	1661	1825	1655
Cyanide Leach Residue Weight,g	1717	1718	1721	1924	1764	1710	1692	1751	1916	1745
Cyanide Leach Residue Assay, g Au/t	0.06	0.07	0.06	0.05	0.06	0.31	0.31	0.29	0.28	0.24
Cyanide Leach Gold Dissolution, %	91.87	88.51	89.27	89.99	89.47	84.49	85.28	84.39	81.45	87.63
Backcalculated Leach Feed Grade, g Au/t	0.74	0.61	0.56	0.50	0.57	2.00	2.11	1.86	1.51	1.94
(based on leach solution and residue weights and assays)										
Cyanide Consumption, g NaCN	0.17	0.32	0.09	0.47	0.15	0.03	0.27	0.35	0.46	0.20
- kg NaCN/tonne solids in Leach Feed	0.099	0.186	0.052	0.244	0.085	0.018	0.160	0.490	0.240	0.115
Lime Consumption, g CaO	0.64	0.59	0.57	0.70	0.92	0.55	0.43		0.83	0.80
- kg CaO/tonne solids in Leach Feed	0.37	0.34	0.33	0.36	0.52	0.32	0.25	0.00	0.43	0.46
Backcalculated Composite Grade, g Au/t	1.85	1.28	1.86	1.67	1.93	6.09	8.19	7.52	5.06	6.95
(based on cleaned gravity concentrate wt and assay, backcalculated leach feed grade plus an allowance for gold in the portion of gravity cleaner tail used for assay)										
Predicted Grade of Composite from Drill Core Assays, g Au/t	1.58	1.58	1.58	1.58	1.58	6.66	6.66	6.66	6.66	6.66
(based on as received 1/4 core weights and drill core data base assays)										
Calculated Overall Gold Recovery, %	96.0	95.1	96.5	96.4	96.9	95.1	96.2	95.6	94.6	96.3

Table 13.12: Zone D Primary Grind Results

Gravity Separation	ZONE D LG COMPOSITE					ZONE D HG COMPOSITE				
Gravity/Leach Test No.	G81/L73	G5/L74	G3/L75	G96/L104	G7/L76	G48/L77	G6/L78	G4/L79	G97/L105	G8/L80
Grind Size, K80	206	170	137	105	80	215	164	136	100	76
Product Weights,g										
Gravity Concentrate	17.4	14.7	18.1	23.1	14.0	22.0	19.2	17.5	19.0	16.8
Gravity Cleaner Tail	44.7	48.0	42.1	29.5	35.4	44.5	47.2	47.9	33.4	45.0
Gravity Rougher Tail	1932.1	1931.3	1937.3	1943.9	1957.0	1933.0	1926.5	1936.2	1945.5	1951.9
Feed	1994.2	1994.0	1997.5	1996.5	2006.4	1999.5	1992.9	2001.6	1997.9	2013.7
Weight %										
Gravity Concentrate	0.87	0.74	0.91	1.16	0.70	1.10	0.96	0.87	0.95	0.83
Gravity Cleaner Tail	2.24	2.41	2.11	1.48	1.76	2.23	2.37	2.39	1.67	2.23
Gravity Rougher Tail	96.89	96.86	96.99	97.37	97.54	96.67	96.67	96.73	97.38	96.93
Assay, g Au/t										
Gravity Concentrate	76.0	107	56.4	136.0	92.9	145	133	119	168	162
Gravity Cleaner Tail	11.5	25.6	22.1	8.2	5.63	33.3	15.8	16.7	21.1	16.5
Gravity Rougher Tail	0.38	0.56	0.35	0.46	0.41	1.03	1.09	0.65	0.79	0.71
Au Distribution, %										
Gravity Concentrate	51.44	40.46	38.85	73.44	56.50	47.99	47.22	50.38	58.74	56.18
Gravity Cleaner Tail	20.00	31.65	35.35	5.65	8.66	22.21	13.84	19.27	12.97	15.26
Gravity Rougher Tail	28.56	27.90	25.80	20.90	34.85	29.80	38.94	30.35	28.29	28.55
Feed	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00
Backcalculated Composite Assay using Gravity Results										
Gold Grade, g Au/t	1.29	1.94	1.32	2.14	1.15	3.33	2.71	2.07	2.72	2.41
Cyanide Leaching of Gravity Tailing										
Calculated Cyanide Leach Feed										
Weight Gravity Rougher Tail, g	1686.1	1782.5	1680.7	1906.3	1816.3	1668.7	1782.8	1754.4	1910.6	1811.5
Assay of Gravity Rougher Tail	0.38	0.56	0.35	0.46	0.41	1.03	1.09	0.65	0.79	0.71
Weight Gravity Cleaner Tail, g	18.69	26.66	30.45	8.60	22.15	33.53	35.88	36.78	12.10	32.37
Assay of Gravity Cleaner Tail	11.50	25.56	22.07	8.20	5.63	33.26	15.81	16.68	21.10	16.46
Weight Cyanide Leach Feed, g	1704.8	1809.1	1711.2	1914.9	1838.5	1702.2	1818.6	1791.2	1922.7	1843.8
Calculated Grade of Leach Feed	0.50	0.93	0.74	0.49	0.47	1.66	1.38	0.98	0.92	0.99
(based on gravity tail weights and assays)										
Leach Feed Pulp Density, %solids by wt	50	50	50	50	50	50	50	50	50	50
Leach Feed Cyanide Strength, mg NaCN/L	2000	2000	2000	2000	2000	2000	2000	2000	2000	2000
Leach Feed pH	11.0	11.0	11.0	11.0	11.0	11.0	11.0	11.0	11.0	11.0
Start Leach Feed Solution Volume, mL	1704.8	1809.1	1711.2	1914.9	1838.5	1702.2	1818.6	1791.2	1922.7	1843.8
Cyanide Solution Sample Assay, g Au/t										
8h 30mL sample removed	0.50	0.99	0.58	0.51	0.40	1.19	0.10	1.09	0.74	0.83
24h 30mL sample removed	0.52	1.04	0.66	0.53	0.40	1.36	1.06	1.15	0.77	0.85
32h 30mL sample removed	0.52	1.04	0.67	0.54	0.40	1.37	1.07	1.17	0.77	0.85
48h	0.52	1.04	0.67	0.53	0.40	1.39	1.07	1.17	0.76	0.84
End of Leach Solution Volume, mL	1615	1719	1621	1825	1748	1612	1729	1701	1833	1754
Cyanide Leach Residue Weight,g	1705	1809	1711	1915	1838	1702	1819	1791	1923	1844
Cyanide Leach Residue Assay, g Au/t	0.12	0.09	0.11	0.09	0.08	0.21	0.21	0.19	0.23	0.27
Cyanide Leach Gold Dissolution, %	81.24	92.03	85.87	85.48	83.33	86.84	83.38	86.01	76.77	75.68
Backcalculated Leach Feed Grade, g Au/t	0.64	1.13	0.78	0.62	0.48	1.60	1.26	1.36	0.99	1.11
(based on leach solution and residue weights and assays)										
Cyanide Consumption, g NaCN	0.17	0.45	0.00	0.60	0.37	0.09	0.11	0.10	0.51	0.49
- kg NaCN/tonne solids in Leach Feed	0.100	0.249	0.000	0.313	0.201	0.053	0.060	0.056	0.265	0.266
Lime Consumption, g CaO	0.80	0.87	0.86	1.02	1.17	0.56	0.55	0.71	0.79	1.00
- kg CaO/tonne solids in Leach Feed	0.47	0.48	0.50	0.53	0.64	0.33	0.30	0.40	0.41	0.54
Backcalculated Composite Grade, g Au/t	1.42	2.13	1.35	2.26	1.15	3.25	2.57	2.43	2.79	2.52
(based on cleaned gravity concentrate wt and assay, backcalculated leach feed grade plus an allowance for gold in the portion of gravity cleaner tail used for assay)										
Predicted Grade of Composite from Drill Core Assays, g Au/t	1.51	1.51	1.51	1.51	1.51	5.34	5.34	5.34	5.34	5.34
(based on as received 1/4 core weights and drill core data base assays)										
Calculated Overall Gold Recovery, %	90.9	95.3	91.4	96.1	92.7	93.2	91.2	93.1	90.4	89.3

13.3.4 Grade Composite Testwork

13.3.4.1 Head Grade – Gold Recovery Algorithms

A total of 47 grade composites from Zones A through D were tested to delineate the relationship between gold recovery and mineralisation gold head grade. A 2 kg charge of each composite was ground to a nominal P 80 of 100 µm and then subjected to a gravity concentration step, followed by separate cyanide leaches of the gravity concentrate and the gravity tailing. The gravity concentrate was leached with a cyanide concentration of 2000 mg of NaCN per litre, and the gravity tailing was leached with a cyanide concentration of 500 mg of NaCN per litre. The test results are detailed in Tables 13.13 to 13.16 (overleaf) and summarised in the graphs that follow.

The results show that with increasing gold feed grade, the amount of gold recovered into the gravity concentrate increased from 70 to 80%. There was very little difference in the gravity concentration results between Zones A through D, as seen in Figure 13-11.

Figure 13-11: Grade Composites from Zones A-D

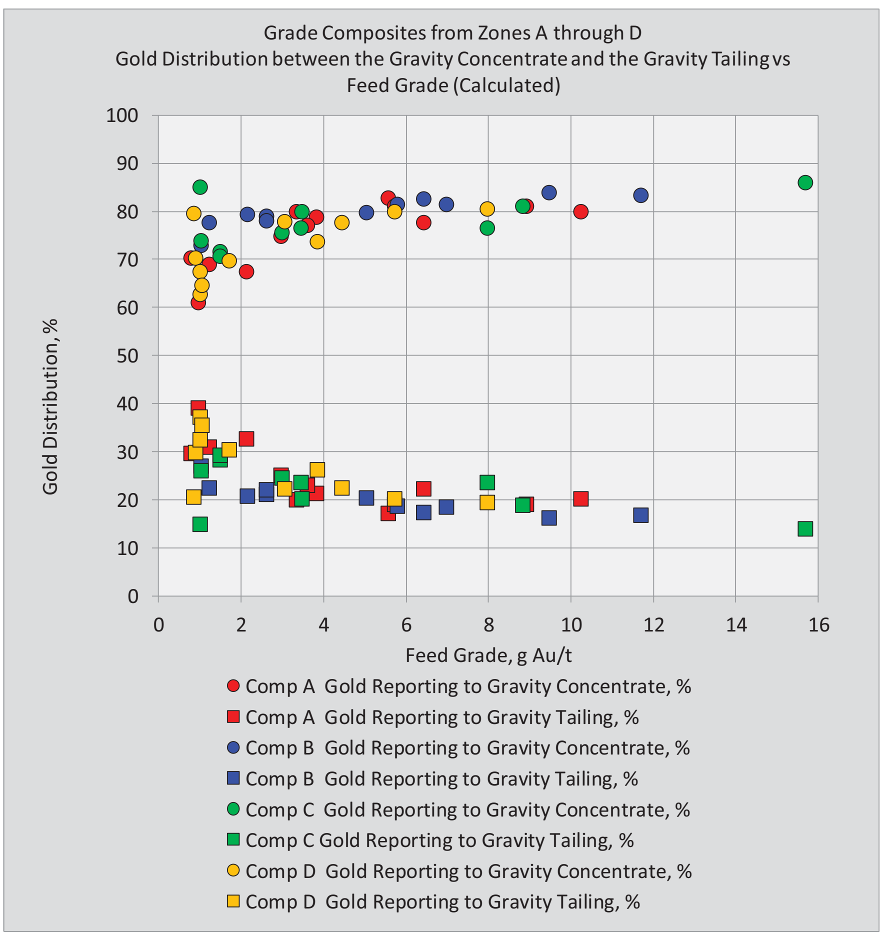


Table 13.13: Zone A Grade Composites

A ZONE GRADE COMPOSITES	**A1**	**A2**	**A3**	**A4**	**A5**	**A6**	**A7**	**A8**	**A9**	**A10**	**A11**	**A12**	**A13**
Gravity Separation													
Gravity Test No.	**122**	**123**	**124**	**125**	**126**	**127**	**128**	**129**	**130**	**131**	**132**	**133**	**134**
Product Weights,g													
Gravity Concentrate	55.2	63.00	62.9	55.0	57.8	68.00	65.10	73.4	66.0	66.00	63.0	72.00	70.00
Gravity Tail	1947.5	1940.8	1941.5	1948.2	1948.0	1936.9	1934.6	1931.9	1938.1	1941.3	1942.9	1925.6	1931.8
Feed	2002.7	2003.8	2004.4	2003.2	2005.8	2004.9	1999.7	2005.3	2004.1	2007.3	2005.9	1997.6	2001.8
Weight %													
Gravity Concentrate	2.76	3.14	3.14	2.75	2.88	3.39	3.26	3.66	3.29	3.29	3.14	3.60	3.50
Gravity Tail	97.24	96.86	96.86	97.25	97.12	96.61	96.74	96.34	96.71	96.71	96.86	96.40	96.50
Assays (backcalculated from leach tests), g Au/t													
Gravity Concentrate	21.42	17.47	71.05	31.04	49.56	78.93	92.64	75.94	140.23	151.92	147.42	200.32	234.25
Gravity Tail	0.39	0.24	0.77	0.39	0.71	0.69	0.84	0.86	0.99	1.48	1.12	1.76	2.13
Assay of Actual Gravity Tail Sample Split	0.17	0.20	0.69	0.45	0.66	0.63	0.88	0.86	1.12	1.71	1.22	1.60	2.48
Au Distribution, %													
Gravity Concentrate	61.02	70.31	74.86	69.00	67.34	79.99	78.80	77.07	82.80	77.68	81.00	80.98	79.94
Gravity Tail	38.98	29.69	25.14	31.00	32.66	20.01	21.20	22.93	17.20	22.32	19.00	19.02	20.06
Backcalculated Ore Feed Grade, g Au/t	**0.97**	**0.78**	**2.98**	**1.24**	**2.12**	**3.35**	**3.83**	**3.61**	**5.58**	**6.43**	**5.72**	**8.92**	**10.25**
(calculated using backcalculated head grades of gravity concentrate and tail leaches)													
Grade of Composite Preparation Head Sample, g Au/t	**0.17**	**0.45**	**6.59**	**0.63**	**1.27**	**1.73**	**1.54**	**2.80**	**3.70**	**4.07**	**9.29**	**8.70**	**15.44**
Head Grade Predicted from Drill Core Assays, g Au/t	**0.28**	**0.65**	**1.00**	**1.39**	**1.78**	**2.20**	**2.71**	**3.42**	**5.04**	**6.98**	**9.33**	**17.71**	**43.63**
Cyanide Leaching of Gravity Concentrate													
Leach Test No.	**171**	**172**	**173**	**174**	**175**	**176**	**177**	**178**	**179**	**180**	**181**	**182**	**183**
Leach Feed Pulp Density, %solids by wt	10.9	12.3	12.3	10.9	11.4	13.1	12.6	14.0	12.8	12.8	12.3	13.8	13.5
Leach Feed Cyanide Strength, mg NaCN/L	2000	2000	2000	2000	2000	2000	2000	2000	2000	2000	2000	2000	2000
Leach Feed pH	11	11	11	11	11	11	11	11	11	11	11	11	11
Start Leach Feed Solution Volume, mL	450	450	450	450	450	450	450	450	450	450	450	450	450
Cyanide Solution Sample Assay, g Au/t													
8h 24mL sample removed	1.69	2.15	7.08	3.02	4.54	7.91	8.97	10.33	15.00	16.90	14.80	27.10	28.20
24h 24mL sample removed	2.41	2.27	9.49	3.57	6.15	11.36	12.63	11.18	19.50	21.60	19.30	31.00	32.70
32h 24mL sample removed	2.38	2.20	9.33	3.47	3.49	11.06	12.20	10.95	19.00	20.50	19.30	29.50	32.30
48h	2.38	2.19	9.06	3.38	5.80	10.86	12.00	10.90	18.40	19.80	18.40	28.40	31.60
End of Leach Solution Volume, mL	420	420	420	420	420	420	420	420	420	420	420	420	420
Cyanide Leach Residue Weight,g	55.2	63.0	62.9	55.0	57.8	68.0	65.1	73.4	66.0	66.0	63.0	72.0	70.0
Cyanide Leach Residue Assay, g Au/t	0.49	0.35	0.67	0.84	1.53	1.15	2.76	2.96	3.68	4.47	4.41	5.45	11.10
Cyanide Leach Gold Dissolution, %	97.7	98.0	99.1	97.3	96.9	98.5	97.0	96.1	97.4	97.1	97.0	97.3	95.2
Backcalculated Gravity Concentrate Grade, g Au/t	21.42	17.47	71.05	31.04	49.56	78.93	92.64	75.94	140.23	151.92	147.42	200.32	232.65
(based on leach solution and residue weights and assays)													
Cyanide Consumption, g NaCN	0.20	0.14	0.1	0.2	0.2	0.16	0.12	0.2	0.2	0.13	0.2	0.17	0.14
- kg NaCN/tonne solids in Leach Feed	3.62	2.22	2.23	2.91	2.94	2.35	1.84	2.18	2.88	1.97	2.54	2.36	2.00
Lime Consumption, g CaO	0.17	0.19	0.1	0.1	0.1	0.12	0.13	0.2	0.1	0.13	0.1	0.20	0.16
- kg CaO/tonne solids in Leach Feed	3.08	3.02	1.91	2.55	1.73	1.76	2.00	2.18	1.52	1.97	1.90	2.78	2.29
Cyanide Leaching of Gravity Tailing													
Leach Test No.	**218**	**219**	**220**	**221**	**222**	**223**	**224**	**225**	**226**	**227**	**228**	**229**	**230**
Leach Feed Pulp Density, %solids by wt	50.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0
Leach Feed Cyanide Strength, mg NaCN/L	500	500	500	500	500	500	500	500	500	500	500	500	500
Leach Feed pH	11	11	11	11	11	11	11	11	11	11	11	11	11
Start Leach Feed Solution Volume, mL	1804.0	1805.0	1805.0	1815.0	1812.0	1801.0	1796.0	1796.0	1801.0	1796.0	1903.0	1879.0	1795.0
Cyanide Solution Sample Assay, g Au/t													
8h 30mL sample removed	0.28	0.21	0.63	0.31	0.55	0.58	0.67	0.67	0.75	0.97	0.75	0.95	1.39
24h 30mL sample removed	0.35	0.22	0.74	0.34	0.65	0.66	0.76	0.76	0.90	1.21	0.90	1.25	1.65
32h 30mL sample removed	0.38	0.23	0.75	0.35	0.64	0.64	0.76	0.76	0.89	1.21	0.89	1.28	1.65
48h	0.38	0.23	0.75	0.36	0.65	0.66	0.76	0.76	0.91	1.25	0.92	1.28	1.66
End of Leach Solution Volume, mL	1714	1715	1715	1725	1722	1711	1706	1706	1711	1706	1813	1789	1705
Cyanide Leach Residue Weight,g	1804.0	1805.0	1805.0	1815.0	1812.0	1801.0	1796.0	1796.0	1801.0	1796.0	1903.0	1879.0	1795.0
Cyanide Leach Residue Assay, g Au/t	0.010	0.010	0.025	0.035	0.065	0.035	0.080	0.100	0.085	0.240	0.205	0.485	0.475
Cyanide Leach Gold Dissolution, %	97.4	95.8	96.8	91.1	90.9	95.0	90.5	88.4	91.4	83.8	81.7	72.4	77.7
Backcalculated Gravity Tailing Grade, g Au/t	0.39	0.24	0.77	0.39	0.71	0.69	0.84	0.86	0.99	1.48	1.12	1.76	2.13
(based on leach solution and residue weights and assays)													
Cyanide Consumption, g NaCN	0.16	0.12	0.19	0.10	0.12	0.16	0.19	0.16	0.16	0.17	0.11	0.29	0.17
- kg NaCN/tonne solids in Leach Feed	0.09	0.07	0.11	0.06	0.07	0.09	0.11	0.09	0.09	0.09	0.06	0.15	0.09
Lime Consumption, g CaO	1.64	1.26	1.42	1.46	1.33	1.39	1.58	1.65	1.46	1.75	1.44	1.60	1.53
- kg CaO/tonne solids in Leach Feed	0.91	0.70	0.79	0.80	0.73	0.77	0.88	0.92	0.81	0.97	0.76	0.85	0.85
Gold Recovered from Gravity Conc Leach	59.62	68.90	74.16	67.13	65.26	78.82	76.46	74.07	80.63	75.40	78.57	78.78	76.13
Gold Recovered from Gravity Tail Leach	37.98	28.45	24.32	28.24	29.68	19.00	19.17	20.26	15.72	18.71	15.53	13.78	15.59
Overall Gold Recovery, %	**97.6**	**97.4**	**98.5**	**95.4**	**94.9**	**97.8**	**95.6**	**94.3**	**96.4**	**94.1**	**94.1**	**92.6**	**91.7**
(based on results of gravity conc and tail leaches)													
Overall Reagant Consumption, kg/t													
NaCN	0.19	0.13	0.17	0.13	0.15	0.17	0.16	0.17	0.18	0.16	0.14	0.23	0.16
CaO	0.97	0.77	0.82	0.85	0.76	0.81	0.92	0.96	0.83	1.01	0.79	0.92	0.90

Table 13.14: Zone B Grade Composites

B ZONE GRADE COMPOSITES	B21	B22	B23	B24	B25	B26	B27	B28	B29	B30	B31	B32
Gravity Separation												
Gravity Test No.	**135**	**136**	**137**	**138**	**139**	**140**	**141**	**142**	**143**	**144**	**145**	**146**
Product Weights,g												
Gravity Concentrate	56.0	54.40	57.0	60.2	63.5	63.00	66.40	71.6	63.3	94.90	68.6	70.80
Gravity Tail	1951.8	1947.5	1949.2	1942.2	1942.5	1942.8	1942.8	1937.1	1934.3	1912.3	1941.2	1935.1
Feed	2007.8	2001.9	2006.2	2002.4	2006.0	2005.8	2009.2	2008.7	1997.6	2007.2	2009.8	2005.9
Weight %												
Gravity Concentrate	2.79	2.72	2.84	3.01	3.17	3.14	3.30	3.56	3.17	4.73	3.41	3.53
Gravity Tail	97.21	97.28	97.16	96.99	96.83	96.86	96.70	96.44	96.83	95.27	96.59	96.47
Assays (backcalculated from leach tests), g Au/t												
Gravity Concentrate	33.86	27.53	60.10	68.60	64.66	150.21	172.32	149.31	126.83	167.94	285.20	806.87
Gravity Tail	0.28	0.28	0.46	0.57	0.60	1.12	1.34	1.16	1.06	1.61	2.02	5.27
Assay of Actual Gravity Tail Sample Split	0.42	0.31	0.51	0.51	1.15	0.53	1.50	1.20	1.04	1.59	2.17	4.84
Au Distribution, %												
Gravity Concentrate	77.67	72.99	79.31	78.92	77.96	81.36	81.49	82.65	79.71	83.80	83.27	84.86
Gravity Tail	22.33	27.01	20.69	21.08	22.04	18.64	18.51	17.35	20.29	16.20	16.73	15.14
Backcalculated Ore Feed Grade, g Au/t	**1.22**	**1.03**	**2.15**	**2.61**	**2.63**	**5.80**	**6.99**	**6.44**	**5.04**	**9.47**	**11.69**	**33.56**
(calculated using backcalculated head grades of gravity concentrate and tail leaches)												
Grade of Composite Preparation Head Sample, g Au/t	**0.45**	**1.14**	**1.15**	**1.74**	**2.73**	**2.48**	**10.54**	**3.75**	**3.24**	**5.18**	**10.01**	**17.06**
Head Grade Predicted from Drill Core Assays, g Au/t	**0.21**	**0.66**	**1.48**	**2.23**	**2.77**	**3.43**	**4.45**	**5.84**	**8.22**	**12.40**	**20.72**	**58.23**
Cyanide Leaching of Gravity Concentrate												
Leach Test No.	**184**	**185**	**186**	**187**	**188**	**189**	**190**	**191**	**192**	**193**	**194**	**195**
Leach Feed Pulp Density, %solids by wt	11.1	10.8	11.2	11.8	12.4	12.3	12.9	13.7	12.3	17.4	13.2	13.6
Leach Feed Cyanide Strength, mg NaCN/L	2000	2000	2000	2000	2000	2000	2000	2000	2000	2000	2000	2000
Leach Feed pH	11	11	11	11	11	11	11	11	11	11	11	11
Start Leach Feed Solution Volume, mL	450	450	450	450	450	450	450	450	450	450	450	450
Cyanide Solution Sample Assay, g Au/t												
8h 24mL sample removed	2.98	2.69	5.94	6.02	6.71	16.20	19.10	16.90	12.30	24.40	32.00	86.00
24h 24mL sample removed	2.79	3.12	6.24	8.29	8.52	20.20	24.50	22.30	16.00	31.90	39.30	121.00
32h 24mL sample removed	3.78	3.06	5.73	8.18	8.10	19.30	23.70	21.30	15.30	31.20	37.60	117.90
48h	3.67	2.84	5.41	8.00	7.99	18.60	22.50	20.30	15.50	31.20	37.60	114.60
End of Leach Solution Volume, mL	420	420	420	420	420	420	420	420	420	420	420	420
Cyanide Leach Residue Weight,g	56.0	54.4	57.0	60.2	63.5	63.0	66.4	71.6	63.3	94.9	68.6	70.8
Cyanide Leach Residue Assay, g Au/t	2.24	1.69	12.70	3.82	3.00	4.99	5.68	9.95	7.46	7.73	16.90	16.90
Cyanide Leach Gold Dissolution, %	93.38	93.86	78.87	94.43	95.36	96.68	96.70	93.34	94.12	95.40	94.07	97.91
Backcalculated Leach Feed Grade, g Au/t	33.86	27.53	60.10	68.60	64.66	150.21	172.32	149.31	126.83	167.94	285.20	806.87
(based on leach solution and residue weights and assays)												
Cyanide Consumption, g NaCN	0.11	0.15	0.14	0.17	0.15	0.15	0.21	0.17	0.23	0.13	0.15	0.23
- kg NaCN/tonne solids in Leach Feed	1.96	2.76	2.46	2.82	2.36	2.38	3.16	2.37	3.63	1.37	2.19	3.25
Lime Consumption, g CaO	0.15	0.14	0.11	0.09	0.09	0.11	0.13	0.16	0.09	0.14	0.11	0.14
- kg CaO/tonne solids in Leach Feed	2.68	2.57	1.93	1.50	1.42	1.75	1.96	2.23	1.42	1.48	1.60	1.98
Cyanide Leaching of Gravity Tailing												
Leach Test No.	**231**	**232**	**233**	**234**	**235**	**236**	**237**	**238**	**239**	**240**	**241**	**242**
Leach Feed Pulp Density, %solids by wt	50.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0
Leach Feed Cyanide Strength, mg NaCN/L	500	500	500	500	500	500	500	500	500	500	500	500
Leach Feed pH	11	11	11	11	11	11	11	11	11	11	11	11
Start Leach Feed Solution Volume, mL	1816.0	1798.0	1813.0	1912.0	1912.0	1912.0	1964.0	1850.0	1850.0	1873.0	1895.0	1898.0
Cyanide Solution Sample Assay, g Au/t												
8h 30mL sample removed	0.18	0.22	0.33	0.36	0.38	0.81	1.00	0.83	0.76	1.26	1.29	4.04
24h 30mL sample removed	0.23	0.26	0.43	0.48	0.50	0.97	1.16	0.95	0.88	1.34	1.61	4.66
32h 30mL sample removed	0.23	0.24	0.41	0.48	0.52	0.95	1.15	0.94	0.87	1.31	1.60	4.62
48h	0.23	0.25	0.42	0.48	0.54	0.99	1.16	0.94	0.89	1.30	1.62	4.68
End of Leach Solution Volume, mL	1726	1708	1723	1822	1822	1822	1874	1760	1760	1783	1805	1808
Cyanide Leach Residue Weight,g	1815.0	1797.0	1813.0	1912.0	1908.0	1912.0	1963.0	1849.0	1894.0	1872.0	1895.0	1898.0
Cyanide Leach Residue Assay, g Au/t	0.050	0.035	0.040	0.090	0.060	0.130	0.180	0.220	0.190	0.310	0.410	0.600
Cyanide Leach Gold Dissolution, %	82.1	87.7	91.3	84.2	90.0	88.4	86.5	81.0	82.0	80.8	79.7	88.6
Backcalculated Gravity Tailing Grade, g Au/t	0.28	0.28	0.46	0.57	0.60	1.12	1.34	1.16	1.06	1.61	2.02	5.27
(based on leach solution and residue weights and assays)												
Cyanide Consumption, g NaCN	0.16	0.12	0.19	0.10	0.12	0.16	0.19	0.16	0.16	0.17	0.11	0.29
- kg NaCN/tonne solids in Leach Feed	0.09	0.07	0.10	0.05	0.06	0.08	0.10	0.09	0.08	0.09	0.06	0.15
Lime Consumption, g CaO	1.64	1.26	1.42	1.46	1.33	1.39	1.58	1.65	1.46	1.75	1.44	1.60
- kg CaO/tonne solids in Leach Feed	0.90	0.70	0.78	0.76	0.70	0.73	0.80	0.89	0.77	0.93	0.76	0.84
Gold Recovered from Gravity Conc Leach	72.53	68.50	62.55	74.52	74.34	78.65	78.80	77.14	75.02	79.95	78.34	83.08
Gold Recovered from Gravity Tail Leach	18.33	23.69	18.88	17.74	19.83	16.47	16.02	14.06	16.65	13.08	13.34	13.42
Overall Gold Recovery, %	**90.9**	**92.2**	**81.4**	**92.3**	**94.2**	**95.1**	**94.8**	**91.2**	**91.7**	**93.0**	**91.7**	**96.5**
(based on results of gravity conc and tail leaches)												
Overall Reagant Consumption, kg/t												
NaCN	0.14	0.14	0.17	0.14	0.14	0.16	0.20	0.17	0.20	0.15	0.13	0.26
CaO	0.95	0.75	0.82	0.79	0.72	0.76	0.84	0.94	0.79	0.96	0.79	0.88

Table 13.15: Zone C Grade Composites

C Zone Grade Composites	C41	C42	C43	C44	C45	C46	C47	C48	C49	C50	C51
Gravity Separation											
Gravity Test No.	**147**	**148**	**149**	**155**	**151**	**152**	**153**	**154**	**150**	**156**	**157**
Product Weights,g											
Gravity Concentrate	53.2	55.90	54.5	58.1	58.5	64.00	55.70	67.8	71.8	77.80	74.3
Gravity Tail	1951.2	1947.7	1951.0	1948.6	1954.2	1951.2	1949.8	1945.6	1944.7	1929.5	1927.0
Feed	2004.4	2003.6	2005.5	2006.7	2012.7	2015.2	2005.5	2013.4	2016.5	2007.3	2001.3
Weight %											
Gravity Concentrate	2.65	2.79	2.72	2.90	2.91	3.18	2.78	3.37	3.56	3.88	3.71
Gravity Tail	97.35	97.21	97.28	97.10	97.09	96.82	97.22	96.63	96.44	96.12	96.29
Assays (backcalculated from leach tests), g Au/t											
Gravity Concentrate	32.14	27.07	39.18	36.26	95.83	71.03	95.10	212.53	170.98	480.27	363.55
Gravity Tail	0.15	0.27	0.43	0.45	0.72	0.76	0.84	1.73	1.94	4.04	2.28
Assay of Actual Gravity Tail Sample Split	0.15	0.25	0.33	0.39	0.60	0.64	0.68	1.51	1.99	4.06	1.99
Au Distribution, %											
Gravity Concentrate	85.06	73.91	71.66	70.72	79.91	75.52	76.43	81.09	76.46	82.75	86.00
Gravity Tail	14.94	26.09	28.34	29.28	20.09	24.48	23.57	18.91	23.54	17.25	14.00
Backcalculated Ore Feed Grade, g Au/t	**1.00**	**1.02**	**1.49**	**1.48**	**3.49**	**2.99**	**3.46**	**8.83**	**7.96**	**22.49**	**15.69**
(calculated using backcalculated head grades of gravity concentrate and tail leaches)											
Grade of Composite Preparation Head Sample, g Au/t	**0.23**	**0.61**	**0.39**	**1.94**	**1.79**	**2.95**	**1.52**	**7.17**	**7.30**	**25.08**	**13.79**
Head Grade Predicted from Drill Core Assays, g Au/t	**0.13**	**0.33**	**0.58**	**1.04**	**1.82**	**3.07**	**4.87**	**7.89**	**11.91**	**18.34**	**39.98**
Cyanide Leaching of Gravity Concentrate											
Leach Test No.	**196**	**197**	**198**	**204**	**200**	**201**	**202**	**203**	**199**	**205**	**206**
Leach Feed Pulp Density, %solids by wt	10.6	11.0	10.8	11.4	11.5	12.5	11.0	13.1	13.8	14.7	14.2
Leach Feed Cyanide Strength, mg NaCN/L	2000	2000	2000	2000	2000	2000	2000	2000	2000	2000	2000
Leach Feed pH	11	11	11	11	11	11	11	11	11	11	11
Start Leach Feed Solution Volume, mL	450	450	450	450	450	450	450	450	450	450	450
Cyanide Solution Sample Assay, g Au/t											
8h 24mL sample removed	1.66	2.30	2.92	3.13	8.74	6.54	6.43	17.20	21.30	0.35	40.20
24h 24mL sample removed	2.85	2.79	4.28	4.16	11.50	8.74	9.28	28.50	24.60	78.30	55.60
32h 24mL sample removed	3.09	2.90	4.17	4.20	11.26	8.60	9.01	29.00	23.80	78.20	54.30
48h	3.58	2.99	4.35	4.07	10.90	8.60	10.39	28.20	22.70	75.00	52.50
End of Leach Solution Volume, mL	420	420	420	420	420	420	420	420	420	420	420
Cyanide Leach Residue Weight,g	53.2	55.9	54.5	58.1	58.5	64.0	55.7	67.8	71.8	77.8	74.3
Cyanide Leach Residue Assay, g Au/t	0.45	1.17	0.65	2.09	4.65	5.64	6.10	11.40	14.90	27.00	18.30
Cyanide Leach Gold Dissolution, %	98.6	95.7	98.3	94.2	95.1	92.1	93.6	94.6	91.3	94.4	95.0
Backcalculated Leach Feed Grade, g Au/t	32.14	27.07	39.18	36.26	95.83	71.03	95.10	212.53	170.98	480.27	363.55
(based on leach solution and residue weights and assays)											
Cyanide Consumption, g NaCN	0.16	0.11	0.24	0.13	0.20	0.13	0.20	0.09	0.24	1.07	0.14
- kg NaCN/tonne solids in Leach Feed	3.01	1.97	4.40	2.24	3.42	2.03	3.59	1.33	3.34	13.75	1.88
Lime Consumption, g CaO	0.09	0.11	0.13	0.25	0.11	0.10	0.11	0.24	0.14	0.28	0.21
- kg CaO/tonne solids in Leach Feed	1.69	1.97	2.39	4.30	1.88	1.56	1.97	3.54	1.95	3.60	2.83
Cyanide Leaching of Gravity Tailing											
Leach Test No.	**243**	**244**	**245**	**251**	**247**	**248**	**249**	**250**	**246**	**252**	**253**
Leach Feed Pulp Density, %solids by wt	50.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0
Leach Feed Cyanide Strength, mg NaCN/L	500	500	500	500	500	500	500	500	500	500	500
Leach Feed pH	11	11	11	11	11	11	11	11	11	11	11
Start Leach Feed Solution Volume, mL	1898	1909.00	1909.0	1901.0	1909.0	1909.00	1910.00	1901.0	1909.0	1892.00	1892.00
Cyanide Solution Sample Assay, g Au/t											
8h 30mL sample removed	0.13	0.18	0.30	0.32	0.53	0.39	0.50	1.13	1.21	2.82	1.51
24h 30mL sample removed	0.13	0.21	0.37	0.37	0.59	0.55	0.60	1.32	1.41	3.18	1.85
32h 30mL sample removed	0.13	0.22	0.37	0.37	0.59	0.56	0.60	1.33	1.42	3.11	1.83
48h	0.13	0.22	0.39	0.37	0.59	0.57	0.61	1.33	1.42	3.19	1.84
End of Leach Solution Volume, mL	1808	1819	1819	1811	1819	1819	1820	1811	1819	1802	1802
Cyanide Leach Residue Weight,g	1913.0	1909.0	1910.0	1909.0	1918.0	1914.0	1910.0	1901.0	1900.0	1890.0	1885.0
Cyanide Leach Residue Assay, g Au/t	0.025	0.055	0.045	0.080	0.135	0.190	0.230	0.400	0.520	0.850	0.440
Cyanide Leach Gold Dissolution, %	83.8	79.9	89.6	82.1	81.3	74.8	72.6	76.8	73.2	78.9	80.7
Backcalculated Gravity Tailing Grade, g Au/t	0.15	0.27	0.43	0.45	0.72	0.76	0.84	1.73	1.94	4.04	2.28
(based on leach solution and residue weights and assays)											
Cyanide Consumption, g NaCN	0.02	0.14	0.28	0.14	0.16	0.52	0.10	0.21	0.21	0.08	0.16
- kg NaCN/tonne solids in Leach Feed	0.01	0.07	0.15	0.07	0.08	0.27	0.05	0.11	0.11	0.04	0.08
Lime Consumption, g CaO	1.01	1.07	1.17	1.01	1.48	1.18	1.03	1.47	1.29	1.14	0.82
- kg CaO/tonne solids in Leach Feed	0.53	0.56	0.61	0.53	0.77	0.62	0.54	0.77	0.68	0.60	0.44
Gold Recovered from Gravity Conc Leach	83.86	70.71	70.48	66.64	76.03	69.52	71.52	76.74	69.80	78.10	81.67
Gold Recovered from Gravity Tail Leach	12.52	20.86	25.39	24.05	16.33	18.32	17.10	14.53	17.24	13.62	11.30
Overall Gold Recovery, %	**96.4**	**91.6**	**95.9**	**90.7**	**92.4**	**87.8**	**88.6**	**91.3**	**87.0**	**91.7**	**93.0**
(based on results of gravity conc and tail leaches)											
Overall Reagent Consumption, kg/t											
NaCN	0.09	0.13	0.26	0.14	0.18	0.33	0.15	0.15	0.23	0.57	0.15
CaO	0.56	0.60	0.66	0.64	0.80	0.65	0.58	0.87	0.72	0.72	0.52

Table 13.16: Zone D Grade Composites

D Zone Grade Composites	**D61**	**D62**	**D63**	**D64**	**D65**	**D66**	**D67**	**D68**	**D69**	**D70**	**D71**
Gravity Separation											
Gravity Test No.	**158**	**159**	**160**	**161**	**162**	**163**	**164**	**165**	**166**	**167**	**168**
Product Weights,g											
Gravity Concentrate	61.8	53.40	59.5	53.0	51.7	64.00	56.90	65.1	67.8	60.80	79.3
Gravity Tail	1957.0	1952.8	1951.3	1948.3	1950.5	1951.1	1953.0	1943.0	1935.8	1947.9	1932.2
Feed	2018.8	2006.2	2010.8	2001.3	2002.2	2015.1	2009.9	2008.1	2003.6	2008.7	2011.5
Weight %											
Gravity Concentrate	3.06	2.66	2.96	2.65	2.58	3.18	2.83	3.24	3.38	3.03	3.94
Gravity Tail	96.94	97.34	97.04	97.35	97.42	96.82	97.17	96.76	96.62	96.97	96.06
Assays (backcalculated from leach tests), g Au/t											
Gravity Concentrate	21.89	23.37	22.87	23.84	26.12	37.39	83.84	106.42	84.10	150.70	162.93
Gravity Tail	0.18	0.27	0.34	0.38	0.38	0.53	0.70	1.03	1.05	1.19	1.62
Assay of Actual Gravity Tail Sample Split	0.13	0.17	0.27	0.34	0.54	0.45	0.65	0.83	0.98	1.16	1.45
Au Distribution, %											
Gravity Concentrate	79.53	70.19	67.46	62.79	64.56	69.65	77.75	77.60	73.75	79.84	80.53
Gravity Tail	20.47	29.81	32.54	37.21	35.44	30.35	22.25	22.40	26.25	20.16	19.47
Backcalculated Ore Feed Grade, g Au/t	**0.84**	**0.89**	**1.00**	**1.01**	**1.04**	**1.70**	**3.05**	**4.45**	**3.86**	**5.71**	**7.98**
(calculated using backcalculated head grades of gravity concentrate and tail leaches)											
Grade of Composite Preparation Head Sample, g Au/t	**0.17**	**0.24**	**0.72**	**1.19**	**0.42**	**0.70**	**2.06**	**2.70**	**10.43**	**4.42**	**5.57**
Head Grade Predicted from Drill Core Assays, g Au/t	**0.13**	**0.39**	**0.63**	**0.87**	**1.13**	**1.51**	**2.13**	**2.93**	**4.19**	**6.12**	**14.20**
Cyanide Leaching of Gravity Concentrate											
Leach Test No.	**207**	**208**	**209**	**210**	**211**	**212**	**213**	**214**	**215**	**216**	**217**
Leach Feed Pulp Density, %solids by wt	12.1	10.6	11.7	10.5	10.3	12.5	11.2	12.6	13.1	11.9	15.0
Leach Feed Cyanide Strength, mg NaCN/L	2000	2000	2000	2000	2000	2000	2000	2000	2000	2000	2000
Leach Feed pH	11	11	11	11	11	11	11	11	11	11	11
Start Leach Feed Solution Volume, mL	450	450	450	450	450	450	450	450	450	450	450
Cyanide Solution Sample Assay, g Au/t											
8h 24mL sample removed	1.39	1.56	1.89	1.89	1.80	3.57	5.72	10.83	7.91	11.86	16.80
24h 24mL sample removed	2.68	2.55	2.75	2.56	2.58	4.69	9.60	14.00	10.97	17.80	25.40
32h 24mL sample removed	2.70	2.59	2.75	2.52	2.58	4.69	9.54	13.50	10.70	17.70	25.70
48h	2.75	2.53	2.65	2.41	2.52	4.57	9.26	13.00	10.40	17.30	24.90
End of Leach Solution Volume, mL	420	420	420	420	420	420	420	420	420	420	420
Cyanide Leach Residue Weight,g	61.8	53.4	59.5	53.0	51.7	64.0	56.9	65.1	67.8	60.8	79.3
Cyanide Leach Residue Assay, g Au/t	0.57	0.46	1.18	1.59	2.42	2.54	5.00	8.42	9.20	12.50	10.50
Cyanide Leach Gold Dissolution, %	97.4	98.0	94.8	93.3	90.7	93.2	94.0	92.1	89.1	91.7	93.6
Backcalculated Leach Feed Grade, g Au/t	21.89	23.37	22.87	23.84	26.12	37.39	83.84	106.42	84.10	150.70	162.93
(based on leach solution and residue weights and assays)											
Cyanide Consumption, g NaCN	0.12	0.11	0.12	0.20	0.16	0.16	0.19	0.14	0.15	0.17	0.12
- kg NaCN/tonne solids in Leach Feed	1.94	2.06	2.02	3.77	3.09	2.50	3.34	2.15	2.21	2.80	1.51
Lime Consumption, g CaO	0.23	0.19	0.19	0.25	0.22	0.19	0.24	0.27	0.24	0.19	0.15
- kg CaO/tonne solids in Leach Feed	3.72	3.56	3.19	4.72	4.26	2.97	4.22	4.15	3.54	3.13	1.89
Cyanide Leaching of Gravity Tailing											
Leach Test No.	**254**	**255**	**256**	**257**	**258**	**259**	**260**	**261**	**262**	**263**	**264**
Leach Feed Pulp Density, %solids by wt	50.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0
Leach Feed Cyanide Strength, mg NaCN/L	500	500	500	500	500	500	500	500	500	500	500
Leach Feed pH	11	11	11	11	11	11	11	11	11	11	11
Start Leach Feed Solution Volume, mL	1892	1892.00	1892.0	1911.0	1913.0	1913.00	1914.00	1903.0	1896.0	1909.00	1887.0
Cyanide Solution Sample Assay, g Au/t											
8h 30mL sample removed	0.15	0.24	0.28	0.29	0.30	0.42	0.51	0.69	0.67	0.75	1.03
24h 30mL sample removed	0.15	0.24	0.28	0.32	0.32	0.44	0.58	0.78	0.78	0.92	1.22
32h 30mL sample removed	0.15	0.25	0.28	0.32	0.32	0.43	0.58	0.78	0.78	0.93	1.23
48h	0.15	0.25	0.29	0.33	0.32	0.44	0.58	0.77	0.78	0.91	1.24
End of Leach Solution Volume, mL	1802	1802	1802	1821	1823	1823	1824	1813	1806	1819	1797
Cyanide Leach Residue Weight,g	1919.0	1917.0	1913.0	1909.0	1911.0	1914.0	1914.0	1903.0	1896.0	1909.0	1887.0
Cyanide Leach Residue Assay, g Au/t	0.030	0.025	0.050	0.055	0.060	0.095	0.120	0.260	0.270	0.280	0.380
Cyanide Leach Gold Dissolution, %	83.1	90.8	85.1	85.7	84.2	82.2	82.8	74.7	74.2	76.4	76.5
Backcalculated Gravity Tailing Grade, g Au/t	0.18	0.27	0.34	0.38	0.38	0.53	0.70	1.03	1.05	1.19	1.62
(based on leach solution and residue weights and assays)											
Cyanide Consumption, g NaCN	0.14	0.14	0.16	0.16	0.16	0.12	0.33	0.19	0.29	0.18	0.39
- kg NaCN/tonne solids in Leach Feed	0.07	0.07	0.08	0.08	0.08	0.06	0.17	0.10	0.15	0.09	0.21
Lime Consumption, g CaO	1.34	1.25	1.35	1.52	1.47	1.90	1.20	1.43	1.94	1.21	1.40
- kg CaO/tonne solids in Leach Feed	0.70	0.65	0.71	0.80	0.77	0.99	0.63	0.75	1.02	0.63	0.74
Gold Recovered from Gravity Conc Leach	77.46	68.81	63.98	58.60	58.58	64.92	73.12	71.46	65.68	73.22	75.34
Gold Recovered from Gravity Tail Leach	17.02	27.07	27.70	31.89	29.84	24.95	18.43	16.74	19.49	15.41	14.89
Overall Gold Recovery, %	**94.5**	**95.9**	**91.7**	**90.5**	**88.4**	**89.9**	**91.5**	**88.2**	**85.2**	**88.6**	**90.2**
(based on results of gravity conc and tail leaches)											
Overall Reagant Consumption, kg/t											
NaCN	0.13	0.13	0.14	0.18	0.16	0.14	0.26	0.17	0.22	0.18	0.26
CaO	0.79	0.73	0.78	0.90	0.86	1.06	0.73	0.86	1.11	0.71	0.79

The results of cyanide leaching of the gravity concentrate, shown graphically in Figure 13-12, indicate that:

- cyanide leaching of the gravity concentrate dissolved between 89 and 99% of the contained gold.
- there was a noticeable decrease in gold leach recovery proceeding from the south of the deposit (Zone A) to the north of the deposit (Zone D).
- for Zones A, C and D, the gold leach recovery was marginally reduced when leaching gravity concentrate originating from high-grade samples. This is an unusual phenomenon and likely related to a change in gold mineralogy with increasing gold head grade. The gold leach recovery for leaching gravity tailing from Zone B appears independent of the feed grade.

The results of cyanide leaching of the gravity tailing, shown graphically below in Figure 13-13, indicate that:

- cyanide leaching of the gravity tailing dissolved between 72 and 98 % of the contained gold.
- there was a noticeable decrease in gold leach recovery proceeding from the south of the deposit (Zone A) to the north of the deposit (Zone D).
- for zones A through D, the gold leach recovery was reduced when leaching gravity tailing originating from high-grade samples. The drop-off in leach gold recovery with increasing feed grade was greater when leaching gravity tailing compared to leaching gravity concentrate.

The overall gold recovery has two components, namely the gold recovered from leaching the gravity concentrate and the gold recovered from leaching the gravity tailing. The gold recovered from leaching the gravity concentrate is simply the gold distribution reporting to the gravity concentrate multiplied by the gravity concentrate leach recovery, and similarly the gold recovered from leaching the gravity tailing is simply the gold distribution reporting to the gravity tailing multiplied by the gravity leach recovery. The two recovery components, and the overall gold recovery, are shown in Figure 13-14.

The overall gold recovery is shown in Figure 13-15 with an expanded x-axis. Although there is a fair scatter in the results, recovery algorithms can be drawn through the points available for each of the zones as shown in Figure 13-16 through 13-20. Except for Zone B, the overall gold recovery reduces as the feed grade increases. This is driven primarily by the reduction in recovery when leaching the gravity tailing from higher feed grade material.

Figure 13-12: Gravity Concentrate Leach Recovery vs. Gravity Concentrate Grade

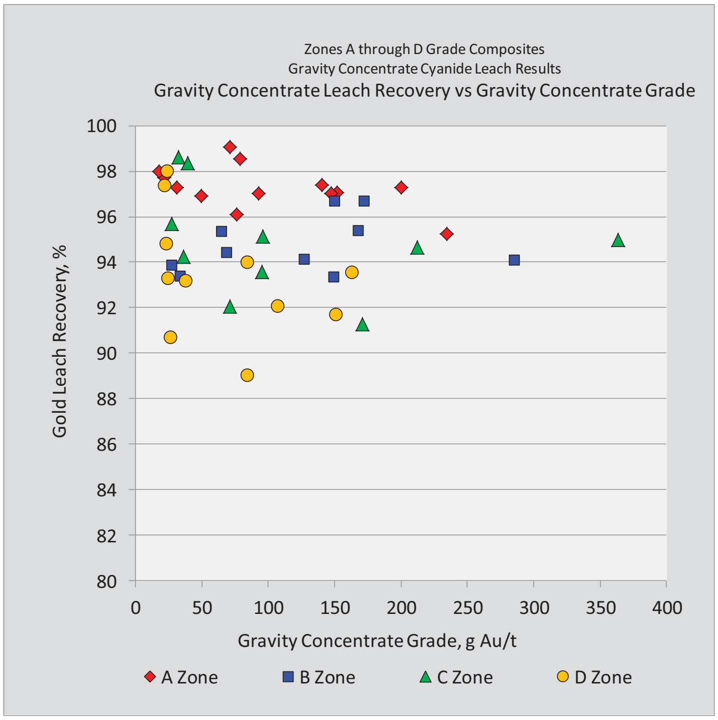


Figure 13-13: Gravity Tail Leach Recovery vs. Gravity Tail Grade

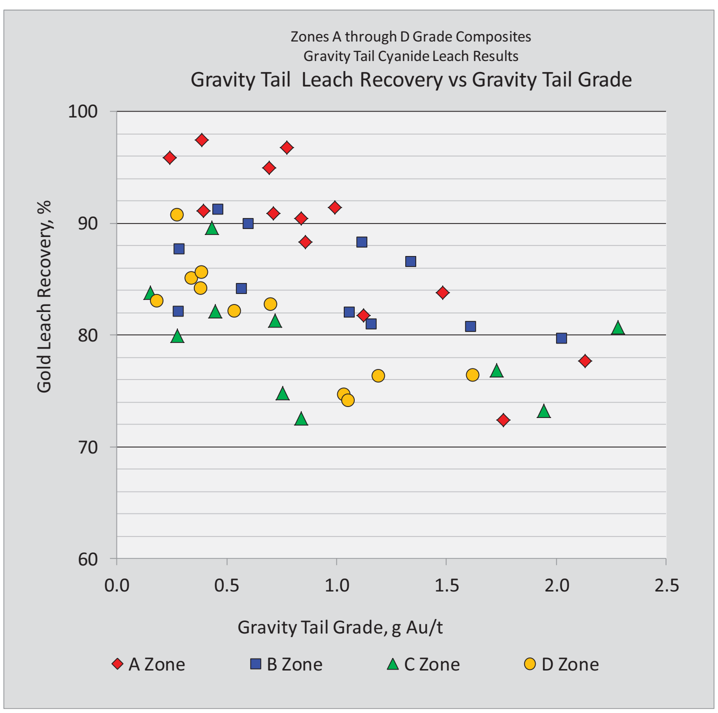


Figure 13-14: Gravity Tailing vs. Gold Feed Grade

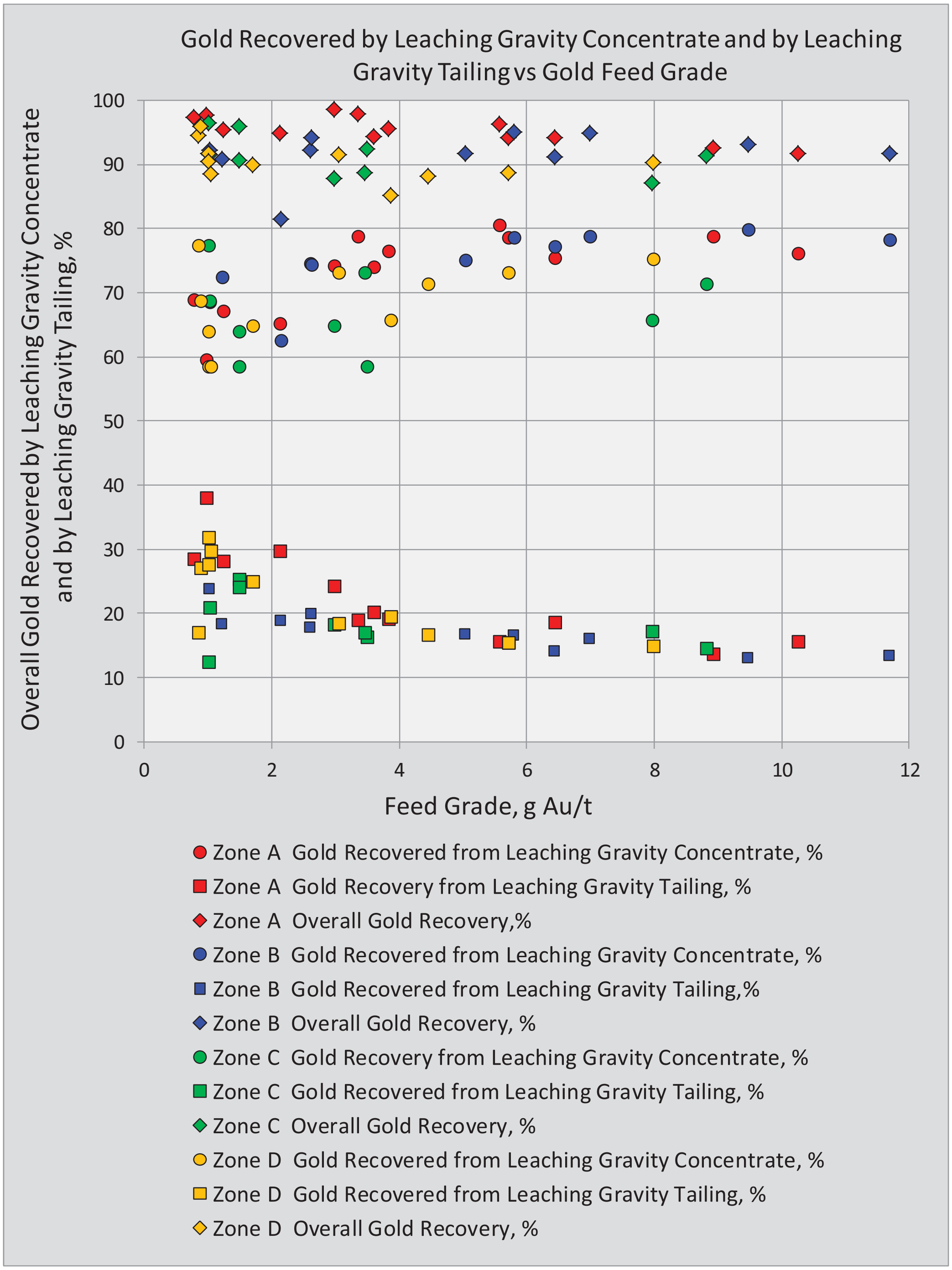


Figure 13-15: Tailing vs. Gold Feed Grade

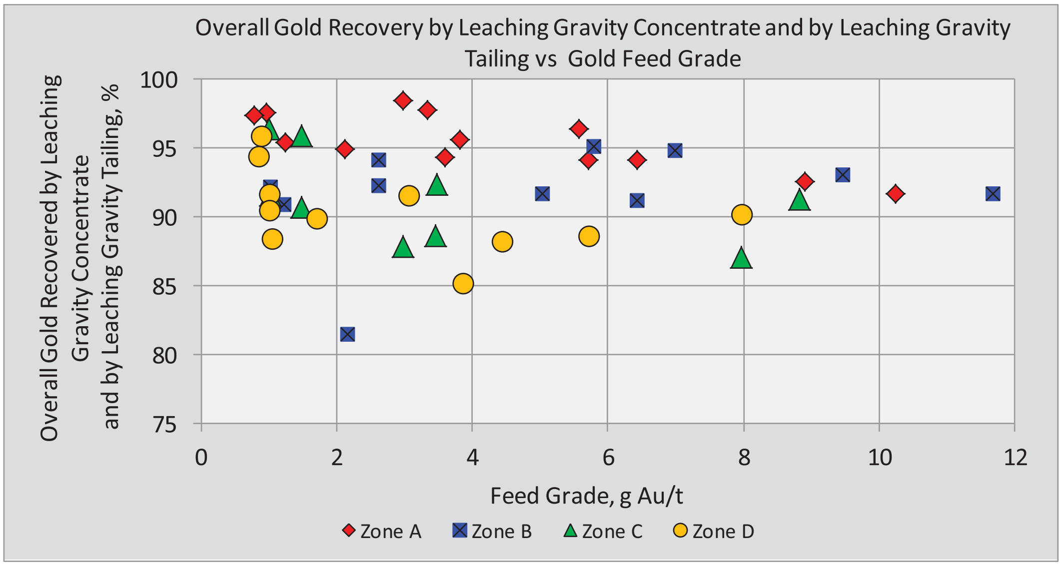


Figure 13-16: Zone A Overall Gold Recovery

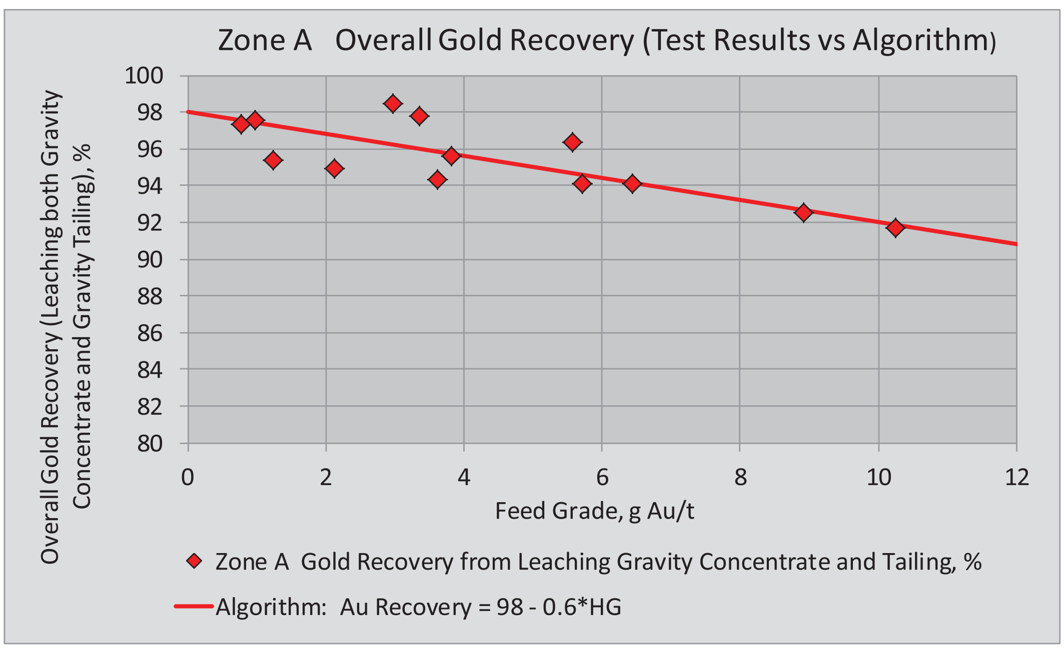


Figure 13-17: Zone B Overall Gold Recovery

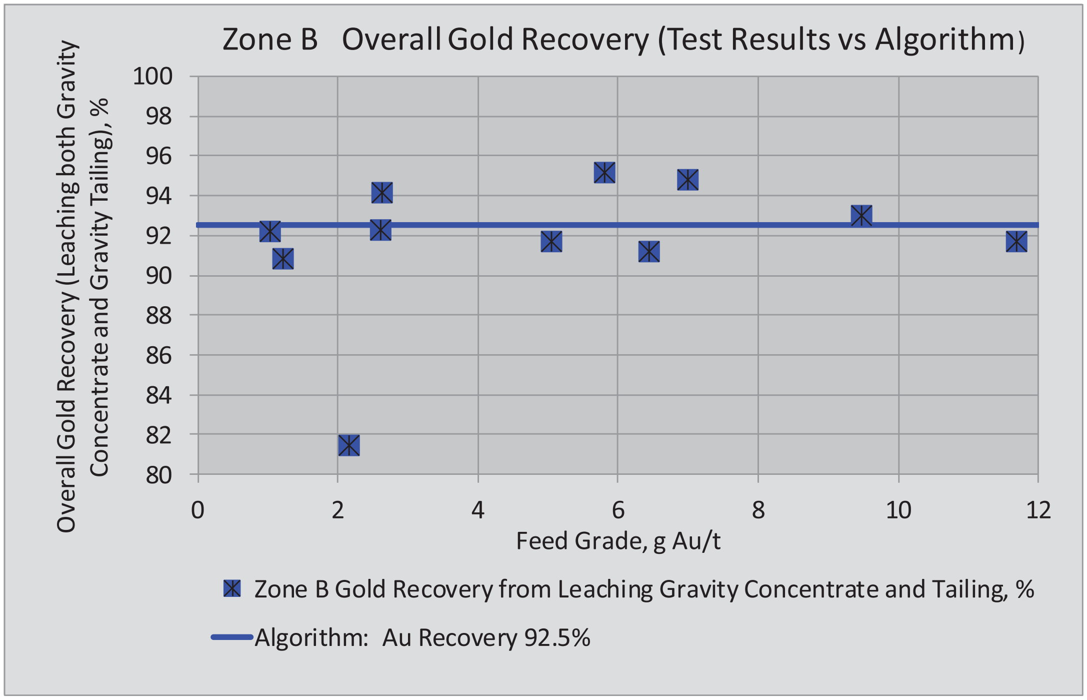


Figure 13-18: Zone C Overall Gold Recovery

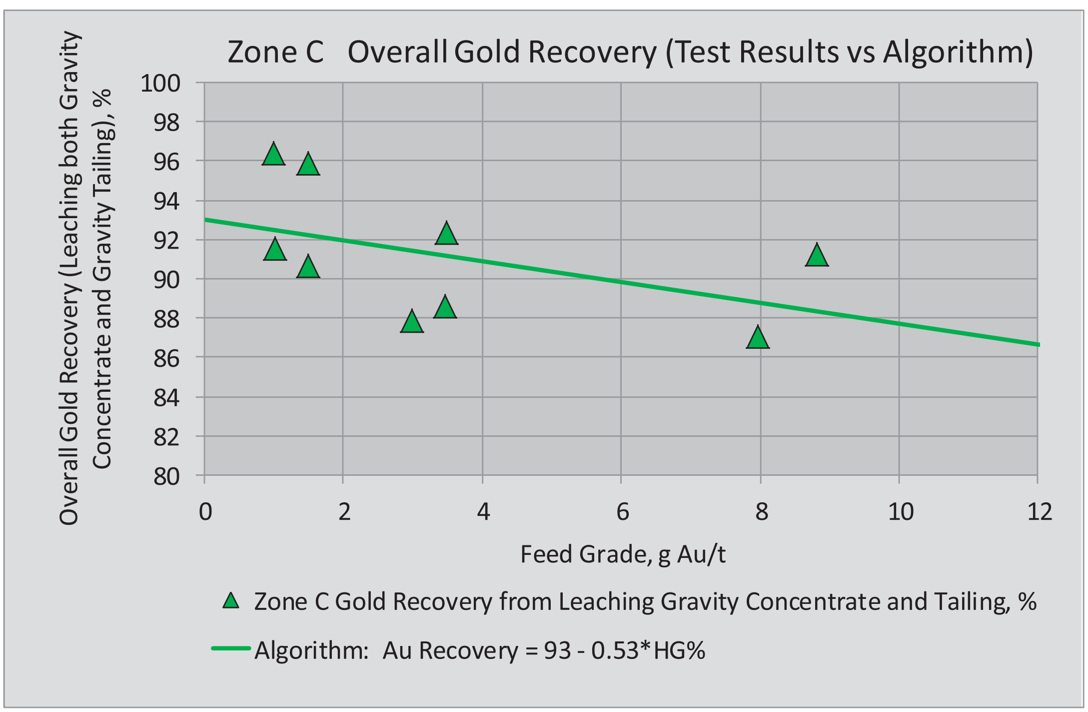


Figure 13-19: Zone D Overall Gold Recovery

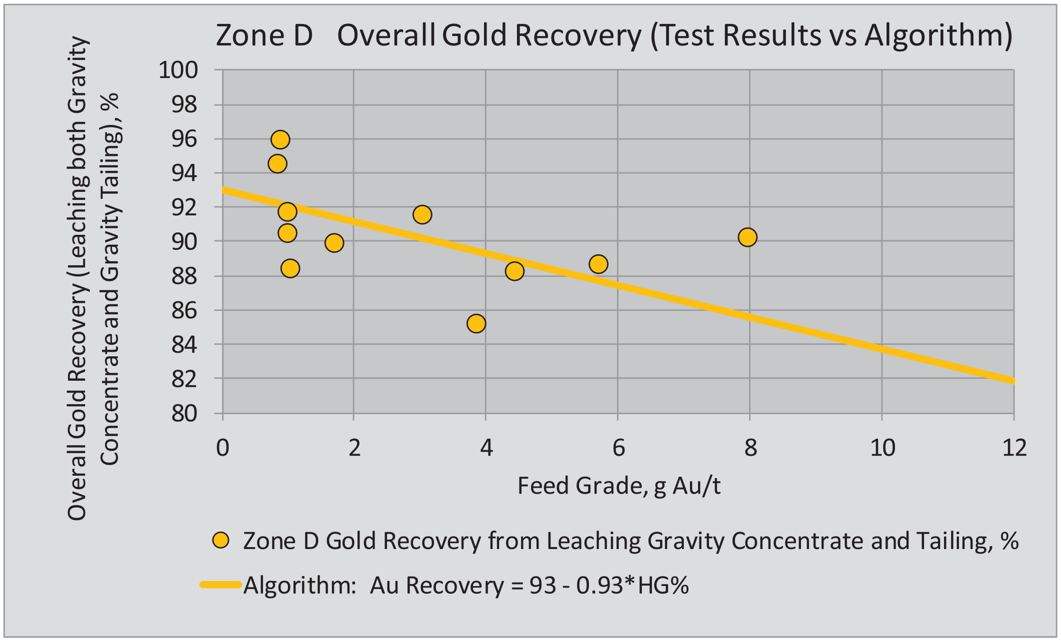
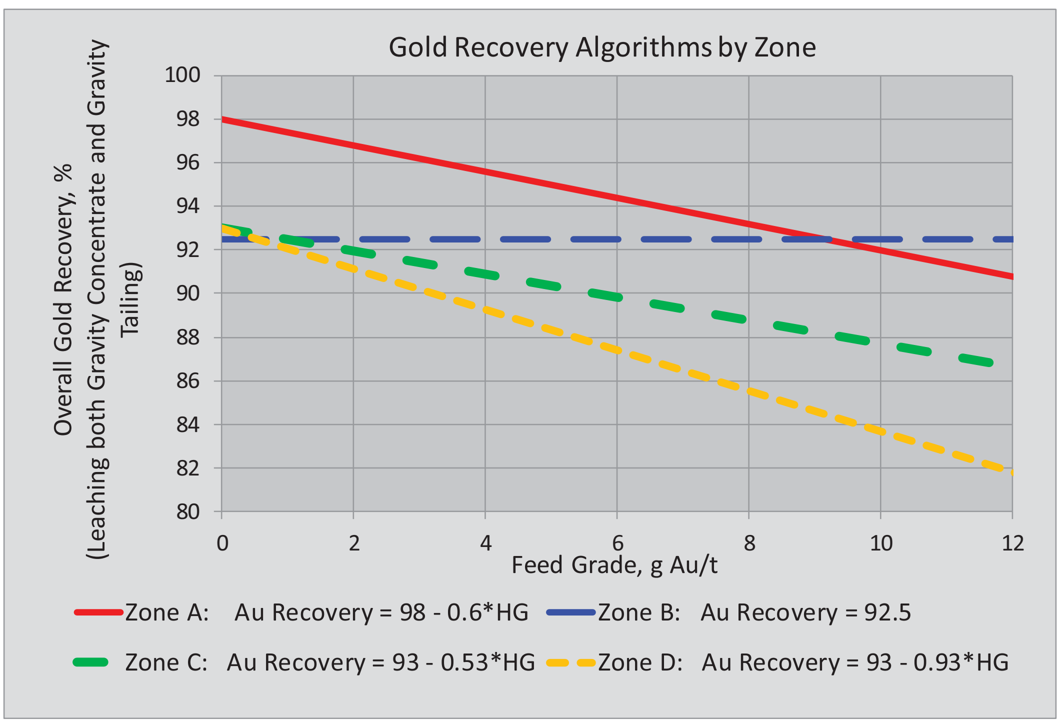


Figure 13-20: Gold Recovery Algorithms by Zone



13.3.4.2 Reagent Consumption

Cyanide consumption, shown in Figures 13-21 and 13-22, averaged 2.5 kg NaCN per tonne of gravity concentrate, and 0.10 kg NaCN per tonne of gravity tailing.

Figure 13-21: Cyanide Consumption for Leaching Gravity Concentrate

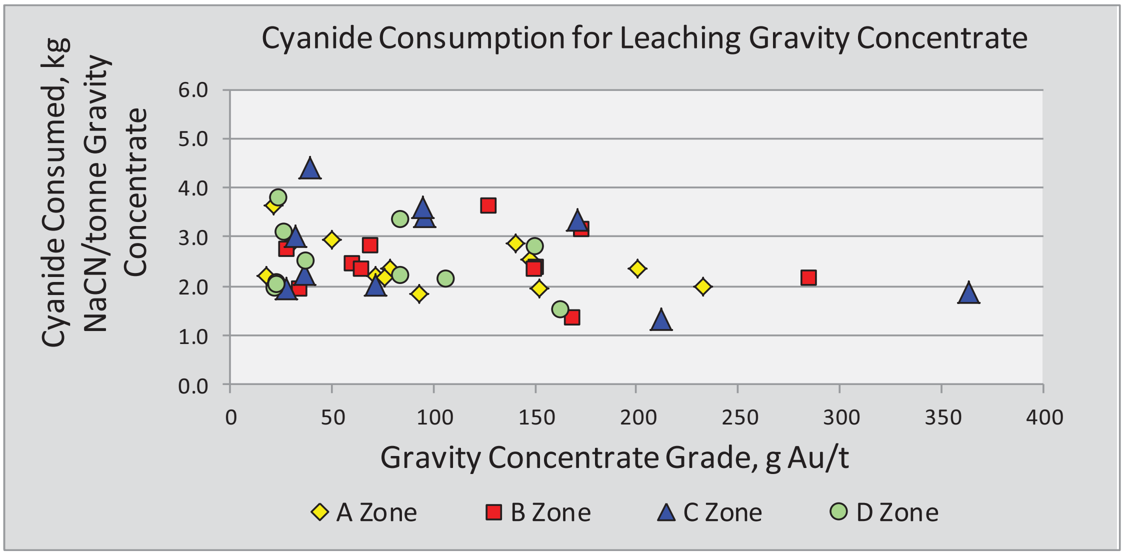
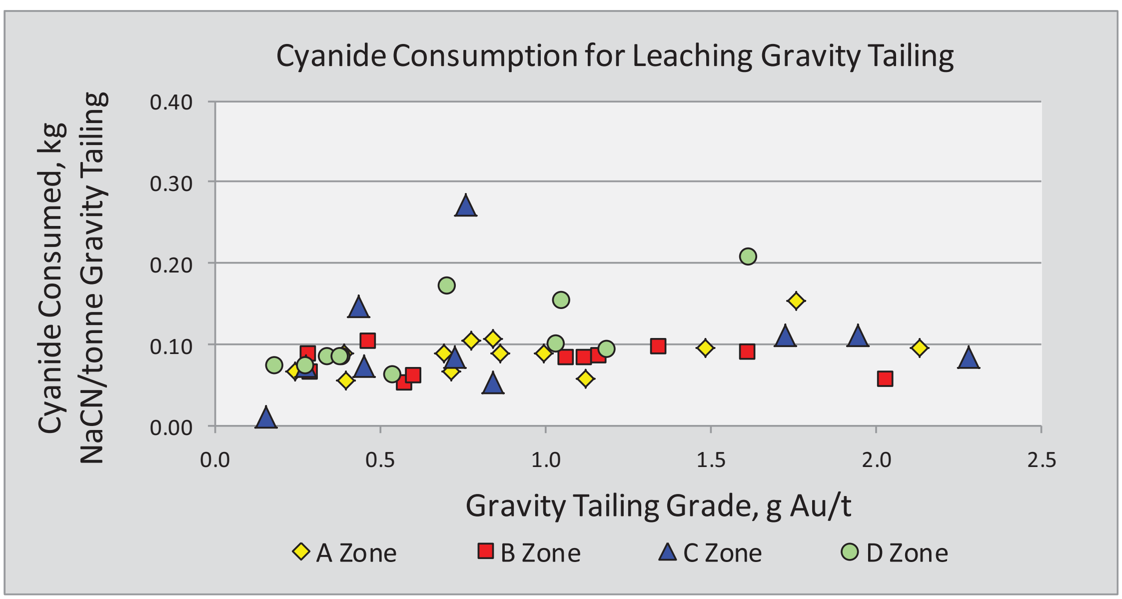
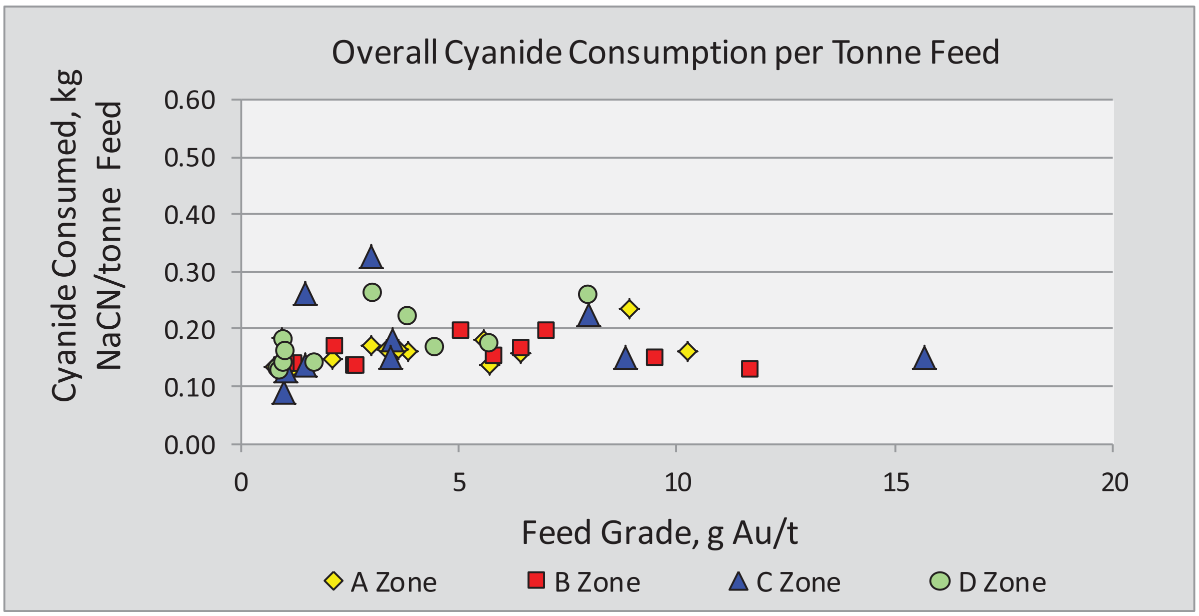


Figure 13-22: Cyanide Consumption for Leaching Gravity Tailing



The overall cyanide consumption ranged from 0.10 to 0.30 kg NaCN per tonne of Grade Composite feed, as reflected in Figure 13-23. It should be noted that these consumptions are the specific cyanide requirement to leach the gold and do not include cyanide that will inevitably be left in solution at the end of the gravity concentrate and gravity tailing leaches. Although in normal plant practice, every effort would be made to recycle cyanide from leach solutions, the actual plant cyanide consumptions will be closer to 4 kg NaCN per tonne of gravity concentrate and 0.35 kg NaCN per tonne of gravity tailing. Based on the relative weights of gravity concentrate on gravity tailing, this calculates to an overall consumption of 0.43 kg NaCN per tonne of plant feed. A consumption of 0.50 kg NaCN per tonne feed is appropriate for use in calculating operating costs.

Figure 13-23: Overall Cyanide Consumption per Tonne Feed



Lime consumption, shown in Figures 13-24 and 13-25, ranged from 1.5 to 5.0 kg CaO per tonne of gravity concentrate, with the highest consumption measured for Zone D material. Lime consumption ranged from 0.5 to 1.0 kg CaO per tonne of gravity tailing. The overall lime consumption ranged from 0.5 to 1.1 kg CaO per tonne of Grade Composite feed, as reflected in Figure 13-26. A consumption of 1.00 kg CaO per tonne feed is appropriate for use in calculating operating costs.

Figure 13-24: Lime Consumption for Leaching Gravity Concentrate

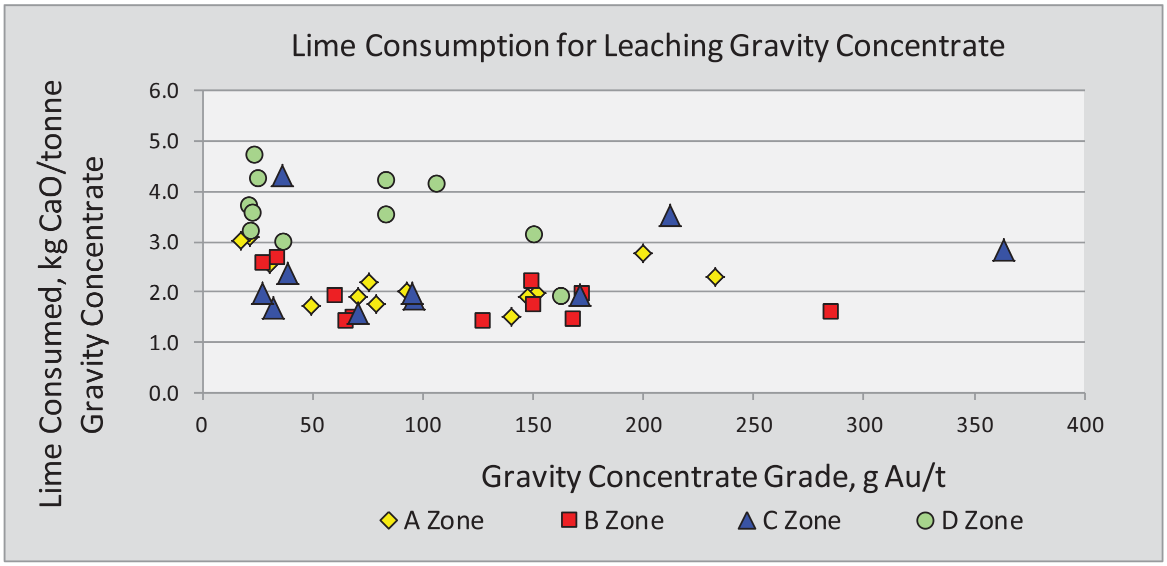


Figure 13-25: Lime Consumption for Leaching Gravity Tailing

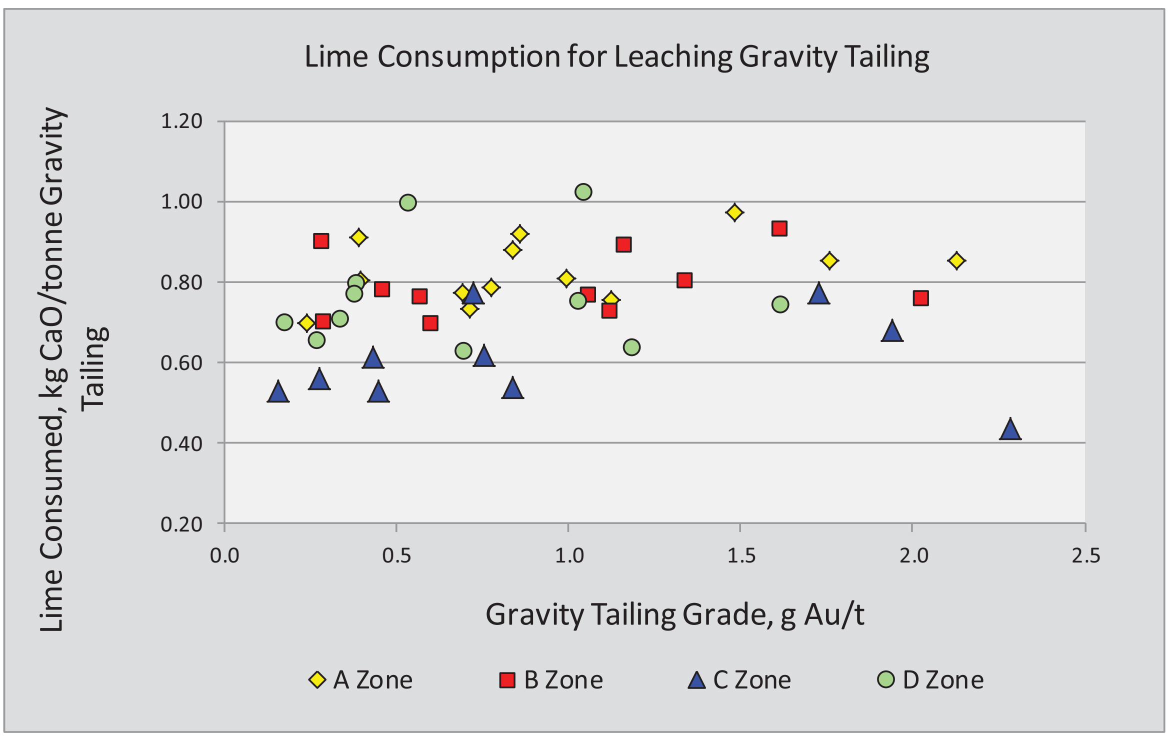
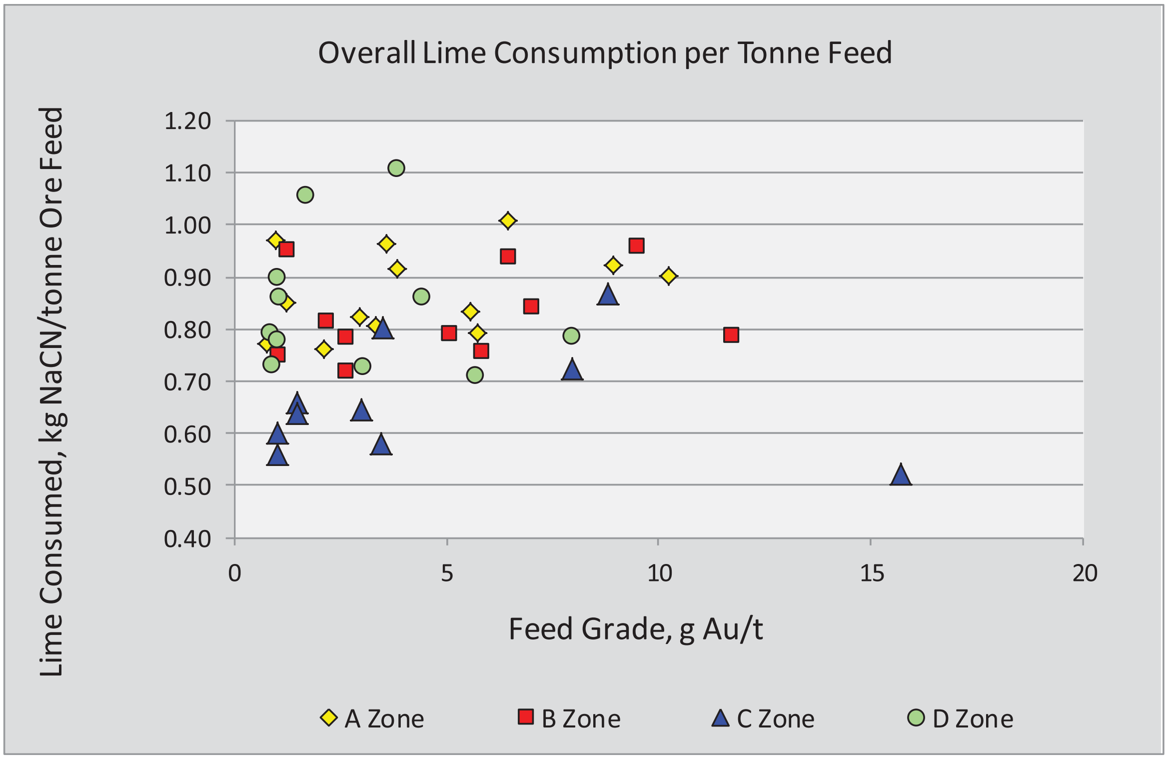


Figure 13-26: Overall Lime Consumption per Tonne Feed



13.3.4.3 Leach Kinetics and Required Residence Time

The arithmetic mean of the leach recovery with time has been calculated for all 47 grade composite tests, for leaching the gravity concentrate and also for leaching the gravity tailing. The results are summarised in Table 13.17 and Figure 13-27 below.

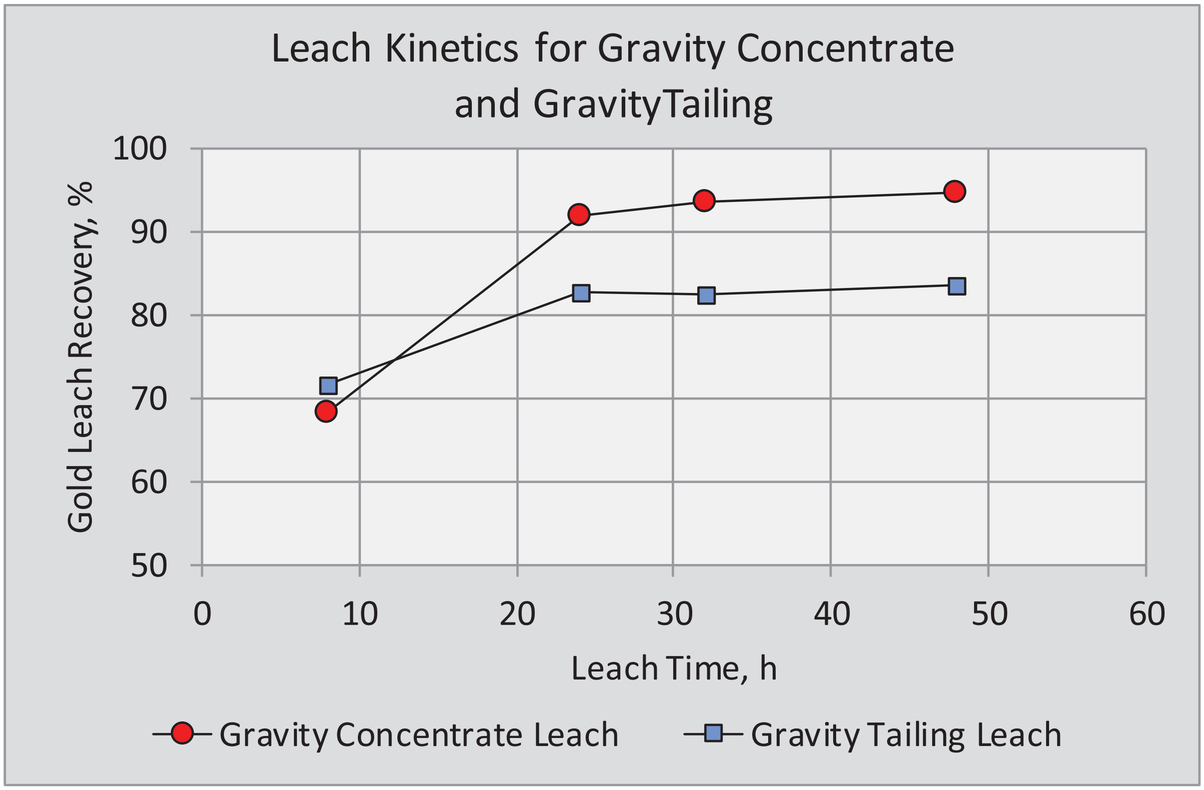
From the graph it can be seen that gold is still leaching very slowly from the gravity concentrate after 48 hours. Normally in plant operation, the gravity concentrate leach residue would be put to the head of the gravity tail leach, and therefore would be given additional leach time. This should be sufficient to dissolve any additional recoverable gold.

Table 13.17: Kinetic Leach Recovery Data for Leaching Gravity Concentrate & Gravity Tailing

Leach Time, h	Gravity Concentrate Leach Recovery, % (mean of all Grade Composite Tests)	Gravity Tailing Leach Recovery, % (mean of all Grade Composite Tests)
8	68.2	71.7
24	91.9	82.8
32	93.5	82.6
48	94.9	83.6

Note: Excludes obvious major anomalous results.

Figure 13-27: Leach Kinetics for Gravity Concentrate & Gravity Tailing



Referring to Table 13.18, which summarises the effect of residence time on leach recovery, the results indicate there is little advantage to leaching the gravity tailing for longer than 24 hours. The leach recovery is increased by less than 1% by doubling the leach residence time to 48 hours, and given the relatively low-grade of the gravity tailing, additional residence time past 24 hours will not be cost-effective.

Table 13.18: Effect of Leach Residence Time on Leach Recovery

Leach Time	Gravity Concentrate Leach Recovery, %												
h	A1	A2	A3	A4	A5	A6	A7	A8	A9	A10	A11	A12	A13
8	64.3	87.9	71.3	79.6	71.3	66.3	66.9	83.4	72.9	75.8	71.7	84.6	77.9
24	93.1	95.4	97.2	96.3	98.3	96.7	95.7	92.7	96.6	98.8	95.2	99.1	92.5
32	94.9	95.6	98.7	96.7	61.3	97.2	95.6	93.7	97.2	97.1	98.2	97.6	94.3
48	97.7	98.0	99.1	97.3	96.9	98.5	97.0	96.1	97.4	97.0	97.0	97.3	95.3
	B21	B22	B23	B24	B25	B26	B27	B28	B29	B30	B31	B32	
8	70.7	80.8	78.0	65.6	73.5	77.0	75.1	71.1	68.9	68.9	73.6	67.7	
24	68.5	96.0	84.3	91.8	95.2	98.0	98.2	95.6	91.4	91.7	92.3	96.8	
32	93.0	97.2	80.5	93.5	93.7	96.9	98.2	94.5	90.4	92.7	91.4	97.4	
48	93.4	93.9	78.9	94.4	95.4	96.7	96.7	93.3	94.1	95.4	94.1	97.9	
	C41	C42	C43	C44	C45	C46	C47	C48	C49	C50	C51		
8	43.7	68.4	63.3	78.1	70.2	64.7	54.6	53.7	66.9	0.4	67.0		
24	75.7	84.8	94.2	92.3	94.0	88.0	80.0	89.9	90.5	92.2	94.1		
32	84.0	90.5	94.8	92.3	95.0	89.4	80.3	94.2	94.0	95.0	95.0		
48	98.6	95.7	98.3	91.3	95.1	92.1	93.6	94.6	94.2	94.4	95.0		
	D61	D62	D63	D64	D65	D66	D67	D68	D69	D70	D71		
8	46.2	56.3	62.5	67.3	60.0	67.1	54.0	70.3	62.4	58.2	58.5		
24	89.6	92.9	92.3	92.7	87.3	89.8	91.4	92.7	88.0	88.6	89.6		
32	93.0	97.1	95.1	94.2	89.9	92.6	93.7	92.4	88.6	90.8	93.4		
48	97.4	98.0	94.8	93.3	90.7	93.2	94.0	92.1	89.1	91.7	93.6		
Leach Time	Gravity Tailing Leach Recovery, %												
h	A1	A2	A3	A4	A5	A6	A7	A8	A9	A10	A11	A12	A13
8	92.6	87.7	81.5	78.7	77.1	83.7	79.9	78.0	75.6	65.3	66.9	54.0	65.3
24	115.4	91.8	95.5	86.2	90.9	95.0	90.5	88.4	90.5	77.3	80.0	70.8	77.3
32	125.0	95.8	96.8	88.7	89.6	92.2	90.5	88.4	89.5	77.3	79.2	71.3	77.3
48	96.7	95.8	96.8	91.1	90.9	95.0	90.5	88.4	91.4	77.7	81.7	72.4	77.7
	B21	B22	B23	B24	B25	B26	B27	B28	B29	B30	B31	B32	
8	64.5	77.3	72.0	63.4	63.7	72.6	74.8	71.7	70.2	78.3	63.7	76.7	
24	82.1	91.2	93.4	84.2	83.5	86.7	86.6	81.9	81.2	83.1	79.3	88.3	
32	82.1	84.4	89.2	84.2	86.8	85.0	85.8	81.0	80.3	81.3	78.8	87.5	
48	82.1	87.7	91.3	84.2	90.0	88.4	86.5	81.0	82.0	80.8	79.7	88.6	
	C41	C42	C43	C44	C45	C46	C47	C48	C49	C50	C51		
8	83.8	65.6	69.3	71.2	73.1	51.5	59.7	65.4	62.6	69.9	66.4		
24	83.8	76.4	85.2	82.1	81.3	72.3	71.4	76.3	72.7	78.7	81.1		
32	83.8	79.9	85.2	82.1	81.3	73.6	71.4	76.8	73.2	77.1	80.3		
48	83.8	79.9	89.6	82.1	81.3	74.8	72.6	76.8	73.2	78.9	80.7		
	D61	D62	D63	D64	D65	D66	D67	D68	D69	D70	D71		
8	85.5	87.3	82.3	75.5	79.0	78.6	73.0	67.1	63.9	63.1	63.7		
24	85.5	87.3	82.3	83.2	84.2	82.2	82.8	75.7	74.2	77.2	75.3		
32	85.5	90.8	82.3	83.2	84.2	80.4	82.8	75.7	74.2	78.0	75.9		
48	85.5	90.8	85.1	85.7	84.2	82.2	82.8	74.7	74.2	76.4	76.5		

13.3.4.4 Head Grade Reconciliation

Based on mineral resource and metallurgical testwork to date, gold mineralisation in the Magambazi deposit appears to be very spotty or nuggety, making it difficult to reproduce individual assays on the same sample. Summarised in Table 13.19 (overleaf) are listings of the gold assays for the Grade Composites from each mineralised zone, firstly as determined from the testwork back calculated head assays, secondly from the head assays that were made during the sample preparation of each of the composites, and thirdly from the calculated composite assay based on the as received weight of each constituent drill core interval and the assay of that interval specified in the drill core database.

The most accurate estimate of the composite gold content will be the back calculated head grade from the testwork. Essentially, this is an assay that uses a 2 kg sample for the assay determination. The other assays described above are compared to the back calculated head grade in the graphs of Figures 13-28 through 13-30 given below.

The gold grade of head assay samples split out during the sample preparation of the Grade Composites are in rough agreement with the gold grade back calculated from the metallurgical test results, see Figure 13-28 below, but there is still a relatively wide scatter in the results indicative of a mineralisation nugget effect. The majority of the head assay samples, generated during sample preparation of the composites, assay lower than the back calculated 2kg metallurgical test assay, with a small percentage assaying higher than the met assay. This is indicative of material containing nugget gold.

The Grade Composite gold assay predicted from the drill core weights as received and the gold assays taken from the drill core database can also be compared with the gold grade back calculated from metallurgical testwork, as shown in Figures 13-29 and 13-30. This provides a very interesting comparison and illustrates that, for the higher grade composites, the composite grade predicted using the drill core database assays is significantly higher than the assay back calculated from the metallurgical testwork. Conversely, for low-grade composites, the composite grade predicted using drill core database assays is significantly lower than that back calculated from the metallurgical testwork. This suggests that the higher grade assays in the drill core database are overstated and the lower grade assays in the drill core database are understated.

Table 13.19: Comparison of Composite Gold Assays (g Au/t)

Grade Composite	Testwork Back Calculated Head Grade	Sample Prep Head Grade Assay Sample	Drill Core Weighted Average	Arsenic Assay,%
A1	0.97	0.17	0.28	0.02
A2	0.78	0.45	0.65	0.04
A3	2.98	6.59	1.00	0.05
A4	1.24	0.63	1.39	0.08
A5	2.12	1.27	1.78	0.19
A6	3.35	1.73	2.20	0.16
A7	3.83	1.54	2.71	0.44
A8	3.61	2.80	3.42	0.50
A9	5.58	3.70	5.04	0.47
A10	6.43	4.07	6.98	0.83
A11	5.72	9.29	9.33	0.66
A12	8.92	8.70	17.71	1.14
A13	10.25	15.44	43.63	1.75
B21	1.22	0.45	0.21	0.19
B22	1.03	1.14	0.66	0.11
B23	2.15	1.15	1.48	0.17
B24	2.61	1.74	2.23	0.35
B25	2.63	2.73	2.77	0.31
B26	5.80	2.48	3.43	0.40
B27	6.99	10.54	4.45	0.57
B28	6.44	3.75	5.84	0.78
B29	5.04	3.24	8.22	0.69
B30	9.47	5.18	12.40	0.89
B31	11.69	10.01	20.72	1.44
B32	33.56	17.06	58.23	1.29
C41	1.00	0.23	0.13	0.02
C42	1.02	0.61	0.33	0.12
C43	1.49	0.39	0.58	0.06
C44	1.48	1.94	1.04	0.15
C45	3.49	1.79	1.82	0.33
C46	2.99	2.95	3.07	0.51
C47	3.46	1.52	4.87	0.44
C48	8.83	7.17	7.89	0.96
C49	7.96	7.30	11.91	1.54
C50	22.49	25.08	18.34	2.02
C51	15.69	13.79	39.98	1.41
D61	0.84	0.17	0.13	0.04
D62	0.89	0.24	0.39	0.03
D63	1.00	0.72	0.63	0.09
D64	1.01	1.19	0.87	0.13
D65	1.04	0.42	1.13	0.18
D66	1.70	0.70	1.51	0.31
D67	3.05	2.06	2.13	0.34
D68	4.45	2.70	2.93	0.68
D69	3.86	10.43	4.19	0.80
D70	5.71	4.42	6.12	0.92
D71	7.98	5.57	14.20	0.83

Figure 13-28: Gold Assay of Head Grade Sample from Sample Preparation vs. Gold Grade of Composite Back-Calculated from Metallurgical Testwork

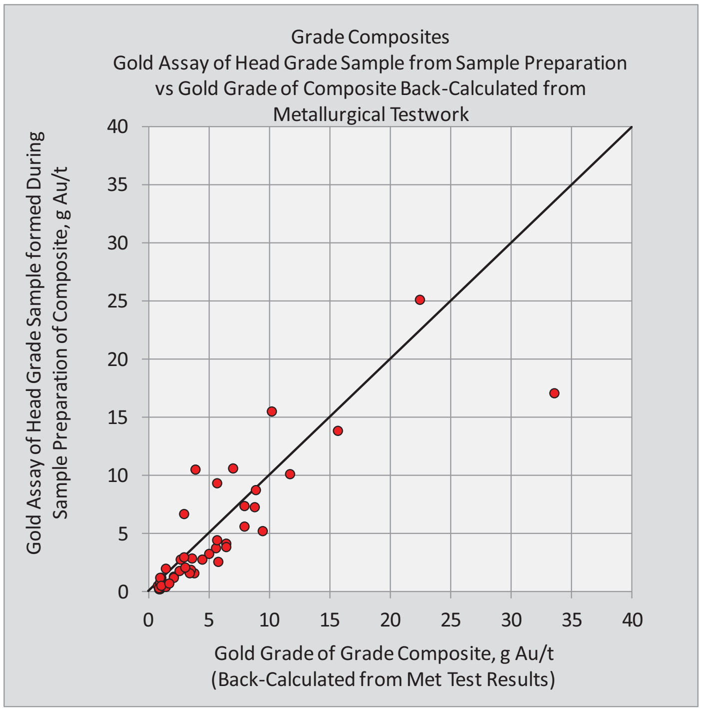


Figure 13-29: Gold Assay of Grade Composite based on Drill Core Weights & Gold Assays in the Drill Core vs. Gold Grade of Composite Back-Calculated from Metallurgical Testwork

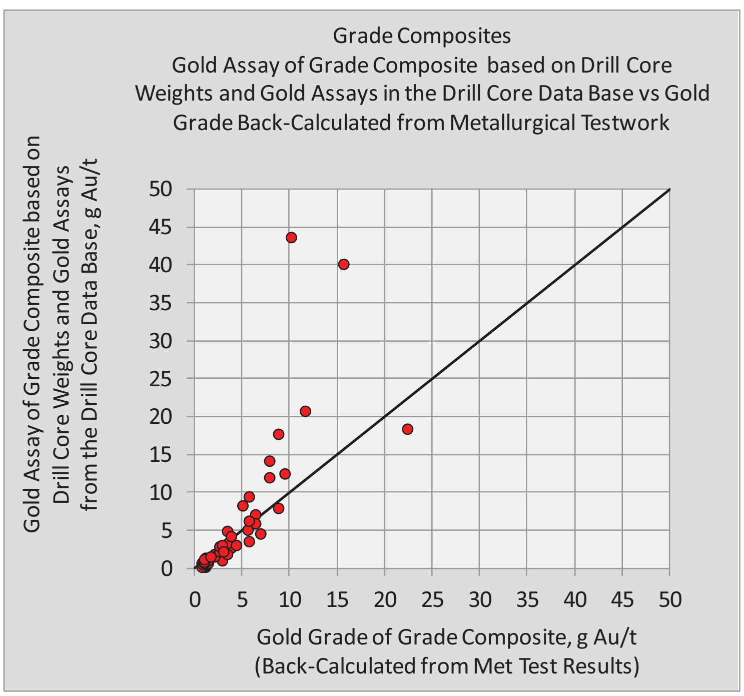
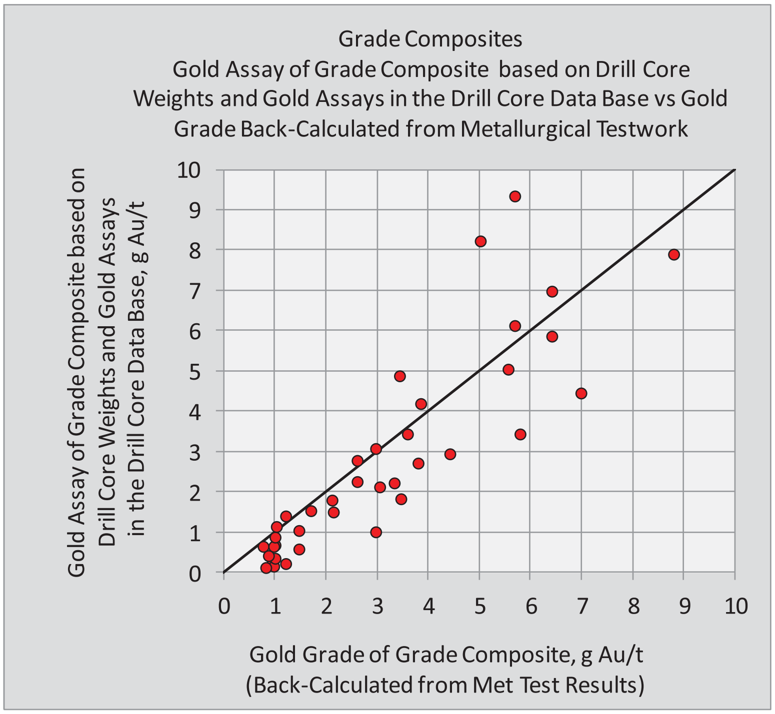


Figure 13-30: Gold Assay of Grade Composite based on Drill Core Weights & Gold Assays in the Drill Core vs. Gold Grade Back-Calculated from Metallurgical Testwork



To further illustrate this point, Figures 13-31 and 13-32 below show a plot of the ratio of the composite assay using the drill core database divided by the composite assay using back calculated metallurgical testwork, against the back calculated metallurgical testwork grade. The second graph, Figure 13-32, shows an expanded scale x-axis, along with trend lines calculated using a power relationship.

It is recommended that this discrepancy between composite grades predicted from drill core assays and composite grades predicted from back calculated metallurgical results, be investigated further. An attempt should be made to estimate whether the apparent overstating of high-grade drill core assays is offset by the understating of the low-grade drill core assays. This will obviously relate to the amount of metal in the mineral resource estimate associated with high-grade drill core information and that associated with low-grade drill core information.

It is also suggested that some 20 remaining quarter core intercepts that have high gold assays be crushed and pulverised completely, and then split into two halves. One half should be cyanide bottle roll leached, and the other half split into 16 equal parts for fire assaying. This exercise will indicate the degree of variability in the high-grade samples, and whether a large sample that is 'assayed' by bottle roll cyanide leaching can better estimate the grade of the intercept.

Figure 13-31: Ratio of Metallurgical Test Back-Calculated Grade to Predicted Head Grade using Drill Core Assays vs. Predicted Head Grade from Drill Core Assays

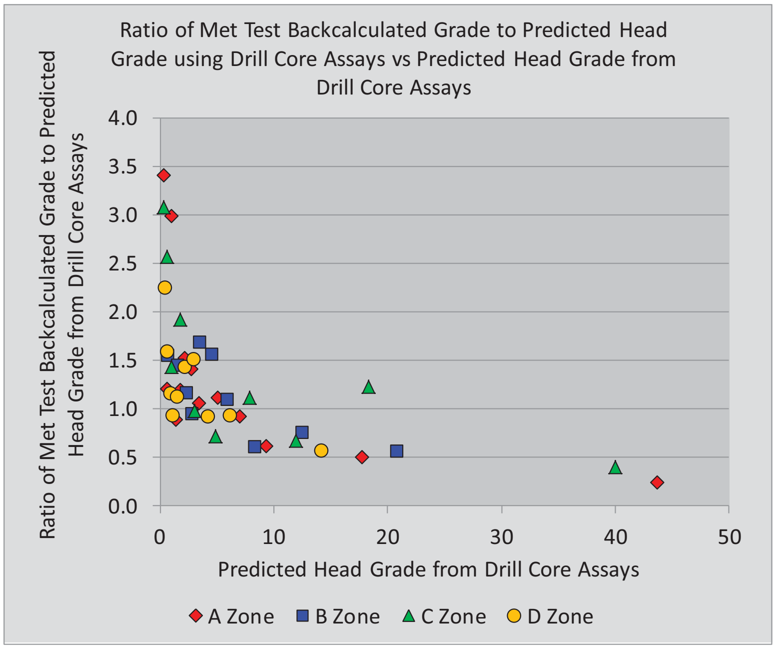
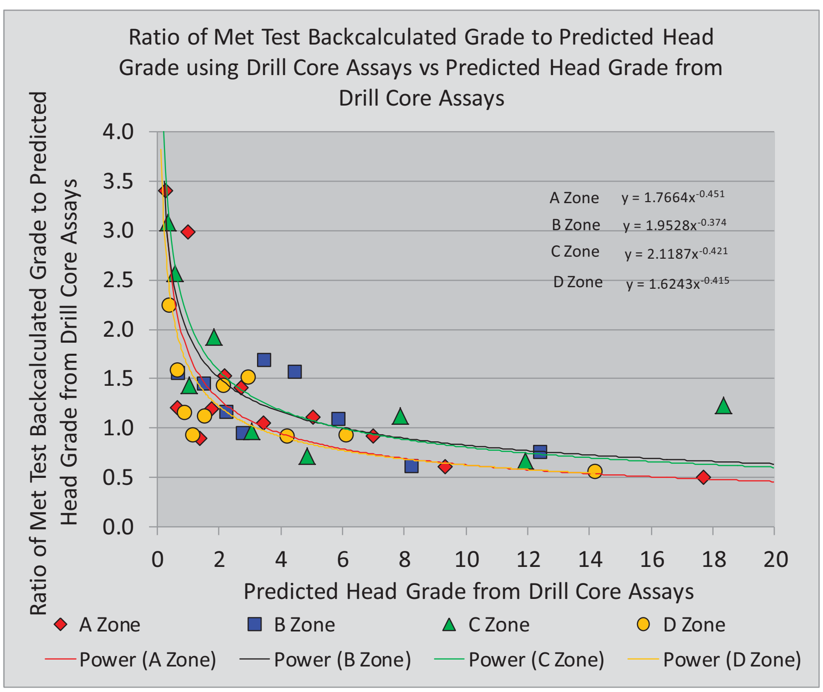


Figure 13-32: Ratio of Met Test Back-Calculated Grade to Predicted Head Grade using Drill Core Assays vs. Predicted Head Grade from Drill Core Assays



13.3.5 Flowsheet Using Leaching of Combined Gravity & Flotation Concentrate

To minimise the amount of material subjected to cyanide leaching, testwork was carried out on the low-grade and high-grade master composites of Zones A through D, to investigate whether satisfactory gold recoveries could be collected into a combined gravity concentrate and flotation concentrate that represented a small weight percentage of the mineralised feed.

Two kilogram sample charges were subjected to a Knelson gravity separation and thereafter, the gravity tailing was floated using the collector reagents potassium amyl xanthate and Cytec 3477 to produce three timed bulk rougher flotation concentrates. The results are presented in Table 13.20 and demonstrate that over 90% of the gold in the feed could be recovered into a combined gravity-flotation concentrate, representing a mass pull of less than 10% of the feed weight.

Table 13.20: Results from Knelson Gravity Separation followed by Flotation

Low Grade Master Composite	Tests :		315A/315B									
Product	Weight		Assay - percent or g/t					Distribution - percent				
	grams	%	Fe	S	Au	C	As	Fe	S	Au	C	As
Knelson Gravity Concentrate	68.8	3.4	7.7	4.35	29.1	0.19	2.43	7.1	11.3	71.8	1.6	43.3
Bulk Ro Float Conc 1	31.7	1.6	34.8	24.4	14.9	11.7	3.32	14.7	29.2	17.0	46.3	27.3
Bulk Ro Float Conc 2	17.8	0.9	48.3	29.1	3.9	0.23	0.53	11.4	19.6	2.5	0.5	2.5
Bulk Ro Float Conc 3	17.6	0.9	45.5	27.5	2.2	0.24	0.34	10.7	18.3	1.4	0.5	1.6
Bulk Ro Tail	1859.1	93.2	2.3	0.31	0.11	0.22	0.05	56.2	21.7	7.3	51.1	25.4
Feed	1995.0	100	3.8	1.33	1.4	0.40	0.19	100	100	100	100	100
Knelson Conc + Ro Float Concs	135.9	6.8	24.2	15.3	19.0	2.88	2.12	43.8	78.3	92.7	48.9	74.6

High Grade Master Composite	Tests :		316A/316B									
Product	Weight		Assay - percent or g/t					Distribution - percent				
	grams	%	Fe	S	Au	C	As	Fe	S	Au	C	As
Knelson Gravity Concentrate	77.1	3.8	11.9	5.58	65.7	0.21	8.46	9.9	13.1	73.5	1.3	47.0
Bulk Ro Float Conc 1	52.6	2.6	35.0	23.3	25.0	12.5	8.04	19.8	37.3	19.0	54.7	30.5
Bulk Ro Float Conc 2	31.8	1.6	43.3	25.5	4.8	0.37	1.54	14.8	24.7	2.2	1.0	3.5
Bulk Ro Float Conc 3	12.4	0.6	46.5	27.0	2.9	0.24	1.00	6.2	10.2	0.5	0.2	0.9
Bulk Ro Tail	1828.9	91.3	2.5	0.27	0.18	0.28	0.14	49.3	14.8	4.8	42.8	18.0
Feed	2002.8	100	4.6	1.64	3.4	0.60	0.69	100	100	100	100	100
Knelson Conc + Ro Float Concs	173.9	8.7	27.1	16.1	37.8	3.96	6.53	50.7	85.2	95.2	57.2	82.0

Having demonstrated that acceptable gold recoveries could be achieved into a combined gravity and flotation concentrate, additional tests were performed using the same low-grade and high-grade master composites. In these additional tests, gravity and flotation concentrates were produced and combined, and then leached for 48 hours using a cyanide concentration of 2,000 ppm. Test results are summarised in Tables 13.21 and 13.22.

Table 13.21: Results from Knelson Gravity Separation followed by Flotation & Leaching (Low Grade Composite)

Produce Knelson+Float Concs					Tests :			317A/317B				
Product	Weight		Assay - percent or g/t					Distribution - percent				
	grams	%	Fe	S	Au	C	As	Fe	S	Au	C	As
Knelson Conc + Ro Float Concs	175.0	8.75			19.74					96.4		
Rougher Float Tail	1824.4	91.2			0.07					3.6		
Feed	1999.4	100			1.79					100		
Knelson Conc + Ro Float Concs	175.0	8.75			19.74					96.4		

Leach Test on Knelson+Float Concentrate	Test :	328		2000ppm NaCN and pH 11	
Product	Time h	Volume or Mass	Units	Assay - g/t Gold	Distribution - percent Gold
Cyanide Liquor (8 hr)	8	1530	ml	1.89	83.8
Cyanide Liquor (24 hr)	24	1500	ml	2.15	95.1
Cyanide Liquor (32 hr)	32	1470	ml	2.16	95.5
Cyanide Liquor (48 hr)	48	1440	ml	2.16	95.5
Cyanidation Tails	-	175	g	0.89	4.5
Calculated Feed		175	g	19.74	100

Table 13.22: Results from Knelson Gravity Separation followed by Flotation & Leaching (High Grade Composite)

Produce Knelson+Float Concs					Tests :			318A/318B				
Product	Weight		Assay - percent or g/t					Distribution - percent				
	grams	%	Fe	S	Au	C	As	Fe	S	Au	C	As
Knelson Conc + Ro Float Concs	203.4	10.13			61.00					96.9		
Rougher Float Tail	1804.5	89.87			0.22					3.1		
Feed	2007.9	100			6.38					100		
Knelson Conc + Ro Float Concs	203.4	10.13			61.00					96.9		

Leach Test on Knelson+Float Concentrate	Test :	329		2000ppm NaCN and pH 11	
Product	Time h	Volume or Mass	Units	Assay - g/t Gold	Distribution - percent Gold
Cyanide Liquor (8 hr)	8	1530	ml	6.70	82.8
Cyanide Liquor (24 hr)	24	1500	ml	7.73	95.3
Cyanide Liquor (32 hr)	32	1470	ml	7.75	95.5
Cyanide Liquor (48 hr)	48	1440	ml	7.70	95.0
Cyanidation Tails	-	203	g	3.07	5.0
Calculated Feed		203.4	g	61.00	100

Overall Recovery of Gold by Leaching Combined Knelson+Float Concs	92.1	%
Cyanide Consumption	7.24	kg NaCN/tonne Knelson +Float Conc
	0.73	kg NaCN/tonne Fresh Process Feed
Lime Consumption	3.1	kg CaO/tonne Knelson +Float Conc
	0.31	kg CaO/tonne Fresh Process Feed

For the low-grade master composite, 96.4% of the gold in the feed was recovered into the combined gravity-flotation concentrate. Cyanide leaching of this combined concentrate dissolved 95.5% of the contained gold, giving an overall gold recovery of 92.1%. Results for the high-grade master composite were similar, with 96.9% of the gold recovered into the combined gravity-flotation concentrate, and leaching of this combined concentrate dissolving 95.0% of the contained gold, for an overall gold recovery of 92.1%. Cyanide consumption in leaching was relatively high when expressed in terms of kilograms NaCN per tonne of combined gravity+flotation concentrate, but was significantly lower and acceptable when expressed in terms of kilograms NaCN per tonne of fresh feed. Cyanide consumption was 0.63 and 0.73kg NaCN/tonne fresh process feed for the low-grade and high-grade master composites respectively.

There are some anomalies in the testwork results above. For example, the bulk rougher flotation tailing in test 315 was 0.11 g of gold per tonne compared to a grade of 0.07 g in test 317 run under the same conditions. Back calculated head grades for the two low-grade composite tests and also for the two high-grade composite tests do not check particularly well. Additional testwork is certainly required, preferably using all eight of the low-grade and high-grade Zones A through D composites, to substantiate and confirm the results of the tests reported above.

However, assuming the results above are indeed representative of this type of flowsheet, they are very encouraging. Significant advantages may be gained from an environmental and waste management standpoint if it is possible to cyanide leach less than 10% of the process plant fresh feed and achieve gold recoveries over 90%.

14 MINERAL RESOURCE ESTIMATES

This resource is the first reported mineral resource for the Magambazi project. 397 core holes, drilled beginning in 2009, were utilized for this estimate. A site visit was made from Feb. 14th - 16th, 2012 to see the project, to collect independent samples, to meet the exploration team and to discuss the geologic setting of the deposit.

14.1 Available Data

This initial mineral resource estimate for Magambazi is based on assay data available to February 29, 2012. Results from 397 holes have been utilized for this estimate; all holes were diamond drill core holes. Figure 14-1 shows drill hole locations as well as the limits of the mineral resource model. The estimation block model geometry is listed in Table 14.1. The block size of 5 x 5 x 5 metres was selected to provide a reasonable level of selectivity in support of the low production rate (<6,000 tpd) anticipated for the project. A second, larger block model was used to cover sufficient area to allow pit optimization. This model, at more than 11 million cells, was not practical to use directly for estimation. The estimation model was imported into the larger framework for pit optimization.

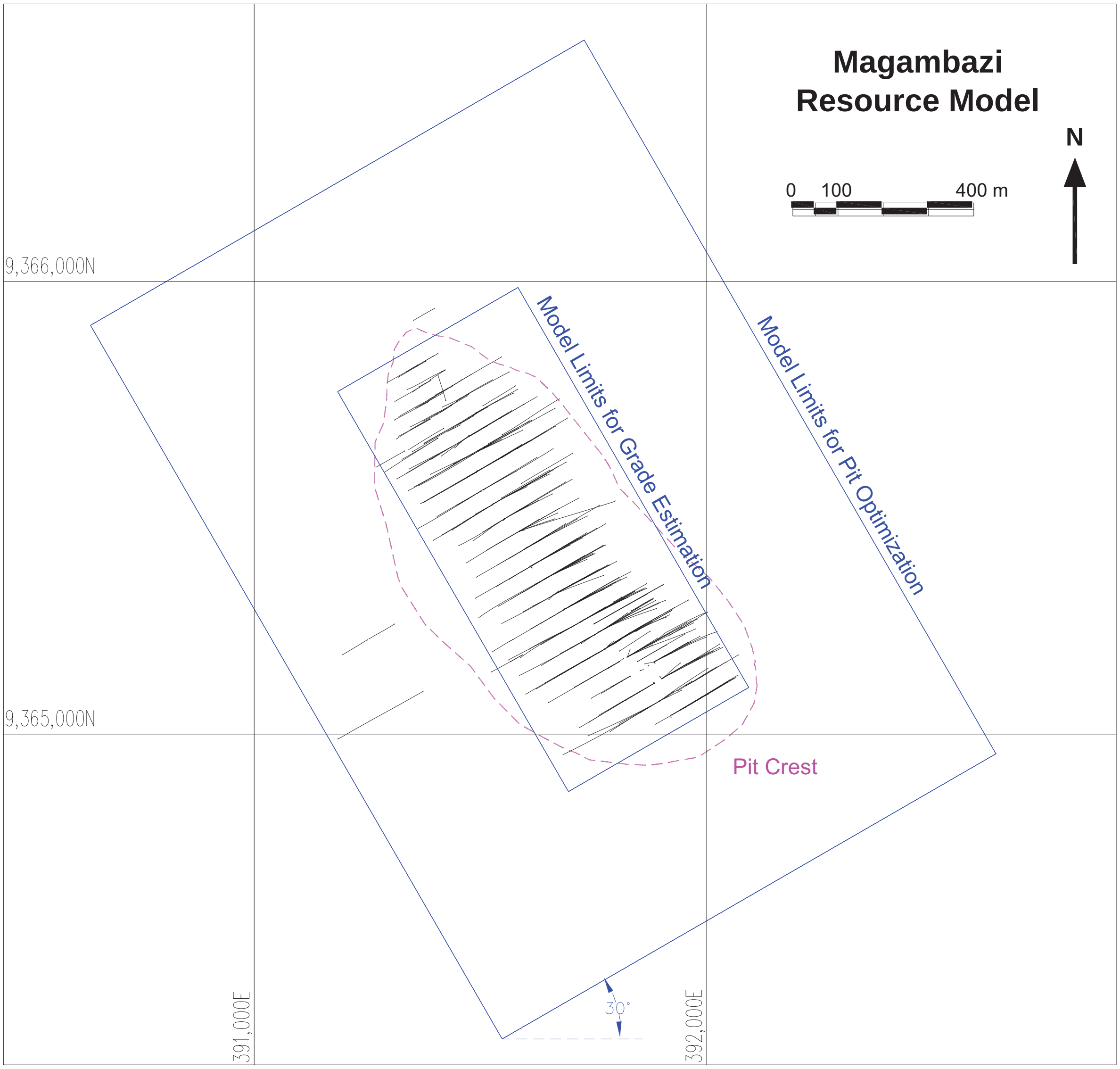
Since disclosure of the initial Magambazi resource, an additional 69 holes have been drilled within the larger model framework used for pit optimization. The resource estimate has not been revised to include this drilling.

Table 14.1: Resource Block Model Setup

Block	X	Y	Z
Origin(1)	391,694.5304	9,364,872.9062	900
Size (m)	5	5	5
No. blocks	92	204	120
Rotation	30° counter-clockwise about origin		

(1) SW model top, block edge.

Figure 14-1: Available Drilling & Block Model Outline



Source: Archibald et al., 2012.

14.2 Sample Compositing

Sample data was composited to a downhole length of 5 m. 92% of samples were one metre in length; however the high variability of assay values dictated the necessity of compositing to a longer length for grade interpolation. The choice of a 5 m composite length was made based on its match with the block height, as well as its associated reduction of grade variance to a more reasonable level.

Pending assays were ignored in the compositing process; unsampled intervals were set to a default value of 0.001 g/t. 196 composites of less than 2.5 m were removed from the dataset after it was determined that this did not fundamentally impact the distribution of grades.

14.3 Geologic Model

The geologic model at Magambazi consists of two predominant rock types. A cap of paragneiss is generally present on the hilltop overlying the garnet-amphibolite basement rocks. Metamorphic grade is sufficiently high that precise lithology determination can be ambiguous, and the recognition of distinct structural features difficult. Core inspection at site illustrated generally well developed foliation and minor folding, but little in the way of distinct structural features or structural association with the mineralisation.

Overburden was not modeled as a separate unit for this mineral resource estimate. Interpolation of a 2D model of bedrock depth below topography was attempted, however several factors made this process unworkable at this time. Inconsistent logging of various soil units, as opposed to saprolitic weathering made selection of the top of bedrock difficult in some holes. The present topographic surface plots above most hole collars which would make implementation of an interpolated bedrock surface quite arbitrary. Where logged in 261 holes, ‘soil’ vertical thickness ranges from 0.7 to 11.4 m and averages 2.3 m. The average vertical gap between topography and hole collar locations is 4.3 m.

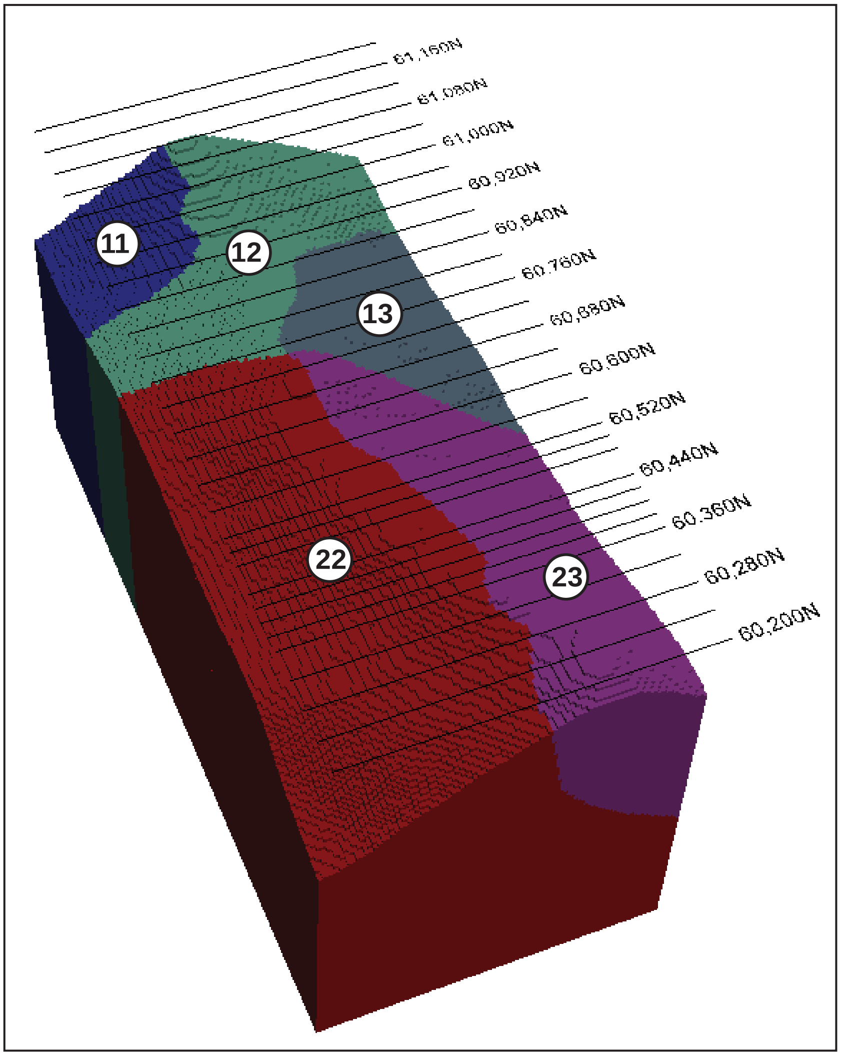
Examination of grade by logged lithologic units showed highest grades associated with zones of silicification, deformed quartz veins, and garnet silica rocks (GASIL). These units are generally narrow and poorly correlated between sections (see Table 14.2), possibly a result of post mineralisation deformation. With this in mind and given the relatively high density of drilling information, a decision was made to use grade shells to domain the deposit for grade estimation.

Table 14.2: Logged Lithology Intervals by Decreasing Average Grade

			Intersection Length (m)		
Logged "Lith1"		**Count**	**Mean**	**Max**	**(g/t)**
SIL	Silicified Intensely	65	2.8	27.0	8.92
SILGA	Silica-Garnet (silica>garnet)	6	1.5	3.0	2.72
GASIL	Garnet-Silica (garnet>silica)	1,013	4.0	41.0	1.17
QV	Quartz Vein	56	1.5	4.0	0.91
AMPL	Amphibolite (Leucco-<40% amph)	153	5.5	52.0	0.41
AMP	Amphibolite	2,978	18.7	228.0	0.20
GNSK	Gneiss Kyanite rich/present	904	12.6	109.0	0.15
DIKEBT	biotite dikelet	4	2.3	3.0	0.14
AMPact	Actinolitic Amphibole	178	2.8	25.0	0.13
GNS	Gneiss	1,884	7.8	119.0	0.12
RSY	Soil Yellow	16	1.8	4.0	0.11
RSO	Soil Orange	171	1.9	11.0	0.08
RSR	Soil Red	48	1.6	4.0	0.08
RSG	Soil Grey	8	1.5	3.0	0.08
SAP	Saprock	357	4.6	32.0	0.08
GNSB	Gneiss feldspar-QTZ_BIO	36	6.4	28.0	0.07
AMPM	Amphibolite Mottled	272	17.1	85.0	0.07
RSB	Soil Brown	48	1.5	8.0	0.06
CL	Core Loss	195	1.2	5.0	0.04
DOL	? Dolerite	1	3.0	3.0	0.04
QDF	? Likely QFD	3	2.3	3.0	0.04
QFD	Quartzfeldspathic vein	9	2.0	5.0	0.03
PEG	Pegmatite	1	1.0	1.0	0.03
PYX	Pyroxenite	1	1.0	1.0	0.03
RSYB	Soil Yellow Brown	3	2.0	3.0	0.02
AMP/PYX	Amphibolite /Pyroxenite	1	3.0	3.0	0.00
SOIL	SOIL	1	1.0	1.0	0.00
Total		**8,412**	**11.3**	**228.0**	**0.23**

Sectional interpretation was used as the basis for dividing the deposit into five structural or directional domains. In the north, moving from west to east across strike, mineralisation trends from a shallow easterly dip to shallow westerly to steep westerly (domains 11-13). In the south the shallow eastern dip zone is not present (domains 22 and 23); see Figure 14-2.

Figure 14-2: Isometric View of Five Interpreted Structural Domains

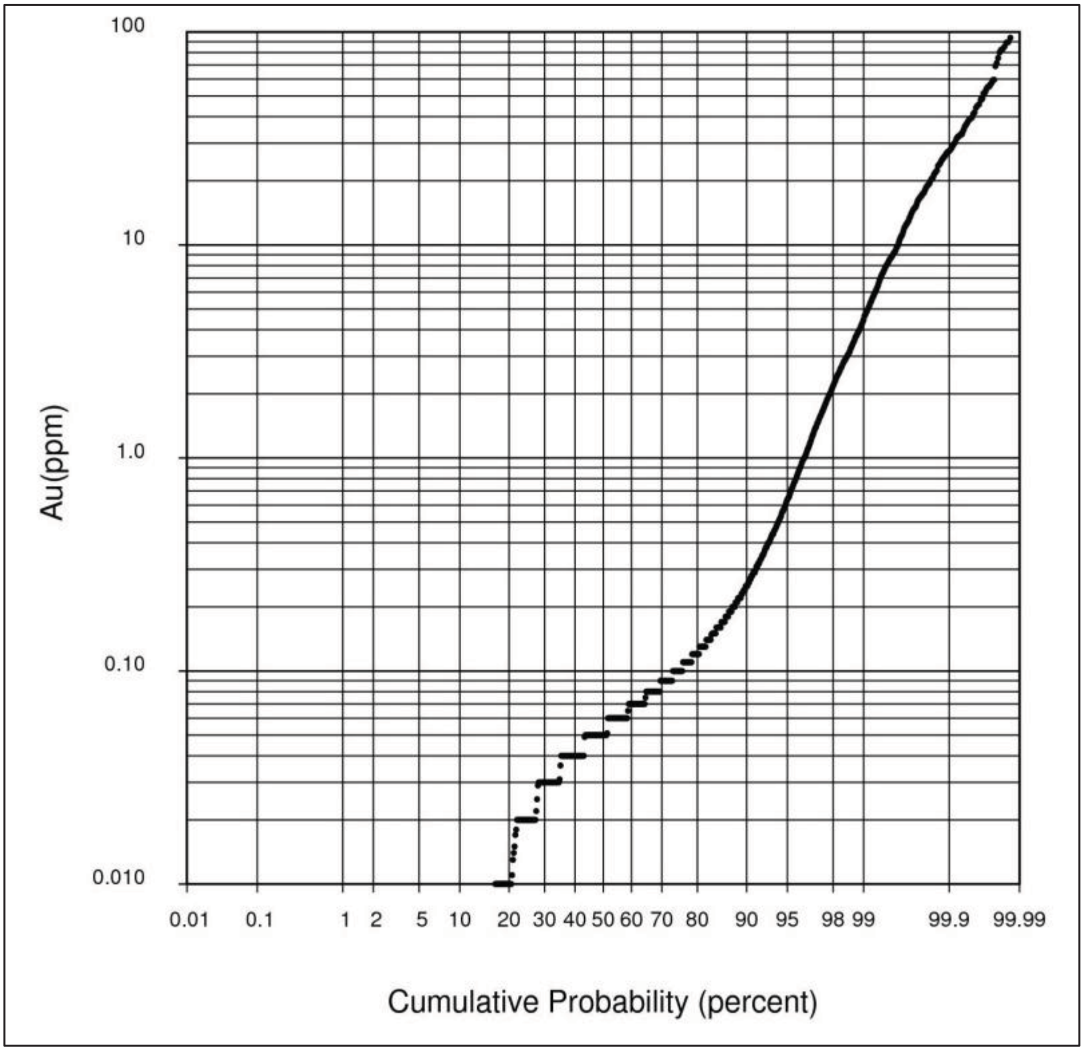


14.4 Grade Domain Modeling

Manually interpreted grade outlines are maintained on section by site personnel for exploration planning purposes. However these shapes are not digitized consistently enough along strike to be used to create through-going volumes. A process of grade shell generation using indicators was therefore selected as a preferred method for domain modeling.

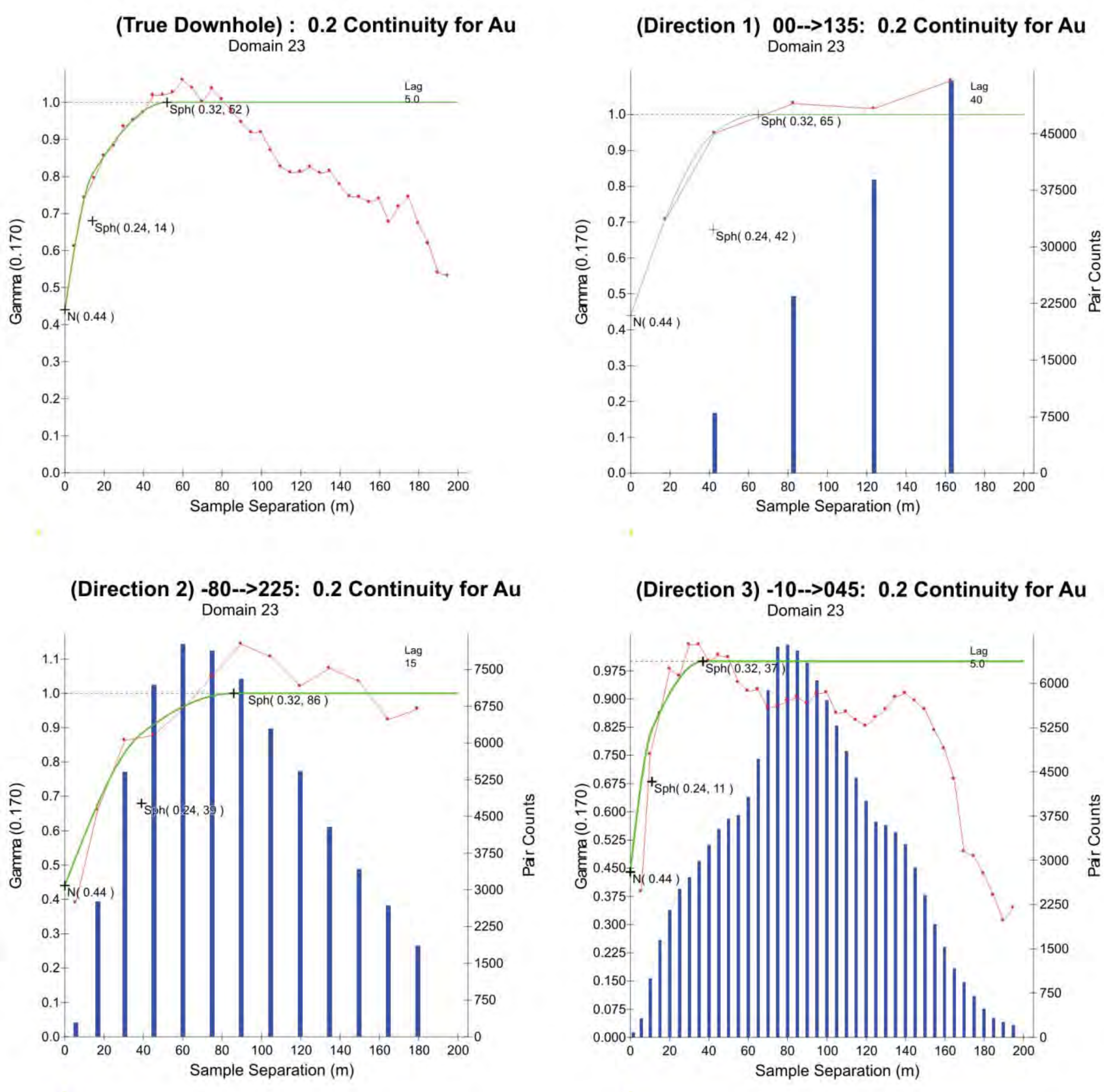
The goal of the approach was to separate very low grade material from that with economic potential; the indicator threshold was therefore chosen at a level below economic value by examination of a log-probability plot of gold assays (Figure 14-3). A threshold of 0.20 g/t was selected to differentiate potentially mineralised volumes from background low-grade material.

Figure 14-3: Probability Lot – All Gold Assays



Interpolation of indicators was by ordinary kriging within the five interpreted directional domains. A 150 metre spherical search was use for sample selection with anisotropic variogram models in each domain. Variogram model details are listed in Table 14.3. In each directional domain the nugget effect and variance contributions, for each structure, were derived from downhole experimental variograms. In all domains, the nugget effect is high, reflecting observations made in the analysis of sampling QA/QC results as well as in metallurgical testwork. Anisotropic directions were determined from variogram maps and ranges were fit to directional variogram plots. Example variograms for domain 23 are presented in Figure 14-4.

Figure 14-4: Domain 23 0.20 g/t Indicator Variograms



A minimum of four, maximum of 16 samples and a maximum of 3 samples per hole, and soft boundaries between directional domains, was used for indicator estimation. This requirement for two holes lead to the best correspondence with manually interpreted grade zones, the supporting assay data and with interpreted structure on visual interrogation of cross-sections.

Table 14.3: Indicator Variogram Models

Directional	Nugget	Rotation		Direction	Spherical Model 1		Spherical Model 2	
Domain	Effect	(axis)	(RHR)	(dip/azi)	Sill	Range(m)	Sill	Range(m)
11	0.42	Z	-140	-30/140	0.25	30	0.33	50
		X	-30	00/055		18		26
		Z	90	60/145		18		26
12	0.50	Z	-70	-20/245	0.19	56	0.31	68
		X	20	-02/335		94		134
		Z	-85	-70/070		71		82
13	0.61	Z	-140	25/230	0.17	25	0.22	62
		X	-90	-65/230		55		65
		Z	-25	00/140		20		40
22	0.58	Z	-45	00/135	0.28	32	0.14	144
		X	10	-10/225		50		81
		Z	0	-80/045		44		100
23	0.44	Z	-45	00/135	0.24	42	0.32	65
		X	80	-80/225		39		86
		Z	0	-10/045		11		37

In order to designate blocks as inside or outside of the grade shells, a probability level was selected within each directional domain. This selection was made by back-tagging composite data with estimated indicator probabilities and then selecting the probability level that resulted in the fewest composites being assigned to the wrong grade bin (above and below the indicator threshold).

The selected probability values are presented in Table 14.1. These were used, within each of the directional domains, to code blocks and to tag individual composites as inside or outside the potentially mineralised zone.

Table 14.4: Indicator Probability Thresholds

Directional Domain	Indicator Probability Threshold
11	0.45
12	0.37
13	0.30
22	0.37
23	0.41

14.5 Grade Capping

Grade capping is utilized to control the impact of extreme, outlier high-grade samples on the overall mineral resource estimate. The decision was made to cap grades after compositing as opposed to capping raw assays. Typically this decision is taken when sample lengths are highly variable and normalization of sample intervals is warranted prior to compositing. In this case the vast majority of sample lengths are a constant 1 m, but the assay variability is such that compositing of raw assays, prior to capping high-grade outliers, was felt to be more reflective of average grades over mineralised intervals.

The levels selected as being outliers to the general population were determined by examining histograms and probability plots within the low-grade and potentially mineralised domains. Uncapped and capped composite statistics are presented in Table 14.5. Selected cap levels have reduced the coefficient of variation (CV) in both grade domains, to levels acceptable for the conventional estimation of grade.

Table 14.5: 5 m Composite Grade Capping

		Au (g/t)			Capped Au (g/t)			
Shell	**Count**	**Mean**	**Max**	**CV**	**No.Cap'd**	**Mean**	**Max**	**CV**
1 (<0.2 g/t)	15,211	0.09	18.14	3.5	24	0.08	2.50	1.8
2 (≥0.2 g/t)	2,877	1.26	124.77	3.2	18	1.11	15.00	1.9
Total:	18,088	0.27	124.77		42	0.24	15.00	

The amount of gold metal removed through the capping process was evaluated by comparing capped and uncapped nearest neighbor models. In total, 11% metal was removed through the capping of grades as outlined above. As the geologic model is improved in future models, and if grade uncertainty and variability becomes better understood this level of metal removal could be reduced in upcoming mineral resource estimates.

14.6 Grade Interpolation

Grade interpolation was carried out initially with hard boundaries between the low-grade and the potentially mineralised shells as derived from the kriging of indicators outlined above. A second pass, for the higher grade domain only, used the same orientation and ellipse size with all the samples in an effort to fill more of the potentially mineralised blocks. Only 0.6% of the higher grade blocks were estimated in the second pass.

Estimation was by inverse distance cubed weighting (ID^3). The interpolation approach is well suited to Magambazi where grades are quite variable and potentially discontinuous.

Search anisotropy was derived from the indicator variogram models in each directional domain. Search orientations and ranges are listed in Table 14.6. Relatively few samples were used for grade estimation with the goal of preserving local variability encountered in drilling. The potentially mineralised blocks were estimated using a minimum of three samples, a maximum of 12 and a maximum of 5 samples per hole. In the second high-grade pass and for all low-grade blocks, estimation required a minimum of three samples, a maximum of 16 and a maximum of 5 samples per hole.

Table 14.6: ID^3 Search Parameters

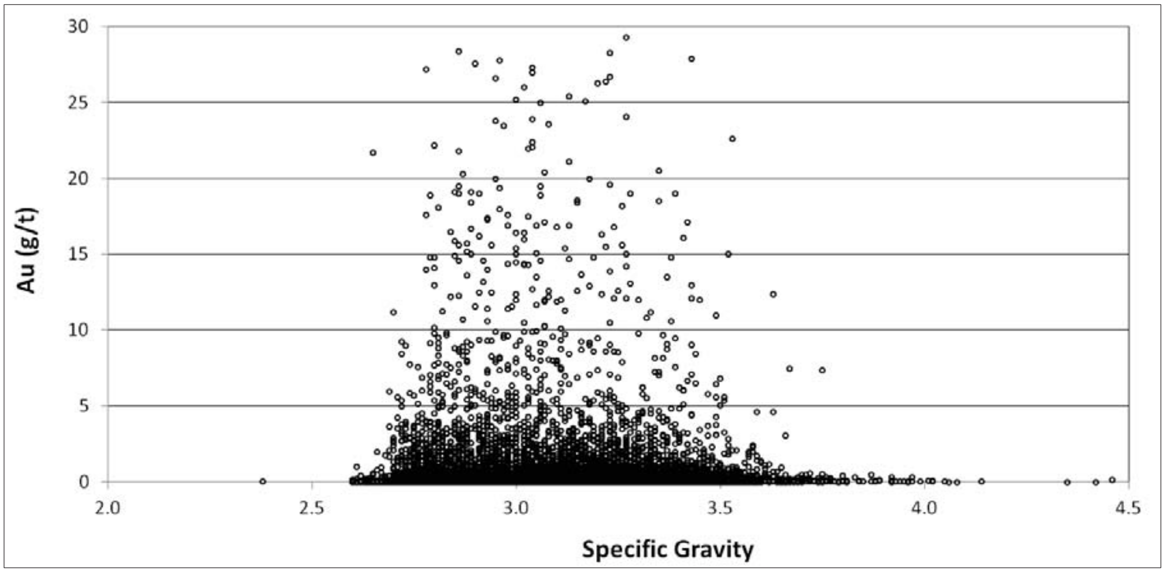
Directional Domain	Direction (axis)	(dip/azi)	Distance (m)
11	X	-30/140	50
	Y	00/055	35
	Z	60/145	35
12	X	-20/245	65
	Y	-02/335	135
	Z	-70/070	80
13	X	25/230	65
	Y	-65/230	65
	Z	00/140	45
22	X	00/135	100
	Y	-10/225	55
	Z	-80/045	75
23	X	00/135	65
	Y	-80/225	85
	Z	-10/045	40

14.7 Density Assignment

Density assignment was based on the results of 50,384 measurements. Of these 11,948 samples were within the gneiss solids and averaged 2.82 t/m^3 with an inter-quartile range of 0.10; 38,436 measurements fell outside the gneiss solids and were measured to have an average density of 3.17 t/m^3 with an inter-quartile range of 0.14. These average values were applied to the block model by rock type.

The high average density values were initially a concern to the author in terms of potentially overstating tonnage. To help validate specific gravity, values were plotted against assay results from the core intervals from which density measurements were taken; see Figure 14-5. This plot showed that the average densities used for the mineral resource are reasonable for the distribution of grades.

Figure 14-5: Assay Grade vs. Specific Gravity



14.8 Model Validation

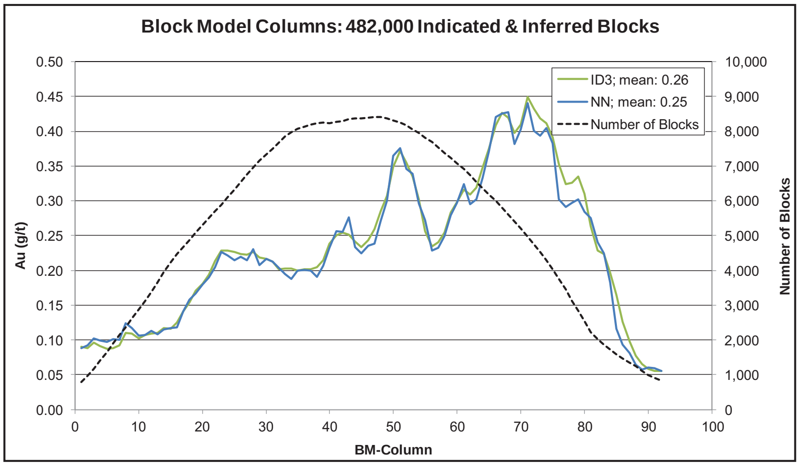
A nearest neighbor (NN) model was estimated using the same domain matching as the ID^3 estimate. The NN model was used to check various aspects of the estimation process.

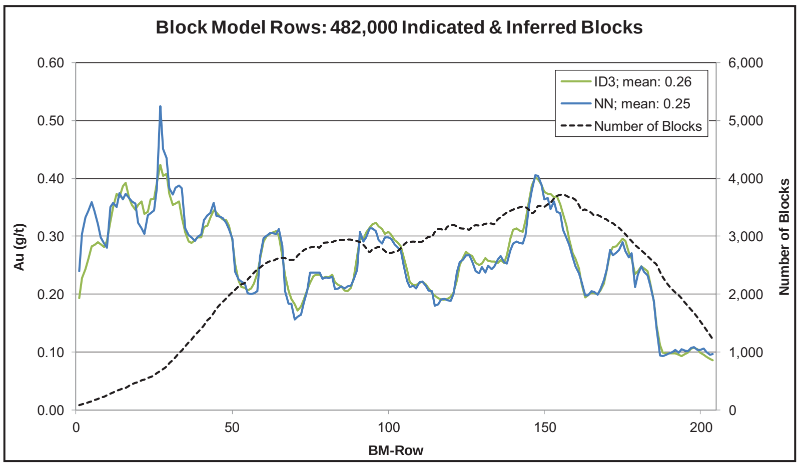
Estimated grades were validated to ensure consistency with supporting composite data. Visual checks, comparing assay and composite values with block grades on plans and sections, showed good correlation.

More quantitative validation was made by generating swath plots along block model rows, columns and levels to spatially compare the resource model against NN results. During the estimation process plots were generated and used to calibrate ID^3 parameters. Plots of all indicated and inferred blocks (Figure 14-6) show acceptable spatial correlation between estimated blocks and the supporting composite data. In areas of significant difference between the two models there are relatively few blocks contributing to the average grades.

The degree of estimation smoothing was assessed by comparing the ID^3 estimate against the variance corrected NN model. The NN model was rescaled to a 5 x 5 x 5 m selective mining unit using an average variogram model and applying the indirect lognormal correction. Figure 14-7 compares the two models on a grade and tonnage basis. In the range of potential cut-off grades the ID^3 model has higher tonnage and lower grade. The coefficient of variation of the ID^3 model is 19% lower than that of the corrected NN model. This level of smoothing is appropriate and acceptable.

Figure 14-6: Swath Plots Comparing ID^3 & NN Estimates





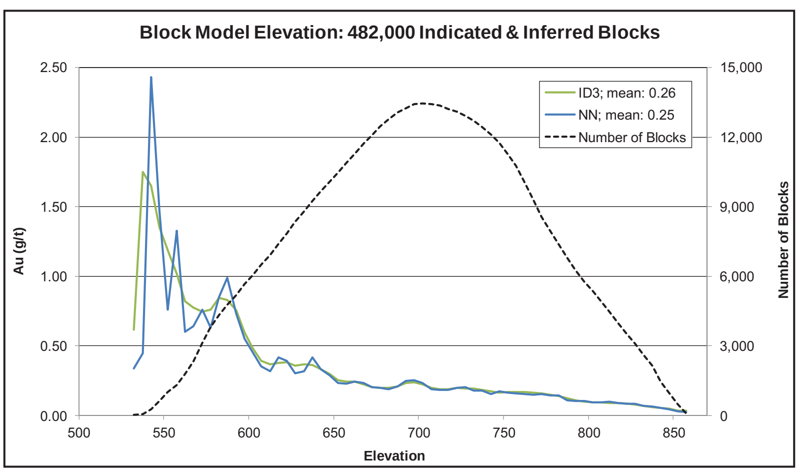
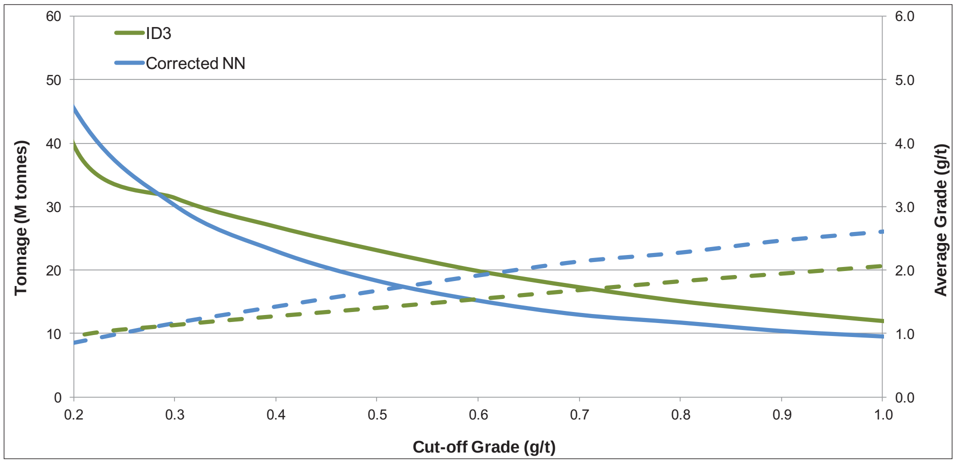


Figure 14-7: Grade-Tonnage Comparison between ID^3 & Variance Corrected NN Model



14.9 Mineral Resource Classification & Tabulation

This estimate was classified based on spatial parameters related to available composite data. These parameters are:

- the minimum number of holes used to estimate grade
- the average distance to samples used to estimate grade
- the distance to the closest sample used in the estimate
- the distance to the second closest sample
- the distance of the third closest sample.

Classification criteria were established iteratively by visually assessing the impact of parameter adjustment on resultant maps of classified blocks. The goal was to have reasonably cohesive volumes rather than a scattered patchwork of indicated and inferred blocks, while assigning the indicated category in a justified pattern based on sampled locations. The application of these parameters is listed in Table 14.7.

As a second step, any indicated block estimated with influence of a QA/QC problem sample was down-graded to the inferred category. Approximately 35% of the inferred mineral resource has been downgraded from indicated. See section 11.5.1 for a discussion of the QA/QC issues.

Table 14.7: Mineral Resource Classification Criteria

	No. Holes	Max. Distance (m) to:			Avg. Distance
Category	min.	closest	2^{nd} closest	3^{rd} closest	max. (m)
Indicated	2	7.5	15		
	3	10	20	30	
	4				25
	5	- - - - - any distance - - - - -			
Inferred	Remainder estimated and within pit shell				

Measures were taken to validate that the mineral resource meets the condition of "reasonable prospects of economic extraction" as suggested under National Instrument 43-101. To this end, a pit shell was generated using a gold price of US$1,250 per ounce and an overall pit slope of 40° for the purpose of mineral resource tabulation. Only blocks within the pit volume were included in this mineral resource estimate.

The Magambazi mineral resource is presented in Table 14.8 for a range of cut-off grades. The cut-off of 0.50 grams per tonne was selected as the mineral resource base case considering potentially reasonable prospects for economic extraction by conventional surface mining and mineral processing methods. All estimates resulting from each cut-off grade must meet the test of "reasonable prospects of economic extraction".

Table 14.8: Magambazi Estimated Mineral Resource

Cut-off Grade (g/t)	Indicated			Inferred		
	Tonnes (kt)	Au (g/t)	Au (oz)	Tonnes (kt)	Au (g/t)	Au (oz)
0.30	19,685	1.23	777,500	9,256	1.09	324,500
0.40	17,218	1.36	750,300	7,831	1.23	308,800
0.50	**15,186**	**1.48**	**721,300**	**6,683**	**1.36**	**292,400**
0.60	13,392	1.60	689,900	5,593	1.52	273,400
0.70	11,884	1.72	658,700	4,791	1.67	256,800
1.00	8,593	2.07	570,600	3,058	2.14	210,700

Using a cut-off grade of 0.50 grams per tonne gold, Magambazi is estimated to contain 15.2 million tonnes in the indicated category grading 1.48 grams per tonne gold and containing 721,300 ounces of gold, as well as 6.7 million tonnes in the inferred category grading 1.36 grams per tonne gold and containing 292,400 ounces of gold.

15 MINERAL RESERVE ESTIMATES

As this report relates to description of an initial mineral resource estimate, mineral reserves have not been calculated and this section is not applicable at this time.

16 MINING METHODS

As this report relates to the description of an initial mineral resource estimate, mining methods have not been evaluated or established and this section is not applicable at this time.

17 RECOVERY METHODS

As this report relates to description of an initial mineral resource estimate, recovery methods have not been evaluated and this section is not applicable at this time.

18 PROJECT INFRASTRUCTURE

As this report relates to the description of an initial mineral resource estimate, project infrastructure has not been evaluated or established and this section is not applicable at this time.

19 MARKET STUDIES & CONTRACTS

As this report relates to the description of an initial mineral resource estimate, product marketing and sales contracts have not been evaluated or established and this section is not applicable at this time.

20 ENVIRONMENTAL STUDIES, PERMITTING AND SOCIAL OR COMMUNITY IMPACT

In early 2012, Canaco mobilized an experienced team of environmental and socio-economic professionals to establish the project baseline conditions which would serve as a permanent reference for the project area. To this end, Rescan Environmental Services Ltd and its associated team of local/national Tanzanian specialists is currently undertaking baseline monitoring and field reviews of the project area.

Key information being developed during baseline monitoring includes water supply identification; measurement of local wet and dry season climatic conditions; and assembly of important local/regional information that will serve as input to subsequent planning and development. Although establishment and monitoring of environmental and socio-economic baseline studies are a longer term activity, the knowledge and information gained from these activities will provide helpful context and understanding for subsequent project development activities. In particular, information gathered through ongoing environmental and socio-economic baseline work will be used to understand the project setting and how it interacts with local and national communities.

20.1 Environmental Studies

Canaco has initiated baseline environmental and socio-economic studies in 2012 with the aim of completing an Environmental Impact Assessment ("EIA") for the project, during subsequent development work and compatible with International Financial Committee (IFC) standards. In particular, field teams were mobilized and initial field reviews conducted during the wet season of 2012. These reviews include initial work to establish field conditions and baseline determination in the following areas:

- meteorology
- hydrology
- hydrogeology
- water quality
- vegetation
- wildlife
- socio-economic conditions.

Meteorology studies included the installation of a weather station at the Canaco camp, approximately 5 km north of the Magambazi hill. Regional government data has also been collected for an initial determination of local and regional climate conditions. Available records from 1980 to 1997 and 2002 to 2010 indicate that average annual rainfall in the nearby town of Handeni is 767 mm. Rainfall is bimodal, with short rains each year in December and long rains during March to May. The combination of relatively low rainfall and well-drained soils results in infrequent surface water flows. Most stream courses in the area are class 0 or 1, i.e., small, intermittent streams. As an initial step in collection of local data, hydrology stations have been installed to measure seasonal flows in the two class 2 streams within the concession, but these streams have been observed to be dry during the wettest portion of 2012 and, anecdotally, for much of the year. Local residents source their water from surface water and near-surface groundwater. This water was sampled as part of the current baseline program during the long rains in 2012. Baseline hydrogeology drilling was also conducted during February-May, 2012. Data on groundwater presence, connectivity and quality is being gathered and a baseline groundwater model is planned for late 2012.

The exploration and mining lease, and surrounding area, is predominantly low rolling plain supporting Miombo woodland, with shifting agriculture in lowland areas. Small hills, including the Magambazi hill, capture moisture from offshore winds and support a mixture of various coastal vegetation types. Wildlife species are typical of agricultural areas with yellow baboons and bush pigs being the most common wildlife, along with a variety of mongoose and reptile species as well as a diverse avian community.

Additional, baseline studies, including mapping of vegetation, wildlife and other environmental resources and collection of meteorological, vegetation and water quality samples are ongoing and are planned to be documented in mid 2013.

20.2 Waste & Tailings Impoundment & Water Management

As this report relates to description of an initial mineral resource estimate, planning, design and other specific factors related to the impoundment of tailing and waste materials, as well as management of water resources, have not yet been evaluated. Further development of the project should include early consideration to the environmental and other impacts associated with these important facilities and aspects of the project.

20.3 Project Permitting

Project permitting activities are being advanced and planned to accommodate national and international standards in two phases. As part of the first phase of these activities, a Tanzanian Ministry of Mines - compliant Environmental Assessment report was prepared and submitted to the National Environmental Management Council of Tanzania in February 2012. On August 27, 2012, the National Environmental Management Council approved the document. Canaco is now required to produce an Environmental Management Plan that will then be incorporated into the Forest Reserve Management Plan, prior to commencement of development activities.

20.4 Social & Community Requirements

Canaco has been working with local communities to establish a relationship based on open communication and cooperation since it purchased the property in 2007. To this end, Canaco has engaged local leaders, and has initiated several community development projects including road building as well as refurbishment and staffing of a local community school. Canaco has also worked with regional and national government departments to establish a sound relationship.

During 2012, baseline socio-economic research was initiated to lay the ground work for an internationally-compliant EIA process. To date, this baseline research has included interviews with federal, regional, municipal, village authorities and local people, including farmers and artisanal miners.

20.5 Mine Closure

As this report relates to description of an initial mineral resource estimate, design and other factors related to mine closure have not yet been evaluated. Further development of the project should include early consideration to the environmental and other impacts associated with closure of all project facilities and the closure planning should begin early in the planning of tailing, waste, mining, processing and infrastructure facilities.

21 CAPITAL & OPERATING COSTS

As this report relates to the description of an initial mineral resource estimate, capital and operating costs have not been evaluated or established and this section is not applicable at this time.

22 ECONOMIC ANALYSIS

As this report relates to the description of an initial mineral resource estimate, an economic analysis of the project has not been undertaken and this section is not applicable at this time.

23 ADJACENT PROPERTIES

Additional information is not available to report and this section is not applicable.

24 OTHER RELEVANT DATA & INFORMATION

Additional information is not available to report and this section is not applicable.

25 INTERPRETATIONS & CONCLUSIONS

25.1 Interpretations & Conclusions

The Handeni drill hole database contains approximately 121,846 metres of drilling in 471 holes (the reader is directed to Table 10.1, Summary of Drilling at the Handeni Project), of which approximately 102,646 metres of drilling in 397 holes were used for mineral resource estimation. Following a detailed review of the QA/QC aspects of the drilling methods, laboratory procedures, data validation and the associated database, the Magambazi drilling database was found to be of sufficient quality to support the initial mineral resource estimate (Archibald *et al.,* 2012). Canaco has followed industry standard QA/QC procedures of inserting standard reference samples, blanks and duplicates into the stream of core samples sent for analysis, and maintaining careful chain of custody procedures. Continuity of the mineralised zones was established through geological characteristics, geostatistical analyses and mineralisation patterns, and these parameters formed the basis for modeling.

Mineral resource estimation was performed using Gemcom software. Uniform downhole 5 m composites were used to estimate 5 x 5 x 5 m blocks. Grades for gold were estimated by inverse distance cubed interpolation within two grade domains. Low-grade and potentially mineralised domains were derived by ordinary kriging of a 0.20 gram per tonne indicator applied to the composite data. Composite grades were capped in the two domains at 2.50 and 15 grams per tonne respectively. The interpolation of indicators and of grade was carried out with a search oriented parallel to one of five interpreted structural trends. Rock densities were based on averages derived from more than 50,000 measurements. Resource classification was based on geometric parameters associated with sample location and drill density. It should be noted that approximately 35% of the inferred mineral resource has been down-graded from an indicated category classification to an inferred category classification, pending resolution of unresolved QA/QC sample fails, and due to the decrease in confidence associated with the affected gold assays.

Measures were taken to validate that the mineral resource meets the condition of “reasonable prospects of economic extraction” as required under National Instrument 43-101 and practice standards of the CIM. To this end, a pit shell was generated using a gold price of US$1,250 per ounce and an overall pit slope of 40° for the purpose of mineral resource tabulation. Only blocks within the pit volume were included in this mineral resource estimate and Table 25.1 presents a summary of the estimated mineral resource for a range of cut-off grades. A cut-off grade of 0.50 gram per tonne was selected as the mineral resource base case considering extraction by conventional surface mining and mineral processing methods. At a 0.50 gram per tonne gold cut-off grade, the Magambazi area contains an indicated mineral resource of 15.186 Mt grading 1.48 g/t Au (for 721,300 oz Au) plus an inferred mineral resource 6.683 Mt grading 1.36 g/t Au (for 292,400 oz Au).

Table 25.1: Cut-off Grade Sensitivities

	Indicated			Inferred		
Cut-off grade (g/t Au)	Tonnes (kt)	Average grade (g/t Au)	Contained gold (oz)	Tonnes (kt)	Average grade (g/t Au)	Contained gold (oz)
0.3	19,685	1.23	777,500	9,256	1.09	324,500
0.4	17,218	1.36	750,300	7,831	1.23	308,800
0.5	**15,186**	**1.48**	**721,300**	**6,683**	**1.36**	**292,400**
0.6	13,392	1.60	689,900	5,593	1.52	273,400
0.7	11,884	1.72	658,700	4,791	1.67	256,800
1.0	8,593	2.07	570,600	3,058	2.14	210,700

In parallel with mineral resource estimation, Canaco has completed other work in support of the mineral resource estimate and in preparation for subsequent project stages. This work focused on understanding the metallurgical characteristics of gold mineralisation at the Magambazi area and on-going, environmental and socio-economic baseline studies.

Through this work, it was found that mineralisation from the Magambazi deposit of the Handeni project may be processed using conventional gravity concentration and cyanide leaching to recover the contained gold. The deposit has been divided into four zones, Zones A through D, along strike proceeding from south to north. Extensive composites representing a wide range of gold grade from each of these zones have been used to produce the gold recovery algorithms in Table 25.2 and shown graphically in Figure 25-1.

Table 25.2: Gold Percentage Recovery Algorithms by Zone

Zone A	Overall Gold Recovery = 98 - 0.6*HG
Zone B	Overall Gold Recovery = 92.5
Zone C	Overall Gold Recovery = 93 - 0.53*HG
Zone D	Overall Gold Recovery = 93 - 0.93*HG

Further to the above points, it should be noted that:

- Gold recovery is lower for mineralisation originating in the north of the deposit, represented by Zones C and D, than in the South represented by Zones A and B.
- Gold recovery is reduced as the feed grade mineralisation increases. Gold in the Magambazi deposit is closely associated with arsenic and two arsenic minerals have been identified, namely arsenopyrite and lollingite. It is likely that the reduction in gold recovery is due to a change of mineralogy and gold distribution between these two minerals as the gold content of the mineralisation increases. This aspect of the mineralogy should be investigated further.
- Differences were observed between metallurgical composite sample grades predicted from drill core assays and those back-calculated from metallurgical results. Further metallurgical testwork should be completed to understand or reconcile these differences. This observation

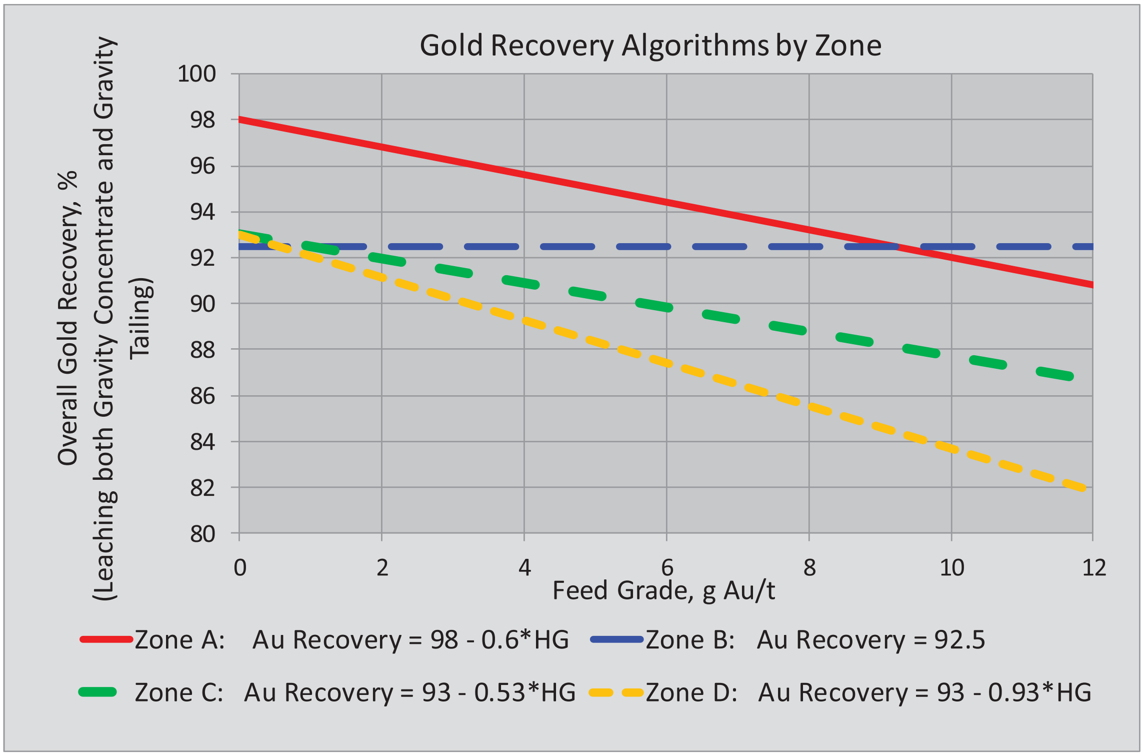
also indicates that application of grade capping practices during the mineral resource estimation are appropriate.

- The Magambazi area contains medium hard mineralised material with an average Bond Work Index of 16.6. It is considered medium abrasive with an average abrasion index of 0.30.

The flowsheet suggested for processing mineralised material from the Magambazi area should comprise:

- Three stage crushing to a P80 of 6 mm.
- Single stage ball milling to a P80 product size of 180 to 200 µm, assuming the deposit might eventually be mined by open pit methods. Testwork has shown the Magambazi deposit to contain medium hard mineralised material with an average Bond Work Index of 16.6. It is considered medium abrasive with an average abrasion index of 0.30.
- Gravity concentration installed in the grinding circuit should be expected to recover approximately 70% of the gold in the plant feed into a gravity rougher concentrate representing approximately 2% of the mass feed. In this approach, the gravity concentrate should be subjected to cyanide leaching using a cyanide concentration of 2000 ppm for a residence time of 48 hours.
- The ground process feed, after removal of the gravity concentrate, should be subjected to cyanide leaching using a cyanide concentration of 500 ppm for a residence time of 24 hours. The cyanide leaching should be carried out in a series of eight tanks, the first two tanks operated as straight leach tanks with the remaining six tanks operated as carbon in pulp tanks in a carousel arrangement.
- Cyanide consumption in the testwork averaged 2.5 kg NaCN per tonne of gravity concentrate, and 0.10 kg NaCN per tonne of gravity tailing. The overall cyanide consumption ranged from 0.10 to 0.30 kg NaCN per tonne of Grade Composite feed. It should be noted that these consumptions are the specific cyanide requirement to leach the gold and they do not include cyanide that will inevitably be left in solution at the end of the gravity concentrate and gravity tailing leaches. Whilst every effort will be made to recycle cyanide from leach solutions, the actual plant cyanide consumptions would be expected to be closer to 4 kg NaCN per tonne of gravity concentrate and 0.35 kg NaCN per tonne of gravity tailing. Based on the relative weights of gravity concentrate on gravity tailing, this calculates to an overall consumption of 0.43 kg NaCN per tonne of plant feed. A consumption of 0.50 kg NaCN per tonne feed is suggested for use in calculating operating costs.
- Lime consumption ranged from 1.5 to 5.0 kg CaO per tonne of gravity concentrate, with the highest consumption measured for Zone D material. Lime consumption ranged from 0.5 to 1.0 kg CaO per tonne of gravity tailing. The overall lime consumption ranged from 0.5 to 1.1 kg CaO per tonne of plant feed. A consumption of 1.00 kg CaO per tonne plant feed is suggested for use in calculating operating costs.

Figure 25-1: Gold Recovery Algorithms by Zone



An alternative was also investigated for incorporation of flotation into the process flowsheet. To that end and to minimize the amount of material subjected to cyanide leaching, preliminary testwork has been carried out on low-grade and high-grade master composites of Zones A through D, to investigate whether satisfactory gold recoveries could be collected into a combined gravity concentrate and flotation concentrate that represented a small weight percentage of the plant feed.

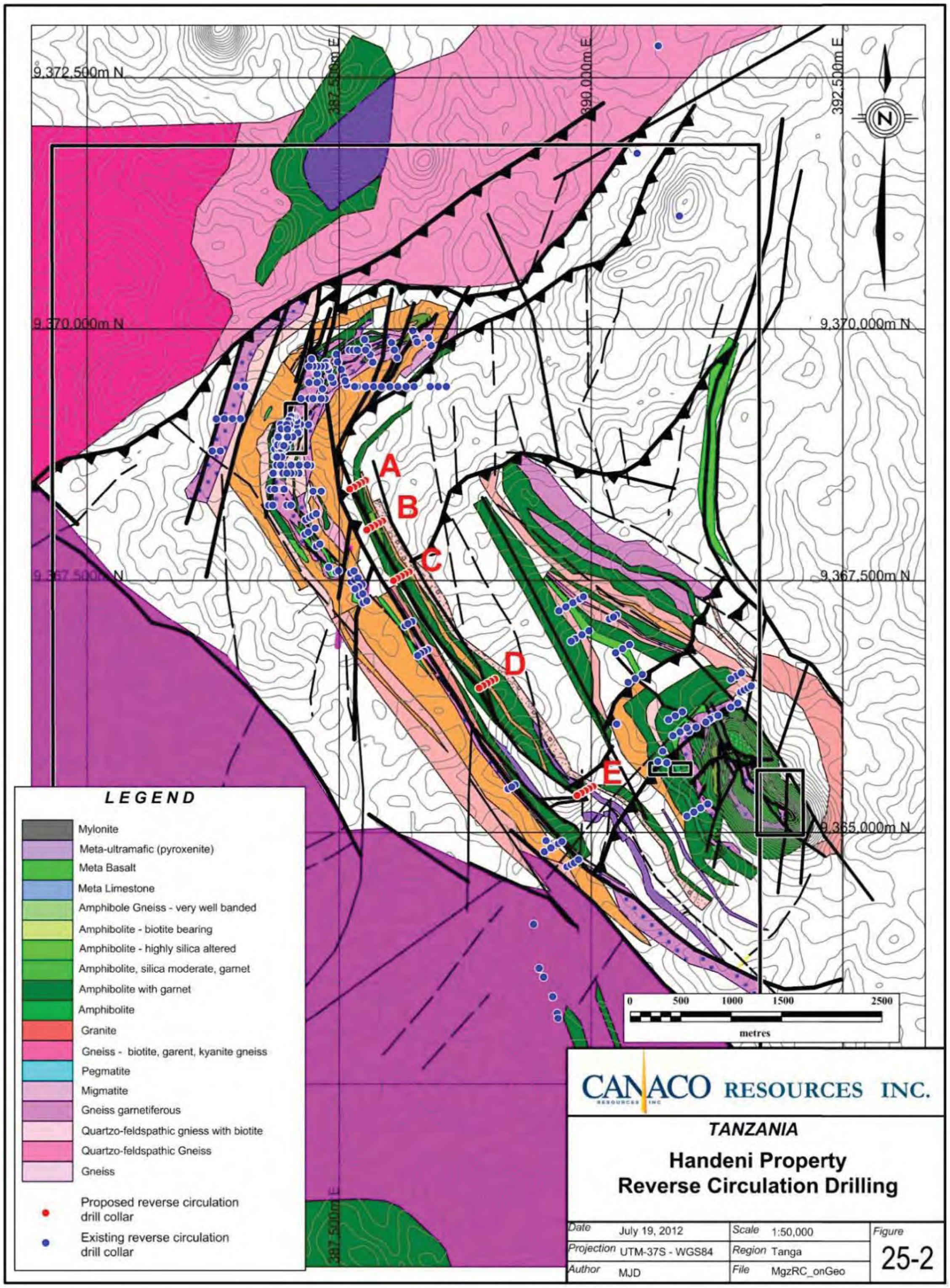
For the low-grade master composite, 96.4% of the gold was recovered into the combined gravity-flotation concentrate, and leaching this combined concentrate dissolved 95.5% of the contained gold, giving an overall gold recovery of 92.1%. Results for the high-grade master composites were similar, with 96.9% of the gold recovered into the combined gravity-flotation concentrate, and leaching this combined concentrate dissolving 95.0% of the contained gold, for an overall gold recovery of 92.1%.

Although these results are preliminary and should be substantiated by further testwork on the high-grade and low-grade composites representing Zones A through D, they are encouraging. This gravity-flotation-leach flowsheet may offer significant advantages from an environmental and waste management standpoint if it is possible to cyanide leach less than 10% of the process plant fresh feed and achieve gold recoveries over 90%.

Based on the results of the XRF trace element geochemistry study a revision of the geological model at Magambazi was required. The revised model attributes the presence of gold mineralisation within the GASIL unit to rheological contrasts. The GASIL unit likely represents the top of a differentiated basalt flow, which has undergone seafloor hydrothermal alteration, prior to being covered by a relatively impermeable sedimentary rock sequence consisting of shale, siltstone and sandstone. The brittle nature of the GASIL, combined with the impermeable overlying lithologies resulted in a highly favourable location for later gold-bearing mineralising fluids.

The exploration implications for the revised model suggest that additional exploration should focus on thick amphibolite (basalt) sequences which are overlain by paragneiss, and adjacent to observed or interpreted fault structures. Additional information such as soil anomalism, elevated gold concentrations in shallow RAB drilling samples, artisanal workings, or IP anomalies, could all act as vectors for the presence of gold mineralization. In order to test this exploration model limited drilling is recommend at five areas (A-E) to the west of Magambazi (Figure 25-2). Each area should have a fence of five holes drilled over the amphibolite unit (identified from airborne magnetic data and outcrop mapping), with targets A, D and E drilled first due to the proximity of artisanal gold workings in these areas. It is important that the amphibolite-paragneiss contact be tested since the uppermost part of the amphibolite is the target unit. If positive results are obtained then areas B and C should be drilled, with a second phase of diamond drilling to test tenor and continuity of mineralisation.

Figure 25-2: Location for proposed verification drilling



Source: Canaco, 2013.

25.2 Risks & Opportunities

This report is based on the best information and data available at the time of writing. However, certain reasonable assumptions and interpretations have been made to develop concepts and estimates that are included herein. With this in mind, certain risks, opportunities and uncertainties exist that may impact the geological interpretation, estimated mineral resource, metallurgical recoveries, capital cost, operating cost, prospects for economic viability and other aspects of the project. In particular, the following points highlight a variety of known and unknown risks, uncertainties and other factors that could cause actual events or results to differ from those expressed or implied by the forward-looking statements in this report.

In general, such factors could include uncertainty of future development of, or production at, the Magambazi area. Risks and uncertainties associated with new mining ventures are as follows:

- risks and uncertainties relating to the interpretation of, and statistical inferences drawn from drill results, sampling, geologic interpretation, grade and continuity of the Magambazi mineral deposit
- risks related to governmental regulations, including environmental regulations
- risks related to the delay in obtaining, or failure to obtain or maintain required land access agreements and permits, or non-compliance with land access agreements and permits
- increased costs and restrictions on a Magambazi operation due to compliance with environmental laws and regulations
- risks related to reclamation activities
- uncertainties related to title and surface rights to the Magambazi property
- risks related to political instability and unexpected regulatory change
- currency fluctuations
- difficulty in recruitment and retention of skilled, qualified personnel and management for the mineral project development and eventual operation of a mine
- project delays and operational issues
- risks related to Canaco's ability to obtain adequate financing for further development
- commodity price fluctuations
- risks related to general economic conditions
- increased costs affecting the mineral exploration and mining industry
- risks associated with labour unrest or strikes
- risks pertaining to the sale of materials produced on site
- risks related to the taxation of profits earned at an eventual operation
- risks related to unjustified PLs and PMLs
- unpredictable risks and hazards related to the development and operation of a mine or mine property that are beyond Canaco's control.

In particular, the project group has identified the factors in the following section as being particularly noteworthy in terms of potentially affecting Magambazi development.

25.2.1 Risks & Uncertainties

During the course of the exploration, mineral resource estimation and metallurgical testwork, the project team identified the following risks that may have a negative impact on the project.

- Political and Community Risk - Political uncertainty associated with project stakeholders is a potential risk. While Canaco is working closely with all stakeholders, opposition to the project by one or several parties could delay further exploration, development, construction or metal production from the project, if the project is judged viable at a future development stage. An ongoing dialogue with all stakeholders and a community relations approach is being planned to mitigate this risk.
- Staffing, Competition & Commercial Risk - Risks at Handeni associated with establishment and ongoing mineral exploration/development operations, including competition, are typical for any new mining venture. Competition will exist in the workplace for skilled workers. The remote location and country risks may further impact this project's ability to attract and retain qualified technical and non-technical staff.
- The Permitting and Government Approval Process - In Tanzania the permitting and approval process can be lengthy. Canaco has indicated that their Executive has experience in permitting projects in developing nations, and has begun addressing this potential issue through submission of a Tanzanian EIA application that is currently under review.
- Project Development Financing – Financing can be more difficult when developing an international project in a developing country. Canaco has addressed this potential issue early by initiating baseline environmental and socioeconomic work, with the aim of producing an EIA compatible with International Finance Committee requirements.

25.2.2 Opportunities

During the course of the exploration, mineral resource estimation and metallurgical testwork, the project group identified opportunities that may have a positive impact on the project.

- Geological Model Refinement – An enhanced understanding of the mineralisation at Magambazi and its relationship to observed geological controls could benefit on-going exploration on the Handeni Property through the identification of new targets, and the resource model through the refinement of geological constraints.
- Resolution of QA/QC Issues – A significant proportion of the inferred resource category was downgraded from indicated based on the influence of unresolved QA/QC issues. Resolution of these issues through re-assaying will increase the confidence in the associated gold assays thereby allowing affected resource blocks to be upgraded from inferred to indicated category.

26 RECOMMENDATIONS

It is recommended that the path forward for the Handeni/Magambazi project should include the following main activities during the next phases of the project:

Phase I

Conducting detailed geochemistry on existing core samples, and carrying out drilling in new target areas based on an updated geological model. This program will include:

- Niton handheld XRF data collection on existing drill core pulps at Magambazi and Kwadijava should be performed to determine the geochemical signatures for mineralisation and protolith determination. This information will be used to target mineralisation on the Handeni licences and other Canaco-owned properties in eastern Tanzania. It is anticipated that this work will take approximately two to three months to complete.
- Three RC drilling fences (totaling 2250 m) should be drilled on the western side of Magambazi Hill, approximately from Kuta to Kwadijava, to test a gold target characterized by: a pronounced magnetic high; the presence of NW-SE trending faults; anomalous gold concentration detected in shallow (<20 m) RAB drilling; and the presence of artisanal workings. The purpose of this drilling is to target a thick amphibolite sequence (mafic lava), associated with overlying paragneiss that is cut by later mineralising faults.

Phase II

Conducting additional RC drilling and subsequent diamond drilling in identified areas of interest, further metallurgical testwork, and an engineering and project assessment study based on a revised resource estimate. This program will include:

- Two additional infill RC fences should be drilled if the initial RC drilling program results are encouraging.
- Any targets that produce encouraging grades and intervals during RC drilling (Phase I) should be followed-up with a four hole diamond drill program to refine the geological information and test the tenor and continuity of mineralisation. This drilling is contingent on the RC drilling results (Phase I).
- Further metallurgical testwork should be undertaken to investigate:
    - opportunities for reduction of cyanide consumption
    - incorporation of flotation in the process flowsheet

- improvement in the understanding of differences observed between composite grades predicted from drill core assays and those back-calculated from metallurgical results

- An update to the resource estimate should be carried out incorporating the 44 drillholes which occur in the resource outline but are excluded from the current resource estimation.
- An Engineering and Project Assessment that involves the continuation of initial trade-off studies, evaluation and development of a program to address grade discrepancies, possible bulk sampling, and expanding land permit.

In total, the cost of this work is expected to be up to approximately $1,459,000. A summary of the expenditure break-down is presented in Table 26-1.

Table 26.1: Summary of Expenditure

Proposed Work (Phase I)	Cost per Unit	Cost ($US)
Magambazi - Kwadijava RC drilling program (2,250 m; 15 holes; 2,250 samples)	$100 per meter; $25 per sample assay	281,250
Additional XRF analysis (25,000 m; 50 holes; 50,000 readings) and Au assay geochemical sampling (2,000 samples) and integration with previous results (20 days)	60 days @ $500 per day; $25 per sample; 20 days @ $1000 per day	100,000
Subtotal		**381,250**
Proposed Work (Phase II)		**Cost ($US)**
Magambazi - Kwadijava RC drilling program (1500 m; 10 holes; 1,500 samples)	$100 per meter; $25 per sample assay	187,500
Diamond drilling (600 m; 4 holes; 1,200 samples)	$250 per meter; $42 per sample Au+42 element assay	200,400
Metallurgical test work and reports	$150,000 per comprehensive test program	150,000
Updated resource estimation and report writing	25 days @ $1,600 per day	40,000
Engineering and Project Assessment (including bulk sampling)	180 days @ $2,778 per day	500,000
Subtotal		**1,077,900**
Total expenditure		**1,459,150**

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Appendix A

Reverse Circulation & Diamond Drilling Results

Table A.1. Reverse Circulation (RC) Drillholes in the Handeni Property

HOLE ID	Easting	Easting	Azimuth (°)	Dip (°)	Total Depth (m)	Max. Au (ppm)	PROSPECT
MGZC001	386910	9368901	99	-55	110	6.47	Kwadijava
MGZC002	386870	9368900	90	-55	162	0.07	Kwadijava
MGZC003	386912	9368982	102	-55	91	0.47	Kwadijava
MGZC007	386881	9368820	100	-55	90	2.81	Kwadijava
MGZC008	386862	9368820	100	-55	120	0.02	Kwadijava
MGZC009	386863	9368740	100	-55	84	4.08	Kwadijava
MGZC012	386931	9368420	100	-55	126	2.11	Kwadijava
MGZC013	386980	9368260	95	-55	186	0.37	Kwadijava
MGZC014	387020	9368260	270	-55	186	0.18	Kwadijava
MGZC015	386953	9368420	270	-55	132	0.87	Kwadijava
MGZC016	386950	9368820	270	-55	80	0.77	Kwadijava
MGZC017	386977	9368837	270	-55	84	0.30	Kwadijava
MGZC018	386999	9368903	277	-55	126	0.88	Kwadijava
MGZC019	386995	9368979	280	-55	80	0.47	Kwadijava
MGZC020	386873	9368581	270	-55	150	0.11	Kwadijava
MGZC021	390708	9365817	0	-90	93	0.09	Magambazi Flats
MGZC022	390663	9372826	0	-90	101	-	Far North
MGZC023	390748	9365700	0	-90	100	1.34	Magambazi Flats
MGZC024	390659	9365712	0	-90	106	**1.05**	Magambazi Flats
MGZC025	390251	9366087	0	-90	155	0.12	Magambazi Flats
MGZC026	391453	9366295	0	-90	150	**0.07**	Magambazi Flats
MGZC027	391384	9366255	0	-90	127	**0.09**	Magambazi Flats
MGZC028	391086	9365252	0	-90	150	**0.07**	Kuta
MGZC029	391155	9365292	0	-90	200	**0.07**	Kuta
MGZC030	391017	9365212	0	-90	146	**0.09**	Kuta
MGZC031	390947	9365172	0	-90	150	**0.04**	Kuta
MGZC032	387240	9368400	273	-55	225	0.33	Kwadijava
MGZC033	387320	9368400	273	-55	115	0.08	Kwadijava
MGZC034	387194	9367993	240	-55	140	**0.13**	Kwadijava South
MGZC035	387159	9367974	240	-55	91	**0.1**	Kwadijava South
MGZC036	387261	9368033	240	-55	160	**0.15**	Kwadijava South
MGZC037	387274	9367855	240	-55	145	0.47	Kwadijava South
MGZC038	387307	9367875	240	-55	150	**0.51**	Kwadijava South
MGZC039	387469	9367597	243	-55	150	1.46	Kwadijava South
MGZC040	387492	9367611	240	-55	200	8.44	Kwadijava South
MGZC041	391206	9366152	0	-90	200	**0.12**	Magambazi Flats
MGZC042	391175	9366136	0	-90	140	**0.06**	Magambazi Flats
MGZC043	391257	9366173	0	-90	150	**0.08**	Magambazi Flats
MGZC044	391135	9366107	0	-90	150	**0.06**	Magambazi Flats
MGZC045	391038	9366055	0	-90	150	**0.11**	Magambazi Flats
MGZC046	390968	9366015	0	-90	150	**0.05**	Magambazi Flats
MGZC047	389481	9363661	0	-90	123	0.24	Magambazi West
MGZC048	386930	9368941	90	-55	78	4.72	Kwadijava
MGZC049	386937	9368975	98	-55	75	5.97	Kwadijava
MGZC050	386942	9369020	96.5	-54.5	75	15.50	Kwadijava
MGZC051	386956	9368899	259	-55.5	65	6.25	Kwadijava
MGZC052	386963	9368938	264	-56.5	63	2.21	Kwadijava
MGZC053	386973	9368980	266.5	-54	63	7.10	Kwadijava
MGZC054	386979	9369009	263	-56.5	57	13.80	Kwadijava
MGZC055	386996	9369065	264	-56.5	45	1.81	Kwadijava
MGZC056	387007	9369101	270	-55	33	2.00	Kwadijava
MGZC057	387037	9369104	270	-55	33	0.82	Kwadijava
MGZC058	387040	9369061	269	-55.5	81	0.21	Kwadijava
MGZC059	387120	9369320	269.5	-60	136	0.33	Majiri
MGZC060	386978	9368654	266	-55	135	1.09	Kwadijava
MGZC061	387064	9368659	269	-57	153	2.57	Kwadijava
MGZC062	387139	9368660	266.5	-55.5	126	0.09	Kwadijava
MGZC063	387217	9368657	265	-55	144	0.20	Kwadijava
MGZC064	387115	9369064	265.5	-58	159	0.33	Kwadijava

HOLE ID	Easting	Easting	Azimuth (°)	Dip (°)	Total Depth (m)	Max. Au (ppm)	PROSPECT
MGZC065	387196	9369061	268	-58.5	159	0.62	Kwadijava
MGZC066	387394	9367647	239	-55.5	80	0.53	Kwadijava South
MGZC067	387360	9369320	268.5	-63	181	0.43	Majiri
MGZC068	387320	9369320	270	-61	151	1.21	Majiri
MGZC069	387280	9369320	274	-61.5	135	2.89	Majiri
MGZC070	387200	9369320	272	-63	120	0.72	Majiri
MGZC071	387241	9369672	338	-61.5	74	0.25	Majiri
MGZC072	387266	9369602	338.5	-60.5	75	0.84	Majiri
MGZC073	387252	9369640	341	-60	62	0.54	Majiri
MGZC074	387279	9369565	341	-62.5	81	0.26	Majiri
MGZC075	387307	9369489	337	-58.5	105	0.23	Majiri
MGZC076	387433	9369492	338	-58.5	141	3.53	Majiri
MGZC077	387334	9369415	0	-90	136	2.51	Majiri
MGZC078	387365	9369679	340	-62	62	0.63	Majiri
MGZC079	387378	9369642	343	-59.5	75	0.62	Majiri
MGZC080	387470	9369762	345	-62	69	0.32	Majiri
MGZC081	387484	9369684	341.5	-62	81	0.19	Majiri
MGZC082	387518	9369609	342	-78.5	120	0.23	Majiri
MGZC083	387546	9369535	341	-59.5	160	2.66	Majiri
MGZC084	387751	9369905	350.5	-61.5	120	0.67	Majiri
MGZC085	387778	9369831	340.5	-63.5	73	0.38	Majiri
MGZC086	387806	9369756	339	-60.5	97	0.36	Majiri
MGZC087	387833	9369681	314.5	-61	120	1.75	Majiri
MGZC088	388017	9369876	339	-60.5	63	0.18	Majiri
MGZC089	388045	9369801	338	-62	90	0.66	Majiri
MGZC090	388072	9369725	314.5	-63.5	84	0.6	Majiri
MGZC091	388229	9369995	341	-61.5	39	0.08	Majiri
MGZC092	388243	9369957	338	-62	54	0.54	Majiri
MGZC093	388257	9369920	338.5	-60	60	0.18	Majiri
MGZC094	388270	9369883	337.5	-61.5	60	0.28	Majiri
MGZC095	388383	9369924	338	-56.5	46	0.67	Majiri
MGZC096	388410	9369849	340.5	-65	60	0.49	Majiri
MGZC097	387169	9368117	239.5	-56.5	105	0.73	Kwadijava South
MGZC098	387203	9368137	235	-57	128	0.63	Kwadijava South
MGZC099	387238	9368157	235	-56	135	0.33	Kwadijava South
MGZC100	387273	9368177	230	-56.5	153	0.36	Kwadijava South
MGZC101	389525	9363574	0	-90	153	0.12	Magambazi West
MGZC102	386910	9368860	98.5	-59	81	1.81	Kwadijava
MGZC103	386956	9369063	94	-55.5	51	0.08	Kwadijava
MGZC104	386917	9369062	93	-57	60	0.08	Kwadijava
MGZC105	387076	9369059	266	-58	80	0.36	Kwadijava
MGZC106	386902	9368820	96	-58	90	0.93	Kwadijava
MGZC107	386920	9368825	116	-55	91	0.70	Kwadijava
MGZC108	387091	9368979	265	-55	81	0.58	Kwadijava
MGZC109	390874	9371136	0	-90	128	0.13	Far North
MGZC110	390454	9371757	0	-90	95	0.18	Far North
MGZC111	386891	9368740	98.5	-57.5	94	0.95	Kwadijava
MGZC112	386912	9368740	99	-57	87	1.10	Kwadijava
MGZC113	386930	9368740	99	-55	99	0.75	Kwadijava
MGZC114	386889	9368860	95.5	-57	75	0.42	Kwadijava
MGZC115	386930	9368860	97	-58.5	93	3.14	Kwadijava
MGZC116	386895	9368900	96.5	-53	75	0.61	Kwadijava
MGZC117	386930	9368900	98.5	-55	81	3.45	Kwadijava
MGZC118	386910	9368940	98.5	-57.5	75	4.33	Kwadijava
MGZC119	386924	9369020	100	-54.5	63	0.32	Kwadijava
MGZC120	386900	9368580	267.5	-58.5	64	0.11	Kwadijava
MGZC121	386920	9368580	268	-57.5	72	0.26	Kwadijava
MGZC122	386940	9368580	263	-57	78	0.15	Kwadijava
MGZC123	386980	9368580	265	-54.5	96	0.14	Kwadijava
MGZC124	387020	9368580	266.5	-55.5	120	1.65	Kwadijava
MGZC125	387100	9368580	268	-58.5	106	0.43	Kwadijava

HOLE ID	Easting	Easting	Azimuth (°)	Dip (°)	Total Depth (m)	Max. Au (ppm)	PROSPECT
MGZC126	387022	9368660	265	-56.5	94	0.50	Kwadijava
MGZC127	387102	9368660	268.5	-55.5	120	0.36	Kwadijava
MGZC128	387183	9368660	270	-59.5	152	0.20	Kwadijava
MGZC129	386880	9368660	268.5	-56	54	0.98	Kwadijava
MGZC130	386901	9368660	268.5	-56	60	0.34	Kwadijava
MGZC131	386918	9368660	267	-58	54	0.14	Kwadijava
MGZC132	387040	9368940	255.5	-57.5	78	0.22	Kwadijava
MGZC133	387613	9367588	238.5	-55	120	0.02	Kwadijava South
MGZC134	387647	9367608	242.5	-57	132	0.02	Kwadijava South
MGZC135	387618	9367499	238.5	-55	72	0.06	Kwadijava South
MGZC136	387653	9367519	241.5	-54	83	0.53	Kwadijava South
MGZC137	387687	9367539	240.5	-53.5	120	0.02	Kwadijava South
MGZC138	387727	9367470	241.5	-53.5	132	0.17	Kwadijava South
MGZC139	387693	9367450	237	-54.5	120	0.29	Kwadijava South
MGZC140	387658	9367430	237.5	-56	80	1.82	Kwadijava South
MGZC141	387698	9367360	235.5	-57.5	111	0.10	Kwadijava South
MGZC142	387733	9367380	238.5	-55	121	0.02	Kwadijava South
MGZC143	387738	9367291	240	-56.5	126	0.01	Kwadijava South
MGZC144	387773	9367311	241	-55	156	0.03	Kwadijava South
MGZC145	389426	9364099	0	-90	130	0.037	Magambazi West
MGZC146	389426	9364099	0	-90	100	0.013	Magambazi West
MGZC147	389617	9363378	0	-90	120	0.01	Magambazi West
MGZC148	389661	9363213	0	-90	120	0.007	Magambazi West
MGZC148A	389669	9363164	0	-90	28	0.005	Magambazi West
MGZC149	387080	9369100	277.5	-59	75	0.33	Kwadijava
MGZC150	387060	9369140	277	-53.5	81	0.14	Kwadijava
MGZC151	387040	9369140	274	-57.5	63	0.12	Kwadijava
MGZC152	387020	9369140	271	-55	60	0.07	Kwadijava
MGZC153	387017	9369100	270	-56.5	70	9.63	Kwadijava
MGZC154	386997	9369100	270.5	-54.5	70	0.15	Kwadijava
MGZC155	386980	9369060	276.5	-52.5	70	1.47	Kwadijava
MGZC156	387010	9369060	271	-53	45	4.51	Kwadijava
MGZC157	386895	9368940	94	-55.5	75	0.12	Kwadijava
MGZC158	386987	9369017	266.5	-56	63	9.23	Kwadijava
MGZC159	386987	9368938	267	-53.5	69	0.80	Kwadijava
MGZC160	386950	9368854	98.5	-55	87	1.05	Kwadijava
MGZC161	386880	9368740	96.5	-52	81	18.80	Kwadijava
MGZC162	386320	9368800	242	-57	159	0.383	Kiajani
MGZC163	386240	9368800	239	-56	105	0.029	Kiajani
MGZC164	386560	9369440	237.5	-59.5	153	0.092	Kiajani
MGZC165	386480	9369440	238.5	-55	159	0.382	Kiajani
MGZC166	386520	9369120	237.5	-56.5	171	0.101	Kiajani
MGZC167	386440	9369120	238.5	-55.5	153	0.78	Kiajani
MGZC168	386800	9368260	267.5	-58.5	33	0.01	Kwadijava
MGZC169	386840	9368260	270.5	-57.5	33	0.02	Kwadijava
MGZC170	386820	9368420	270	-55.5	45	0.17	Kwadijava
MGZC171	386860	9368420	271.5	-58	51	0.57	Kwadijava
MGZC172	386845	9368580	272.5	-56	45	0.02	Kwadijava
MGZC173	387050	9368580	274	-57	99	1.59	Kwadijava
MGZC174	387200	9369480	272.5	-52	75	0.108	Majiri
MGZC175	387280	9369480	275	-56.5	87	0.144	Majiri
MGZC176	387440	9369480	272.5	-57	135	1.575	Majiri
MGZC177	387419	9369530	336.5	-63	117	0.69	Majiri
MGZC178	387392	9369606	338.5	-62	81	0.683	Majiri
MGZC179	387360	9369640	273.5	-55	75	0.203	Majiri
MGZC180	387320	9369640	271	-57	63	0.685	Majiri
MGZC181	387280	9369640	273	-58	63	1.725	Majiri
MGZC182	387240	9369640	272	-56	53	0.25	Majiri
MGZC183	387200	9369640	270	-57	39	0.374	Majiri
MGZC184	387240	9369320	271	-62.5	117	0.182	Majiri
MGZC185	387573	9369459	345	-63.5	57	0.011	Majiri

HOLE ID	Easting	Easting	Azimuth (°)	Dip (°)	Total Depth (m)	Max. Au (ppm)	PROSPECT
MGZC186	387560	9369496	344	-64.5	111	0.215	Majiri
MGZC187	387225	9369715	340.5	-59.5	57	0.064	Majiri
MGZC188	387680	9369440	271	-55.5	106	0.082	Majiri
MGZC189	387760	9369440	243.5	-57	69	0.089	Majiri
MGZC190	387840	9369440	273	-52	45	0.055	Majiri
MGZC191	387920	9369440	273.5	-53.5	57	0.033	Majiri
MGZC192	388000	9369440	276.5	-53	51	0.022	Majiri
MGZC193	388080	9369440	272	-53.5	57	0.04	Majiri
MGZC194	388160	9369440	274	-56	75	0.057	Majiri
MGZC195	388240	9369440	272	-54.5	93	0.049	Majiri
MGZC196	387653	9369440	271.5	-55	111	0.077	Majiri
MGZC197	388400	9369440	274.5	-53	153	0.047	Majiri
MGZC198	388480	9369440	276	-58.5	170	0.064	Majiri
MGZC199	388560	9369440	267.5	-57.5	171	0.006	Majiri
MGZC200	387600	9369800	266	-57.5	105	0.437	Majiri
MGZC201	387640	9369800	270	-59.5	105	0.329	Majiri
MGZC202	387680	9369800	272	-58	117	0.308	Majiri
MGZC203	387760	9369800	268.5	-56	140	0.725	Majiri
MGZC204	390505	9366579	65.5	-62.5	165	0.111	Bahati
MGZC205	389838	9366933	61.5	-55	165	0.219	Bahati
MGZC206	389907	9366973	55.5	-57.5	177	0.024	Bahati
MGZC207	389977	9367013	57	-55.5	135	0.016	Bahati
MGZC208	390180	9367130	242	-57	159	0.018	Bahati
MGZC209	390250	9367170	243	-58.5	105	0.006	Bahati
MGZC210	390220	9367150	241	-57	140	0.013	Bahati
MGZC211	389800	9366910	243	-55	117	0.029	Bahati
MGZC212	390435	9366539	60	-55	141	0.056	Bahati
MGZC213	390366	9366499	60	-55	159	0.074	Bahati
MGZC214	390241	9366796	60	-55	147	2.61	Bahati
MGZC215	390310	9366836	60	-55	162	0.088	Bahati
MGZC216	390379	9366876	60	-55	145	0.07	Bahati
MGZC217	389817	9367290	60	-55	141	0.04	Bahati
MGZC218	389886	9367330	60	-55	141	0.057	Bahati
MGZC219	389921	9367350	60	-55	139	0.066	Bahati
MGZC220	389747	9367250	60	-55	172	0.035	Bahati
MGZC221	389678	9367210	60	-55	171	0.089	Bahati
MGZC222	391483	9366405	60	-55	147	0.012	Junction
MGZC223	391517	9366425	60	-55	155	0.11	Junction
MGZC224	391552	9366445	60	-55	153	3.13	Junction
MGZC225	391587	9366465	60	-55	150	0.012	Junction
MGZC226	391489	9366593	60	-55	150	0.017	Junction
MGZC227	391437	9366563	60	-55	150	0.026	Junction
MGZC228	391385	9366533	60	-55	150	0.026	Junction
MGZC229	390903	9366209	240	-55	165	0.018	Magambazi Flats
MGZC230	390834	9366169	240	-55	135	0.019	Magambazi Flats
MGZC231	390765	9366129	240	-55	130	0.062	Magambazi Flats
MGZC232	390810	9365970	240	-55	144	0.035	Magambazi Flats
MGZC233	390879	9366010	240	-55	164	0.062	Magambazi Flats
MGZC234	390949	9366050	240	-55	165	0.02	Magambazi Flats
MGZC235	390708	9365817	0	-90	90	0.16	Magambazi Flats
MGZC235A	390708	9365817	0	-90	25		Magambazi Flats
MGZC236	389244	9365482	60	-55	150	0.35	MK South
MGZC237	389210	9365462	60	-55	159	1.63	MK South
MGZC238	389175	9365442	568	-55	163	0.64	MK South
MGZC239	389604	9364858	60	-55	153	0.49	MK South
MGZC240	389639	9364878	60	-55	153	0.2	MK South
MGZC241	389674	9364898	60	-55	141	0.41	MK South
MGZC242	389708	9364918	60	-55	123	0.47	MK South
MGZC243	389535	9364819	60	-55	171	0.23	MK South
MGZC244	389759	9364670	60	-55	170	0.29	MK South
MGZC245	389799	9364690	60	-55	159	2.75	MK South

HOLE ID	Easting	Easting	Azimuth (°)	Dip (°)	Total Depth (m)	Max. Au (ppm)	PROSPECT
MGZC246	389831	9364707	60	-55	111	0.92	MK South
MGZC247	389600	9364856	60	-60	174	1.39	MK South
MGZC248	389551	9364928	60	-55	157	0.41	MK South
MGZC249	389872	9364740		-90	120	1.09	MK South
MGZC250	388149	9367063	240	-55	81	0.17	Kwadijava South
MGZC251	388219	9367104	240	-55	140	1.52	Kwadijava South
MGZC252	388376	9366827	240	-55	116	0.26	Kwadijava South
MGZC253	388342	9366810	240	-55	117	0.39	Kwadijava South
MGZC254	388306	9366789	240	-55	113	0.12	Kwadijava South
MGZC255	388276	9366770	240	-55	145	0.16	Kwadijava South
MGZC256	388180	9367085	240	-55	120	0.13	Kwadijava South
MGZC257	386360	9369120	270	-55	150	1.59	Kiajani
MGZC258	386279	9369118	270	-55	100	0.32	Kiajani

All maximum Au concentrations over 1 m intervals except those in bold, which are over 4 m. A blank value in this column means the assay has not been released.

Table A.2. Diamond Drilling Conducted at the Magambazi deposit, Handeni Property

Hole ID		From (m)	To (m)	Interval (m)	Au (g/t)	Local Azimuth	Dip
MGZD001		113.0	118.0	5.0	1.8†	90.0	-50.0
		148.0	207.0	59.0	4.28		
	including	154.0	166.0	12.0	4.18		
	including	189.0	206.0	17.0	10.39		
MGZD002		239.0	242.0	3.0	1.53	90.0	-75.0
		255.0	272.6	17.6	0.93		
MGZD003		218.2	219.2	1.0	4.80	90.0	-61.0
MGZD004		110.0	137.0	27.0	2.82	90.0	-50.0
	including	113.0	120.5	7.5	2.85		
	including	127.0	137.0	10.0	5.15		
MGZD005		128.0	169.0	41.0	3.32	90.0	-65.0
	including	128.0	144.0	16.0	3.34		
	including	161.0	169.0	8.0	9.95		
MGZD006		157.0	160.76	3.76	1.31†	90.0	-50.0
		200.7	202.00	1.30	3.02		
MGZD007		156.6	196.2‡	39.61	3.55*	90.0	-79.0
	including	156.6	170.13‡	13.50	4.01		
	including	184.0	196.21‡	12.21	6.99		
MGZD008		55.0	71.0	16.0	1.47†	90.0	-50.0
		90.0	93.6	3.6	5.65†		
		119.0	136.7	17.7‡	0.83†		
	including	119.0	122.3	3.3	1.99†		
MGZD009		61.0	66.0	5.0	1.55†	90.0	-73.0
		175.0	177.7	2.7	10.95		
		216.0	226.7	10.7	1.45†		
MGZD010		81.0	90.0	9.0	1.13	89.0	-50.0
MGZD011		139.0	181.1	42.1	2.42	90.0	-48.0
	including	139.0	146.0	7.0	1.37		
	including	157.3	181.1	23.8	3.86		
MGZD012		170.8	227.0	56.2	6.38*	90.0	-59.0
	including	170.8	189.0	18.2	7.94*		
	including	196.0	226.0	30.0	6.99*		
MGZD013		175.0	178.0	3.0	1.26	92.0	-65.0
MGZD014		41.0	46.0	5.0	1.53	87.0	-61.5
		160.0	161.0	1.0	7.55		
MGZD015		149.0	154.0	5.0	2.10	87.0	-73.0
		200.0	210.0	10.0	2.76		
MGZD016		124.0	148.0	24.0	1.72†	87.0	-81.0
	including	135.0	140.0	5.0	5.17		
		170.0	172.0	2.0	2.13†		
		236.7	246.0	9.3	3.72†		
	including	240.7	246.0	5.3	5.86		
	including	240.7	244.2	3.5	8.30		
MGZD017		94.0	99.0	5.0	3.07	87.0	-81.0
MGZD018		21.0	24.7	3.7	2.25	10.0	-50.0
MGZD019		70.0	88.0	18.0	2.48*	267.0	-50.0
	including	70.0	78.0	8.0	3.82*		
		100.0	103.0	3.0	3.04		
MGZD020		63.0	63.7	0.7	4.00	30.0	-90.0
MGZD021		158.0	166.1	8.1	0.53	103.0	-51.0
		216.0	217.0	1.0	22.4†		
MGZD022		150.0	158.0	8.0	1.10	92.0	-65.0
MGZD023		22.0	27.4	5.4	1.44	267.0	-55.0
		54.7	85.0	30.3	3.47*		
	including	70.0	76.3	6.3	5.61*		
MGZD024		64.4	72.4	8.0	3.25	267.0	-55.0
MGZD025		41.4	52.6	11.2	1.33	267.0	-55.0
		75.0	87.0	12.0	2.65		
MGZD026		87.7	95.7	8.0	1.73	267.0	-55.0
MGZD027		99.0	126.7	27.7	2.18	267.0	-55.0
	including	99.0	106.4	7.4	4.05		

Hole ID		From (m)	To (m)	Interval (m)	Au (g/t)	Local Azimuth	Dip
MGZD028		180.0	191.0	11.0	2.03	275.0	-55.0
		200.0	202.1	2.1	5.58		
MGZD029		169.0	182.6	13.6	1.71	275.0	-55.0
	including	177.0	182.6	5.6	3.27		
MGZD030	No significant results					270.0	-55.0
MGZD031		82.0	84.4	2.4	10.18	275.0	-55.0
MGZD032		73.0	83.1	10.1	1.23	275.0	-55.0
MGZD033		42.0	44.8	2.8	1.60	275.0	-55.0
MGZD034		43.0	58.4	15.4	1.85	275.0	-55.0
MGZD035		166.0	176.5	10.5	2.40	90.0	-55.6
	including	168.1	174.4	6.3	3.12		
		201.0	217.0	16.0	5.46		
	including	206.7	216.1	9.4	8.59		
MGZD036		202.0	207.4	5.4	5.10	90.0	-63.0
		219.0	267.0	48.0	2.67		
	including	224.0	231.0	7.0	6.21		
		240.4	254.04‡	13.64‡	4.54		
MGZD037		132.0	136.0	4.0	1.04	90.0	-72.0
MGZD038		219.7	235.0	15.3	1.87	90.0	-65.0
	including	219.7	226.4	6.7	2.64		
	including	229.9	232.0	2.1	4.07		
MGZD039		199.0	202.5	3.5	1.69	90.0	-71.0
		233.3	249.2	15.9	2.00		
	including	233.3	238.0	4.7	3.47		
	including	245.0	249.2	4.2	3.12*		
MGZD040		102.0	136.6	34.6	1.36	90.0	-90.0
	including	103.0	115.0	12.0	2.83		
	including	106.0	109.5	3.5	7.71		
		211.0	214.8	3.8	19.83		
MGZD041		191.0	198.0	7.0	4.71	98.0	-79.0
		228.4	233.7	5.3	1.74		
		278.0	280.1	2.1	2.85		
MGZD042		178.7	186.7	8.0	3.80	90.0	-58.0
		198.0	205.7	7.7	5.42		
		226.0	241.7‡	15.7‡	2.01*		
	including	226.0	230.2	4.2	5.87		
MGZD043		149.7	159.9	10.2	2.87	101.0	-75.0
		224.0	227.8	3.8	3.36		
		247.0	268.2	21.2	4.80		
	including	247.0	258.0	11.0	7.90		
MGZD044		153.0	157.0	4.0	2.85†	90.0	-68.0
		261.4	281.0	19.6	2.42*		
	including	261.4	272.9	11.5	3.21*		
MGZD045		246.0	267.7	21.7	6.66*	90.0	-81.5
	including	246.0	255.5	9.5	12.45*		
MGZD046		138.7	144.7	6.0	0.68	90.0	-64.5
MGZD047	No significant results					95.0	-62.4
MGZD048		109.0	169.0	60.0	1.67	93.0	-74.0
	including	109.0	132.5	23.5	2.86		
MGZD049		146.1	147.7	1.6	1.72	94.0	-85.0
MGZD050	No significant results					270.0	-75.0
MGZD051		14.0	24.4	10.4	1.18	273.0	-73.0
MGZD052		39.7	50.0	10.3	1.99	267.0	-69.5
	including	39.7	41.1	1.4	12.12		
MGZD053		52.0	85.0	33.0	3.39	265.0	-74.5
	including	70.8	80.7	9.9	6.25		
MGZD054		33.7	40.0	6.3	0.92	272.0	-57.0
		55.0	70.0	15.0	1.29		
MGZD055		21.7	34.1	12.4	0.97*	271.0	-62.0
		47.0	69.0	22.0	1.22		
MGZD056		8.0	13.0	5.0	0.89	269.0	-55.0
		42.0	66.4	24.4	1.37*		
	including	42.0	53.1	11.1	2.29		
MGZD057	No significant results					275.0	-85.0

Hole ID		From (m)	To (m)	Interval (m)	Au (g/t)	Local Azimuth	Dip
MGZD058		33.0	50.0	17.0	0.76	360.0	-89.0
	including	45.4	50.0	4.6	1.56		
MGZD059		129.0	132.0	3.0	9.44	268.0	-41.0
MGZD060		82.0	89.4	7.4	2.32	270.0	-55.0
MGZD061		54.0	59.0	5.0	1.43*	93.0	-74.6
MGZD062		100.0	122.4	22.4	0.99	88.0	-67.5
MGZD063		119.0	149.2	30.2	1.64	89.0	-79.5
MGZD064		269.0	271.0	2.4	1.36	91.0	-72.8
		257.0	259.1	2.1	1.60		
MGZD065	No significant results					90.0	-48.5
MGZD066		153.0	157.0	4.0	1.21†	90.0	-64.5
		230.0	267.0	37.0	12.45		
		244.0	267.0	23.0	19.14		
		276.0	278.0	2.0	7.83*		
MGZD067		54.7	123.0	68.3	1.90	90.0	-74.2
	including	99.7	113.0	13.3	4.35		
MGZD068		55.7	89.0	33.3	2.46	91.0	-80.5
	including	56.7	61.7	5.0	8.04		
		78.0	84.7	6.7	5.41		
MGZD069		85.0	91.0	6.0	1.36	94.5	-80.0
MGZD070		66.0	75.1	9.1	1.55	88.0	-49.5
	including	73.0	75.1	2.1	6.04		
MGZD071		122.4	134.3	11.9	2.44	262.0	-85.5
	including	128.7	133.6	4.9	3.33		
MGZD072		131.0	144.0	13.0	0.47	91.0	-44.5
	including	142.0	144.0	2.0	1.42		
MGZD073		138.4	148.9	10.5	1.22	93.0	-71.0
	including	140.5	148.2	7.7	1.55		
		182.0	214.0	32.0	9.27		
	including	196.0	212.4	16.4	17.56		
MGZD074		267.0	268.0	1.0	1.00	90.0	-89.0
MGZD075		188.0	207.0	19.0	1.03	90.0	-63.0
	including	204.0	207.0	3.0	3.12		
MGZD076		213.0	237.0	24‡	2.64*	90.0	-73.0
	including	223.7	231.0	7.3	5.70		
MGZD077		208.0	244.0	36.0	1.65	89.0	-78.0
	including	214.6	233.0	18.4	3.01		
	including	218.8	223.7	4.9	6.45		
MGZD078		143.0	145.0	2.0	7.45†	117.0	-89.0
		274.4	276.0	1.6	1.08		
MGZD079		226.0	253.0	27.0	4.29	92.0	-73.0
	including	239.0	253.0	14.0	6.21		
MGZD080		202.0	212.0	10.0	1.66	92.0	-66.0
MGZD081		146.7	152.7	6.0	0.93	90.0	-57.5
MGZD082		256.7	272.3	15.6	6.60	91.0	-67.0
	including	261.0	271.6	10.6	8.39		
MGZD083		91.0	108.0	17.0	24.96*	300.0	-89.0
	including	102.0	108.0	6.0	30.14*		
MGZD084		229.4	236.0	6.6	2.32†	90.0	-65.0
		248.0	254.0	6.0	1.68†		
		269.0	282.4	13.4	13.54		
	including	269.0	275.0	6.0	29.40		
MGZD085		128.0	129.0	1.0	2.09	90.0	-68.0
MGZD086		122.0	124.0	2.0	2.78†	89.0	-53.5
		150.0	155.0	5.0	5.38		
		218.0	223.0	5.0	1.34†		
MGZD087		197.0	226.0	29.0	1.18	96.5	-58.5
	including	197.0	212.0	15.0	1.99		
MGZD088		222.0	237.0	15.0	4.19	92.0	-70.5
	including	222.0	225.8	3.8	7.87†		
		264.0	275.2	11.2	4.03		
	including	264.7	268.2	3.5	6.97†		
MGZD089		208.0	211.5	3.5	4.84	92.0	-54.5
MGZD090		264.3	269.9	5.6	5.22	90.0	-72.0
MGZD091	No significant results					90.0	-45.0

Hole ID		From (m)	To (m)	Interval (m)	Au (g/t)	Local Azimuth	Dip
MGZD092	No significant results					90.0	-67.0
MGZD093		205.9	236.0	30.1	1.55	89.0	-60.5
MGZD094		89.0	91.0	2.0	1.77†	92.0	-78.0
		119.0	121.0	2.0	2.3†		
MGZD095		139.0	144.0	5.0	1.47†	92.0	-56.5
		159.0	167.4	8.4	1.73†		
MGZD096		141.0	189.6	48.6	14.81	87.0	-54.0
	including	141.0	153.0	12.0	1.55		
	including	172.8	189.6	16.8	41.51		
		180.5	188.9	8.4	80.90		
MGZD097		244.0	261.1	17.1	1.44	88.5	-78.0
MGZD098		142.0	143.0	1.0	19.8†	90.5	-61.5
		203.2	256.4	53.2	9.51		
	including	231.2	255.0	23.8	15.08		
MGZD099		180.0	184.5	4.5	2.46	88.0	-61.0
		224.0	241.4	17.4	6.10		
	including	230.7	237.0	6.3	14.35		
		261.0	263.8	2.8	4.41†		
MGZD100	No significant results†					268.5	-61.0
MGZD101		151.0	155.0	4.0	4.46	51.0	-87.0
		239.7	245.3	5.6	1.86		
		261.0	263.7	2.7	2.24		
		294.0	301.0	7.0	5.81		
MGZD102	No significant results					269.5	-47.5
		177.6	192.0	14.4	1.42		
		208.0	214.3	6.3	1.28		
MGZD104		63.4	77.4	14.0	1.38	88.0	-75.0
	including	63.4	67.6	4.2	2.89		
MGZD105		14.0	23.1	9.1	1.28	90.0	-72.0
MGZD106		35.1	38.6	3.5	1.03	90.0	-65.0
MGZD107		204.0	252.3	48.3	7.14	89.0	-61.0
	including	230.6	248.1	17.5	14.61		
MGZD108		32.4	42.9	10.5	0.79	268.5	-55.0
	including	32.4	36.6	4.2	1.23		
		62.3	64.4	2.1	2.34		
		79.7	81.8	2.1	1.80		
MGZD109		91.0	94.0	3.0	1.27	269.0	-57.0
MGZD110		9.5	16.5	7.0	1.37	271.5	-69.0
		31.1	42.3	11.2	3.35		
MGZD111		8.0	22.1	14.1	1.15	270.0	-52.0
		32.6	38.1	5.5	1.20		
MGZD112	No significant results					269.0	-54.5
MGZD113		15.1	28.4	13.3	1.30	269.5	-53.5
	including	20.7	28.4	7.7	1.61		
MGZD114		14.4	17.9	3.5	1.28	270.0	-55.5
		22.1	34.0	11.9	0.98		
		48.7	51.5	2.8	1.74		
MGZD115	No significant results					271.0	-55.0
MGZD116		59.0	69.0	10.0	1.47	89.5	-64.5
MGZD117		112.3	121.0	8.7	38.76	83.5	-86.0
MGZD118		42.0	76.5	34.5	2.04	270.0	-46.0
	including	42.0	59.7	17.7	2.72		
	including	66.0	76.5	10.5	1.97		
MGZD119		88.3	91.8	3.5	2.06	271.0	-55.0
MGZD120	No significant results					88.0	-62.5
MGZD121	No significant results					90.0	-53.0
MGZD122		91.7	93.8	2.1	2.82	250.5	-82.0
		110.7	118.0	7.3	2.31		
MGZD123		23.0	25.7	2.7	2.38	92.0	-84.0
		53.0	61.0	8.0	2.60		
		76.0	80.0	4.0	4.45		
		98.0	107.4	9.4	3.98		
MGZD124		83.0	87.0	4.0	6.63	260.5	-71.5
		129.5	143.0	13.5	2.02		
	including	129.5	133.0	3.5	3.71		

Hole ID		From (m)	To (m)	Interval (m)	Au (g/t)	Local Azimuth	Dip
MGZD125		90.1	119.5	29.4	1.71	89.0	-78.0
	including	111.8	116.7	4.9	5.44		
MGZD126		34.0	38.0	4.0	1.18	91.5	-66.5
		68.0	71.0	3.0	1.38		
		154.0	158.2	4.2	8.94		
MGZD127		101.6	114.0	12.4	1.16	89.0	-44.5
	including	111.0	114.0	3.0	2.43		
MGZD128		238.0	261.9	23.9	1.25	88.0	-69.0
	including	238.0	243.2	5.2	2.74		
MGZD129		283.0	300.5	17.5	7.29	47.5	-89.5
	including	296.0	300.5	4.5	17.42		
MGZD130		70.0	71.0	1.0	3.05	269.0	-73.0
MGZD131		209.0	211.0	2.0	1.95	90.0	-81.0
		269.0	275.2	6.2	3.92		
	including	272.4	275.2	2.8	7.32		
		316.0	317.0	1.0	18.90		
MGZD132		284.0	295.4	11.4	1.31	88.0	-82.5
	including	289.0	291.4	2.4	3.95		
MGZD133		222.7	233.15	10.45	0.99	90.0	-82.0
	including	222.7	225.5	2.8	2.11		
MGZD134		195.7	230.0	34.3	2.01	90.0	-82.0
	including	221.6	229.3	7.7	6.19		
		271.0	276.0	5.0	1.47		
MGZD135		140.0	152.0	12.0	2.86	90.5	-80.5
	including	140.7	146.3	5.6	5.78		
		262.7	266.2	3.5	2.73		
MGZD136		244.0	247.0	3.0	1.61	250.0	-89.0
		259.7	261.8	2.1	2.34		
		289.7	294.0	4.3	3.21		
MGZD137	No significant results					88.5	-75.0
MGZD138		56.4	72.5	16.1	1.03	91.5	-45.0
	including	69.7	71.8	2.1	3.54		
MGZD139	No significant results					88.5	-60.0
MGZD140		51.0	52.0	1.0	1.14	90.5	-46.0
MGZD141		59.0	63.0	4.0	1.01	88.0	-46.0
MGZD142		187.4	191.0	3.6	2.08	91.6	-73.0
MGZD143	No significant results					91.0	-56.5
MGZD144		78.5	88.3	9.8	3.00	93.0	-62.0
MGZD145		28.0	30.0	2.0	1.95	88.5	-44.5
		95.0	97.0	2.0	1.09		
MGZD146		116.0	117.0	1.0	1.50	91.0	-58.5
MGZD147		139.5	157.7	18.2	3.24	89.5	-64.7
	including	139.5	145.1	5.6	6.95*		
MGZD148		246.0	250.0	4.0	1.12*	87.0	-53.0
MGZD149		67.7	89.4	21.7	3.75*	89.0	-46.0
	including	78.9	85.2‡	6.3‡	5.54*		
MGZD150	No significant results					90.0	-55.0
MGZD151		194.7	196.1	1.4	5.71*	91.0	-65.5
MGZD152		72.0	129.7	57.7	3.02	88.5	-53.5
	including	72.0	98.0	26.0	5.33		
MGZD153		211.0	245.2	34.2	3.71	91.0	-69.0
	including	227.0	238.9	11.9	6.99		
MGZD154		16.0	20.0	4.0	1.96	88.5	-73.5
		231.8	241.6	9.8	3.62		
	including	238.1	240.9	2.8	7.79*		
MGZD155		63.0	70.0	7.0	2.40	87.0	-60.5
MGZD156		220.0	222.4	2.4	3.37	140.0	-90.0
MGZD157		230.4	239.5	9.1	4.30	88.0	-81.0
	including	232.5	238.1‡	5.6	6.01		
MGZD158	No significant results					89.0	-54.5
MGZD159		66.0	69.1	3.1	3.16	92.0	-48.5
MGZD160		224.8	231.8	7.0	1.49	191.0	-90.0

Hole ID		From (m)	To (m)	Interval (m)	Au (g/t)	Local Azimuth	Dip
MGZD161		169.7	187.2	17.5	2.95	273.0	-80.0
	including	183.0	187.2	4.2	7.89		
		215.0	238.7	23.7	1.65*		
	including	221.0	226.1	5.1	3.95*		
MGZD162		151.0	168.0	17.0	2.90	89.0	-82.0
	including	156.2	159.0	2.8	9.90		
MGZD163		257.0	260.0	3.0	30.20	59.5	-89.0
MGZD164		194.0	201.0	7.0	1.86	91.5	-43.5
	including	198.0	201.0	3.0	3.67		
MGZD165		156.0	159.0	3.0	1.71	269.5	-70.6
		226.0	227.0	1.0	5.28		
MGZD166		156.6	159.0	2.4	1.07	130.0	-90.0
MGZD167		154.8	161.1	6.3	1.41*	91.0	-55.0
MGZD168	No significant results					88.0	-59.5
MGZD169		60.3	67.0	6.7	0.67	91.0	-55.0
MGZD170	No significant results					269.0	-61.0
MGZD171	No significant results					88.0	-72.0
MGZD172		23.0	63.0	40.0	2.96*	87.5	-50.5
	including	23.0	27.9	4.9	4.3*		
	including	55.3	63.0	7.7	4.89		
MGZD173		160.7	167.0	6.3	1.17	90.5	-62.5
		214.7	219.6	4.9	1.07		
		237.0	239.0	2.0	2.64		
MGZD174		46.7	59.3	12.6	6.26	91.5	-62.5
	including	50.2	56.5	6.3	11		
		72.4	78	5.6	6.31*		
		83.6	94.1	10.5	11.27*		
MGZD175		177.7	203.0	25.3	1.08	88.5	-83.0
	including	195.9	197.3	1.4	5.46		
MGZD176	No significant results					88.0	-48.5
MGZD177		99.0	100.0	1.0	3.17	90.0	-45.5
MGZD178		229.0	278.0	49.0	3.92	91.0	-71.5
	including	229.0	238.3	9.3	11.62		
		268.0	278.0	10.0	5.47*		
MGZD179	No significant results					68.0	-90.0
MGZD180	No significant results					90.5	-57.5
MGZD181		158.7	166.4	7.7	1.51	88.5	-69.0
		177.8	192.0	14.2	3.49		
	including	178.5	184.1	5.6	7.66		
		232.0	236.2	4.2	1.91		
MGZD182		143.0	144.4	1.4	1.30	92.5	-58.5
		152.1	154.9	2.8	1.56		
MGZD183	No significant results					87.0	-78.5
MGZD184		73.0	77.2	4.2	3.08	92.0	-59.5
MGZD185	No significant results					91.5	-46.0
MGZD186	No significant results					88.0	-44.5
MGZD187		150.0	153.0	3.0	0.95	86.0	-76.5
MGZD188		237.0	256.1	19.1	2.59	90.0	-77.5
	including	237.0	240.1	3.1	9.86		
MGZD189		101.0	104.0	3.0	2.26	88.5	-45.5
MGZD190		126.0	129.1	3.1	1.34	90.0	-85.0
	including	127.7	129.1	1.4	2.40		
		264.0	266.0	2.0	14.69		
MGZD191		139.1	153.1	14.0	4.07*	87.0	-66.0
MGZD192		142.0	143.0	1.0	1.47	90.0	-53.0
MGZD193	No significant results					90.5	-57.5
MGZD194		166.4	167.1	0.7	1.28	91.5	-53.0
MGZD195		100.0	120.0	20.0	1.65*	88.5	-55.5
	including	116.0	120.0	4.0	3.63		
MGZD196		186.0	215.8	29.8	2.03	89.0	-69.0
	including	189.1	196.8	7.7	6.11		
MGZD197		161	174	13	2.24*	64.0	-85.5
		247.1	294.1	47.0	1.82*	64.0	-85.5
	including	247.1	249.2	2.1	15.05*		
	and including	287.8	294.1	6.3	4.41		

Hole ID		From (m)	To (m)	Interval (m)	Au (g/t)	Local Azimuth	Dip
MGZD198		136.0	150.0	14.0	2.06	88.5	-65.0
	including	138.8	144.4	5.6	4.21		
MGZD199		154.0	165.0	11.0	0.96	90.5	-44.5
	including	161.0	165.0	4.0	1.65		
MGZD200		100.7	102.8	2.1	1.27	90.0	-77.5
		116.0	124.0	8.0	0.84		
MGZD201		183.7	198.0	14.3	4.64*	90.0	-79.5
	including	190.7	194.2	3.5	15.79		
		262.5	266.0	3.5	7.30		
		278.6	282.8	4.2	5.48*		
MGZD202		266.0	269.8	3.8	2.03	120.0	-89.5
		137.0	139.0	2.0	36.95		
MGZD203		235.1	255.4	20.3	6.93	89.0	-74.0
MGZD204	No significant results					0.0	-90.0
MGZD205		127.0	134.0	7.0	4.79*	88.0	-73.0
MGZD206	No significant results					268.0	-79.5
MGZD207		118.7	150.0	31.3	3.11	90.5	-55.0
	including	132.1	135.6	3.5	7.90		
MGZD208	No significant results					97.0	-88.0
MGZD209		107.0	111.0	4.0	16.34*	26.0	-90.0
MGZD210		149.1	154.0	4.9	5.48	91.5	-65.5
		167.7	182.0	14.3	3.39		
	including	176.1	180.3	4.2	7.73		
MGZD211		235.0	247.1	12.1	1.31	250.0	-90.0
	including	245.0	247.1	2.1	4.36		
		278.0	294.9	16.9	3.25		
MGZD212	No significant results					88.0	-74.0
MGZD213	No significant results					87.5	-71.5
MGZD214		192.0	193.0	1.0	51.40	89.5	-66.5
MGZD215		217.7	239.4	21.7	2.74	88.0	-77.8
	including	224.0	230.3	6.3	6.51		
MGZD216		123.0	128.0	5.0	1.03	87.5	-77.5
MGZD217	No significant results					90.5	-85.0
MGZD218		162.4	167.3	4.9	1.27	88.0	-66.5
		179.7	208.4	28.7	2.72		
	including	179.7	188.8	9.1	7.62		
		227.0	231.1	4.1	3.62		
MGZD219	No significant results					88.0	-77.0
MGZD220		135.0	142.0	7.0	1.95	90.5	-78.0
	including	137.0	140.0	3.0	3.87		
		261.7	264.5	2.8	9.12		
MGZD221		205.0	206.0	1.0	2.90	87.5	-77.5
MGZD222		255.0	290.0	35.0	6.45	91.0	-87.5
MGZD223	No significant results					268.5	-89.0
MGZD224		141.0	149.0	8.0	4.05	88.0	-86.5
		195.0	225.0	30.0	2.83		
	including	213.0	219.5	6.5	9.71		
		253.0	278.1	25.1	2.31		
MGZD225		256.0	257.0	1.0	9.48	86.5	-86.0
		281.7	286.6	4.9	1.81		
MGZD226		289.8	291.2	1.4	5.97	270.5	-86.5
MGZD227		281.0	292.0	11.0	2.20	70.0	-88.5
	including	283.0	284.0	1.0	20.40		
MGZD228	No significant results					88.5	-84.5
MGZD229	No significant results					268.0	-81.0
MGZD230		242.2	249.2	7.0	3.03	271.0	-87.0
	including	244.3	245.7	1.4	11.43		
MGZD231		240.0	241.0	1.0	4.57	270.0	-80.5
MGZD232		194.0	213.4	19.4	1.12	67.0	-88.5
	including	205.7	208.0	2.3	5.14		
		253.0	287.0	34.0	1.88		
	including	253.0	260.4	7.4	5.87		
MGZD233	No significant results					268.0	-83.5
MGZD234		294.0	297.0	3.0	7.04	266.5	-85.5
MGZD235	No significant results					269.5	-66.5

Hole ID		From (m)	To (m)	Interval (m)	Au (g/t)	Local Azimuth	Dip
MGZD236	No significant results					268.0	-81.0
MGZD237		254.0	269.0	15.0	1.13	271.0	-85.0
	including	256.1	258.2	2.1	3.34		
MGZD238		292.7	305.0	12.3	1.73	268.5	-83.0
	including	292.7	294.1	1.4	8.13		
MGZD239	No significant results					272.5	-88.0
MGZD240		136.0	140.0	4.0	3.21	268.5	-86.0
MGZD241	No significant results					270.0	-75.5
MGZD242	No significant results					271.5	-77.5
MGZD243		238.00	239.00	1.00	26.30	271.5	-78.0
MGZD244	No significant results					92.5	-82.0
MGZD245		238.5	263.9	25.4	1.18	90.5	-72.0
	including	258	262.5	4.5	2.4		
MGZD246		145.7	156.2	10.5	1.16*	91.5	-62.5
		199	202	3	1.6		
MGZD247	No significant results					270.0	-83.0
MGZD248		159.5	162.3	2.8	2.74	88.5	-51.5
MGZD249		249.0	260.0	11.0	1.37	90.0	-82.0
	including	253.0	254.0	1.0	8.28		
MGZD250		217.0	223.0	6.0	1.68	87.0	-84.5
		239.0	244.0	5.0	1.52		
MGZD251		235.9	242.2	6.3	1.41	88.0	-62.5
	including	240.8	242.2	1.4	4.34		
MGZD252		79.00	89.00	10.00	1.67	268.5	-82.5
	including	79.00	86.00	7.00	2.15		
MGZD253		241.0	256.1	15.1	3.27	267.0	-87.5
	including	248.7	256.1	7.4	6.05		
MGZD254		254.0	270.7	16.7	3.13	87.0	-75.5
	including	263.7	270.7	7.0	5.87		
MGZD255	No significant results					89.5	-51.0
MGZD256		193.4	221.8	28.4	3.01	88.0	-87.0
	including	219.0	221.1	2.1	23.67		
		267.0	274.0	7.0	3.58		
MGZD257		153.6	157.1	3.5	1.64	87.5	-57.5
MGZD258		207.0	210.0	3.0	4.59	270.0	-89.5
		253.0	260.0	7.0	3.61		
MGZD259	No significant results					89.0	-46.0
MGZD260		172.0	187.0	15.0	1.77	87.5	-83.5
	including	172.0	176.2	4.2	3.89		
		255.7	270.0	14.3	1.06		
MGZD261	No significant results					267.0	-77.5
MGZD262		235.7	261.8	26.1	0.85	88.0	-84.0
MGZD263	No significant results					89.5	-61.5
MGZD264		242.0‡	246.00	3.0‡	3.3*	267.5	-84.0
		258.00	263.60	5.60	3.22*		
MGZD265		154.4	209.7	55.3	3.18	92.0	-52.5
	including	178.9	199.9	21.0	6.33		
	including	179.6	188.7	9.1	8.81		
MGZD266	No significant results					0.0	-90.0
MGZD267		173.7	196.0	22.3	3.12	91.0	-63.5
	including	189.4	194.3	4.9	9.89		
MGZD268		251.0	267.5	16.5	3.01	269.5	-78.0
	including	264.7	267.5	2.8	10.03*		
		294.0	299.5	5.5	9.39		
	including	297.4	299.5	2.1	23.24		
MGZD269		247.0	254.0	7.0	1.12	91.0	-75.5
MGZD270	No significant results					92.0	-71.5
MGZD271		21.3	24.8	3.5	11.09*	92.5	-61.2
		85.0	114.0	29.0	1.23		
	including	98.9	103.1	4.2	3.12		
MGZD272		262.3	270.0	7.7	2.08	264.0	-86.0
		200.0	214.8	14.8	1.18*		
	including	212.0	214.8	2.8	3.41*		

Hole ID		From (m)	To (m)	Interval (m)	Au (g/t)	Local Azimuth	Dip
MGZD273		15.4	19.0	3.6	5.18	87.0	-48.5
		45.1	57.0	11.9	1.22		
		76.2	86.0	9.8‡	1.36		
MGZD274		61.00	71.00	10.00	1.26	92.0	-45.0
MGZD275		229.0	254.2	25.2	3.06	90.0	-78.5
	including	241.6	245.8	4.2	6.48		
MGZD276		195.0	219.5	24.5	2.23	272.5	-86.0
	including	201.0	203.4	2.4	8.11		
MGZD277		230.0	233.7	3.7	10.15	90.5	-68.0
		249.0	279.0	30.0	4.78†		
	including	249.0	267.0	18.0	7.97†		
	and including	272.8	279.0	6.2	12.17†		
MGZD278	No significant results					87.0	-85.0
MGZD279		250.5	262.2	11.7	1.21	270.0	-80.5
	including	250.5	252.6	2.1	3.23		
MGZD280		246.1	258.2	12.1	2.38	269.5	-81.5
	including	254.7	257.5	2.8	5.48		
		282.7	289.0	6.3	1.23		
MGZD281	No significant results					89.0	-82.0
MGZD282		74.9	80.0	5.1	1.33	90.5	-70.5
MGZD283		231.0	238.6	7.6	3.74	271.0	-88.5
	including	236.5	238.6	2.1	8.25		
MGZD284		200.0	202.0	2.0	45.06	239.5	-88.0
		275.0	286.0	11.0	14.75		
	including	282.2	285.0	2.8	56.17*		
MGZD285		38.0	40.4	2.4	5.95	88.5	-49.0
MGZD286		270.0	275.0	5.0	1.93	270.0	-76.5
MGZD287	No significant results					268.0	-76.0
MGZD288		245.0	265.0	20.0	1.75	268.5	-83.5
	including	258.4	265.0	6.6	4.65		
MGZD289		43.0	45.1	2.1	1.41	88.5	-47.0
MGZD290		74.4	78.5	4.1	2.91	88.0	-77.0
MGZD291	No significant results					88.0	-84.5
MGZD292	No significant results					90.0	-50.5
MGZD293	No significant results					268.5	-71.0
MGZD294		291.0	297.0	6.0	2.87	268.5	-83.0
	including	291.0	293.4	2.4	5.88*		
MGZD295		211.0	216.0	5.0	12.67	269.5	-80.0
		262.0	278.4	16.4	1.19		
MGZD296	No significant results					89.5	-52.0
MGZD297	No significant results					91.0	-75.5
MGZD298		213.0	223.0	10.0	1.63	269.5	-86.5
MGZD299		241.0	245.2	4.2	1.19	58.0	-85.0
MGZD300		143.0	148.0	5.0	2.05	88.0	-48.5
MGZD301		276.0	282.0	6.0	5.26	269.5	-75.5
MGZD302	No significant results					89.0	-46.0
MGZD303		205.0	226.0	21.0	2.01	269.5	-76.0
		255.0	266.0	11.0	2.74		
		297.0	305.3	8.3	8.84		
MGZD304	No significant results					268.5	-65.0
MGZD305	No significant results					88.5	-63.5
MGZD306		309.0	311.4	2.4	4.9*	271.0	-79.0
MGZD307		50.0	63.0	13.0	4.78	89.5	-45.0
	including	51.0	55.4	4.4	12.71		
MGZD308	No significant results					90.0	-60.0
MGZD309	No significant results					89.0	-57.5
MGZD310		100.0	105.0	5.0	0.80	59.5	-45.0
MGZD311	No significant results					90.0	-56.0
MGZD312	No significant results					90.0	-48.0
MGZD313	No significant results					90.5	-45.5
MGZD314		154.0	156.1	2.1	3.42	272.0	-54.5
MGZD315		146.0	155	9	0.76	90.5	-82.0
MGZD316	No significant results					92.5	-46.5
MGZD317	No significant results					90.0	-55.5

Hole ID		From (m)	To (m)	Interval (m)	Au (g/t)	Local Azimuth	Dip
MGZD318		138.6	198	59.4	3.98	90.0	-69.5
	including	185.5	193.2	7.7	12.13		
MGZD319	No significant results					88.5	-49.0
MGZD320		151.7	154.5	2.8	4.98	268.0	-56.0
MGZD321		107.0	116.8	9.8	1.08*	88.5	-45.5
MGZD322		170.0	175.6	5.6	11.54	90.5	-78.0
MGZD323		152.0	164.0	12.0	1.50	269.5	-66.5
	including	160.0	163.0	3.0	4.34		
MGZD324		236.4	254.0	17.6	1.63	273.5	-84.5
MGZD325	No significant results					270.5	-84.0
MGZD326	No significant results					90.0	-62.0
MGZD327	No significant results					88.5	-53.0
MGZD328		41.0	44.4	3.4	1.67	88.6	-45.5
MGZD329		67.0	72	5	1.38*	90.0	-46.0
MGZD330		121.0	128.0	7.0	2.80	90.5	-84.5
		190.7	195.6	4.9	2.98		
		251.0	258.0	7.0	5.76		
	including	252.4	254.5	2.1	18.18		
MGZD331		159.0	186.0	27.0	1.11	270.0	-77.0
MGZD332		293	299	6	3.97	270.5	-82.5
MGZD333		119.0	125.2	6.2	1.23	269.5	-70.5
		140.0	145.0	5.0	1.02		
		213.0	216.0	3.0	3.06		
MGZD334		27.8	41.0	13.2	1.28	269.5	-54.0
	including	35.0	38.5	3.5	2.77		
MGZD335	No significant results					269.0	-73.0
MGZD336		201.0	206.0	5.0	5.56	242.0	-79.5
		271.0	277.0	6.0	3.36		
MGZD337		90.4	114.2	23.8	2.80	91.0	-71.0
	including	98.1	105.1	7.0	5.31		
MGZD338	No significant results					270.0	-73.0
MGZD339		185.0	206.0	21.0	1.01	240.5	-63.5
		214.7	221.0	6.3	1.45		
	including	214.7	216.8	2.1	3.16		
MGZD340		288.00	294.00	6.00	3.13	270.0	-78.5
MGZD341		112.0	131.0	19.0	1.56	239.5	-63.5
	including	118.0	123.5	5.5	2.92		
		146.0	158.5	12.5	2.90		
	including	148.7	151.5 ‡	2.8	9.77		
MGZD342		132.5	139.0	6.5	0.97	240.0	-54.0
MGZD343	No significant results					269.5	-58.0
MGZD344		103.0	114.0	11.0	1.03	238.5	-70.0
MGZD345	No significant results					240.0	-51.5
MGZD346		254.0	261.0	7.0	1.05	269.5	-74.5
		292.0	309.6	17.6	1.85		
	including	305.4	308.2	2.8	6.24		
MGZD347	No significant results					238.5	-57.0
MGZD348	No significant results					239.0	-71.5
MGZD349	No significant results					241.5	-69.5
MGZD350		273.0	280	7	3.47*	273.0	-86.5
MGZD351	No significant results					270.0	-74.5
MGZD352	No significant results					270.0	-65.5
MGZD353		148.0	153.0	5.0	1.23	236.5	-68.5
MGZD354		121	126	5	0.86	271.0	-68.0
MGZD355	No significant results					273.0	-81.0
MGZD356	No significant results					269.0	-46.0
MGZD357	No significant results					272.0	-63.5
MGZD358	No significant results					268.5	-60.5
MGZD359	No significant results					271.5	-64.0
MGZD360		179.70	182.00	2.30	5.99*	271.5	-73.5
MGZD361	No significant results					269.5	-77.0
MGZD362		195.5	205	9.5	1.61	268.0	-88.5
	including	195.5	198.3	2.8	3.9*		
MGZD363	No significant results					269.5	-59.0
MGZD364	No significant results					270.0	-53.0

Hole ID		From (m)	To (m)	Interval (m)	Au (g/t)	Local Azimuth	Dip
MGZD365	No significant results					271.5	-54.5
MGZD366	No significant results					270.5	-55.5
MGZD367	No significant results					271.5	-59.5
MGZD368	No significant results					270.5	-73.0
MGZD369	No significant results					271.0	-76.0
MGZD370		151	159.8	8.8	4.23	270.5	-66.5
	including	157	159.8	2.8	12.12		
MGZD371	No significant results					270.5	-66.5
MGZD372	No significant results					269.5	-81.0
MGZD373		151	163	12	1.35	269.0	-67.5
	including	153	157	4	2.08		
MGZD374	No significant results					269.0	-67.5
MGZD375	No significant results					271.0	-64.5
MGZD376	No significant results					89.0	-83.0
MGZD377	No significant results					269.0	-80.0
MGZD378	No significant results					268.0	-50.0
MGZD379	No significant results					271.5	-59.0
MGZD380	No significant results					270.0	-58.5
MGZD381	No significant results					271.0	-69.0
MGZD382	No significant results					269.0	-75.5
MGZD383	No significant results					272.0	-66.0
MGZD384	No significant results					269.5	-53.5
MGZD385		288.7	291.5	2.8	3.56	240.5	-88.5
MGZD386	No significant results					270.0	-70.0
MGZD387	No significant results					90.0	-86.0
MGZD388	No significant results					270.0	-67.0
MGZD389		202.7	204.1	1.4	1.65	268.5	-70.0
MGZD390	No significant results					91.0	-61.5
MGZD391	No significant results					268.0	-58.0
MGZD392		121.00	128.00	7.00	1.55	89.0	-80.0
MGZD393		183.5	189.1	5.6	3.18	61.0	-63.5
		196.0	239.4	43.4	5.37		
	including	219.8	239.4	19.6	9.37		
MGZD394		176.1	185.2	9.1	1.33	89.5	-77.0
	including	177.5	181.7	4.2	2.12		
		205.4	209.6	4.2	12.07		
		257.5	264.5	7	4.35		
MGZD395		253	256	3	7.66*	87.0	-75.5
		257	265.3	8.3	2.17		
	including	261.8	263.2	1.4	2.1*		
MGZD396	No significant results					268.5	-69.0
MGZD397	No significant results					91.5	-78.0
MGZD398		174.7	204	29.3	5.29*	91.0	-55.5
	including	184.5	192.9	8.4	13.51*		
MGZD399		195	213.1	18.1	1.21	269.5	-83.5
MGZD400		156	160	4	2.3	89.0	-66.5
		205.5	235.4	29.9	1.37*		
	including	205.5	210.4	4.9	3.58*		
MGZD401		132.8	137.0	4.2	2.69	59.5	-45.0
MGZD402		205.3	210.9	5.6	1.97	90.0	-68.5
		212.3	217.9	5.6	2.18		
MGZD403		173.7	191.2	17.5	5.21	90.0	-53.5
	including	187.7	191.2	3.5	12.47		
		195.7	198.5	2.8	6.58		
MGZD404	No significant results					90.0	-71.0
MGZD405	No significant results					270.0	-72.0
MGZD406		238.7	242	3.3	3.29	90.0	-68.0
MGZD407		241	243.1	2.1	28.68	270.0	-73.5
MGZD408	No significant results					270.0	-60.0
MGZD409	No significant results					90.0	-86.5
MGZD410	No significant results					90.0	-66.5
MGZD411	No significant results					90.0	-59.5
MGZD412	No significant results					90.5	-47.0

Hole ID		From (m)	To (m)	Interval (m)	Au (g/t)	Local Azimuth	Dip
MGZD413		214	218.9	4.9	5.13	90.0	-84.0
		241.3	244.1	2.8	7.38		
		271	283	12	0.92		
MGZD414		281.8	284.6	2.8	3.90	90.0	-88.5
MGZD415		260	261	1	23.90	270.0	-86.0
MGZD416	No significant results					267.5	-72.0
MGZD417		186	190.9	4.9	2.37	90.5	-76.5
	including	186	188.1	2.1	4.87		
		195.1	197.2	2.9	4.42		
MGZD418	No significant results					270.0	-84.0
MGZD419	No significant results					91.0	-45.5
MGZD420		152	156.5	4.5	2.14	89.5	-60.0
		179.2	200	20.8	2.84		
	including	192.5	195.3	2.8	10.17		
		203	206.1	3.1	15.98		
MGZD421	No significant results					89.5	-48.5
MGZD422	No significant results					270.5	-69.0
MGZD423	No significant results					268.5	-61.0
MGZD424		7	20	13	2.89	90.0	-45.0
	including	11.2	16.1	4.9	4.92		
MGZD425		37	46	9	0.82	90.0	-45.0
MGZD426	No significant results					270.0	-74.0
MGZD427	No significant results					90.0	-50.5
MGZD428		23	25.1	2.1	4.33	90.0	-68.5
		32.7	35.5	2.8	1.88		
		42.7	51.1	8.4	1.74		
		53.2	53.9	0.7	7.4		
		58.1	64.4	6.3	2.16		
		67.9	70.7	2.8	1.72		
		72.8	79.8	7	2.36		
	including	72.8	77	4.2	3.43		
MGZD429		30	33	3	2.34	270.0	-55.0
MGZD430	No significant results					90.0	-64.0
MGZD431	No significant results					90.0	-76.0
MGZD432		18.7	22.2	3.5	22.05	270.0	-45.0
		32	34.8	2.8	1.49		
		63	67.2	4.2	2.35		
	including	65.8	67.2	1.4	4.73		
MGZD433	No significant results					270.0	-72.0
MGZD434		175	189.8	14.8	2.31	90.0	-65.0
	including	179	187	8	2.18		
		221	222	1	3.00		
MGZD435	No significant results					90.0	-60.0
MGZD436	No significant results					0.0	-90.0
MGZD438	No significant results					90.0	-45.0
MGZD439		279	281	2	3.02	270.0	-45.0
MGZD440		7	8	1	2.41	270.0	-52.5
		20	23	3	1.75		
MGZD441		35	37	2	0.37	90.00	-45.0
MGZD442	No significant results					270.00	-45.0
MGZD443	No significant results					270.00	-50.0
MGZD445	No significant results					90.00	-54.0
MGZD446	No significant results					270.00	-70.0
MGZD448		87	89	2	0.80	270.00	-50.0
MGZD449		261	263	2	0.83	270.00	-75
MGZD450	No significant results					270.00	-50.0
MGZD451		128	129	1	0.75	60.00	-57.5
MGZD452	No significant results					240.00	-60.0
MGZD453	No significant results					240.00	-70.0
MGZD454	No significant results					60.00	-50.5
MGZD455		2	4	2	0.45	270.00	-50.0
MGZD456		52	54.1	2.1	0.49	90.00	-54.0
MGZD457	No samples taken					270.00	-80.0
MGZD458	No significant results					90.00	-50.0
MGZD459	No significant results					270.00	-75.0

Hole ID		From (m)	To (m)	Interval (m)	Au (g/t)	Local Azimuth	Dip
MGZD460	No significant results					270.00	-45.0
MGZD461		136	141	5	0.91	90.00	-46.0
MGZD462	No significant results					90.00	-46.0
MGZD463	No significant results					270.00	-88.0
MGZD464	No significant results					270.00	-50.0
MGZD465	No significant results					270.00	-75.0
MGZD466	No significant results					270.00	-90.0
MGZD467	No significant results					90.00	-45.0
MGZD468	No significant results					90.00	-46.0
MGZD469	No significant results					90.00	-60.0

* Recalculated assay due to QAQC procedure; † New interval not reported from previous release; ‡ Change to depth or interval

Table A.3. Diamond Drilling Conducted at the Majiri prospect, Handeni Property

Hole ID		From (m)	To (m)	Interval (m)	Au (g/t)	Local Azimuth	Dip
MGZD437		15.00	16.00	1.00	3.98	73.0	-45.0
MGZD444		4.00	5.00	1.00	0.71	73.00	-45.0
		33.00	35.00	2.00	0.40		
MGZD447	No significant results					73.00	-45.0

Appendix B

Independent Sample & Assay Validation Certificates (February 2012)

Client: **Advantage Geoservices Ltd.**
11076 238 Street
Maple Ridge BC V2W 1E6 Canada

AcmeLabs Acme Analytical Laboratories (Vancouver) Ltd.
1020 Cordova St. East Vancouver BC V6A 4A3 Canada

www.acmelab.com

Submitted By:	James Gray
Receiving Lab:	Canada-Vancouver
Received:	February 29, 2012
Report Date:	March 19, 2012
Page:	1 of 2

CERTIFICATE OF ANALYSIS VAN12000905.2

CLIENT JOB INFORMATION

Project:	None Given
Shipment ID:	
P.O. Number	
Number of Samples:	6

SAMPLE DISPOSAL

RTRN-PLP	Return
RTRN-RJT	Return

Acme does not accept responsibility for samples left at the laboratory after 90 days without prior written instructions for sample storage or return.

SAMPLE PREPARATION AND ANALYTICAL PROCEDURES

Method Code	Number of Samples	Code Description	Test Wgt (g)	Report Status	Lab
R200-250	5	Crush, split and pulverize 250 g rock to 200 mesh			VAN
G601-G610	6	Lead Collection Fire - Assay Fusion - AAS Finish	50	Completed	VAN
7AX1	6	1:1:1 Aqua Regia digestion ICP-ES/ICP-MS analysis	1	Completed	VAN

ADDITIONAL COMMENTS

Version 2: Revised STD SF-3A Mn

Invoice To: Canaco Tanzania Limited
PO Box 72488
Dar Es Salaam
Tanzania

CC:

AcmeLabs Acme Analytical Laboratories (Vancouver) Ltd.
1020 Cordova St. East Vancouver BC V6A 4A3 Canada
Phone (604) 253-3158 Fax (604) 253-1716
www.acmelab.com

Client: Advantage Geoservices Ltd.
11076 238 Street
Maple Ridge BC V2W 1E6 Canada

Project: None Given
Report Date: March 19, 2012

CERTIFICATE OF ANALYSIS VAN12000905.2

	Method	WGHT	G6-50	7AX	7AX	7AX	7AX	7AX	7AX	7AX	7AX	7AX	7AX	7AX	7AX	7AX	7AX	7AX	7AX	7AX	7AX
	Analyte	Wgt	Au	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Th	Sr	Cd	Sb	Bi	V	Ca
	Unit	kg	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%
	MDL	0.01	0.005	0.5	0.5	0.5	5	0.5	0.5	0.5	5	0.01	5	0.5	0.5	5	0.5	0.5	0.5	10	0.01
JNG-01	Drill Core	1.26	3.279	1.1	140.9	2.0	88	8.2	63.7	58.3	437	5.86	10500	<0.5	1.3	8	<0.5	1.6	<0.5	31	1.08
JNG-02	Drill Core	1.24	0.122	0.7	72.1	1.1	38	<0.5	2.5	25.7	469	3.86	73	<0.5	1.3	14	<0.5	1.3	<0.5	<10	1.45
JNG-03	Drill Core	0.97	0.546	<0.5	21.2	0.8	41	<0.5	2.8	39.0	391	3.33	29	<0.5	<0.5	5	<0.5	0.6	<0.5	96	0.82
JNG-04	Drill Core	1.02	0.442	1.7	20.5	0.7	87	<0.5	1.1	9.6	498	4.38	28	<0.5	1.2	17	<0.5	1.1	<0.5	<10	1.69
JNG-05	Rock Pulp	0.14	1.390	2.0	168.6	24.8	388	3.0	12.5	3.7	54	2.22	17	<0.5	<0.5	21	1.9	0.8	1.3	<10	0.15
JNG-06	Rock	0.73	0.007	0.9	20.1	8.7	43	<0.5	16.3	7.3	279	2.17	<5	1.5	13.6	19	<0.5	<0.5	<0.5	31	0.42

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Client: **Advantage Geoservices Ltd.**
11076 238 Street
Maple Ridge BC V2W 1E6 Canada

Project: None Given
Report Date: March 19, 2012

CERTIFICATE OF ANALYSIS VAN12000905.2

	Method	7AX	7AX	7AX	7AX	7AX	7AX	7AX	7AX	7AX	7AX	7AX	7AX	7AX	7AX	7AX	7AX
	Analyte	P	La	Cr	Mg	Ba	Ti	Al	Na	K	W	Hg	Sc	Tl	S	Ga	Se
	Unit	%	ppm	ppm	%	ppm	%	%	%	%	ppm	ppm	ppm	ppm	%	ppm	ppm
	MDL	0.001	0.5	0.5	0.01	5	0.001	0.01	0.01	0.01	0.5	0.05	0.5	0.5	0.05	5	2
JNG-01	Drill Core	0.077	6.1	3.8	0.47	54	0.194	1.05	0.07	0.15	3.2	<0.05	7.0	<0.5	2.22	<5	<2
JNG-02	Drill Core	0.118	7.1	2.3	0.25	19	0.310	1.07	0.04	0.03	0.5	<0.05	7.8	<0.5	0.99	<5	<2
JNG-03	Drill Core	0.031	1.4	1.9	0.48	11	0.222	0.93	0.09	0.06	1.4	<0.05	7.7	<0.5	0.43	<5	4
JNG-04	Drill Core	0.126	11.7	2.1	0.15	38	0.121	1.04	0.06	0.05	<0.5	<0.05	6.7	<0.5	1.08	<5	<2
JNG-05	Rock Pulp	0.003	0.7	24.1	0.03	1256	0.004	0.10	0.01	0.03	<0.5	<0.05	0.9	<0.5	2.19	<5	3
JNG-06	Rock	0.043	49.7	23.6	0.50	96	0.134	0.87	0.09	0.51	<0.5	<0.05	3.2	<0.5	0.06	<5	2

Appendix C

Grade Composite Listing

A ZONE LOW GRADE COMPOSITE (SECTIONS 60240 through 60400)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60240	MGZD189	60.0	60.7	0.7	D42666	1.13	2.01	1.41	2.27				Comp A6
60240	MGZD189	60.7	61.4	0.7	D42667	1.06	0.39	0.27	0.41				Comp A1
60240	MGZD189	61.4	62.1	0.7	D42668	1.04	0.57	0.40	0.59	2.10	2.08	0.99	Comp A2
60240	MGZD193	175.0	176.0	1.0	D43752	1.55	2.39	2.39	3.70	1.00	2.39	2.39	Comp A6
60240	MGZD195	73.7	74.4	0.7	D44666	1	1.55	1.09	1.55				Comp A4
60240	MGZD195	74.4	75.1	0.7	D44667	1.07	0.81	0.57	0.87	1.40	1.65	1.18	Comp A3
60240	MGZD198	136.0	136.7	0.7	D45282	1.17	1.67	1.17	1.95				Comp A5
60240	MGZD198	136.7	137.4	0.7	D45283	1.1	0.56	0.39	0.62				Comp A2
60240	MGZD198	137.4	138.1	0.7	D45284	1.17	0.24	0.17	0.28				Comp A1
60240	MGZD198	138.1	138.8	0.7	D45285	1.14	0.27	0.19	0.31				Comp A1
60240	MGZD198	138.8	139.5	0.7	D45286	1.12	8.00	5.60	8.96				Comp A11
60240	MGZD198	139.5	140.2	0.7	D45287	1.04	1.26	0.88	1.31	4.20	8.40	2.00	Comp A4
60240	MGZD199	46.0	47.0	1.0	D48472	1.63	1.17	1.17	1.91				Comp A3
60240	MGZD199	47.0	48.0	1.0	D48473	1.74	0.34	0.34	0.59				Comp A1
60240	MGZD199	48.0	49.0	1.0	D48474	1.59	0.69	0.69	1.10	3.00	2.20	0.73	Comp A2
60240	MGZD199	154.0	155.0	1.0	D48592	1.81	1.24	1.24	2.24				Comp A4
60240	MGZD199	155.0	156.0	1.0	D48593	1.81	1.43	1.43	2.59	2.00	2.67	1.34	Comp A4
60240	MGZD199	161.0	161.7	0.7	D48601	1.19	4.97	3.48	5.92				Comp A9
60240	MGZD199	161.7	162.4	0.7	D48602	1.07	1.39	0.97	1.49				Comp A4
60240	MGZD199	162.4	163.1	0.7	D48603	1.13	0.05	0.04	0.06				Comp A1
60240	MGZD199	163.1	164.0	0.9	D48604	1.62	0.79	0.71	1.29				Comp A2
60240	MGZD199	164.0	165.0	1.0	D48605	1.82	1.41	1.41	2.56	4.00	6.61	1.65	Comp A4
60240	MGZD214	0.0	1.0	1.0	D49988	1.67	0.83	0.83	1.38				Comp A3
60240	MGZD214	1.0	2.0	1.0	D49989	0.81	0.39	0.39	0.32				Comp A1
60240	MGZD214	2.0	3.0	1.0	D49990	0.97	0.74	0.74	0.72	3.00	1.96	0.65	Comp A2
60240	MGZD221	0.0	1.0	1.0	D52283	0.95	0.31	0.31	0.29				Comp A1
60240	MGZD221	1.0	2.0	1.0	D52284	0.43	0.85	0.85	0.37				Comp A3
60240	MGZD221	3.0	4.0	1.0	D52286	0.97	0.37	0.37	0.36	4.00	3.39	0.85	Comp A1
60240	MGZD221	205.0	206.0	1.0	D52511	1.53	2.90	2.90	4.44	1.00	2.90	2.90	Comp A7
60240	MGZD247	38.0	39.0	1.0	D64009	1.46	0.59	0.59	0.86				Comp A2
60240	MGZD247	39.0	40.0	1.0	D64010	1.64	1.47	1.47	2.41	2.00	2.06	1.03	Comp A4
60240	MGZD255	51.0	52.0	1.0	D66222	1.92	0.56	0.56	1.08				Comp A2
60240	MGZD255	52.0	53.0	1.0	D66223	1.9	0.39	0.39	0.74				Comp A1
60240	MGZD255	53.0	54.0	1.0	D66224	1.78	0.46	0.46	0.82				Comp A1
60240	MGZD255	54.0	55.0	1.0	D66225	1.85	0.47	0.47	0.87				Comp A1
60240	MGZD255	55.0	56.0	1.0	D66226	1.87	0.73	0.73	1.37				Comp A2
60240	MGZD255	56.0	57.0	1.0	D66227	1.83	1.87	1.87	3.42	6.00	4.48	0.75	Comp A5
60240	MGZD270	85.0	86.0	1.0	D72322	1.81	1.17	1.17	2.12				Comp A3
60240	MGZD270	86.0	87.0	1.0	D72323	1.86	2.12	2.12	3.94	2.00	3.29	1.65	Comp A6
60240	MGZD289	27.0	28.0	1.0	D78414	1.71	1.41	1.41	2.41	1.00	1.41	1.41	Comp A4
60240	MGZD289	43.7	44.4	0.7	D78436	1.27	2.29	1.60	2.91				Comp A6
60240	MGZD289	44.4	45.1	0.7	D78437	1.35	1.01	0.71	1.36	2.10	2.97	1.41	Comp A3
60280	MGZD094	89.0	90.0	1.0	D16227	1.04	3.05	3.05	3.17				Comp A8
60280	MGZD094	90.0	91.0	1.0	D16228	0.94	0.48	0.48	0.45	2.00	3.53	1.77	Comp A1
60280	MGZD094	119.0	120.0	1.0	D11803	1.35	2.77	2.77	3.74				Comp A7
60280	MGZD094	120.0	121.0	1.0	D11804	1.36	1.82	1.82	2.48	2.00	4.59	2.30	Comp A5
60280	MGZD094	220.7	221.4	0.7	D11915	0.74	1.63	1.14	1.21				Comp A5
60280	MGZD094	221.4	222.1	0.7	D11916	0.72	1.37	0.96	0.99	1.40	2.10	1.50	Comp A4
60280	MGZD155	63.0	63.7	0.7	D33561	1.13	1.66	1.16	1.88				Comp A5
60280	MGZD155	63.7	64.4	0.7	D33562	1.42	1.61	1.13	2.29				Comp A5
60280	MGZD155	64.4	65.1	0.7	D33563	1.23	2.57	1.80	3.16				Comp A7
60280	MGZD155	65.1	65.8	0.7	D33564	1.1	3.35	2.35	3.69				Comp A8
60280	MGZD155	65.8	66.5	0.7	D33565	1.76	3.66	2.56	6.44				Comp A8
60280	MGZD155	66.5	67.2	0.7	D33566	0.89	1.07	0.75	0.95				Comp A3
60280	MGZD155	67.2	67.9	0.7	D33567	1.18	5.18	3.63	6.11				Comp A9
60280	MGZD155	67.9	68.6	0.7	D33568	1.25	3.91	2.74	4.89	5.60	16.11	2.88	Comp A8
60280	MGZD159	41.0	42.0	1.0	D34641	1.6	1.38	1.38	2.21	1.00	1.38	1.38	Comp A4
60280	MGZD159	51.0	51.7	0.7	D34652	1.34	1.95	1.37	2.61	0.70	1.37	1.95	Comp A5

A ZONE   LOW GRADE COMPOSITE   (SECTIONS 60240 through 60400)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60280	MGZD200	98.0	99.0	1.0	D45783	1.72	0.40	0.40	0.69				Comp A1
60280	MGZD200	99.0	100.0	1.0	D45784	1.52	0.29	0.29	0.44				Comp A1
60280	MGZD200	100.0	100.7	0.7	D45785	1.1	0.43	0.30	0.47				Comp A1
60280	MGZD200	100.7	101.4	0.7	D45786	1.07	1.56	1.09	1.67				Comp A4
60280	MGZD200	101.4	102.1	0.7	D45787	1.07	0.95	0.66	1.02				Comp A3
60280	MGZD200	102.1	102.8	0.7	D45788	1.07	1.30	0.91	1.39				Comp A4
60280	MGZD200	102.8	103.5	0.7	D45789	1.12	0.56	0.39	0.63	5.50	4.05	0.74	Comp A2
60280	MGZD200	116.0	117.0	1.0	D45805	1.6	1.75	1.75	2.80				Comp A5
60280	MGZD200	117.0	118.0	1.0	D45806	1.73	1.81	1.81	3.13	2.00	3.56	1.78	Comp A5
60280	MGZD200	123.0	124.0	1.0	D45812	1.73	2.30	2.30	3.98	1.00	2.30	2.30	Comp A6
60280	MGZD200	140.0	141.0	1.0	D45831	1.58	2.77	2.77	4.38	1.00	2.77	2.77	Comp A7
60280	MGZD200	185.0	186.0	1.0	D45882	1.69	1.76	1.76	2.98				Comp A5
60280	MGZD200	186.0	187.0	1.0	D45883	1.64	0.64	0.64	1.04	2.00	2.40	1.20	Comp A2
60280	MGZD213	55.0	56.0	1.0	D49764	1.57	1.32	1.32	2.08				Comp A4
60280	MGZD213	56.0	57.0	1.0	D49765	1.53	1.42	1.42	2.17	2.00	2.74	1.37	Comp A4
60280	MGZD213	216.0	217.0	1.0	D49943	1.84	1.08	1.08	1.99				Comp A3
60280	MGZD213	217.0	218.0	1.0	D49944	1.84	0.03	0.03	0.05				Comp A1
60280	MGZD213	218.0	219.0	1.0	D49945	1.8	0.04	0.04	0.06				Comp A1
60280	MGZD213	219.0	220.0	1.0	D49947	1.56	0.99	0.99	1.54	4.00	2.13	0.53	Comp A3
60280	MGZD217	124.0	125.0	1.0	D51099	1.66	0.75	0.75	1.25				Comp A2
60280	MGZD217	125.0	126.0	1.0	D51100	1	0.52	0.52	0.52	2.00	1.27	0.64	Comp A2
60280	MGZD217	130.0	131.0	1.0	D51106	1.75	0.53	0.53	0.93				Comp A2
60280	MGZD217	131.0	132.0	1.0	D51107	1.75	1.21	1.21	2.11	2.00	1.74	0.87	Comp A4
60280	MGZD217	253.0	254.0	1.0	D51242	1.8	1.52	1.52	2.74				Comp A4
60280	MGZD217	254.0	255.0	1.0	D51243	1.72	3.16	3.16	5.44	2.00	4.69	2.34	Comp A8
60280	MGZD223	44.0	45.0	1.0	D53901	1.69	1.46	1.46	2.46	1.00	1.46	1.46	Comp A4
60280	MGZD223	49.0	50.0	1.0	D53906	1.6	1.76	1.76	2.81				Comp A5
60280	MGZD223	50.0	51.0	1.0	D53907	1.47	0.93	0.93	1.37				Comp A3
60280	MGZD223	51.0	52.0	1.0	D53908	1.55	0.94	0.94	1.46	3.00	3.63	1.21	Comp A3
60280	MGZD282	76.3	77.0	0.7	D75871	1.16	3.84	2.69	4.45				Comp A8
60280	MGZD282	77.0	78.0	1.0	D75872	1.72	1.66	1.66	2.86				Comp A5
60280	MGZD282	78.0	79.0	1.0	D75873	1.62	0.93	0.93	1.51				Comp A3
60280	MGZD282	80.0	81.0	1.0	D75876	1.7	0.21	0.21	0.36				Comp A1
60280	MGZD282	81.0	82.0	1.0	D75877	1.62	0.68	0.68	1.10	5.70	6.78	1.19	Comp A2
60320	MGZD008	20.0	21.0	1.0	D01886	0.98	1.00	1.00	0.98	1.00	1.00	1.00	Comp A3
60320	MGZD008	33.0	34.0	1.0	D01901	1.12	1.73	1.73	1.94				Comp A5
60320	MGZD008	34.0	35.0	1.0	D01902	1.18	1.72	1.72	2.03	2.00	3.45	1.73	Comp A5
60320	MGZD008	55.0	56.0	1.0	D01926	1.22	2.00	2.00	2.44				Comp A6
60320	MGZD008	56.0	57.0	1.0	D01927	1.18	0.91	0.91	1.07				Comp A3
60320	MGZD008	57.0	58.0	1.0	D01928	1.2	0.84	0.84	1.01				Comp A3
60320	MGZD008	58.0	59.0	1.0	D01929	1.46	2.08	2.08	3.04	4.00	5.83	1.46	Comp A6
60320	MGZD008	66.0	67.0	1.0	D01938	1.31	1.95	1.95	2.55	1.00	1.95	1.95	Comp A5
60320	MGZD008	120.3	121.0	0.7	D00677	0.94	4.56	3.28	4.29				Comp A9
60320	MGZD008	121.0	122.3	1.3	D00678	1.45	1.57	2.04	2.28	2.00	5.32	2.66	Comp A4
60320	MGZD009	87.5	88.8	1.3	D00722	1.56	0.42	0.55	0.66				Comp A1
60320	MGZD009	88.8	90.0	1.2	D00723	1.4	1.40	1.68	1.96				Comp A4
60320	MGZD009	90.0	90.7	0.7	D00724	0.84	0.61	0.43	0.51	3.20	2.65	0.83	Comp A2
60320	MGZD009	222.0	223.0	1.0	D04049	1.07	2.17	2.17	2.32	1.00	2.17	2.17	Comp A6
60320	MGZD014	23.0	24.0	1.0	D01372	1.96	1.88	1.88	3.68				Comp A5
60320	MGZD014	24.0	25.0	1.0	D01373	2.16	0.03	0.03	0.06				Comp A1
60320	MGZD014	25.0	26.0	1.0	D01374	1.96	1.83	1.83	3.59				Comp A5
60320	MGZD014	26.0	27.0	1.0	D01375	1.87	0.58	0.58	1.08				Comp A2
60320	MGZD014	27.0	28.0	1.0	D01376	1.12	0.05	0.05	0.06				Comp A1
60320	MGZD014	28.0	29.0	1.0	D01377	1.13	0.24	0.24	0.27				Comp A1
60320	MGZD014	29.0	30.0	1.0	D01379	1.11	0.98	0.98	1.09				Comp A3
60320	MGZD014	30.0	31.0	1.0	D01380	1.26	1.17	1.17	1.47	8.00	6.76	0.85	Comp A3
60320	MGZD014	41.0	42.0	1.0	D02073	1.16	1.75	1.75	2.03				Comp A5
60320	MGZD014	42.0	43.0	1.0	D02074	1.31	2.38	2.38	3.12				Comp A6
60320	MGZD014	43.0	44.0	1.0	D02075	1.2	1.03	1.03	1.24				Comp A3
60320	MGZD014	44.0	45.0	1.0	D02076	1.2	1.04	1.04	1.25				Comp A3
60320	MGZD014	45.0	46.0	1.0	D02077	1.24	1.44	1.44	1.79	5.00	7.64	1.53	Comp A4
60320	MGZD014	60.0	61.0	1.0	D01387	1.23	2.46	2.46	3.03				Comp A7

A ZONE LOW GRADE COMPOSITE (SECTIONS 60240 through 60400)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60320	MGZD014	119.0	120.0	1.0	D01417	1.25	2.95	2.95	3.69	1.00	2.95	2.95	Comp A7
60320	MGZD014	170.0	171.0	1.0	D03541	1.37	1.19	1.19	1.63	1.00	1.19	1.19	Comp A3
60320	MGZD017	86.0	87.0	1.0	D01331	1.26	0.41	0.41	0.52				Comp A1
60320	MGZD017	87.0	88.0	1.0	D01332	1.1	1.85	1.85	2.04				Comp A5
60320	MGZD017	88.0	89.0	1.0	D01334	0.88	0.62	0.62	0.55				Comp A2
60320	MGZD017	89.0	90.0	1.0	D01335	1.23	0.69	0.69	0.85				Comp A2
60320	MGZD017	90.0	91.0	1.0	D01336	1.14	0.71	0.71	0.81				Comp A2
60320	MGZD017	91.0	92.0	1.0	D01337	1.13	0.39	0.39	0.44				Comp A1
60320	MGZD017	92.0	93.0	1.0	D01338	1.1	0.74	0.74	0.81				Comp A2
60320	MGZD017	93.0	94.0	1.0	D01339	1.31	0.68	0.68	0.89				Comp A2
60320	MGZD017	94.0	95.0	1.0	D01340	1.22	1.32	1.32	1.61				Comp A4
60320	MGZD017	95.0	96.0	1.0	D01341	1.24	3.00	3.00	3.72				Comp A8
60320	MGZD017	96.0	97.0	1.0	D01342	1.19	2.43	2.43	2.89				Comp A7
60320	MGZD017	97.0	98.0	1.0	D01343	1.19	4.98	4.98	5.93				Comp A9
60320	MGZD017	98.0	99.0	1.0	D01344	1.3	3.60	3.60	4.68				Comp A8
60320	MGZD017	99.0	100.0	1.0	D01345	1.26	1.26	1.26	1.59	14.00	22.68	1.62	Comp A4
60320	MGZD017	175.0	176.0	1.0	D16322	1.41	2.24	2.24	3.16	1.00	2.24	2.24	Comp A6
60320	MGZD083	130.0	131.0	1.0	D09628	1.33	2.00	2.00	2.66	1.00	2.00	2.00	Comp A6
60320	MGZD083	260.0	261.0	1.0	D09770	1.27	1.66	1.66	2.11				Comp A5
60320	MGZD083	261.0	262.0	1.0	D09772	1.27	0.88	0.88	1.12	2.00	2.54	1.27	Comp A3
60320	MGZD123	23.0	24.0	1.0	D21962	1.08	2.20	2.20	2.38				Comp A6
60320	MGZD123	24.0	25.0	1.0	D21963	1.04	0.70	0.70	0.73				Comp A2
60320	MGZD123	25.0	25.7	0.7	D21964	0.77	5.02	3.51	3.87	2.70	6.41	2.38	Comp A9
60320	MGZD123	37.0	37.7	0.7	D21979	0.82	1.21	0.85	0.99	0.70	0.85	1.21	Comp A4
60320	MGZD123	39.1	40.0	0.9	D21982	1.07	0.95	0.85	1.02				Comp A3
60320	MGZD123	40.0	40.7	0.7	D21983	0.82	0.27	0.19	0.22				Comp A1
60320	MGZD123	40.7	41.4	0.7	D21984	0.86	0.86	0.60	0.74				Comp A3
60320	MGZD123	41.4	42.1	0.7	D21985	0.84	2.11	1.48	1.77	3.00	3.12	1.04	Comp A6
60320	MGZD123	53.0	54.0	1.0	D21999	1.2	2.14	2.14	2.57	1.00	2.14	2.14	Comp A6
60320	MGZD123	67.0	68.0	1.0	D22014	1.17	2.01	2.01	2.35	1.00	2.01	2.01	Comp A6
60320	MGZD123	106.7	107.4	0.7	D22062	0.84	2.07	1.45	1.74	0.70	1.45	2.07	Comp A6
60320	MGZD123	124.0	125.0	1.0	D22082	1.27	2.15	2.15	2.73	1.00	2.15	2.15	Comp A6
60320	MGZD123	156.0	156.7	0.7	D22119	0.83	1.48	1.04	1.23				Comp A4
60320	MGZD123	156.7	157.4	0.7	D22120	0.75	2.57	1.80	1.93	1.40	2.84	2.03	Comp A7
60320	MGZD126	35.0	36.0	1.0	D23890	1.26	1.53	1.53	1.93				Comp A4
60320	MGZD126	36.0	37.0	1.0	D23891	1.29	1.01	1.01	1.30				Comp A3
60320	MGZD126	37.0	38.0	1.0	D23892	1.26	1.82	1.82	2.29	3.00	4.36	1.45	Comp A5
60320	MGZD126	48.0	49.0	1.0	D23905	1.24	1.27	1.27	1.57	1.00	1.27	1.27	Comp A4
60320	MGZD126	68.0	69.0	1.0	D23927	1.17	2.14	2.14	2.50				Comp A6
60320	MGZD126	69.0	70.0	1.0	D23928	1.4	1.53	1.53	2.14	2.00	3.67	1.84	Comp A4
60320	MGZD126	138.0	139.0	1.0	D24004	1.43	2.36	2.36	3.37	1.00	2.36	2.36	Comp A6
60320	MGZD126	175.7	176.4	0.7	D24048	0.76	3.00	2.10	2.28				Comp A8
60320	MGZD126	176.4	177.1	0.7	D24049	0.9	1.44	1.01	1.30	1.40	3.11	2.22	Comp A4
60320	MGZD126	185.0	186.0	1.0	D24059	1.19	1.27	1.27	1.51	1.00	1.27	1.27	Comp A4
60320	MGZD209	121.0	122.0	1.0	D47613	1.62	0.94	0.94	1.52				Comp A3
60320	MGZD209	122.0	123.0	1.0	D47614	1.46	1.07	1.07	1.57				Comp A3
60320	MGZD209	123.0	124.0	1.0	D47615	1.54	0.96	0.96	1.48				Comp A3
60320	MGZD209	124.0	125.0	1.0	D47616	1.76	0.22	0.22	0.39				Comp A1
60320	MGZD209	125.0	126.0	1.0	D47617	1.9	0.67	0.67	1.27	5.00	3.86	0.77	Comp A2
60320	MGZD261	120.8	121.5	0.7	D68022	1.34	1.04	0.73	1.39	0.70	0.73	1.04	Comp A3
60320	MGZD271	62.0	63.0	1.0	D71580	1.99	0.56	0.56	1.11				Comp A2
60320	MGZD271	63.0	64.0	1.0	D71581	1.91	0.77	0.77	1.47				Comp A2
60320	MGZD271	64.0	64.7	0.7	D71582	1.21	0.44	0.31	0.53				Comp A1
60320	MGZD271	64.7	65.4	0.7	D71583	1	1.32	0.92	1.32	3.40	2.56	0.75	Comp A4
60320	MGZD273	0.0	1.0	1.0	D72053	1.2	0.94	0.94	1.13				Comp A3
60320	MGZD273	1.0	2.0	1.0	D72054	1.45	3.52	3.52	5.10	2.00	4.46	2.23	Comp A8
60320	MGZD273	43.0	43.7	0.7	D72103	1.35	0.68	0.48	0.92				Comp A2
60320	MGZD273	43.7	44.4	0.7	D72104	1.24	0.58	0.41	0.72				Comp A2
60320	MGZD273	44.4	45.1	0.7	D72105	1.31	0.81	0.57	1.06				Comp A3
60320	MGZD273	45.1	45.8	0.7	D72106	1.34	1.01	0.71	1.35				Comp A3
60320	MGZD273	45.8	46.5	0.7	D72107	1.22	2.33	1.63	2.84				Comp A6
60320	MGZD273	46.5	47.2	0.7	D72108	1.12	2.19	1.53	2.45				Comp A6

A ZONE LOW GRADE COMPOSITE (SECTIONS 60240 through 60400)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60320	MGZD273	47.9	48.6	0.7	D72110	1.23	0.18	0.13	0.22				Comp A1
60320	MGZD273	48.6	49.3	0.7	D72111	1.07	0.57	0.40	0.61				Comp A2
60320	MGZD273	49.3	50.0	0.7	D72112	1.07	2.22	1.55	2.38	7.00	7.93	1.13	Comp A6
60320	MGZD273	76.2	76.9	0.7	D72150	0.98	2.73	1.91	2.68				Comp A7
60320	MGZD273	76.9	77.6	0.7	D72151	1.04	2.54	1.78	2.64	1.40	3.69	2.63	Comp A7
60320	MGZD290	233.0	234.0	1.0	D78829	1.55	1.15	1.15	1.78	1.00	1.15	1.15	Comp A3
60360	MGZD007	100.0	101.0	1.0	D05579	0.9	2.43	2.43	2.19	1.00	2.43	2.43	Comp A7
60360	MGZD015	151.0	152.0	1.0	D01114	1.23	1.28	1.28	1.57				Comp A4
60360	MGZD015	152.0	153.0	1.0	D01115	1.1	5.06	5.06	5.57				Comp A9
60360	MGZD015	153.0	154.0	1.0	D01116	1.26	1.09	1.09	1.37	3.00	7.43	2.48	Comp A3
60360	MGZD015	200.0	201.0	1.0	D01169	1.14	3.43	3.43	3.91				Comp A8
60360	MGZD015	201.0	202.0	1.0	D01170	0.99	1.60	1.60	1.58				Comp A5
60360	MGZD015	202.0	203.0	1.0	D01172	1.06	1.75	1.75	1.86				Comp A5
60360	MGZD015	203.0	204.0	1.0	D01173	1.21	3.87	3.87	4.68				Comp A8
60360	MGZD015	204.0	205.0	1.0	D01174	1.06	5.20	5.20	5.51				Comp A9
60360	MGZD015	205.0	206.0	1.0	D01175	0.84	2.82	2.82	2.37				Comp A7
60360	MGZD015	206.0	207.0	1.0	D01176	1.08	3.15	3.15	3.40				Comp A8
60360	MGZD015	207.0	208.0	1.0	D01177	1.15	1.68	1.68	1.93				Comp A5
60360	MGZD015	208.0	209.0	1.0	D01178	1.09	0.65	0.65	0.71				Comp A2
60360	MGZD015	209.0	210.0	1.0	D01179	1.13	3.41	3.41	3.85	10.00	27.56	2.76	Comp A8
60360	MGZD016	79.3	80.0	0.7	D01197	0.76	1.90	1.33	1.44				Comp A5
60360	MGZD016	80.0	80.7	0.7	D01199	0.77	3.30	2.31	2.54	1.40	3.64	2.60	Comp A8
60360	MGZD016	124.0	125.0	1.0	D05310	1.19	1.68	1.68	2.00				Comp A5
60360	MGZD016	125.0	126.0	1.0	D05311	1.18	1.70	1.70	2.01	2.00	3.38	1.69	Comp A5
60360	MGZD016	139.3	140.0	0.7	D01217	0.68	2.32	1.62	1.58				Comp A6
60360	MGZD016	140.0	140.7	0.7	D01218	0.67	0.71	0.50	0.48				Comp A2
60360	MGZD016	140.7	141.4	0.7	D01219	0.91	0.81	0.57	0.74				Comp A3
60360	MGZD016	141.4	142.1	0.7	D01220	0.94	0.42	0.29	0.39				Comp A1
60360	MGZD016	142.1	143.0	0.9	D01222	1.19	1.04	0.94	1.24				Comp A3
60360	MGZD016	143.0	144.0	1.0	D01223	1.42	0.57	0.57	0.81	4.70	4.49	0.95	Comp A2
60360	MGZD016	170.0	171.0	1.0	D01229	1.14	1.11	1.11	1.27				Comp A3
60360	MGZD016	171.0	172.0	1.0	D01230	1.21	3.15	3.15	3.81	2.00	4.26	2.13	Comp A8
60360	MGZD016	217.0	218.0	1.0	D04024	1.24	2.68	2.68	3.32	1.00	2.68	2.68	Comp A7
60360	MGZD016	228.0	229.0	1.0	D01260	1.16	2.64	2.64	3.06	1.00	2.64	2.64	Comp A7
60360	MGZD016	236.7	237.4	0.7	D01272	0.84	2.81	1.97	2.36				Comp A7
60360	MGZD016	237.4	238.1	0.7	D01274	0.86	1.60	1.12	1.38	1.40	3.09	2.21	Comp A5
60360	MGZD040	113.4	114.1	0.7	D03352	0.73	1.17	0.82	0.85				Comp A3
60360	MGZD040	114.1	115.0	0.9	D03353	0.92	1.60	1.44	1.47	1.60	2.26	1.41	Comp A5
60360	MGZD040	119.0	120.0	1.0	D03359	1.13	2.71	2.71	3.06	1.00	2.71	2.71	Comp A7
60360	MGZD040	132.4	133.1	0.7	D03375	0.7	2.07	1.45	1.45	0.70	1.45	2.07	Comp A6
60360	MGZD040	135.2	135.9	0.7	D03379	0.65	1.00	0.70	0.65				Comp A3
60360	MGZD040	135.9	136.6	0.7	D03380	0.8	2.63	1.84	2.10	1.40	2.54	1.81	Comp A7
60360	MGZD078	274.4	275.1	0.7	D08948	0.8	2.03	1.42	1.62	0.70	1.42	2.03	Comp A6
60360	MGZD163	124.0	125.0	1.0	D35933	1.41	2.77	2.77	3.91	1.00	2.77	2.77	Comp A7
60360	MGZD190	127.7	128.4	0.7	D43984	0.85	3.27	2.29	2.78				Comp A8
60360	MGZD190	128.4	129.1	0.7	D43985	0.82	1.53	1.07	1.25	1.40	3.36	2.40	Comp A4
60360	MGZD207	118.7	119.4	0.7	D47252	0.89	1.98	1.39	1.76				Comp A5
60360	MGZD207	119.4	120.1	0.7	D47253	0.91	3.02	2.11	2.75				Comp A8
60360	MGZD207	120.1	120.8	0.7	D47254	0.91	3.11	2.18	2.83	2.10	5.68	2.70	Comp A8
60360	MGZD210	152.6	153.3	0.7	D48350	0.8	2.56	1.79	2.05				Comp A7
60360	MGZD210	153.3	154.0	0.7	D48351	0.74	2.45	1.71	1.81	1.40	3.51	2.51	Comp A7
60360	MGZD215	170.4	171.1	0.7	D50507	0.81	2.96	2.07	2.40	0.70	2.07	2.96	Comp A7
60360	MGZD215	233.1	233.8	0.7	D50586	0.9	2.19	1.53	1.97				Comp A6
60360	MGZD215	233.8	234.5	0.7	D50587	0.94	2.39	1.67	2.25	1.40	3.21	2.29	Comp A6
60400	MGZD010	81.0	82.0	1.0	D08349	0.99	1.34	1.34	1.33				Comp A4
60400	MGZD010	82.0	83.0	1.0	D08350	1.03	0.75	0.75	0.77				Comp A2
60400	MGZD010	83.0	84.0	1.0	D08351	1.03	2.27	2.27	2.34				Comp A6
60400	MGZD010	84.0	85.0	1.0	D08352	1.14	0.22	0.22	0.25				Comp A1
60400	MGZD010	85.0	86.0	1.0	D08353	1.06	0.24	0.24	0.25				Comp A1
60400	MGZD010	86.0	87.0	1.0	D08354	0.99	2.83	2.83	2.80	6.00	7.65	1.28	Comp A7
60400	MGZD039	160.0	160.7	0.7	D03241	1.12	0.33	0.23	0.37				Comp A1
60400	MGZD039	160.7	161.4	0.7	D03242	0.98	2.50	1.75	2.45	1.40	1.98	1.42	Comp A7

A ZONE LOW GRADE COMPOSITE (SECTIONS 60240 through 60400)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60400	MGZD041	278.7	279.4	0.7	D04481	0.8	3.46	2.42	2.77				Comp A8
60400	MGZD041	279.4	280.1	0.7	D04482	0.74	1.97	1.38	1.46	2.10	5.99	2.85	Comp A5
60400	MGZD227	297.0	298.0	1.0	D56668	1.76	2.69	2.69	4.73	1.00	2.69	2.69	Comp A7
60400	MGZD254	156.0	157.0	1.0	D65983	1.64	2.31	2.31	3.79				Comp A6
60400	MGZD254	157.0	158.0	1.0	D65984	1.78	0.78	0.78	1.39	2.00	3.09	1.55	Comp A2
60400	MGZD254	187.1	187.8	0.7	D66019	1.11	0.68	0.48	0.75				Comp A2
60400	MGZD254	187.8	188.5	0.7	D66020	1.03	2.31	1.62	2.38	1.40	2.09	1.49	Comp A6
Composite grade (based on (drill core grade x thickness) and meterage, assumes uniform core density)				227.4 m			1.61	365.1					
Composite grade (based on as-received intercept weights and drill core assays)						317.2	1.57		498.0				

A ZONE HIGH GRADE COMPOSITE (SECTIONS 60240 through 60400)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60240	MGZD189	102.0	103.0	1.0	D42713	1.46	3.69	3.69	5.38				Comp A8
60240	MGZD189	103.0	104.0	1.0	D42714	1.53	2.77	2.77	4.24	2.00	6.46	3.23	Comp A7
60240	MGZD195	100.0	101.0	1.0	D44695	1.6	10.00	10.00	16.00	1.00	10.00	10.00	Comp A11
60240	MGZD195	116.0	117.0	1.0	D44713	1.6	1.44	1.44	2.30				Comp A4
60240	MGZD195	117.0	118.0	1.0	D44714	1.61	2.37	2.37	3.81				Comp A6
60240	MGZD195	118.0	119.0	1.0	D44715	1.53	8.62	8.62	13.18				Comp A11
60240	MGZD195	119.0	120.0	1.0	D44716	1.53	2.09	2.09	3.19	4.00	14.51	3.63	Comp A6
60240	MGZD198	143.7	144.4	0.7	D45292	1.02	21.70	15.19	22.13				Comp A12
60240	MGZD198	144.4	145.1	0.7	D45293	1.17	2.06	1.44	2.41	1.40	16.63	11.88	Comp A6
60240	MGZD214	192.0	193.0	1.0	D50203	1.81	51.40	51.40	93.03	1.00	51.40	51.40	Comp A13
60280	MGZD130	70.0	71.0	1.0	D26033	1.39	3.05	3.05	4.24	1.00	3.05	3.05	Comp A8
60280	MGZD159	67.0	67.7	0.7	D34670	1.26	8.60	6.02	10.84				Comp A11
60280	MGZD159	67.7	68.4	0.7	D34672	1.31	4.12	2.88	5.40	1.40	8.90	6.36	Comp A9
60280	MGZD213	77.0	78.0	1.0	D49788	1.56	3.72	3.72	5.80	1.00	3.72	3.72	Comp A8
60320	MGZD008	62.0	63.0	1.0	D01934	1.14	6.70	6.70	7.64	1.00	6.70	6.70	Comp A10
60320	MGZD008	69.0	70.0	1.0	D01941	1.23	3.43	3.43	4.22				Comp A8
60320	MGZD008	70.0	71.0	1.0	D01942	1.03	3.85	3.85	3.97	2.00	7.28	3.64	Comp A8
60320	MGZD008	92.4	93.6	1.2	D00647	1.6	15.60	19.19	24.96	1.20	19.19	15.99	Comp A12
60320	MGZD008	136.0	136.7	0.7	D00694	0.83	7.27	5.09	6.03	0.70	5.09	7.27	Comp A10
60320	MGZD009	31.0	32.0	1.0	D05625	1.04	3.98	3.98	4.14	1.00	3.98	3.98	Comp A8
60320	MGZD009	63.0	64.0	1.0	D01977	1.29	5.60	5.60	7.22				Comp A9
60320	MGZD009	64.0	65.0	1.0	D01979	1.23	0.80	0.80	0.98	2.00	6.40	3.20	Comp A3
60320	MGZD009	153.0	153.7	0.7	D00748	0.78	3.33	2.36	2.60				Comp A8
60320	MGZD009	158.0	159.0	1.0	D00755	1.18	2.79	2.79	3.29	1.70	5.15	3.03	Comp A7
60320	MGZD009	176.0	176.7	0.7	D00775	0.78	9.81	6.87	7.65				Comp A11
60320	MGZD009	176.7	177.7	1.0	D00776	1.24	22.40	22.40	27.78	1.70	29.27	17.22	Comp A12
60320	MGZD009	216.0	217.0	1.0	D04041	1.27	3.09	3.09	3.92				Comp A8
60320	MGZD009	217.0	218.0	1.0	D04042	1.29	3.74	3.74	4.82	2.00	6.83	3.42	Comp A8
60320	MGZD009	226.0	226.7	0.7	D09454	0.8	8.59	6.01	6.87	0.70	6.01	8.59	Comp A11
60320	MGZD014	160.0	161.0	1.0	D03530	1.2	7.55	7.55	9.06	1.00	7.55	7.55	Comp A10
60320	MGZD017	222.0	223.0	1.0	D08560	1.18	6.85	6.85	8.08				Comp A10
60320	MGZD017	223.0	224.0	1.0	D08561	1.25	3.00	3.00	3.75	2.00	9.85	4.93	Comp A8
60320	MGZD123	57.0	57.7	0.7	D22003	0.94	19.20	13.44	18.05				Comp A12
60320	MGZD123	57.7	58.4	0.7	D22004	0.94	1.28	0.90	1.20				Comp A4
60320	MGZD123	58.4	59.1	0.7	D22005	0.96	2.36	1.65	2.27	2.10	15.99	7.61	Comp A6
60320	MGZD123	76.0	77.0	1.0	D22025	1.19	12.40	12.40	14.76				Comp A12
60320	MGZD123	77.0	78.0	1.0	D22026	1.23	2.32	2.32	2.85				Comp A6
60320	MGZD123	78.0	79.0	1.0	D22027	1.16	0.05	0.05	0.06				Comp A1
60320	MGZD123	79.0	80.0	1.0	D22028	1.22	3.04	3.04	3.71	4.00	17.81	4.45	Comp A8
60320	MGZD123	98.7	99.4	0.7	D22050	0.78	8.90	6.23	6.94				Comp A11
60320	MGZD123	99.4	100.1	0.7	D22051	0.81	19.50	13.65	15.80				Comp A12
60320	MGZD123	100.1	100.8	0.7	D22052	0.77	0.71	0.50	0.55				Comp A2
60320	MGZD123	100.8	101.5	0.7	D22053	0.78	2.86	2.00	2.23				Comp A7
60320	MGZD123	101.5	102.2	0.7	D22054	0.7	8.08	5.66	5.66				Comp A11
60320	MGZD123	102.2	102.9	0.7	D22055	0.74	1.20	0.84	0.89				Comp A4
60320	MGZD123	102.9	103.6	0.7	D22056	0.79	5.70	3.99	4.50				Comp A9
60320	MGZD123	103.6	104.3	0.7	D22057	0.78	2.68	1.88	2.09	5.60	34.74	6.20	Comp A7
60320	MGZD126	154.0	154.7	0.7	D24022	0.87	7.85	5.49	6.83				Comp A10
60320	MGZD126	154.7	155.4	0.7	D24023	0.82	39.40	27.58	32.31				Comp A13
60320	MGZD126	155.4	156.1	0.7	D24024	0.89	0.31	0.22	0.28				Comp A1
60320	MGZD126	156.1	156.8	0.7	D24025	0.93	5.07	3.55	4.72	2.80	36.84	13.16	Comp A9
60320	MGZD209	58.0	59.0	1.0	D47543	1.41	5.77	5.77	8.13				Comp A9
60320	MGZD209	59.0	60.0	1.0	D47544	1.46	1.80	1.80	2.62	2.00	7.56	3.78	Comp A5
60320	MGZD209	109.0	110.0	1.0	D47601	1.48	19.30	19.30	28.56				Comp A12
60320	MGZD209	110.0	111.0	1.0	D47602	1.48	45.50	45.50	67.34	2.00	64.80	32.40	Comp A13
60320	MGZD271	21.3	22.0	0.7	D71528	1.17	36.00	25.20	42.12				Comp A13
60320	MGZD271	22.0	22.7	0.7	D71529	1.23	3.08	2.16	3.79				Comp A8
60320	MGZD271	22.7	23.4	0.7	D71530	1.25	2.28	1.60	2.85				Comp A6

A ZONE   HIGH GRADE COMPOSITE   (SECTIONS 60240 through 60400)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60320	MGZD271	23.4	24.1	0.7	D71531	1.19	10.30	7.21	12.26				Comp A11
60320	MGZD271	24.1	24.8	0.7	D71532	1.35	3.77	2.64	5.09	3.50	38.80	11.09	Comp A8
60320	MGZD271	66.1	66.8	0.7	D71585	1.1	8.80	6.16	9.68	0.70	6.16	8.80	Comp A11
60320	MGZD271	85.0	85.7	0.7	D71608	1.02	4.10	2.87	4.18				Comp A9
60320	MGZD271	85.7	86.4	0.7	D71609	0.85	3.40	2.38	2.89	1.40	5.25	3.75	Comp A8
60320	MGZD271	90.6	91.3	0.7	D71616	1.17	2.97	2.08	3.47				Comp A7
60320	MGZD271	91.3	92.0	0.7	D71617	1.31	6.09	4.26	7.98	1.40	6.34	4.53	Comp A10
60320	MGZD271	98.9	99.6	0.7	D71627	0.95	5.13	3.59	4.87				Comp A9
60320	MGZD271	99.6	100.3	0.7	D71628	1.15	1.81	1.27	2.08				Comp A5
60320	MGZD271	100.3	101.0	0.7	D71629	1.13	0.39	0.27	0.44				Comp A1
60320	MGZD271	101.0	101.7	0.7	D71630	1.04	0.55	0.39	0.57				Comp A2
60320	MGZD271	101.7	102.4	0.7	D71631	1.15	4.30	3.01	4.95				Comp A9
60320	MGZD271	102.4	103.1	0.7	D71632	1.12	6.54	4.58	7.32	4.20	13.10	3.12	Comp A10
60320	MGZD271	113.0	114.0	1.0	D71645	1.52	5.15	5.15	7.83	1.00	5.15	5.15	Comp A9
60320	MGZD273	15.4	16.1	0.7	D72070	1.23	15.10	10.57	18.57				Comp A12
60320	MGZD273	16.1	16.8	0.7	D72072	1.23	2.40	1.68	2.95				Comp A7
60320	MGZD273	16.8	17.5	0.7	D72073	1.16	1.37	0.96	1.59				Comp A4
60320	MGZD273	17.5	18.2	0.7	D72074	1.02	7.29	5.10	7.44	2.80	18.31	6.54	Comp A10
60320	MGZD273	55.6	56.3	0.7	D72123	1.3	9.10	6.37	11.83				Comp A11
60320	MGZD273	56.3	57.0	0.7	D72124	1.21	1.18	0.83	1.43	1.40	7.20	5.14	Comp A3
60320	MGZD273	85.0	86.0	1.0	D72161	1.85	8.00	8.00	14.80	1.00	8.00	8.00	Comp A11
60320	MGZD290	40.0	41.0	1.0	D78583	1.41	4.51	4.51	6.36	1.00	4.51	4.51	Comp A9
60320	MGZD290	103.0	104.0	1.0	D78664	1.73	3.97	3.97	6.87	1.00	3.97	3.97	Comp A8
60320	MGZD290	214.0	215.0	1.0	D78806	1.64	5.82	5.82	9.54	1.00	5.82	5.82	Comp A9
60360	MGZD005	128.0	129.0	1.0	D00346	1.37	4.40	4.40	6.03	1.00	4.40	4.40	Comp A9
60360	MGZD005	135.4	137.0	1.6	D00353	0.76	25.00	40.00	19.00				Comp A13
60360	MGZD005	137.0	138.0	1.0	D00354	1.25	1.95	1.95	2.44				Comp A5
60360	MGZD005	138.0	138.7	0.7	D00355	0.71	5.42	3.79	3.85	3.30	45.74	13.86	Comp A9
60360	MGZD005	162.0	163.0	1.0	D00372	0.99	10.50	10.50	10.40				Comp A11
60360	MGZD005	163.0	164.0	1.0	D00373	1.04	38.10	38.10	39.62				Comp A13
60360	MGZD005	164.0	165.0	1.0	D00374	0.98	5.21	5.21	5.11				Comp A9
60360	MGZD005	165.0	166.0	1.0	D00376	0.95	5.86	5.86	5.57				Comp A9
60360	MGZD005	166.0	167.0	1.0	D00377	1.03	0.14	0.14	0.14				Comp A1
60360	MGZD005	167.0	168.0	1.0	D00378	1.12	12.40	12.40	13.89	6.00	72.21	12.04	Comp A12
60360	MGZD015	185.0	186.0	1.0	D01152	1.17	1.10	1.10	1.29				Comp A3
60360	MGZD015	186.0	187.0	1.0	D01154	1.14	5.60	5.60	6.38	2.00	6.70	3.35	Comp A9
60360	MGZD015	216.0	217.0	1.0	D01187	1.17	4.67	4.67	5.46	1.00	4.67	4.67	Comp A9
60360	MGZD016	130.0	130.7	0.7	D01206	0.84	8.76	6.13	7.36	0.70	6.13	8.76	Comp A11
60360	MGZD016	135.0	136.0	1.0	D01212	1.29	22.60	22.60	29.15	1.00	22.60	22.60	Comp A12
60360	MGZD016	240.7	241.4	0.7	D01278	0.81	5.25	3.68	4.25				Comp A9
60360	MGZD016	241.4	242.1	0.7	D01279	0.82	26.40	18.48	21.65				Comp A13
60360	MGZD016	242.1	242.8	0.7	D01280	0.83	3.91	2.74	3.25				Comp A8
60360	MGZD016	242.8	243.5	0.7	D01281	0.8	2.95	2.06	2.36				Comp A7
60360	MGZD016	243.5	244.2	0.7	D01282	0.83	2.98	2.09	2.47	3.50	29.04	8.30	Comp A7
60360	MGZD040	103.0	104.0	1.0	D03337	1.19	1.80	1.80	2.14				Comp A5
60360	MGZD040	104.0	105.0	1.0	D03338	1.07	0.26	0.26	0.28				Comp A1
60360	MGZD040	105.0	106.0	1.0	D03339	1.04	0.50	0.50	0.52				Comp A2
60360	MGZD040	106.0	106.7	0.7	D03340	0.77	2.70	1.89	2.08				Comp A7
60360	MGZD040	106.7	107.4	0.7	D03341	0.75	0.62	0.43	0.47				Comp A2
60360	MGZD040	107.4	108.1	0.7	D03342	0.76	1.55	1.08	1.18				Comp A4
60360	MGZD040	108.1	108.8	0.7	D03344	0.71	5.56	3.89	3.95				Comp A9
60360	MGZD040	108.8	109.5	0.7	D03345	0.76	28.10	19.67	21.36	6.50	29.53	4.54	Comp A13
60360	MGZD040	212.7	213.4	0.7	D03423	0.9	7.35	5.15	6.62				Comp A10
60360	MGZD040	213.4	214.1	0.7	D03424	0.94	75.50	52.85	70.97				Comp A13
60360	MGZD040	214.1	214.8	0.7	D03425	0.93	23.70	16.59	22.04	2.10	74.58	35.52	Comp A12
60360	MGZD078	143.0	144.0	1.0	D16807	1.04	7.30	7.30	7.59				Comp A10
60360	MGZD078	144.0	145.0	1.0	D16808	0.96	7.59	7.59	7.29	2.00	14.89	7.45	Comp A10
60360	MGZD163	257.0	258.0	1.0	D36081	1.76	89.60	89.60	157.70	1.00	89.60	89.60	Comp A13
60360	MGZD190	265.0	266.0	1.0	D44136	1.07	33.80	33.80	36.17	1.00	33.80	33.80	Comp A13
60360	MGZD202	137.0	138.0	1.0	D46412	1.08	41.20	41.20	44.50				Comp A13
60360	MGZD202	138.0	139.0	1.0	D46413	1.09	32.70	32.70	35.64	2.00	73.90	36.95	Comp A13
60360	MGZD202	267.7	268.4	0.7	D46559	0.8	3.16	2.21	2.53				Comp A8
60360	MGZD202	268.4	269.1	0.7	D46560	0.55	2.09	1.46	1.15				Comp A6

A ZONE HIGH GRADE COMPOSITE (SECTIONS 60240 through 60400)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60360	MGZD202	269.1	269.8	0.7	D46561	0.72	4.47	3.13	3.22	2.10	6.80	3.24	Comp A9
60360	MGZD207	123.6	124.3	0.7	D47260	0.88	2.85	2.00	2.51				Comp A7
60360	MGZD207	124.3	125.0	0.7	D47261	0.86	0.93	0.65	0.80				Comp A3
60360	MGZD207	125.0	125.7	0.7	D47262	0.87	21.60	15.12	18.79				Comp A12
60360	MGZD207	125.7	126.4	0.7	D47263	0.88	1.52	1.06	1.34	2.80	18.83	6.73	Comp A4
60360	MGZD207	132.1	132.8	0.7	D47273	0.79	20.90	14.63	16.51				Comp A12
60360	MGZD207	132.8	133.5	0.7	D47274	0.76	8.26	5.78	6.28	1.40	20.41	14.58	Comp A11
60360	MGZD207	134.9	135.6	0.7	D47279	0.78	9.84	6.89	7.68	0.70	6.89	9.84	Comp A11
60360	MGZD207	137.0	137.7	0.7	D47282	0.79	3.06	2.14	2.42	0.70	2.14	3.06	Comp A8
60360	MGZD207	139.8	140.5	0.7	D47286	0.6	3.68	2.58	2.21				Comp A8
60360	MGZD207	140.5	141.2	0.7	D47287	0.57	1.06	0.74	0.60				Comp A3
60360	MGZD207	141.2	141.9	0.7	D47288	0.57	10.00	7.00	5.70				Comp A11
60360	MGZD207	141.9	142.6	0.7	D47289	0.56	0.60	0.42	0.34				Comp A2
60360	MGZD207	142.6	143.3	0.7	D47290	0.52	3.67	2.57	1.91				Comp A8
60360	MGZD207	143.3	144.0	0.7	D47291	0.64	3.54	2.48	2.27				Comp A8
60360	MGZD207	144.0	144.7	0.7	D47292	0.45	4.31	3.02	1.94				Comp A9
60360	MGZD207	144.7	145.4	0.7	D47293	0.87	0.51	0.36	0.44				Comp A2
60360	MGZD207	145.4	146.1	0.7	D47294	0.84	0.81	0.57	0.68				Comp A3
60360	MGZD207	146.1	146.8	0.7	D47295	0.78	2.72	1.90	2.12				Comp A7
60360	MGZD207	146.8	147.5	0.7	D47297	0.96	16.90	11.83	16.22	7.70	33.46	4.35	Comp A12
60360	MGZD210	149.1	149.8	0.7	D48344	0.8	3.03	2.12	2.42				Comp A8
60360	MGZD210	149.8	150.5	0.7	D48345	0.37	25.60	17.92	9.47				Comp A13
60360	MGZD210	150.5	151.2	0.7	D48347	0.84	3.05	2.13	2.56	2.10	22.18	10.56	Comp A8
60360	MGZD210	167.7	168.4	0.7	D48368	0.79	6.85	4.80	5.41	0.70	4.80	6.85	Comp A10
60360	MGZD210	171.2	171.9	0.7	D48374	0.79	3.85	2.70	3.04				Comp A8
60360	MGZD210	171.9	172.6	0.7	D48375	0.81	1.68	1.18	1.36				Comp A5
60360	MGZD210	172.6	173.3	0.7	D48376	0.8	3.73	2.61	2.98				Comp A8
60360	MGZD210	173.3	174.0	0.7	D48377	0.77	3.48	2.44	2.68	2.80	8.92	3.19	Comp A8
60360	MGZD210	176.1	176.8	0.7	D48382	0.78	16.80	11.76	13.10				Comp A12
60360	MGZD210	176.8	177.5	0.7	D48383	0.74	1.32	0.92	0.98				Comp A4
60360	MGZD210	177.5	178.2	0.7	D48384	0.75	13.00	9.10	9.75				Comp A12
60360	MGZD210	178.2	178.9	0.7	D48385	0.73	1.28	0.90	0.93				Comp A4
60360	MGZD210	178.9	179.6	0.7	D48386	0.76	2.18	1.53	1.66				Comp A6
60360	MGZD210	179.6	180.3	0.7	D48387	0.85	11.80	8.26	10.03	4.20	32.47	7.73	Comp A11
60360	MGZD215	103.0	103.7	0.7	D50429	0.81	5.50	3.85	4.46				Comp A9
60360	MGZD215	103.7	104.4	0.7	D50430	0.82	3.39	2.37	2.78				Comp A8
60360	MGZD215	104.4	105.1	0.7	D50431	0.86	3.74	2.62	3.22	2.10	8.84	4.21	Comp A8
60360	MGZD215	217.7	218.4	0.7	D50561	0.75	6.05	4.24	4.54	0.70	4.24	6.05	Comp A10
60360	MGZD215	224.0	224.7	0.7	D50570	0.83	4.29	3.00	3.56				Comp A9
60360	MGZD215	224.7	225.4	0.7	D50572	0.88	1.56	1.09	1.37				Comp A4
60360	MGZD215	225.4	226.1	0.7	D50573	0.84	1.19	0.83	1.00				Comp A3
60360	MGZD215	226.1	226.8	0.7	D50574	0.9	9.97	6.98	8.97				Comp A11
60360	MGZD215	227.5	228.2	0.7	D50577	0.92	1.62	1.13	1.49				Comp A5
60360	MGZD215	228.2	228.9	0.7	D50579	0.85	32.40	22.68	27.54				Comp A13
60360	MGZD215	228.9	229.6	0.7	D50580	0.89	0.78	0.55	0.69				Comp A2
60360	MGZD215	229.6	230.3	0.7	D50581	0.97	5.12	3.58	4.97	6.30	41.03	6.51	Comp A9
60360	MGZD215	238.7	239.4	0.7	D50594	0.88	4.72	3.30	4.15	0.70	3.30	4.72	Comp A9
60400	MGZD038	219.0	219.7	0.7	D03173	0.8	0.57	0.40	0.46				Comp A2
60400	MGZD038	219.7	220.4	0.7	D03174	0.77	8.41	5.89	6.48	1.40	6.29	4.49	Comp A11
60400	MGZD038	225.0	225.7	0.7	D03181	0.69	1.97	1.38	1.36				Comp A5
60400	MGZD038	225.7	226.4	0.7	D03182	0.8	10.10	7.07	8.08	1.40	8.45	6.04	Comp A11
60400	MGZD038	229.9	230.6	0.7	D03188	0.67	5.62	3.93	3.77				Comp A9
60400	MGZD038	230.6	231.3	0.7	D03189	0.68	1.89	1.32	1.29				Comp A5
60400	MGZD038	231.3	232.0	0.7	D03190	0.81	4.71	3.30	3.82	2.10	8.55	4.07	Comp A9
60400	MGZD039	199.0	199.7	0.7	D03251	0.92	1.41	0.99	1.30				Comp A4
60400	MGZD039	199.7	200.4	0.7	D03252	0.78	5.41	3.79	4.22	1.40	4.77	3.41	Comp A9
60400	MGZD039	233.3	234.0	0.7	D03294	0.9	2.15	1.50	1.94				Comp A6
60400	MGZD039	234.0	234.7	0.7	D03295	0.82	1.97	1.38	1.62				Comp A5
60400	MGZD039	234.7	235.4	0.7	D03297	0.8	9.24	6.47	7.39				Comp A11
60400	MGZD039	235.4	236.1	0.7	D03299	0.78	0.53	0.37	0.41				Comp A2
60400	MGZD039	236.1	237.0	0.9	D03300	1.15	0.56	0.50	0.64				Comp A2
60400	MGZD039	237.0	238.0	1.0	D03301	1.18	6.10	6.10	7.20	4.70	16.33	3.47	Comp A10
60400	MGZD039	245.0	245.7	0.7	D03309	0.76	3.28	2.30	2.49				Comp A8

A ZONE HIGH GRADE COMPOSITE (SECTIONS 60240 through 60400)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60400	MGZD039	245.7	246.4	0.7	D03310	0.76	5.60	3.92	4.26				Comp A9
60400	MGZD039	246.4	247.1	0.7	D03311	0.82	3.02	2.11	2.48				Comp A8
60400	MGZD039	247.1	247.8	0.7	D03312	0.72	0.43	0.30	0.31				Comp A1
60400	MGZD039	247.8	248.5	0.7	D03314	0.72	3.28	2.30	2.36				Comp A8
60400	MGZD039	248.5	249.2	0.7	D03315	0.77	3.08	2.16	2.37	4.20	13.08	3.11	Comp A8
60400	MGZD041	195.0	196.0	1.0	D05137	1.21	1.16	1.16	1.40				Comp A3
60400	MGZD041	196.0	197.0	1.0	D05138	1.2	28.60	28.60	34.32	2.00	29.76	14.88	Comp A13
60400	MGZD041	233.0	233.7	0.7	D04464	0.86	3.79	2.65	3.26	0.70	2.65	3.79	Comp A8
60400	MGZD087	198.0	199.0	1.0	D10908	1.27	9.96	9.96	12.65				Comp A11
60400	MGZD087	199.0	200.0	1.0	D10909	1.25	0.81	0.81	1.01	2.00	10.77	5.39	Comp A3
60400	MGZD087	208.4	209.1	0.7	D10922	0.85	3.53	2.47	3.00				Comp A8
60400	MGZD087	209.1	209.8	0.7	D10923	0.83	3.14	2.20	2.61				Comp A8
60400	MGZD087	209.8	210.5	0.7	D10924	0.82	0.72	0.50	0.59				Comp A2
60400	MGZD087	210.5	211.2	0.7	D10925	0.85	4.49	3.14	3.82				Comp A9
60400	MGZD087	211.2	212.0	0.8	D10926	0.97	6.96	5.57	6.75	3.60	13.88	3.86	Comp A10
60400	MGZD089	208.7	209.4	0.7	D11192	0.66	14.60	10.22	9.64				Comp A12
60400	MGZD089	209.4	210.1	0.7	D11193	0.79	7.63	5.34	6.03	1.40	15.56	11.12	Comp A10
60400	MGZD101	152.0	153.0	1.0	D22903	1.15	14.60	14.60	16.79				Comp A12
60400	MGZD101	153.0	154.0	1.0	D22904	1.02	1.74	1.74	1.77	2.00	16.34	8.17	Comp A5
60400	MGZD101	241.1	241.8	0.7	D16002	1.07	1.87	1.31	2.00				Comp A5
60400	MGZD101	241.8	242.5	0.7	D16003	1.04	0.32	0.22	0.33				Comp A1
60400	MGZD101	242.5	243.2	0.7	D16004	1.02	8.78	6.15	8.96	2.10	7.68	3.66	Comp A11
60400	MGZD101	263.0	263.7	0.7	D16028	0.78	7.08	4.96	5.52	0.70	4.96	7.08	Comp A10
60400	MGZD101	296.8	297.5	0.7	D16067	0.89	32.30	22.61	28.75				Comp A13
60400	MGZD101	297.5	298.2	0.7	D16068	0.94	1.41	0.99	1.33				Comp A4
60400	MGZD101	298.2	298.9	0.7	D16069	0.91	4.11	2.88	3.74				Comp A9
60400	MGZD101	298.9	299.6	0.7	D16070	0.87	13.60	9.52	11.83	2.80	35.99	12.86	Comp A12
60400	MGZD227	283.0	284.0	1.0	D56653	1.62	20.40	20.40	33.05	1.00	20.40	20.40	Comp A12
60400	MGZD254	256.0	256.7	0.7	D66099	1.27	1.65	1.15	2.10				Comp A5
60400	MGZD254	256.7	257.4	0.7	D66100	1.44	0.42	0.29	0.60				Comp A1
60400	MGZD254	257.4	258.1	0.7	D66101	1.09	1.75	1.23	1.91				Comp A5
60400	MGZD254	258.1	258.8	0.7	D66102	1.22	1.27	0.89	1.55				Comp A4
60400	MGZD254	258.8	259.5	0.7	D66103	1.26	0.11	0.08	0.14				Comp A1
60400	MGZD254	259.5	260.2	0.7	D66104	1.2	0.37	0.26	0.44				Comp A1
60400	MGZD254	260.2	260.9	0.7	D66105	1.08	1.81	1.27	1.95				Comp A5
60400	MGZD254	260.9	261.6	0.7	D66106	1.08	2.79	1.95	3.01				Comp A7
60400	MGZD254	261.6	262.3	0.7	D66107	0.98	1.87	1.31	1.83				Comp A5
60400	MGZD254	262.3	263.0	0.7	D66108	1.1	1.02	0.71	1.12				Comp A3
60400	MGZD254	263.0	263.7	0.7	D66109	1.02	2.03	1.42	2.07				Comp A6
60400	MGZD254	263.7	264.4	0.7	D66110	0.91	5.71	4.00	5.20				Comp A9
60400	MGZD254	264.4	265.1	0.7	D66111	0.95	7.91	5.54	7.51				Comp A10
60400	MGZD254	265.1	265.8	0.7	D66112	0.95	1.63	1.14	1.55				Comp A5
60400	MGZD254	265.8	266.5	0.7	D66113	0.99	2.19	1.53	2.17				Comp A6
60400	MGZD254	266.5	267.2	0.7	D66114	1.05	3.09	2.16	3.24				Comp A8
60400	MGZD254	267.2	267.9	0.7	D66115	0.97	7.03	4.92	6.82				Comp A10
60400	MGZD254	267.9	268.6	0.7	D66116	1.16	11.60	8.12	13.46				Comp A11
60400	MGZD254	268.6	269.3	0.7	D66117	1.14	2.03	1.42	2.31				Comp A6
60400	MGZD254	269.3	270.0	0.7	D66119	1.03	1.88	1.32	1.94				Comp A5
60400	MGZD254	270.0	270.7	0.7	D66120	1.12	15.60	10.92	17.47	14.70	51.63	3.51	Comp A12
60400	MGZD260	172.0	172.7	0.7	D70220	0.66	3.31	2.32	2.18				Comp A8
60400	MGZD260	172.7	173.4	0.7	D70222	0.63	2.77	1.94	1.75	1.40	4.26	3.04	Comp A7
60400	MGZD260	175.5	176.2	0.7	D70226	0.68	16.90	11.83	11.49				Comp A12
60400	MGZD260	176.2	177.0	0.8	D70227	0.61	1.05	0.84	0.64	1.50	12.67	8.45	Comp A3
60400	MGZD260	185.0	186.0	1.0	D70236	0.88	1.30	1.30	1.14				Comp A4
60400	MGZD260	186.0	187.0	1.0	D70237	0.87	6.09	6.09	5.30	2.00	7.39	3.70	Comp A10
60400	MGZD260	255.7	256.4	0.7	D70316	0.71	16.10	11.27	11.43	0.70	11.27	16.10	Comp A12
60400	MGZD260	286.0	286.7	0.7	D70353	0.58	3.97	2.78	2.30	0.70	2.78	3.97	Comp A8

Composite grade 190.6 m 8.16 1554.7

(based on (drill core grade x thickness) and meterage,assumes uniform core density)

Composite grade 240.49 8.26 1986.0

(based on as-received intercept weights and drill core assays)

B ZONE   LOW GRADE COMPOSITE   (SECTIONS 60440 through 60600)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60440	MGZD002	255	256	1	D00205	1.29	2.75	2.75	3.5475				Comp B25
60440	MGZD002	256	257	1	D00206	1.29	0.32	0.32	0.4128	2	3.07	1.54	Comp B21
60440	MGZD002	259	260	1	D00209	1.27	3.47	3.47	4.4069				Comp B26
60440	MGZD002	260	261	1	D00211	1.18	0.28	0.28	0.3304	2	3.75	1.88	Comp B21
60440	MGZD002	266.6	267.6	1	D00218	1.1	1.61	1.61	1.771				Comp B23
60440	MGZD002	267.6	268.6	1	D00219	1.04	2.99	2.99	3.1096	2	4.6	2.30	Comp B25
60520	MGZD006	158.6	159.35	0.75	D00468	0.83	3.18	2.385	2.6394				Comp B26
60520	MGZD006	159.35	160.06	0.71	D00469	0.69	0.17	0.1207	0.1173				Comp B21
60520	MGZD006	160.06	160.76	0.7	D00470	0.75	1.88	1.316	1.41	2.2	3.8217	1.74	Comp B23
60480	MGZD011	138	139	1	D00806	1.2	0.25	0.25	0.3				Comp B21
60480	MGZD011	139	140	1	D00807	1.2	2.45	2.45	2.94	2	2.7	1.35	Comp B24
60480	MGZD011	143.6	144.8	1.2	D00813	1.42	3.85	4.62	5.467				Comp B26
60480	MGZD011	144.8	146	1.2	D00814	1.42	1.81	2.172	2.5702	2.4	6.792	2.83	Comp B23
60480	MGZD011	157.3	158	0.7	D00828	0.74	2.29	1.603	1.6946				Comp B24
60480	MGZD011	158	158.7	0.7	D00829	0.75	2.96	2.072	2.22	1.4	3.675	2.62	Comp B25
60480	MGZD012	196	197	1	D01024	1.09	1	1	1.09				Comp B23
60480	MGZD012	197	198	1	D01025	1.01	3.01	3.01	3.0401	2	4.01	2.01	Comp B26
60480	MGZD013	229	230	1	D01074	1.16	0.47	0.47	0.5452				Comp B22
60480	MGZD013	230	231	1	D01075	1.02	1.61	1.61	1.6422				Comp B23
60480	MGZD013	231	232	1	D01076	0.99	0.42	0.42	0.4158				Comp B22
60480	MGZD013	232	233	1	D01077	1.06	1.03	1.03	1.0918	4	3.53	0.88	Comp B23
60480	MGZD013	132	133	1	D02013	1.12	0.94	0.94	1.0528				Comp B22
60480	MGZD013	133	134	1	D02014	1.1	1.83	1.83	2.013	2	2.77	1.39	Comp B23
60480	MGZD013	176	177	1	D02042	0.99	2.23	2.23	2.2077				Comp B24
60480	MGZD013	177	178	1	D02043	1.25	1.24	1.24	1.55	2	3.47	1.74	Comp B23
60520	MGZD035	166.7	167.4	0.7	D02956	0.78	2.16	1.512	1.6848				Comp B24
60520	MGZD035	167.4	168.1	0.7	D02957	0.81	1.56	1.092	1.2636				Comp B23
60520	MGZD035	168.1	168.8	0.7	D02958	0.78	4.8	3.36	3.744				Comp B27
60520	MGZD035	168.8	169.5	0.7	D02959	0.74	2.65	1.855	1.961				Comp B25
60520	MGZD035	169.5	170.2	0.7	D02960	0.77	3.4	2.38	2.618	3.5	10.199	2.91	Comp B26
60520	MGZD035	203.4	204.1	0.7	D03003	0.81	3.5	2.45	2.835				Comp B26
60520	MGZD035	204.1	205	0.9	D03004	1.02	0.59	0.531	0.6018	1.6	2.981	1.86	Comp B22
60520	MGZD036	219	220	1	D03099	1.11	2.97	2.97	3.2967	1	2.97	2.97	Comp B25
60520	MGZD036	223	224	1	D03104	1.15	0.8	0.8	0.92				Comp B22
60520	MGZD036	224	225	1	D03105	1.28	3.86	3.86	4.9408	2	4.66	2.33	Comp B26
60560	MGZD042	185	186	1	D04345	1.24	0.74	0.74	0.9176				Comp B22
60560	MGZD042	186	186.7	0.7	D04347	0.81	2.64	1.848	2.1384	1.7	2.588	1.52	Comp B25
60560	MGZD042	231.6	232.3	0.7	D04405	0.77	1	0.7	0.77				Comp B23
60560	MGZD042	232.3	233	0.7	D04406	0.83	1.28	0.896	1.0624				Comp B23
60560	MGZD042	233	234	1	D04407	1.1	0.32	0.32	0.352				Comp B21
60560	MGZD042	234	235	1	D04409	1.09	0.7	0.7	0.763				Comp B22
60560	MGZD042	235	236	1	D04410	1.01	0.56	0.56	0.5656				Comp B22
60560	MGZD042	236	237	1	D04411	1.04	0.76	0.76	0.7904	5.4	3.936	0.73	Comp B22
60560	MGZD044	265	265.7	0.7	D04517	0.84	2.26	1.582	1.8984				Comp B24
60560	MGZD044	265.7	266.4	0.7	D04518	0.72	1.56	1.092	1.1232	1.4	2.674	1.91	Comp B23
60560	MGZD064	257	257.7	0.7	D06727	0.69	3.67	2.569	2.5323				Comp B26
60560	MGZD064	257.7	258.4	0.7	D06728	0.75	0.68	0.476	0.51	1.4	3.045	2.17	Comp B22
60560	MGZD064	269	270	1	D06741	1.08	1.17	1.17	1.2636				Comp B23
60560	MGZD064	270	270.7	0.7	D06742	0.72	2.64	1.848	1.9008	1.7	3.018	1.78	Comp B25
60560	MGZD066	285	286	1	D06931	1.35	0.65	0.65	0.8775				Comp B22
60560	MGZD066	286	287	1	D06932	1.26	3	3	3.78	2	3.65	1.83	Comp B26
60600	MGZD084	235	236	1	D10143	1.24	4.38	4.38	5.4312				Comp B27
60600	MGZD084	236	237	1	D10144	1.2	0.23	0.23	0.276	2	4.61	2.31	Comp B21
60600	MGZD084	250	251	1	D10160	1.18	2.22	2.22	2.6196				Comp B24
60600	MGZD084	251	252	1	D10161	1.17	0.33	0.33	0.3861				Comp B21
60600	MGZD084	252	253	1	D10162	1.18	6.17	6.17	7.2806	3	8.72	2.91	Comp B28
60440	MGZD086	218	219	1	D10356	1.29	2.7	2.7	3.483				Comp B25
60440	MGZD086	219	220	1	D10357	1.21	0.46	0.46	0.5566	2	3.16	1.58	Comp B22

B ZONE LOW GRADE COMPOSITE (SECTIONS 60440 through 60600)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60440	MGZD086	222	223	1	D10361	1.19	3.43	3.43	4.0817				Comp B26
60440	MGZD086	223	224	1	D10362	1.22	0.08	0.08	0.0976	2	3.51	1.76	Comp B21
60600	MGZD090	268.5	269.2	0.7	D11447	0.82	0.32	0.224	0.2624				Comp B21
60600	MGZD090	269.2	269.9	0.7	D11448	0.82	4.33	3.031	3.5506	1.4	3.255	2.32	Comp B27
60600	MGZD093	217.1	217.8	0.7	D11702	1	2.82	1.974	2.82				Comp B25
60600	MGZD093	217.8	218.5	0.7	D11703	1.1	1.04	0.728	1.144	1.4	2.702	1.93	Comp B23
60600	MGZD095	142	143	1	D11973	0.96	5.27	5.27	5.0592				Comp B28
60600	MGZD095	143	144	1	D11974	0.95	0.41	0.41	0.3895	2	5.68	2.84	Comp B22
60480	MGZD096	122	123	1	D12272	0.93	2.88	2.88	2.6784	1	2.88	2.88	Comp B25
60480	MGZD096	141	141.7	0.7	D12292	0.73	1.14	0.798	0.8322				Comp B23
60480	MGZD096	141.7	142.4	0.7	D12293	0.77	2.02	1.414	1.5554	1.4	2.212	1.58	Comp B24
60480	MGZD096	151.2	152	0.8	D12307	0.9	2.99	2.392	2.691				Comp B25
60480	MGZD096	152	153	1	D12308	1.05	0.38	0.38	0.399	1.8	2.772	1.54	Comp B21
60480	MGZD012	79	80	1	D12705	1.13	2.21	2.21	2.4973	1	2.21	2.21	Comp B24
60520	MGZD037	133	134	1	D13274	1.11	2.66	2.66	2.9526	1	2.66	2.66	Comp B25
60520	MGZD035	137	138	1	D13820	1.09	2.48	2.48	2.7032				Comp B24
60520	MGZD035	138	139	1	D13822	1.12	0.89	0.89	0.9968	2	3.37	1.69	Comp B22
60560	MGZD066	155	156	1	D14473	1.07	1.03	1.03	1.1021				Comp B23
60560	MGZD066	156	157	1	D14474	1.01	2.19	2.19	2.2119	2	3.22	1.61	Comp B24
60480	MGZD103	130	131	1	D18364	1.11	2.08	2.08	2.3088	1	2.08	2.08	Comp B24
60480	MGZD103	143	144	1	D18379	1.03	0.49	0.49	0.5047	1	0.49	0.49	Comp B22
60480	MGZD103	177.6	178.3	0.7	D18419	0.88	4.52	3.164	3.9776				Comp B27
60480	MGZD103	178.3	179	0.7	D18420	0.9	0.96	0.672	0.864	1.4	3.836	2.74	Comp B22
60480	MGZD103	182.1	182.8	0.7	D18426	0.84	2.09	1.463	1.7556	0.7	1.463	2.09	Comp B24
60480	MGZD103	220.6	221.3	0.7	D18476	0.96	0.72	0.504	0.6912				Comp B22
60480	MGZD103	221.3	222	0.7	D18477	0.95	1.47	1.029	1.3965				Comp B23
60480	MGZD103	222	222.7	0.7	D18479	0.87	2.2	1.54	1.914	2.1	3.073	1.46	Comp B24
60520	MGZD107	227.1	227.8	0.7	D18715	0.94	2.76	1.932	2.5944	0.7	1.932	2.76	Comp B25
60520	MGZD107	243.9	244.6	0.7	D18742	0.87	2.29	1.603	1.9923				Comp B24
60520	MGZD107	244.6	245.3	0.7	D18743	0.82	3.6	2.52	2.952	1.4	4.123	2.94	Comp B26
60520	MGZD106	24.5	25.2	0.7	D18805	0.69	2.31	1.617	1.5939				Comp B24
60520	MGZD106	25.2	25.9	0.7	D18806	0.79	2.29	1.603	1.8091	1.4	3.22	2.30	Comp B24
60520	MGZD106	34.4	35.1	0.7	D18817	0.76	0.89	0.623	0.6764				Comp B22
60520	MGZD106	35.1	35.8	0.7	D18819	0.71	1.21	0.847	0.8591				Comp B23
60520	MGZD106	35.8	36.5	0.7	D18820	0.73	1.35	0.945	0.9855				Comp B23
60520	MGZD106	36.5	37.2	0.7	D18822	0.86	0.67	0.469	0.5762				Comp B22
60520	MGZD106	37.2	37.9	0.7	D18823	0.79	0.09	0.063	0.0711				Comp B21
60520	MGZD106	37.9	38.6	0.7	D18824	0.85	1.82	1.274	1.547	4.2	4.221	1.01	Comp B23
60520	MGZD082	143	144	1	D22714	1.13	1.56	1.56	1.7628				Comp B23
60520	MGZD082	144	145	1	D22715	1.15	0.92	0.92	1.058	2	2.48	1.24	Comp B22
60520	MGZD006	24	25	1	D23620	1.22	2	2	2.44				Comp B24
60520	MGZD006	25	26	1	D23622	1.19	0.01	0.01	0.0119	2	2.01	1.01	Comp B21
60480	MGZD128	238	239	1	D25901	0.35	2.47	2.47	0.8645				Comp B24
60480	MGZD128	239	239.7	0.7	D25902	0.68	1.02	0.714	0.6936				Comp B23
60480	MGZD128	239.7	240.4	0.7	D25903	0.71	0.64	0.448	0.4544				Comp B22
60480	MGZD128	240.4	241.1	0.7	D25904	0.75	3.7	2.59	2.775				Comp B26
60480	MGZD128	241.1	241.8	0.7	D25905	0.73	0.38	0.266	0.2774				Comp B21
60480	MGZD128	241.8	242.5	0.7	D25906	0.75	3.26	2.282	2.445				Comp B26
60480	MGZD128	242.5	243.2	0.7	D25907	0.71	7.82	5.474	5.5522	5.2	14.244	2.74	Comp B29
60440	MGZD129	256.7	257.4	0.7	D26614	0.94	2.05	1.435	1.927				Comp B24
60440	MGZD129	257.4	258.1	0.7	D26615	0.66	1.98	1.386	1.3068	1.4	2.821	2.02	Comp B23
60480	MGZD131	127	128	1	D26865	1.15	0.69	0.69	0.7935				Comp B22
60480	MGZD131	128	129	1	D26866	1.27	1.6	1.6	2.032				Comp B23
60480	MGZD131	129	130	1	D26867	0.89	0.56	0.56	0.4984				Comp B22
60480	MGZD131	130	131	1	D26868	1.06	0.37	0.37	0.3922				Comp B21
60480	MGZD131	131	132	1	D26869	1.17	0.55	0.55	0.6435				Comp B22
60480	MGZD131	132	133	1	D26870	1.1	1.59	1.59	1.749	6	5.36	0.89	Comp B23
60480	MGZD131	200.4	201.1	0.7	D26949	0.88	1.07	0.749	0.9416				Comp B23
60480	MGZD131	201.1	201.8	0.7	D26950	0.8	0.06	0.042	0.048				Comp B21
60480	MGZD131	201.8	202.5	0.7	D26951	1	1.91	1.337	1.91	2.1	2.128	1.01	Comp B23
60480	MGZD131	209	210	1	D26960	1.33	0.47	0.47	0.6251				Comp B22
60480	MGZD131	210	211	1	D26961	1.17	3.42	3.42	4.0014	2	3.89	1.95	Comp B26
60480	MGZD131	280	281	1	D27041	1.1	2.87	2.87	3.157	1	2.87	2.87	Comp B25

B ZONE LOW GRADE COMPOSITE (SECTIONS 60440 through 60600)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60560	MGZD133	222.7	223.4	0.7	D27697	0.92	1.58	1.106	1.4536				Comp B23
60560	MGZD133	223.4	224.1	0.7	D27699	0.79	2.22	1.554	1.7538				Comp B24
60560	MGZD133	224.1	224.8	0.7	D27700	0.89	2.43	1.701	2.1627				Comp B24
60560	MGZD133	224.8	225.5	0.7	D27701	0.87	2.22	1.554	1.9314	2.8	5.915	2.11	Comp B24
60560	MGZD133	231.7	232.4	0.7	D27709	0.75	0.75	0.525	0.5625				Comp B22
60560	MGZD133	232.4	233.15	0.75	D27710	1.02	3.83	2.8725	3.9066	1.5	3.3975	2.27	Comp B26
60520	MGZD134	197.1	197.8	0.7	D27929	0.79	0.99	0.693	0.7821				Comp B22
60520	MGZD134	197.8	198.5	0.7	D27930	0.84	1.87	1.309	1.5708				Comp B23
60520	MGZD134	198.5	199.2	0.7	D27931	0.86	0.15	0.105	0.129				Comp B21
60520	MGZD134	199.2	199.9	0.7	D27932	0.81	0.62	0.434	0.5022				Comp B22
60520	MGZD134	199.9	200.6	0.7	D27933	0.79	2.95	2.065	2.3305				Comp B25
60520	MGZD134	200.6	201.3	0.7	D27934	0.83	1.97	1.379	1.6351	4.2	5.985	1.43	Comp B23
60520	MGZD134	206.1	206.8	0.7	D27942	0.82	2.45	1.715	2.009	0.7	1.715	2.45	Comp B24
60520	MGZD134	216.7	217.4	0.7	D27955	0.85	2.97	2.079	2.5245				Comp B25
60520	MGZD134	217.4	218.1	0.7	D27956	0.92	2.28	1.596	2.0976				Comp B24
60520	MGZD134	218.8	219.5	0.7	D27959	0.94	3.16	2.212	2.9704	2.1	5.887	2.80	Comp B26
60520	MGZD134	221.6	222.3	0.7	D27963	0.89	5	3.5	4.45				Comp B28
60520	MGZD134	222.3	223	0.7	D27964	0.86	0.81	0.567	0.6966	1.4	4.067	2.91	Comp B22
60520	MGZD134	272.4	273.1	0.7	D28025	0.81	1.88	1.316	1.5228				Comp B23
60520	MGZD134	273.1	273.8	0.7	D28026	0.83	3.7	2.59	3.071	1.4	3.906	2.79	Comp B26
60520	MGZD136	196	197	1	D28724	1.47	3.62	3.62	5.3214				Comp B26
60520	MGZD136	197	198	1	D28725	1.36	0.84	0.84	1.1424	2	4.46	2.23	Comp B22
60520	MGZD136	237.2	237.9	0.7	D28770	0.78	2.97	2.079	2.3166				Comp B25
60520	MGZD136	237.9	238.6	0.7	D28772	0.85	0.54	0.378	0.459	1.4	2.457	1.76	Comp B22
60520	MGZD136	244.7	245.4	0.7	D28781	0.76	3.32	2.324	2.5232				Comp B26
60520	MGZD136	245.4	246.1	0.7	D28782	0.76	2.43	1.701	1.8468	1.4	4.025	2.88	Comp B24
60520	MGZD136	259.7	260.4	0.7	D28799	0.76	3.73	2.611	2.8348				Comp B26
60520	MGZD136	260.4	261.1	0.7	D28800	0.78	0.13	0.091	0.1014				Comp B21
60520	MGZD136	261.1	261.8	0.7	D28801	0.8	3.16	2.212	2.528	2.1	4.914	2.34	Comp B26
60520	MGZD136	292.5	293.2	0.7	D28837	0.77	3.82	2.674	2.9414				Comp B26
60520	MGZD136	293.2	294	0.8	D28839	0.91	0.35	0.28	0.3185	1.5	2.954	1.97	Comp B21
60440	MGZD144	154.2	154.9	0.7	D30392	1.44	0.24	0.168	0.3456				Comp B21
60440	MGZD144	154.9	155.6	0.7	D30393	1.21	3.68	2.576	4.4528	1.4	2.744	1.96	Comp B26
60440	MGZD152	101.7	102.4	0.7	D32066	1	1.92	1.344	1.92				Comp B23
60440	MGZD152	102.4	103.1	0.7	D32067	0.7	3.67	2.569	2.569				Comp B26
60440	MGZD152	103.1	103.8	0.7	D32068	0.89	0.3	0.21	0.267				Comp B21
60440	MGZD152	103.8	104.5	0.7	D32069	1.06	0.53	0.371	0.5618				Comp B22
60440	MGZD152	104.5	105.2	0.7	D32070	1.05	2.91	2.037	3.0555	3.5	6.531	1.87	Comp B25
60480	MGZD172	31.4	32.1	0.7	D38408	1.11	3.69	2.583	4.0959				Comp B26
60480	MGZD172	32.1	32.8	0.7	D38409	0.99	2.45	1.715	2.4255				Comp B24
60480	MGZD172	32.8	33.5	0.7	D38410	1.22	2.56	1.792	3.1232	2.1	6.09	2.90	Comp B25
60480	MGZD172	34.9	35.6	0.7	D38413	1.06	3.5	2.45	3.71				Comp B26
60480	MGZD172	35.6	36.3	0.7	D38414	0.93	1.91	1.337	1.7763				Comp B23
60480	MGZD172	36.3	37	0.7	D38415	0.89	1.46	1.022	1.2994				Comp B23
60480	MGZD172	37	37.7	0.7	D38416	0.93	1.47	1.029	1.3671				Comp B23
60480	MGZD172	37.7	38.4	0.7	D38417	0.88	3.16	2.212	2.7808				Comp B26
60480	MGZD172	38.4	39.1	0.7	D38419	0.93	2.43	1.701	2.2599				Comp B24
60480	MGZD172	39.1	39.8	0.7	D38420	0.89	1.32	0.924	1.1748				Comp B23
60480	MGZD172	39.8	40.5	0.7	D38422	0.94	0.45	0.315	0.423				Comp B22
60480	MGZD172	40.5	41.2	0.7	D38423	1.03	0.87	0.609	0.8961				Comp B22
60480	MGZD172	41.2	41.9	0.7	D38424	1.12	8.26	5.782	9.2512				Comp B29
60480	MGZD172	41.9	42.6	0.7	D38425	1.03	3.07	2.149	3.1621				Comp B26
60480	MGZD172	42.6	43.3	0.7	D38426	1.07	0.3	0.21	0.321				Comp B21
60480	MGZD172	43.3	44	0.7	D38427	1.2	5.19	3.633	6.228				Comp B28
60480	MGZD172	44	45	1	D38428	1.6	1.71	1.71	2.736				Comp B23
60480	MGZD172	45	46	1	D38429	1.76	2.07	2.07	3.6432	11.1	27.153	2.45	Comp B24
60440	MGZD201	187.9	188.6	0.7	D45524	0.85	0.69	0.483	0.5865				Comp B22
60440	MGZD201	188.6	189.3	0.7	D45525	0.79	3.65	2.555	2.8835	1.4	3.038	2.17	Comp B26
60480	MGZD211	122	123	1	D48810	1	2.257	2.257	2.257	1	2.257	2.26	Comp B24
60480	MGZD211	235	235.7	0.7	D48936	0.87	1.38	0.966	1.2006				Comp B23
60480	MGZD211	235.7	236.4	0.7	D48937	0.86	0.95	0.665	0.817	1.4	1.631	1.17	Comp B22
60480	MGZD211	236.4	237.1	0.7	D48939	0.81	3.02	2.114	2.4462				Comp B26
60480	MGZD211	237.1	237.8	0.7	D48940	0.72	2.71	1.897	1.9512				Comp B25

B ZONE   LOW GRADE COMPOSITE   (SECTIONS 60440 through 60600)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60480	MGZD211	237.8	238.5	0.7	D48941	0.77	0.64	0.448	0.4928	2.1	4.459	2.12	Comp B22
60480	MGZD211	259.7	260.4	0.7	D48968	0.76	2.89	2.023	2.1964	0.7	2.023	2.89	Comp B25
60480	MGZD216	123	124	1	D50740	0.98	0.576	0.576	0.56448				Comp B22
60480	MGZD216	124	125	1	D50741	1.02	0.972	0.972	0.99144				Comp B22
60480	MGZD216	125	126	1	D50742	1.01	2.21	2.21	2.2321				Comp B24
60480	MGZD216	126	127	1	D50743	1.02	0.744	0.744	0.75888				Comp B22
60480	MGZD216	127	128	1	D50744	0.97	0.648	0.648	0.62856				Comp B22
60480	MGZD216	128	129	1	D50745	1.06	0.414	0.414	0.43884	6	5.564	0.93	Comp B22
60480	MGZD222	210.7	211.4	0.7	D53714	0.86	2.67	1.869	2.2962				Comp B25
60480	MGZD222	211.4	212.1	0.7	D53715	0.91	0.509	0.3563	0.46319	1.4	2.2253	1.59	Comp B22
60480	MGZD222	213.5	214.2	0.7	D53719	0.8	2.65	1.855	2.12				Comp B25
60480	MGZD222	214.2	215	0.8	D53720	1.22	2.12	1.696	2.5864	1.5	3.551	2.37	Comp B24
60480	MGZD222	215	216	1	D53722	1.09	0.628	0.628	0.68452	1	0.628	0.63	Comp B22
60480	MGZD222	264	265	1	D53779	1.31	2.77	2.77	3.6287	1	2.77	2.77	Comp B25
60560	MGZD224	205.3	206	0.7	D54783	0.87	4.15	2.905	3.6105				Comp B27
60560	MGZD224	206	207	1	D54784	1.09	0.52	0.52	0.5668	1.7	3.425	2.01	Comp B22
60560	MGZD224	254.4	255.1	0.7	D54840	0.92	2.78	1.946	2.5576				Comp B25
60560	MGZD224	255.1	256	0.9	D54841	1.12	0.8	0.72	0.896	1.6	2.666	1.67	Comp B22
60520	MGZD231	169	170	1	D56907	1.17	0.33	0.33	0.3861				Comp B21
60520	MGZD231	170	171	1	D56908	1.19	3.75	3.75	4.4625	2	4.08	2.04	Comp B26
60560	MGZD232	278	279	1	D57394	1.21	1.21	1.21	1.4641				Comp B23
60560	MGZD232	279	280	1	D57395	1.2	3.78	3.78	4.536	2	4.99	2.50	Comp B26
60480	MGZD230	260.4	261.1	0.7	D57769	0.74	0.96	0.672	0.7104				Comp B22
60480	MGZD230	261.1	261.8	0.7	D57770	0.78	1.14	0.798	0.8892	1.4	1.47	1.05	Comp B23
60480	MGZD230	261.8	262.5	0.7	D57772	0.84	1.17	0.819	0.9828				Comp B23
60480	MGZD230	262.5	263.2	0.7	D57773	0.79	0.77	0.539	0.6083	1.4	1.358	0.97	Comp B22
60560	MGZD237	264	265	1	D59689	1.19	2.64	2.64	3.1416				Comp B25
60560	MGZD237	265	266	1	D59690	1.32	0.22	0.22	0.2904	2	2.86	1.43	Comp B21
60480	MGZD238	319	320	1	D60128	1.15	2.44	2.44	2.806	1	2.44	2.44	Comp B24
60600	MGZD249	250	251	1	D63839	1.19	2.06	2.06	2.4514	1	2.06	2.06	Comp B24
60520	MGZD265	164.9	165.6	0.7	D69224	0.86	1.48	1.036	1.2728				Comp B23
60520	MGZD265	165.6	166.3	0.7	D69225	0.79	3.35	2.345	2.6465				Comp B26
60520	MGZD265	166.3	167	0.7	D69226	0.76	1.79	1.253	1.3604				Comp B23
60520	MGZD265	167	167.7	0.7	D69227	0.77	3.61	2.527	2.7797	2.8	7.161	2.56	Comp B26
60600	MGZD294	191.2	192	0.8	D80051	1.12	2.66	2.128	2.9792	0.8	2.128	2.66	Comp B25
60600	MGZD294	266	267	1	D80145	1.27	0.48	0.48	0.6096				Comp B22
60600	MGZD294	267	268	1	D80146	1.2	2.32	2.32	2.784	2	2.8	1.40	Comp B24
Composite grade (based on (drill core grade x thickness) and meterage, assumes uniform core density)				183.0 m			1.92	350.9					
Composite grade (based on as-received intercept weights and drill core assays)						216.42	1.94		419.44121				

B ZONE   HIGH GRADE COMPOSITE   (SECTIONS 60440 through 60600)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60440	MGZD002	239	240	1	D00187	1.23	3.11	3.11	3.8253	1	3.11	3.11	Comp B26
60440	MGZD003	218.2	219.2	1	D00254	1.08	4.8	4.8	5.184	1	4.8	4.80	Comp B27
60520	MGZD006	200.7	201.4	0.7	D00516	0.82	3.74	2.618	3.0668				Comp B26
60520	MGZD006	201.4	202	0.6	D00517	0.81	2.19	1.314	1.7739	1.3	3.932	3.02	Comp B24
60480	MGZD011	164	165	1	D00836	1	20.6	20.6	20.6				Comp B31
60480	MGZD011	165	166	1	D00837	1.1	3.08	3.08	3.388				Comp B26
60480	MGZD011	166	167	1	D00838	1.11	0.46	0.46	0.5106				Comp B22
60480	MGZD011	167	168	1	D00839	1.08	5.77	5.77	6.2316				Comp B28
60480	MGZD011	168	169	1	D00841	1.02	1.16	1.16	1.1832				Comp B23
60480	MGZD011	169	170	1	D00842	1.09	0.06	0.06	0.0654				Comp B21
60480	MGZD011	170	170.6	0.6	D00843	0.65	0.09	0.054	0.0585				Comp B21
60480	MGZD011	170.6	171.3	0.7	D00844	0.71	4.49	3.143	3.1879				Comp B27
60480	MGZD011	171.3	172.3	1	D00845	1.07	7.78	7.78	8.3246				Comp B29
60480	MGZD011	172.3	173.3	1	D00847	1.1	9.19	9.19	10.109				Comp B29
60480	MGZD011	173.3	174.3	1	D00848	1	0.07	0.07	0.07				Comp B21
60480	MGZD011	174.3	175.6	1.3	D00849	1.35	5.44	7.072	7.344				Comp B28
60480	MGZD011	175.6	176.3	0.7	D00850	0.73	10	7	7.3				Comp B30
60480	MGZD011	176.3	177	0.7	D00851	0.79	0.83	0.581	0.6557				Comp B22
60480	MGZD011	177	177.7	0.7	D00852	0.81	0.13	0.091	0.1053				Comp B21
60480	MGZD011	177.7	178.7	1	D00853	1.04	2.6	2.6	2.704				Comp B25
60480	MGZD011	178.7	179.4	0.7	D00854	0.72	2.74	1.918	1.9728				Comp B25
60480	MGZD011	179.4	180.4	1	D00856	0.91	13.8	13.8	12.558				Comp B30
60480	MGZD011	180.4	181.1	0.7	D00857	0.72	2.24	1.568	1.6128	17.1	85.997	5.03	Comp B24
60480	MGZD012	170.8	171.5	0.7	D00992	0.7	11.9	8.33	8.33				Comp B30
60480	MGZD012	171.5	172.2	0.7	D00993	0.69	1.52	1.064	1.0488				Comp B23
60480	MGZD012	172.2	173	0.8	D00994	0.84	3.2	2.56	2.688				Comp B26
60480	MGZD012	174	175	1	D00997	1.01	1.85	1.85	1.8685				Comp B23
60480	MGZD012	175	176	1	D00998	1.05	13.6	13.6	14.28				Comp B30
60480	MGZD012	176	177	1	D00999	1.07	0.59	0.59	0.6313				Comp B22
60480	MGZD012	177	178	1	D01000	1.08	0.44	0.44	0.4752				Comp B22
60480	MGZD012	178	178.7	0.7	D01001	0.92	26	18.2	23.92				Comp B31
60480	MGZD012	178.7	179.4	0.7	D01002	0.6	36.6	25.62	21.96				Comp B32
60480	MGZD012	179.4	180.1	0.7	D01004	0.79	0.58	0.406	0.4582				Comp B22
60480	MGZD012	180.1	180.8	0.7	D01005	0.79	1.5	1.05	1.185				Comp B23
60480	MGZD012	180.8	181.5	0.7	D01006	0.73	56.8	39.76	41.464				Comp B32
60480	MGZD012	181.5	182.2	0.7	D01007	0.68	3.69	2.583	2.5092				Comp B26
60480	MGZD012	182.2	183	0.8	D01008	0.7	1.35	1.08	0.945				Comp B23
60480	MGZD012	183	184	1	D01009	1.26	4.18	4.18	5.2668				Comp B27
60480	MGZD012	184	185	1	D01010	1.06	3.07	3.07	3.2542				Comp B26
60480	MGZD012	185	186	1	D01011	0.99	3.47	3.47	3.4353				Comp B26
60480	MGZD012	186	187	1	D01012	1.02	3.03	3.03	3.0906				Comp B26
60480	MGZD012	187	188	1	D01013	1.07	9.93	9.93	10.6251				Comp B29
60480	MGZD012	188	189	1	D01014	1.02	2.42	2.42	2.4684	18.2	145.243	7.98	Comp B24
60480	MGZD012	204	205	1	D01032	1.07	8.76	8.76	9.3732				Comp B29
60480	MGZD012	205	206	1	D01034	1.06	9.28	9.28	9.8368				Comp B29
60480	MGZD012	207	208	1	D01036	1.07	20.3	20.3	21.721				Comp B31
60480	MGZD012	208	209	1	D01037	1.17	30.4	30.4	35.568				Comp B32
60480	MGZD012	209	210	1	D01038	1.27	10.3	10.3	13.081				Comp B30
60480	MGZD012	210	211	1	D01039	1.2	5.98	5.98	7.176				Comp B28
60480	MGZD012	211	212	1	D01040	1.1	3.43	3.43	3.773				Comp B26
60480	MGZD012	212	213	1	D01041	1.11	1.4	1.4	1.554				Comp B23
60480	MGZD012	213	214	1	D01042	1.03	6.28	6.28	6.4684				Comp B28
60480	MGZD012	214	215	1	D01043	1.1	14.6	14.6	16.06				Comp B30
60480	MGZD012	215	216	1	D01044	1.22	12.2	12.2	14.884				Comp B30
60480	MGZD012	216	217	1	D01045	1.09	5.02	5.02	5.4718				Comp B28
60480	MGZD012	217	218	1	D01047	1.25	17.4	17.4	21.75				Comp B31
60480	MGZD012	218	219	1	D01049	1.16	0.04	0.04	0.0464				Comp B21
60480	MGZD012	219	220	1	D01050	1.24	1.28	1.28	1.5872				Comp B23
60480	MGZD012	220	221	1	D01051	1.22	4.54	4.54	5.5388				Comp B27

B ZONE HIGH GRADE COMPOSITE (SECTIONS 60440 through 60600)

Section	HOLE_ID	Meters From	Meters To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60480	MGZD012	221	222	1	D01052	1.26	0.08	0.08	0.1008				Comp B21
60480	MGZD012	222	223	1	D01053	1.25	0.03	0.03	0.0375				Comp B21
60480	MGZD012	223	224	1	D01054	1.23	0.88	0.88	1.0824				Comp B22
60480	MGZD012	224	225	1	D01055	1.25	13.5	13.5	16.875				Comp B30
60480	MGZD012	225	226	1	D01056	1.17	2.97	2.97	3.4749	22	201.17	9.14	Comp B25
60520	MGZD035	172.3	173	0.7	D02964	0.8	7.41	5.187	5.928				Comp B29
60520	MGZD035	173	173.7	0.7	D02965	0.89	4.04	2.828	3.5956				Comp B27
60520	MGZD035	173.7	174.4	0.7	D02966	0.97	4.12	2.884	3.9964	2.1	10.899	5.19	Comp B27
60520	MGZD035	206.7	207.4	0.7	D03007	0.76	7.43	5.201	5.6468				Comp B29
60520	MGZD035	207.4	208.1	0.7	D03008	0.75	6.23	4.361	4.6725				Comp B28
60520	MGZD035	208.1	208.8	0.7	D03009	0.77	39.6	27.72	30.492				Comp B32
60520	MGZD035	208.8	209.5	0.7	D03010	0.74	22.1	15.47	16.354				Comp B31
60520	MGZD035	209.5	210.2	0.7	D03011	0.76	9.89	6.923	7.5164				Comp B29
60520	MGZD035	210.2	210.9	0.7	D03012	0.64	3.32	2.324	2.1248				Comp B26
60520	MGZD035	210.9	211.6	0.7	D03014	0.68	6.29	4.403	4.2772				Comp B28
60520	MGZD035	211.6	212.3	0.7	D03015	0.67	2.97	2.079	1.9899				Comp B25
60520	MGZD035	212.3	213	0.7	D03016	0.79	2.2	1.54	1.738				Comp B24
60520	MGZD035	213	214	1	D03017	1.14	0.51	0.51	0.5814				Comp B22
60520	MGZD035	214	214.7	0.7	D03018	0.73	1.75	1.225	1.2775				Comp B23
60520	MGZD035	214.7	215.4	0.7	D03019	0.81	4.27	2.989	3.4587				Comp B27
60520	MGZD035	215.4	216.1	0.7	D03020	0.8	8.6	6.02	6.88	9.4	80.765	8.59	Comp B29
60520	MGZD035	226.7	227.4	0.7	D03034	0.82	4.68	3.276	3.8376				Comp B27
60520	MGZD035	227.4	228.1	0.7	D03035	0.85	2.14	1.498	1.819	1.4	4.774	3.41	Comp B24
60520	MGZD036	202	203	1	D03079	0.76	9.2	9.2	6.992				Comp B29
60520	MGZD036	203	204	1	D03080	1.12	4.17	4.17	4.6704				Comp B27
60520	MGZD036	204	204.7	0.7	D03081	0.76	0.13	0.091	0.0988				Comp B21
60520	MGZD036	204.7	205.7	1	D03082	1.05	8.72	8.72	9.156				Comp B29
60520	MGZD036	205.7	206.7	1	D03083	1.12	0.08	0.08	0.0896				Comp B21
60520	MGZD036	206.7	207.4	0.7	D03084	0.84	7.57	5.299	6.3588	5.4	27.56	5.10	Comp B29
60520	MGZD036	228	229	1	D03109	1.22	20.6	20.6	25.132				Comp B31
60520	MGZD036	229	230	1	D03110	1.04	16.4	16.4	17.056				Comp B31
60520	MGZD036	230	231	1	D03111	1.15	2.22	2.22	2.553	3	39.22	13.07	Comp B24
60520	MGZD036	240.4	241.1	0.7	D03124	0.76	14	9.8	10.64	0.7	9.8	14.00	Comp B30
60520	MGZD036	247	247.7	0.7	D03131	0.73	20.8	14.56	15.184				Comp B31
60520	MGZD036	247.7	248.4	0.7	D03132	0.75	8.22	5.754	6.165	1.4	20.314	14.51	Comp B29
60520	MGZD036	251.2	251.9	0.7	D03138	0.75	5.79	4.053	4.3425				Comp B28
60520	MGZD036	251.9	252.6	0.7	D03139	0.77	20	14	15.4				Comp B31
60520	MGZD036	252.6	253.3	0.7	D03140	0.74	13.6	9.52	10.064				Comp B30
60520	MGZD036	253.3	254.04	0.74	D03141	0.74	2.5	1.85	1.85	2.8	29.423	10.51	Comp B25
60520	MGZD036	266	267	1	D03159	1.29	11.2	11.2	14.448	1	11.2	11.20	Comp B30
60560	MGZD042	178.7	179.4	0.7	D04337	0.78	6.23	4.361	4.8594				Comp B28
60560	MGZD042	179.4	180.1	0.7	D04338	0.75	4.78	3.346	3.585				Comp B27
60560	MGZD042	180.1	180.8	0.7	D04339	0.78	1.4	0.98	1.092				Comp B23
60560	MGZD042	180.8	181.5	0.7	D04340	0.85	8.39	5.873	7.1315				Comp B29
60560	MGZD042	181.5	182.2	0.7	D04341	0.77	7.68	5.376	5.9136				Comp B29
60560	MGZD042	182.2	183	0.8	D04342	0.97	9.62	7.696	9.3314	4.3	27.632	6.43	Comp B29
60560	MGZD042	200.1	200.8	0.7	D04365	0.74	20.3	14.21	15.022	0.7	14.21	20.30	Comp B31
60560	MGZD042	204	205	1	D04370	1.19	1.94	1.94	2.3086				Comp B23
60560	MGZD042	205	205.7	0.7	D04372	0.7	33	23.1	23.1	1.7	25.04	14.73	Comp B32
60560	MGZD042	227.4	228.1	0.7	D04399	0.81	17.3	12.11	14.013				Comp B31
60560	MGZD042	228.1	228.8	0.7	D04400	0.71	2.51	1.757	1.7821				Comp B25
60560	MGZD042	228.8	229.5	0.7	D04401	0.74	7.6	5.32	5.624				Comp B29
60560	MGZD042	229.5	230.2	0.7	D04402	0.72	3.87	2.709	2.7864	2.8	21.896	7.82	Comp B26
60560	MGZD044	261.4	262.1	0.7	D04511	0.74	22.5	15.75	16.65				Comp B31
60560	MGZD044	262.1	262.8	0.7	D04512	0.67	0.9	0.63	0.603	1.4	16.38	11.70	Comp B22
60560	MGZD044	268.7	269.4	0.7	D04523	0.7	5.95	4.165	4.165				Comp B28
60560	MGZD044	269.4	270.1	0.7	D04524	0.7	1.85	1.295	1.295				Comp B23
60560	MGZD044	270.1	270.8	0.7	D04525	0.68	3.96	2.772	2.6928				Comp B26
60560	MGZD044	270.8	271.5	0.7	D04526	0.78	3.93	2.751	3.0654				Comp B26
60560	MGZD044	271.5	272.2	0.7	D04527	0.78	2.61	1.827	2.0358				Comp B25
60560	MGZD044	272.2	272.9	0.7	D04529	0.81	3.11	2.177	2.5191	4.2	14.987	3.57	Comp B26
60560	MGZD044	280	281	1	D04538	1.29	8.35	8.35	10.7715	1	8.35	8.35	Comp B29
60560	MGZD066	230	231	1	D06869	0.98	2.63	2.63	2.5774				Comp B25
60560	MGZD066	231	232	1	D06870	1.01	3.31	3.31	3.3431				Comp B26

B ZONE HIGH GRADE COMPOSITE (SECTIONS 60440 through 60600)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60560	MGZD066	232	233	1	D06872	0.96	4.16	4.16	3.9936				Comp B27
60560	MGZD066	233	234	1	D06873	1.01	7.03	7.03	7.1003	4	17.13	4.28	Comp B29
60560	MGZD066	244	245	1	D06885	1.17	3.12	3.12	3.6504				Comp B26
60560	MGZD066	245	246	1	D06886	0.89	11.4	11.4	10.146				Comp B30
60560	MGZD066	246	247	1	D06887	0.96	4.13	4.13	3.9648				Comp B27
60560	MGZD066	247	248	1	D06888	1.07	1.66	1.66	1.7762				Comp B23
60560	MGZD066	248	249	1	D06889	0.89	100	100	89				Comp B32
60560	MGZD066	249	250	1	D06890	0.85	14.8	14.8	12.58	6	135.11	22.52	Comp B30
60560	MGZD066	255	256	1	D06897	1.2	1.76	1.76	2.112				Comp B23
60560	MGZD066	256	257	1	D06899	1.34	16.2	16.2	21.708				Comp B31
60560	MGZD066	257	258	1	D06900	0.91	7.88	7.88	7.1708				Comp B29
60560	MGZD066	258	259	1	D06901	1.31	7.63	7.63	9.9953				Comp B29
60560	MGZD066	259	260	1	D06902	0.92	17.2	17.2	15.824				Comp B31
60560	MGZD066	260	261	1	D06903	1.18	0.46	0.46	0.5428				Comp B22
60560	MGZD066	261	262	1	D06904	0.81	5.62	5.62	4.5522				Comp B28
60560	MGZD066	262	263	1	D06905	0.9	20	20	18				Comp B31
60560	MGZD066	263	264	1	D06906	1.02	1.14	1.14	1.1628				Comp B23
60560	MGZD066	264	265	1	D06907	0.94	12.9	12.9	12.126				Comp B30
60560	MGZD066	265	266	1	D06908	0.85	0.06	0.06	0.051				Comp B21
60560	MGZD066	266	267	1	D06909	1.04	12.2	12.2	12.688	12	103.05	8.59	Comp B30
60560	MGZD066	276	277	1	D06920	1.32	14.1	14.1	18.612	1	14.1	14.10	Comp B30
60520	MGZD082	257.4	258.1	0.7	D09403	0.65	3.1	2.17	2.015				Comp B26
60520	MGZD082	258.1	258.8	0.7	D09404	0.65	2.97	2.079	1.9305				Comp B25
60520	MGZD082	258.8	259.5	0.7	D09405	0.65	2.16	1.512	1.404				Comp B24
60520	MGZD082	259.5	260.2	0.7	D09406	0.72	5.78	4.046	4.1616				Comp B28
60520	MGZD082	260.2	261	0.8	D09407	0.79	4.65	3.72	3.6735				Comp B27
60520	MGZD082	261	261.7	0.7	D09408	0.67	11.5	8.05	7.705				Comp B30
60520	MGZD082	261.7	262.4	0.7	D09409	0.65	6.03	4.221	3.9195				Comp B28
60520	MGZD082	262.4	263.1	0.7	D09410	0.68	2.22	1.554	1.5096	5.7	27.352	4.80	Comp B24
60520	MGZD082	266	266.7	0.7	D09414	0.79	1.3	0.91	1.027				Comp B23
60520	MGZD082	266.7	267.4	0.7	D09415	0.89	31.9	22.33	28.391	1.4	23.24	16.60	Comp B32
60520	MGZD082	270.2	270.9	0.7	D09422	0.82	2.58	1.806	2.1156				Comp B25
60520	MGZD082	270.9	271.6	0.7	D09423	0.78	69.1	48.37	53.898	1.4	50.176	35.84	Comp B32
60600	MGZD084	229.4	230.1	0.7	D10134	0.79	3.75	2.625	2.9625				Comp B26
60600	MGZD084	230.1	230.8	0.7	D10135	0.71	4.93	3.451	3.5003				Comp B27
60600	MGZD084	230.8	231.5	0.7	D10136	0.76	0.07	0.049	0.0532				Comp B21
60600	MGZD084	231.5	232.2	0.7	D10137	0.78	4.33	3.031	3.3774				Comp B27
60600	MGZD084	232.2	232.9	0.7	D10139	0.75	2.31	1.617	1.7325	3.5	10.773	3.08	Comp B24
60600	MGZD084	269	270	1	D10181	1.24	1.68	1.68	2.0832				Comp B23
60600	MGZD084	270	271	1	D10182	1.25	100	100	125	2	101.68	50.84	Comp B32
60440	MGZD086	150	150.7	0.7	D10279	0.9	2.05	1.435	1.845				Comp B24
60440	MGZD086	150.7	151.4	0.7	D10280	0.75	4.8	3.36	3.6				Comp B27
60440	MGZD086	151.4	152.1	0.7	D10281	0.8	4.92	3.444	3.936				Comp B27
60440	MGZD086	152.1	152.8	0.7	D10282	0.73	20.4	14.28	14.892				Comp B31
60440	MGZD086	152.8	153.5	0.7	D10283	0.82	3.45	2.415	2.829				Comp B26
60440	MGZD086	153.5	154.2	0.7	D10284	0.73	1.69	1.183	1.2337	4.2	26.117	6.22	Comp B23
60600	MGZD088	223	223.7	0.7	D10576	0.95	1.86	1.302	1.767				Comp B23
60600	MGZD088	223.7	224.4	0.7	D10577	0.72	1.53	1.071	1.1016				Comp B23
60600	MGZD088	224.4	225.1	0.7	D10579	0.85	29.3	20.51	24.905				Comp B31
60600	MGZD088	225.1	225.8	0.7	D10580	0.79	8.77	6.139	6.9283	2.8	29.022	10.36	Comp B29
60600	MGZD088	233.5	234.2	0.7	D10592	0.8	20.9	14.63	16.72				Comp B31
60600	MGZD088	234.2	234.9	0.7	D10593	0.73	2.32	1.624	1.6936				Comp B24
60600	MGZD088	234.9	235.6	0.7	D10594	0.84	0.07	0.049	0.0588				Comp B21
60600	MGZD088	235.6	236.3	0.7	D10595	0.82	18.5	12.95	15.17				Comp B31
60600	MGZD088	236.3	237	0.7	D10597	0.78	2.91	2.037	2.2698	3.5	31.29	8.94	Comp B25
60600	MGZD088	264	264.7	0.7	D10628	0.82	1.5	1.05	1.23				Comp B23
60600	MGZD088	264.7	265.4	0.7	D10629	0.79	6.78	4.746	5.3562				Comp B28
60600	MGZD088	265.4	266.1	0.7	D10630	0.8	6.59	4.613	5.272				Comp B28
60600	MGZD088	266.1	266.8	0.7	D10631	0.83	7.97	5.579	6.6151				Comp B29
60600	MGZD088	266.8	267.5	0.7	D10632	0.86	6.08	4.256	5.2288				Comp B28
60600	MGZD088	267.5	268.2	0.7	D10633	0.78	7.44	5.208	5.8032				Comp B29
60600	MGZD088	268.2	268.9	0.7	D10634	0.72	2.07	1.449	1.4904	4.9	26.901	5.49	Comp B24
60600	MGZD088	271	271.7	0.7	D10639	0.81	3.51	2.457	2.8431				Comp B26
60600	MGZD088	271.7	272.4	0.7	D10640	0.79	1.2	0.84	0.948				Comp B23

B ZONE HIGH GRADE COMPOSITE (SECTIONS 60440 through 60600)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60600	MGZD088	272.4	273.1	0.7	D10641	0.76	2.16	1.512	1.6416				Comp B24
60600	MGZD088	273.1	273.8	0.7	D10642	0.78	0.09	0.063	0.0702				Comp B21
60600	MGZD088	273.8	274.5	0.7	D10643	0.79	17.4	12.18	13.746	3.5	17.052	4.87	Comp B31
60600	MGZD090	265.7	266.4	0.7	D11442	0.74	4.05	2.835	2.997				Comp B27
60600	MGZD090	266.4	267.1	0.7	D11443	0.7	8.32	5.824	5.824				Comp B29
60600	MGZD090	267.1	267.8	0.7	D11444	0.67	22	15.4	14.74	2.1	24.059	11.46	Comp B31
60600	MGZD093	207.3	208	0.7	D11686	0.71	1.99	1.393	1.4129				Comp B23
60600	MGZD093	208	208.7	0.7	D11687	0.74	7.1	4.97	5.254	1.4	6.363	4.54	Comp B29
60600	MGZD093	212.2	212.9	0.7	D11693	0.79	4.66	3.262	3.6814				Comp B27
60600	MGZD093	212.9	213.6	0.7	D11694	0.84	7.03	4.921	5.9052				Comp B29
60600	MGZD093	213.6	214.3	0.7	D11695	0.85	1.97	1.379	1.6745				Comp B23
60600	MGZD093	214.3	215	0.7	D11697	0.95	2.31	1.617	2.1945	2.8	11.179	3.99	Comp B24
60600	MGZD093	224.8	225.5	0.7	D11713	0.79	6.98	4.886	5.5142				Comp B28
60600	MGZD093	225.5	226.2	0.7	D11714	0.83	0.48	0.336	0.3984				Comp B22
60600	MGZD093	226.2	226.9	0.7	D11715	0.76	5.36	3.752	4.0736	2.1	8.974	4.27	Comp B28
60600	MGZD093	233.9	234.6	0.7	D11728	0.79	13.8	9.66	10.902				Comp B30
60600	MGZD093	234.6	235.3	0.7	D11729	0.85	1.76	1.232	1.496	1.4	10.892	7.78	Comp B23
60600	MGZD095	161.8	162.5	0.7	D11995	0.67	2.92	2.044	1.9564				Comp B25
60600	MGZD095	162.5	163.2	0.7	D11997	0.69	0.67	0.469	0.4623				Comp B22
60600	MGZD095	163.2	163.9	0.7	D11999	0.71	10.9	7.63	7.739	2.1	10.143	4.83	Comp B30
60480	MGZD096	147	147.7	0.7	D12301	0.74	8.7	6.09	6.438				Comp B29
60480	MGZD096	147.7	148.4	0.7	D12302	0.65	5.6	3.92	3.64				Comp B28
60480	MGZD096	148.4	149.1	0.7	D12303	0.78	2.5	1.75	1.95	2.1	11.76	5.60	Comp B25
60480	MGZD096	172.8	173.5	0.7	D12333	0.85	3.06	2.142	2.601				Comp B26
60480	MGZD096	173.5	174.2	0.7	D12334	0.87	0.85	0.595	0.7395				Comp B22
60480	MGZD096	174.2	174.9	0.7	D12335	0.7	1.69	1.183	1.183				Comp B23
60480	MGZD096	174.9	175.6	0.7	D12336	0.67	5.23	3.661	3.5041				Comp B28
60480	MGZD096	175.6	176.3	0.7	D12337	0.65	5.05	3.535	3.2825				Comp B28
60480	MGZD096	176.3	177	0.7	D12339	0.66	1.35	0.945	0.891				Comp B23
60480	MGZD096	177	177.7	0.7	D12340	0.7	0.96	0.672	0.672				Comp B22
60480	MGZD096	177.7	178.4	0.7	D12341	0.68	2.89	2.023	1.9652				Comp B25
60480	MGZD096	178.4	179.1	0.7	D12342	0.71	0.31	0.217	0.2201				Comp B21
60480	MGZD096	179.1	179.8	0.7	D12343	0.69	0.22	0.154	0.1518				Comp B21
60480	MGZD096	179.8	180.5	0.7	D12344	0.73	3.5	2.45	2.555				Comp B26
60480	MGZD096	180.5	181.2	0.7	D12345	0.81	27.4	19.18	22.194				Comp B31
60480	MGZD096	181.2	181.9	0.7	D12347	0.73	26.8	18.76	19.564				Comp B31
60480	MGZD096	181.9	182.6	0.7	D12348	0.73	13.5	9.45	9.855				Comp B30
60480	MGZD096	182.6	183.3	0.7	D12349	0.77	6.71	4.697	5.1667				Comp B28
60480	MGZD096	183.3	184	0.7	D12350	0.66	0.62	0.434	0.4092				Comp B22
60480	MGZD096	184	184.7	0.7	D12351	0.75	1.9	1.33	1.425				Comp B23
60480	MGZD096	184.7	185.4	0.7	D12352	0.73	7.21	5.047	5.2633				Comp B29
60480	MGZD096	185.4	186.1	0.7	D12353	0.51	5.44	3.808	2.7744				Comp B28
60480	MGZD096	186.1	186.8	0.7	D12354	0.75	100	70	75				Comp B32
60480	MGZD096	186.8	187.5	0.7	D12355	0.75	9.21	6.447	6.9075				Comp B29
60480	MGZD096	187.5	188.2	0.7	D12356	0.84	22.3	15.61	18.732				Comp B31
60480	MGZD096	188.2	188.9	0.7	D12357	0.7	9.75	6.825	6.825	16.1	179.165	11.13	Comp B29
60440	MGZD001	113	114	1	D12525	1.08	4.64	4.64	5.0112	1	4.64	4.64	Comp B27
60440	MGZD001	116	117	1	D12528	1.15	3.04	3.04	3.496	1	3.04	3.04	Comp B26
60520	MGZD098	142	143	1	D14861	0.92	19.8	19.8	18.216	1	19.8	19.80	Comp B31
60520	MGZD098	203.9	204.6	0.7	D14931	0.68	2.19	1.533	1.4892				Comp B24
60520	MGZD098	204.6	205.3	0.7	D14932	0.65	7.26	5.082	4.719	1.4	6.615	4.73	Comp B29
60520	MGZD098	209.5	210.2	0.7	D14940	0.87	23.8	16.66	20.706				Comp B31
60520	MGZD098	210.2	210.9	0.7	D14941	0.9	0.19	0.133	0.171				Comp B21
60520	MGZD098	213.7	214.4	0.7	D14947	0.84	7.66	5.362	6.4344				Comp B29
60520	MGZD098	214.4	215.1	0.7	D14948	0.86	0.17	0.119	0.1462				Comp B21
60520	MGZD098	215.1	215.8	0.7	D14949	0.92	0.17	0.119	0.1564				Comp B21
60520	MGZD098	215.8	216.5	0.7	D14950	0.78	33.2	23.24	25.896				Comp B32
60520	MGZD098	216.5	217.2	0.7	D14951	0.88	0.29	0.203	0.2552				Comp B21
60520	MGZD098	217.2	217.9	0.7	D14952	0.84	2.84	1.988	2.3856				Comp B25
60520	MGZD098	217.9	218.6	0.7	D14953	0.75	2.26	1.582	1.695				Comp B24
60520	MGZD098	220	220.7	0.7	D14956	0.78	3.74	2.618	2.9172				Comp B26
60520	MGZD098	220.7	221.4	0.7	D14957	0.78	6.41	4.487	4.9998				Comp B28
60520	MGZD098	221.4	222.1	0.7	D14959	0.85	5.94	4.158	5.049				Comp B28
60520	MGZD098	222.1	222.8	0.7	D14960	0.84	1.65	1.155	1.386				Comp B23
60520	MGZD098	222.8	223.5	0.7	D14961	0.84	8.14	5.698	6.8376				Comp B29

B ZONE HIGH GRADE COMPOSITE (SECTIONS 60440 through 60600)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60520	MGZD098	223.5	224.2	0.7	D14962	0.87	0.2	0.14	0.174				Comp B21
60520	MGZD098	224.2	224.9	0.7	D14963	0.88	7.73	5.411	6.8024				Comp B29
60520	MGZD098	224.9	225.6	0.7	D14964	0.72	2.2	1.54	1.584	11.9	88.683	7.45	Comp B24
60520	MGZD098	228.4	229.1	0.7	D14969	0.84	14.1	9.87	11.844				Comp B30
60520	MGZD098	229.1	229.8	0.7	D14970	0.84	7.08	4.956	5.9472	1.4	14.826	10.59	Comp B29
60520	MGZD098	231.2	231.9	0.7	D14974	0.73	10.3	7.21	7.519				Comp B30
60520	MGZD098	231.9	232.6	0.7	D14975	0.85	2	1.4	1.7				Comp B24
60520	MGZD098	232.6	233.3	0.7	D14976	0.75	2.18	1.526	1.635				Comp B24
60520	MGZD098	233.3	234	0.7	D14977	0.71	16.7	11.69	11.857				Comp B31
60520	MGZD098	234	234.7	0.7	D14979	0.72	2.91	2.037	2.0952				Comp B25
60520	MGZD098	234.7	235.4	0.7	D14980	0.6	14	9.8	8.4				Comp B30
60520	MGZD098	235.4	236.1	0.7	D14981	0.7	7.37	5.159	5.159				Comp B29
60520	MGZD098	236.1	236.8	0.7	D14982	0.68	6.48	4.536	4.4064				Comp B28
60520	MGZD098	236.8	237.5	0.7	D14983	0.71	10.4	7.28	7.384				Comp B30
60520	MGZD098	237.5	238.2	0.7	D14984	0.69	6.08	4.256	4.1952				Comp B28
60520	MGZD098	238.2	238.9	0.7	D14985	0.73	18	12.6	13.14				Comp B31
60520	MGZD098	238.9	239.6	0.7	D14986	0.78	8.71	6.097	6.7938				Comp B29
60520	MGZD098	239.6	240.3	0.7	D14987	0.62	2.5	1.75	1.55				Comp B25
60520	MGZD098	240.3	241	0.7	D14988	0.78	2.97	2.079	2.3166				Comp B25
60520	MGZD098	241	241.7	0.7	D14989	0.78	7.09	4.963	5.5302				Comp B29
60520	MGZD098	241.7	242.4	0.7	D14990	0.81	100	70	81				Comp B32
60520	MGZD098	242.4	243.1	0.7	D14991	0.87	29.8	20.86	25.926				Comp B31
60520	MGZD098	243.1	243.8	0.7	D14992	0.8	8.69	6.083	6.952				Comp B29
60520	MGZD098	243.8	244.5	0.7	D14993	0.8	6.14	4.298	4.912				Comp B28
60520	MGZD098	244.5	245.2	0.7	D14994	0.73	3.03	2.121	2.2119				Comp B26
60520	MGZD098	245.2	245.9	0.7	D14995	0.78	3.3	2.31	2.574				Comp B26
60520	MGZD098	245.9	246.6	0.7	D14997	0.94	1.24	0.868	1.1656				Comp B23
60520	MGZD098	246.6	247.3	0.7	D14999	0.64	1.33	0.931	0.8512				Comp B23
60520	MGZD098	247.3	248	0.7	D15000	0.74	1.61	1.127	1.1914				Comp B23
60520	MGZD098	248	248.7	0.7	D15001	0.69	5.09	3.563	3.5121				Comp B28
60520	MGZD098	248.7	249.4	0.7	D15002	0.84	6.61	4.627	5.5524				Comp B28
60520	MGZD098	249.4	250.1	0.7	D15003	0.77	3.57	2.499	2.7489				Comp B26
60520	MGZD098	250.1	250.8	0.7	D15004	0.85	4.59	3.213	3.9015				Comp B27
60520	MGZD098	250.8	251.5	0.7	D15005	0.78	8.11	5.677	6.3258				Comp B29
60520	MGZD098	251.5	252.2	0.7	D15006	0.83	8.16	5.712	6.7728				Comp B29
60520	MGZD098	252.2	252.9	0.7	D15007	0.83	3.68	2.576	3.0544				Comp B26
60520	MGZD098	252.9	253.6	0.7	D15008	0.7	0.48	0.336	0.336				Comp B22
60520	MGZD098	253.6	254.3	0.7	D15009	0.79	6.65	4.655	5.2535				Comp B28
60520	MGZD098	254.3	255	0.7	D15010	0.66	12.8	8.96	8.448				Comp B30
60520	MGZD098	255	255.7	0.7	D15011	0.71	4.24	2.968	3.0104	24.5	235.767	9.62	Comp B27
60560	MGZD099	181	181.7	0.7	D15804	0.79	1.55	1.085	1.2245				Comp B23
60560	MGZD099	181.7	182.4	0.7	D15805	0.75	1.25	0.875	0.9375				Comp B23
60560	MGZD099	182.4	183.1	0.7	D15806	0.81	1.05	0.735	0.8505				Comp B23
60560	MGZD099	183.1	183.8	0.7	D15807	0.83	9.17	6.419	7.6111				Comp B29
60560	MGZD099	183.8	184.5	0.7	D15808	0.88	2.08	1.456	1.8304	3.5	10.57	3.02	Comp B24
60560	MGZD099	223	224	1	D15852	1.22	0.23	0.23	0.2806				Comp B21
60560	MGZD099	224	225	1	D15853	1.09	13.3	13.3	14.497	2	13.53	6.77	Comp B30
60560	MGZD099	230.7	231.4	0.7	D15861	0.83	82.5	57.75	68.475				Comp B32
60560	MGZD099	231.4	232.1	0.7	D15862	0.79	1.07	0.749	0.8453				Comp B23
60560	MGZD099	232.1	232.8	0.7	D15863	0.8	25.3	17.71	20.24	2.1	76.209	36.29	Comp B31
60560	MGZD099	234.9	235.6	0.7	D15867	0.96	4.4	3.08	4.224				Comp B27
60560	MGZD099	235.6	236.3	0.7	D15868	0.97	11.6	8.12	11.252				Comp B30
60560	MGZD099	236.3	237	0.7	D15869	0.83	2.68	1.876	2.2244	2.1	13.076	6.23	Comp B25
60560	MGZD099	261.7	262.4	0.7	D15900	0.79	4.7	3.29	3.713				Comp B27
60560	MGZD099	262.4	263.1	0.7	D15901	0.83	10.9	7.63	9.047				Comp B30
60560	MGZD099	263.1	263.8	0.7	D15902	0.83	1.6	1.12	1.328	2.1	12.04	5.73	Comp B23
60480	MGZD103	142	143	1	D18377	1.17	7.69	7.69	8.9973	1	7.69	7.69	Comp B29
60480	MGZD103	189	189.7	0.7	D18434	0.73	3.15	2.205	2.2995				Comp B26
60480	MGZD103	189.7	190.4	0.7	D18435	0.77	4.81	3.367	3.7037				Comp B27
60480	MGZD103	190.4	191.1	0.7	D18436	0.7	0.44	0.308	0.308				Comp B22
60480	MGZD103	191.1	192	0.9	D18437	0.99	6.52	5.868	6.4548	3	11.748	3.92	Comp B28
60480	MGZD103	208.7	209.4	0.7	D18457	0.73	6.23	4.361	4.5479				Comp B28
60480	MGZD103	209.4	210.1	0.7	D18459	0.67	0.88	0.616	0.5896	1.4	4.977	3.56	Comp B22
60520	MGZD107	204	204.7	0.7	D18680	0.85	1.34	0.938	1.139				Comp B23

B ZONE   HIGH GRADE COMPOSITE   (SECTIONS 60440 through 60600)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60520	MGZD107	204.7	205.4	0.7	D18681	0.82	11	7.7	9.02				Comp B30
60520	MGZD107	205.4	206.1	0.7	D18682	0.81	25.7	17.99	20.817				Comp B31
60520	MGZD107	206.1	206.8	0.7	D18683	0.86	6.21	4.347	5.3406	2.8	30.975	11.06	Comp B28
60520	MGZD107	210.3	211	0.7	D18689	0.79	2	1.4	1.58				Comp B24
60520	MGZD107	211	211.7	0.7	D18690	0.81	2.38	1.666	1.9278				Comp B24
60520	MGZD107	211.7	212.4	0.7	D18691	0.82	6.37	4.459	5.2234				Comp B28
60520	MGZD107	212.4	213.1	0.7	D18692	0.76	4.25	2.975	3.23				Comp B27
60520	MGZD107	213.1	213.8	0.7	D18693	0.75	13	9.1	9.75				Comp B30
60520	MGZD107	213.8	214.5	0.7	D18694	0.76	3.92	2.744	2.9792	4.2	22.344	5.32	Comp B26
60520	MGZD107	216.6	217.3	0.7	D18700	0.76	5.17	3.619	3.9292				Comp B28
60520	MGZD107	217.3	218	0.7	D18701	0.8	1.62	1.134	1.296				Comp B23
60520	MGZD107	218	218.7	0.7	D18702	0.75	1.26	0.882	0.945				Comp B23
60520	MGZD107	218.7	219.4	0.7	D18703	0.78	1.58	1.106	1.2324				Comp B23
60520	MGZD107	219.4	220.1	0.7	D18704	0.79	4.38	3.066	3.4602				Comp B27
60520	MGZD107	220.1	220.8	0.7	D18705	0.75	1.23	0.861	0.9225				Comp B23
60520	MGZD107	220.8	221.5	0.7	D18706	0.74	8.79	6.153	6.5046				Comp B29
60520	MGZD107	221.5	222.2	0.7	D18707	0.83	2.84	1.988	2.3572	5.6	18.809	3.36	Comp B25
60520	MGZD107	223.6	224.3	0.7	D18710	0.81	2.88	2.016	2.3328				Comp B25
60520	MGZD107	224.3	225	0.7	D18711	0.79	7.04	4.928	5.5616	1.4	6.944	4.96	Comp B29
60520	MGZD107	230.6	231.3	0.7	D18722	0.83	15.5	10.85	12.865				Comp B31
60520	MGZD107	231.3	232	0.7	D18723	0.75	7.57	5.299	5.6775				Comp B29
60520	MGZD107	232	232.7	0.7	D18724	0.77	0.36	0.252	0.2772				Comp B21
60520	MGZD107	232.7	233.4	0.7	D18725	0.8	0.59	0.413	0.472				Comp B22
60520	MGZD107	233.4	234.1	0.7	D18726	0.8	2.31	1.617	1.848	3.5	18.431	5.27	Comp B24
60520	MGZD107	236.9	237.6	0.7	D18731	0.78	54.8	38.36	42.744				Comp B32
60520	MGZD107	237.6	238.3	0.7	D18732	0.69	100	70	69				Comp B32
60520	MGZD107	238.3	239	0.7	D18733	0.77	19.7	13.79	15.169	2.1	122.15	58.17	Comp B31
60520	MGZD107	241.1	241.8	0.7	D18737	0.8	4.83	3.381	3.864				Comp B27
60520	MGZD107	241.8	242.5	0.7	D18739	0.88	27.4	19.18	24.112	1.4	22.561	16.11	Comp B31
60520	MGZD107	246.7	247.4	0.7	D18747	0.87	1.6	1.12	1.392				Comp B23
60520	MGZD107	247.4	248.1	0.7	D18748	0.82	14.4	10.08	11.808	1.4	11.2	8.00	Comp B30
60520	MGZD107	250.2	250.9	0.7	D18752	0.87	6.03	4.221	5.2461				Comp B28
60520	MGZD107	250.9	251.6	0.7	D18753	0.93	0.21	0.147	0.1953	1.4	4.368	3.12	Comp B21
60560	MGZD044	155	156	1	D20839	1.07	5.54	5.54	5.9278				Comp B28
60560	MGZD044	156	157	1	D20840	1	3.39	3.39	3.39	2	8.93	4.47	Comp B26
60480	MGZD128	257	257.7	0.7	D25925	0.83	3.28	2.296	2.7224	0.7	2.296	3.28	Comp B26
60480	MGZD128	261.2	261.9	0.7	D25931	0.82	11.9	8.33	9.758	0.7	8.33	11.90	Comp B30
60440	MGZD129	283	284	1	D26645	1.06	46.6	46.6	49.396	1	46.6	46.60	Comp B32
60440	MGZD129	297.7	298.4	0.7	D26662	0.72	45.1	31.57	32.472				Comp B32
60440	MGZD129	298.4	299.1	0.7	D26663	0.83	38.8	27.16	32.204				Comp B32
60440	MGZD129	299.1	299.8	0.7	D26664	0.75	20.8	14.56	15.6				Comp B31
60440	MGZD129	299.8	300.5	0.7	D26665	0.76	2.49	1.743	1.8924	2.8	75.033	26.80	Comp B24
60480	MGZD131	270	271	1	D27028	1.18	1.93	1.93	2.2774				Comp B23
60480	MGZD131	271	271.7	0.7	D27029	0.79	1.59	1.113	1.2561				Comp B23
60480	MGZD131	271.7	272.4	0.7	D27030	0.74	0.49	0.343	0.3626				Comp B22
60480	MGZD131	272.4	273.1	0.7	D27031	0.77	6.02	4.214	4.6354				Comp B28
60480	MGZD131	273.1	273.8	0.7	D27032	0.7	18.8	13.16	13.16				Comp B31
60480	MGZD131	273.8	274.5	0.7	D27033	0.69	2.43	1.701	1.6767				Comp B24
60480	MGZD131	274.5	275.2	0.7	D27034	0.7	2.02	1.414	1.414	5.2	23.875	4.59	Comp B24
60480	MGZD131	316	317	1	D27081	1.17	18.9	18.9	22.113	1	18.9	18.90	Comp B31
60440	MGZD132	289	290	1	D27406	1.44	4.12	4.12	5.9328				Comp B27
60440	MGZD132	290	290.7	0.7	D27407	1.07	0.19	0.133	0.2033				Comp B21
60440	MGZD132	290.7	291.4	0.7	D27408	0.91	7.45	5.215	6.7795	2.4	9.468	3.94	Comp B29
60520	MGZD134	21	22	1	D27734	1.18	8.44	8.44	9.9592	1	8.44	8.44	Comp B29
60520	MGZD134	224.4	225.1	0.7	D27967	0.92	3.25	2.275	2.99				Comp B26
60520	MGZD134	225.1	225.8	0.7	D27968	0.88	27.4	19.18	24.112				Comp B31
60520	MGZD134	225.8	226.5	0.7	D27969	0.92	3.3	2.31	3.036				Comp B26
60520	MGZD134	226.5	227.2	0.7	D27970	0.93	7.63	5.341	7.0959				Comp B29
60520	MGZD134	227.2	227.9	0.7	D27972	0.85	13.4	9.38	11.39				Comp B30
60520	MGZD134	227.9	228.6	0.7	D27973	0.9	4.99	3.493	4.491	4.2	41.979	10.00	Comp B27
60560	MGZD135	140.7	141.4	0.7	D28264	0.68	3.12	2.184	2.1216				Comp B26
60560	MGZD135	141.4	142.1	0.7	D28265	0.7	12.5	8.75	8.75				Comp B30
60560	MGZD135	142.1	142.8	0.7	D28266	0.71	6.72	4.704	4.7712				Comp B28
60560	MGZD135	142.8	143.5	0.7	D28267	0.63	7.84	5.488	4.9392				Comp B29
60560	MGZD135	143.5	144.2	0.7	D28268	0.7	8.97	6.279	6.279				Comp B29

B ZONE HIGH GRADE COMPOSITE (SECTIONS 60440 through 60600)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60560	MGZD135	144.9	145.6	0.7	D28270	0.61	0.67	0.469	0.4087				Comp B22
60560	MGZD135	145.6	146.3	0.7	D28272	0.7	5.78	4.046	4.046	4.9	31.92	6.51	Comp B28
60520	MGZD136	289.7	290.4	0.7	D28833	0.76	5.58	3.906	4.2408				Comp B28
60520	MGZD136	290.4	291.1	0.7	D28834	0.86	9.43	6.601	8.1098	1.4	10.507	7.51	Comp B29
60440	MGZD144	82	82.7	0.7	D30307	1.11	9.2	6.44	10.212				Comp B29
60440	MGZD144	82.7	83.4	0.7	D30308	1.09	2.83	1.981	3.0847	1.4	8.421	6.02	Comp B25
60440	MGZD144	84.8	85.5	0.7	D30311	1.14	4.02	2.814	4.5828				Comp B27
60440	MGZD144	85.5	86.2	0.7	D30312	1.08	0.89	0.623	0.9612				Comp B22
60440	MGZD144	86.2	86.9	0.7	D30313	1.24	4.48	3.136	5.5552				Comp B27
60440	MGZD144	86.9	87.6	0.7	D30314	1.07	3.09	2.163	3.3063				Comp B26
60440	MGZD144	87.6	88.3	0.7	D30315	1	2.69	1.883	2.69	3.5	10.619	3.03	Comp B25
60440	MGZD149	67.7	68.4	0.7	D31173	1.06	2.46	1.722	2.6076				Comp B24
60440	MGZD149	68.4	69.1	0.7	D31174	1.19	6.53	4.571	7.7707				Comp B28
60440	MGZD149	69.1	69.8	0.7	D31175	1.09	1.48	1.036	1.6132				Comp B23
60440	MGZD149	69.8	70.5	0.7	D31176	0.88	0.68	0.476	0.5984				Comp B22
60440	MGZD149	70.5	71.2	0.7	D31177	1.24	13	9.1	16.12				Comp B30
60440	MGZD149	71.2	71.9	0.7	D31179	0.74	3.97	2.779	2.9378				Comp B26
60440	MGZD149	71.9	72.6	0.7	D31180	1.01	1.47	1.029	1.4847				Comp B23
60440	MGZD149	72.6	73.3	0.7	D31181	0.94	3.96	2.772	3.7224				Comp B26
60440	MGZD149	73.3	74	0.7	D31182	0.97	5.71	3.997	5.5387				Comp B28
60440	MGZD149	74	74.7	0.7	D31183	1.16	5.17	3.619	5.9972				Comp B28
60440	MGZD149	74.7	75.4	0.7	D31184	0.9	3.35	2.345	3.015				Comp B26
60440	MGZD149	75.4	76.1	0.7	D31185	0.93	1.46	1.022	1.3578				Comp B23
60440	MGZD149	76.1	76.8	0.7	D31186	0.95	1.27	0.889	1.2065				Comp B23
60440	MGZD149	76.8	77.5	0.7	D31187	0.85	5.88	4.116	4.998				Comp B28
60440	MGZD149	77.5	78.2	0.7	D31188	1.02	0.69	0.483	0.7038				Comp B22
60440	MGZD149	78.2	78.9	0.7	D31189	1.15	0.58	0.406	0.667				Comp B22
60440	MGZD149	78.9	79.6	0.7	D31190	1.05	10.2	7.14	10.71				Comp B30
60440	MGZD149	79.6	80.3	0.7	D31191	1.21	2.68	1.876	3.2428				Comp B25
60440	MGZD149	80.3	81	0.7	D31192	0.91	5.28	3.696	4.8048				Comp B28
60440	MGZD149	81	81.7	0.7	D31193	1.12	1.08	0.756	1.2096				Comp B23
60440	MGZD149	81.7	82.4	0.7	D31194	1.19	0.45	0.315	0.5355				Comp B22
60440	MGZD149	82.4	83.1	0.7	D31195	1.24	8.95	6.265	11.098				Comp B29
60440	MGZD149	83.1	83.8	0.7	D31197	0.89	3.6	2.52	3.204				Comp B26
60440	MGZD149	83.8	84.5	0.7	D31199	0.99	7.74	5.418	7.6626				Comp B29
60440	MGZD149	84.5	85.2	0.7	D31200	0.99	9.85	6.895	9.7515				Comp B29
60440	MGZD149	85.2	85.9	0.7	D31201	1.15	2.4	1.68	2.76				Comp B24
60440	MGZD149	85.9	86.6	0.7	D31202	1.04	3.98	2.786	4.1392	18.9	79.709	4.22	Comp B26
60440	MGZD152	72	72.7	0.7	D32031	1.01	33.1	23.17	33.431				Comp B32
60440	MGZD152	72.7	73.4	0.7	D32032	0.96	2.92	2.044	2.8032				Comp B25
60440	MGZD152	73.4	74.1	0.7	D32033	0.96	2.92	2.044	2.8032				Comp B25
60440	MGZD152	74.1	75	0.9	D32034	1.15	2.11	1.899	2.4265				Comp B24
60440	MGZD152	75	76	1	D32035	1.43	2.08	2.08	2.9744				Comp B24
60440	MGZD152	76	77	1	D32036	1.39	11.2	11.2	15.568				Comp B30
60440	MGZD152	77	78	1	D32037	1.61	5.98	5.98	9.6278				Comp B28
60440	MGZD152	78	79	1	D32039	1.5	11.2	11.2	16.8				Comp B30
60440	MGZD152	79	80	1	D32040	1.54	1.69	1.69	2.6026				Comp B23
60440	MGZD152	80	81	1	D32041	1.5	1.45	1.45	2.175				Comp B23
60440	MGZD152	81	82	1	D32042	1.35	0.49	0.49	0.6615				Comp B22
60440	MGZD152	82	83	1	D32043	1.42	2.76	2.76	3.9192				Comp B25
60440	MGZD152	83	84	1	D32044	1.48	2.46	2.46	3.6408				Comp B24
60440	MGZD152	84	85	1	D32045	1.37	1.33	1.33	1.8221				Comp B23
60440	MGZD152	85	86	1	D32047	1.38	1.52	1.52	2.0976				Comp B23
60440	MGZD152	86	87	1	D32048	1.66	2.18	2.18	3.6188				Comp B24
60440	MGZD152	87	88	1	D32049	1.75	5.93	5.93	10.3775				Comp B28
60440	MGZD152	88	89	1	D32050	1.59	0.32	0.32	0.5088				Comp B21
60440	MGZD152	89	90	1	D32051	1.79	0.35	0.35	0.6265				Comp B21
60440	MGZD152	90	91	1	D32052	1.8	19.4	19.4	34.92				Comp B31
60440	MGZD152	91	92	1	D32053	1.7	0.62	0.62	1.054				Comp B22
60440	MGZD152	92	93	1	D32054	1.39	19.1	19.1	26.549				Comp B31
60440	MGZD152	93	94	1	D32055	1.38	5.4	5.4	7.452				Comp B28
60440	MGZD152	94	95	1	D32056	1.29	2.17	2.17	2.7993				Comp B24
60440	MGZD152	95	96	1	D32057	1.44	1.21	1.21	1.7424				Comp B23
60440	MGZD152	96	97	1	D32059	1.41	7.73	7.73	10.8993				Comp B29
60440	MGZD152	97	98	1	D32060	1.51	2.73	2.73	4.1223	26	138.457	5.33	Comp B25

B ZONE HIGH GRADE COMPOSITE (SECTIONS 60440 through 60600)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60440	MGZD152	114.3	115	0.7	D32086	1.03	5.2	3.64	5.356				Comp B28
60440	MGZD152	115	115.7	0.7	D32087	1.05	0.64	0.448	0.672				Comp B22
60440	MGZD152	115.7	116.4	0.7	D32088	1.29	3.52	2.464	4.5408				Comp B26
60440	MGZD152	116.4	117.1	0.7	D32089	0.95	5.65	3.955	5.3675	2.8	10.507	3.75	Comp B28
60440	MGZD152	129	129.7	0.7	D32109	1.16	5.53	3.871	6.4148	0.7	3.871	5.53	Comp B28
60480	MGZD172	23	23.7	0.7	D38394	1.09	8.05	5.635	8.7745				Comp B29
60480	MGZD172	23.7	24.4	0.7	D38395	1	4.02	2.814	4.02				Comp B27
60480	MGZD172	24.4	25.1	0.7	D38397	1.17	0.67	0.469	0.7839				Comp B22
60480	MGZD172	25.1	25.8	0.7	D38398	1.13	1.48	1.036	1.6724				Comp B23
60480	MGZD172	25.8	26.5	0.7	D38399	1.12	4.19	2.933	4.6928				Comp B27
60480	MGZD172	26.5	27.2	0.7	D38400	1.14	6.18	4.326	7.0452				Comp B28
60480	MGZD172	27.2	27.9	0.7	D38401	1.07	5.65	3.955	6.0455				Comp B28
60480	MGZD172	27.9	28.6	0.7	D38402	1.08	1.33	0.931	1.4364				Comp B23
60480	MGZD172	28.6	29.3	0.7	D38403	1.14	2.37	1.659	2.7018	6.3	23.758	3.77	Comp B24
60480	MGZD172	49.7	50.4	0.7	D38434	0.97	16.8	11.76	16.296				Comp B31
60480	MGZD172	50.4	51.1	0.7	D38435	1.08	1.75	1.225	1.89				Comp B23
60480	MGZD172	51.1	51.8	0.7	D38436	1.06	2.21	1.547	2.3426				Comp B24
60480	MGZD172	51.8	52.5	0.7	D38437	1.2	2.85	1.995	3.42	2.8	16.527	5.90	Comp B25
60480	MGZD172	55.3	56	0.7	D38443	1.26	6.36	4.452	8.0136				Comp B28
60480	MGZD172	56	56.7	0.7	D38444	1.21	1	0.7	1.21				Comp B23
60480	MGZD172	56.7	57.4	0.7	D38445	1.02	12.1	8.47	12.342				Comp B30
60480	MGZD172	57.4	58.1	0.7	D38447	1.14	15.1	10.57	17.214				Comp B31
60480	MGZD172	58.1	58.8	0.7	D38448	1.23	7.79	5.453	9.5817				Comp B29
60480	MGZD172	58.8	59.5	0.7	D38449	1.17	0.2	0.14	0.234				Comp B21
60480	MGZD172	59.5	60.2	0.7	D38450	1.21	0.11	0.077	0.1331				Comp B21
60480	MGZD172	60.2	60.9	0.7	D38451	1.02	3.01	2.107	3.0702				Comp B26
60480	MGZD172	60.9	61.6	0.7	D38452	1.19	3.04	2.128	3.6176				Comp B26
60480	MGZD172	61.6	62.3	0.7	D38453	1.27	0.2	0.14	0.254				Comp B21
60480	MGZD172	62.3	63	0.7	D38454	1.16	4.87	3.409	5.6492	7.7	37.646	4.89	Comp B27
60520	MGZD184	73	73.7	0.7	D40526	1.08	3	2.1	3.24	0.7	2.1	3.00	Comp B26
60520	MGZD184	75.8	76.5	0.7	D40530	1.08	12.5	8.75	13.5				Comp B30
60520	MGZD184	76.5	77.2	0.7	D40531	1.19	2.54	1.778	3.0226	1.4	10.528	7.52	Comp B25
60440	MGZD197	161	162	1	D44926	1.05	17.5	17.5	18.375	1	17.5	17.50	Comp B31
60440	MGZD197	172	173	1	D44937	1.11	1.36	1.36	1.5096				Comp B23
60440	MGZD197	173	174	1	D44939	1.13	4.643	4.643	5.24659	2	6.003	3.00	Comp B27
60440	MGZD197	247.1	247.8	0.7	D45032	0.77	12.6	8.82	9.702				Comp B30
60440	MGZD197	247.8	248.5	0.7	D45033	0.86	25.4	17.78	21.844				Comp B31
60440	MGZD197	248.5	249.2	0.7	D45034	0.77	7.14	4.998	5.4978	2.1	31.598	15.05	Comp B29
60440	MGZD197	260.3	261	0.7	D45052	0.89	2.03	1.421	1.8067				Comp B24
60440	MGZD197	261	261.7	0.7	D45053	0.83	23.5	16.45	19.505	1.4	17.871	12.76	Comp B31
60440	MGZD197	287.1	287.8	0.7	D45087	0.92	0.95	0.665	0.874				Comp B22
60440	MGZD197	287.8	288.5	0.7	D45088	0.9	19	13.3	17.1	1.4	13.965	9.97	Comp B31
60440	MGZD197	293.4	294.1	0.7	D45097	0.93	16.8	11.76	15.624	0.7	11.76	16.80	Comp B31
60440	MGZD201	184.4	185.1	0.7	D45517	0.75	0.36	0.252	0.27				Comp B21
60440	MGZD201	185.1	185.8	0.7	D45519	0.71	7.43	5.201	5.2753	1.4	5.453	3.90	Comp B29
60440	MGZD201	190.7	191.4	0.7	D45528	0.95	51.6	36.12	49.02				Comp B32
60440	MGZD201	191.4	192.1	0.7	D45529	0.9	0.57	0.399	0.513	1.4	36.519	26.09	Comp B22
60440	MGZD201	192.8	193.5	0.7	D45531	0.88	1.87	1.309	1.6456				Comp B23
60440	MGZD201	193.5	194.2	0.7	D45532	0.77	23.9	16.73	18.403	1.4	18.039	12.88	Comp B31
60480	MGZD205	128	129	1	D46889	0.94	10	10	9.4				Comp B30
60480	MGZD205	129	130	1	D46890	0.8	4.253	4.253	3.4024	2	14.253	7.13	Comp B27
60480	MGZD211	183	184	1	D48879	1.01	10	10	10.1	1	10	10.00	Comp B30
60480	MGZD211	245	245.7	0.7	D48950	0.75	3.36	2.352	2.52				Comp B26
60480	MGZD211	245.7	246.4	0.7	D48951	0.8	8.15	5.705	6.52				Comp B29
60480	MGZD211	246.4	247.1	0.7	D48952	0.78	1.56	1.092	1.2168	2.1	9.149	4.36	Comp B23
60480	MGZD211	278	279	1	D48989	1.23	48.1	48.1	59.163	1	48.1	48.10	Comp B32
60480	MGZD211	294.2	294.9	0.7	D49010	0.76	3.75	2.625	2.85	0.7	2.625	3.75	Comp B26
60520	MGZD220	137	138	1	D52103	1.27	3.17	3.17	4.0259				Comp B26
60520	MGZD220	138	139	1	D52104	0.98	6.04	6.04	5.9192				Comp B28
60520	MGZD220	139	140	1	D52105	1.09	2.39	2.39	2.6051	3	11.6	3.87	Comp B24
60520	MGZD220	261.7	262.4	0.7	D52245	0.76	5.4	3.78	4.104				Comp B28
60520	MGZD220	262.4	263.1	0.7	D52247	0.95	29.3	20.51	27.835	1.4	24.29	17.35	Comp B31
60480	MGZD222	191.4	192.1	0.7	D53691	0.9	9.14	6.398	8.226				Comp B29
60480	MGZD222	192.1	192.8	0.7	D53692	0.98	2.84	1.988	2.7832	1.4	8.386	5.99	Comp B25
60480	MGZD222	246	247	1	D53759	1.12	3.46	3.46	3.8752	1	3.46	3.46	Comp B26

B ZONE HIGH GRADE COMPOSITE (SECTIONS 60440 through 60600)

Section	HOLE_ID	Meters From	Meters To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60480	MGZD222	268	269	1	D53783	1.45	7.11	7.11	10.3095	1	7.11	7.11	Comp B29
60480	MGZD222	283.7	284.4	0.7	D53803	0.99	5.56	3.892	5.5044				Comp B28
60480	MGZD222	284.4	285.1	0.7	D53804	1.05	9.04	6.328	9.492				Comp B29
60480	MGZD222	285.1	285.8	0.7	D53805	1.06	1.33	0.931	1.4098				Comp B23
60480	MGZD222	285.8	286.5	0.7	D53806	1.12	5.7	3.99	6.384				Comp B28
60480	MGZD222	286.5	287.2	0.7	D53807	1.01	8.15	5.705	8.2315				Comp B29
60480	MGZD222	287.2	287.9	0.7	D53808	1.05	0.494	0.3458	0.5187				Comp B22
60480	MGZD222	287.9	288.6	0.7	D53809	1.02	0.249	0.1743	0.25398				Comp B21
60480	MGZD222	288.6	289.3	0.7	D53810	0.98	5.94	4.158	5.8212				Comp B28
60480	MGZD222	289.3	290	0.7	D53811	1	2.02	1.414	2.02	6.3	26.9381	4.28	Comp B24
60560	MGZD224	141	142	1	D54708	0.97	1.47	1.47	1.4259				Comp B23
60560	MGZD224	142	143	1	D54709	0.98	11.25	11.25	11.025				Comp B30
60560	MGZD224	143	144	1	D54710	1.1	1.19	1.19	1.309				Comp B23
60560	MGZD224	144	145	1	D54711	0.99	7.85	7.85	7.7715				Comp B29
60560	MGZD224	145	146	1	D54712	1	2.23	2.23	2.23				Comp B24
60560	MGZD224	146	147	1	D54713	0.98	2.47	2.47	2.4206				Comp B24
60560	MGZD224	147	148	1	D54714	1.04	1.605	1.605	1.6692				Comp B23
60560	MGZD224	148	149	1	D54715	1	4.36	4.36	4.36	8	32.425	4.05	Comp B27
60560	MGZD224	199.8	200.5	0.7	D54774	0.84	17.6	12.32	14.784				Comp B31
60560	MGZD224	213	214	1	D54791	1.13	23.6	23.6	26.668	1	23.6	23.60	Comp B31
60560	MGZD224	216	216.7	0.7	D54794	0.88	18.2	12.74	16.016				Comp B31
60560	MGZD224	216.7	217.4	0.7	D54795	0.8	9.71	6.797	7.768				Comp B29
60560	MGZD224	217.4	218.1	0.7	D54797	0.76	0.06	0.042	0.0456				Comp B21
60560	MGZD224	218.1	218.8	0.7	D54799	0.8	7.72	5.404	6.176				Comp B29
60560	MGZD224	218.8	219.5	0.7	D54800	0.94	20	14	18.8	3.5	38.983	11.14	Comp B31
60560	MGZD224	253	253.7	0.7	D54837	0.82	55.5	38.85	45.51	0.7	38.85	55.50	Comp B32
60560	MGZD224	270.7	271.4	0.7	D54861	0.89	2.08	1.456	1.8512				Comp B24
60560	MGZD224	271.4	272.1	0.7	D54862	0.83	5.95	4.165	4.9385				Comp B28
60560	MGZD224	272.1	272.8	0.7	D54863	0.83	1.44	1.008	1.1952	2.1	6.629	3.16	Comp B23
60560	MGZD224	276.7	277.4	0.7	D54869	0.79	5.08	3.556	4.0132				Comp B28
60560	MGZD224	277.4	278.1	0.7	D54870	0.86	1.91	1.337	1.6426	1.4	4.893	3.50	Comp B23
60520	MGZD225	256	257	1	D55181	1.26	9.48	9.48	11.9448				Comp B29
60520	MGZD225	281.7	282.4	0.7	D55210	0.95	1.38	0.966	1.311				Comp B23
60520	MGZD225	282.4	283.1	0.7	D55211	0.86	2.78	1.946	2.3908				Comp B25
60520	MGZD225	283.1	283.8	0.7	D55212	0.89	0.31	0.217	0.2759				Comp B21
60520	MGZD225	283.8	284.5	0.7	D55213	0.85	2.68	1.876	2.278				Comp B25
60520	MGZD225	284.5	285.2	0.7	D55214	0.89	2.47	1.729	2.1983				Comp B24
60520	MGZD225	285.2	285.9	0.7	D55215	0.87	2.02	1.414	1.7574	5.2	17.628	3.39	Comp B24
60440	MGZD226	290.5	291.2	0.7	D55569	0.79	11.4	7.98	9.006	0.7	7.98	11.40	Comp B30
60520	MGZD231	240	241	1	D56986	1.09	4.57	4.57	4.9813	1	4.57	4.57	Comp B27
60560	MGZD232	196.1	196.8	0.7	D57295	0.96	2.79	1.953	2.6784				Comp B25
60560	MGZD232	196.8	197.5	0.7	D57297	0.78	4.39	3.073	3.4242	1.4	5.026	3.59	Comp B27
60560	MGZD232	205.7	206.4	0.7	D57308	0.89	0.98	0.686	0.8722				Comp B22
60560	MGZD232	206.4	207.1	0.7	D57309	0.9	15.5	10.85	13.95	1.4	11.536	8.24	Comp B31
60560	MGZD232	259	259.7	0.7	D57372	0.89	53.8	37.66	47.882				Comp B32
60560	MGZD232	259.7	260.4	0.7	D57373	0.92	2.68	1.876	2.4656	1.4	39.536	28.24	Comp B25
60560	MGZD232	283	283.7	0.7	D57401	0.81	2.57	1.799	2.0817				Comp B25
60560	MGZD232	283.7	284.4	0.7	D57402	0.73	8.47	5.929	6.1831				Comp B29
60560	MGZD232	284.4	285.1	0.7	D57403	0.76	2.33	1.631	1.7708	2.1	9.359	4.46	Comp B24
60480	MGZD230	244.3	245	0.7	D57749	0.83	8.36	5.852	6.9388				Comp B29
60480	MGZD230	245	245.7	0.7	D57750	0.79	14.5	10.15	11.455				Comp B30
60480	MGZD230	245.7	246.4	0.7	D57751	0.75	1.77	1.239	1.3275	2.1	17.241	8.21	Comp B23
60520	MGZD234	294	294.7	0.7	D58627	0.8	1.82	1.274	1.456				Comp B23
60520	MGZD234	294.7	295.4	0.7	D58628	0.92	20.7	14.49	19.044				Comp B31
60520	MGZD234	295.4	296.1	0.7	D58629	0.94	7.21	5.047	6.7774	2.1	20.811	9.91	Comp B29
60560	MGZD237	256.1	256.8	0.7	D59679	0.8	2.35	1.645	1.88				Comp B24
60560	MGZD237	256.8	257.5	0.7	D59680	0.6	6.65	4.655	3.99	1.4	6.3	4.50	Comp B28
60480	MGZD238	292.7	293.4	0.7	D60095	0.79	5.35	3.745	4.2265	0.7	3.745	5.35	Comp B28
60480	MGZD238	293.4	294.1	0.7	D60097	0.77	10.9	7.63	8.393	0.7	7.63	10.90	Comp B30
60480	MGZD238	301	301.7	0.7	D60106	0.71	10.4	7.28	7.384				Comp B30
60480	MGZD238	301.7	302.4	0.7	D60107	0.81	0.23	0.161	0.1863	1.4	7.441	5.31	Comp B21
60440	MGZD245	210	211	1	D62814	1.15	5.84	5.84	6.716	1	5.84	5.84	Comp B28
60440	MGZD245	238.5	239.2	0.7	D62852	0.81	4.86	3.402	3.9366	0.7	3.402	4.86	Comp B27
60440	MGZD245	244.8	245.5	0.7	D62862	0.97	3.79	2.653	3.6763				Comp B26
60440	MGZD245	245.5	246.2	0.7	D62863	0.83	2.81	1.967	2.3323	1.4	4.62	3.30	Comp B25

B ZONE HIGH GRADE COMPOSITE (SECTIONS 60440 through 60600)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60440	MGZD245	255	256	1	D62876	1.19	4.39	4.39	5.2241	1	4.39	4.39	Comp B27
60440	MGZD245	258	259	1	D62880	1.21	5.05	5.05	6.1105	1	5.05	5.05	Comp B28
60440	MGZD245	261.1	261.8	0.7	D62884	0.66	4.78	3.346	3.1548				Comp B27
60440	MGZD245	261.8	262.5	0.7	D62885	0.76	1.76	1.232	1.3376	1.4	4.578	3.27	Comp B23
60600	MGZD249	253	254	1	D63842	1.46	8.28	8.28	12.0888	1	8.28	8.28	Comp B29
60440	MGZD251	240.8	241.5	0.7	D65017	0.71	6.01	4.207	4.2671				Comp B28
60440	MGZD251	241.5	242.2	0.7	D65019	0.54	2.67	1.869	1.4418	1.4	6.076	4.34	Comp B25
60520	MGZD265	156.5	157.2	0.7	D69210	0.98	2.69	1.883	2.6362				Comp B25
60520	MGZD265	157.2	157.9	0.7	D69211	0.62	3.09	2.163	1.9158				Comp B26
60520	MGZD265	157.9	158.6	0.7	D69212	0.64	0.29	0.203	0.1856				Comp B21
60520	MGZD265	158.6	159.3	0.7	D69213	0.7	7	4.9	4.9	2.8	9.149	3.27	Comp B29
60520	MGZD265	174.7	175.4	0.7	D69239	0.81	2.23	1.561	1.8063				Comp B24
60520	MGZD265	175.4	176.1	0.7	D69240	0.73	1.31	0.917	0.9563				Comp B23
60520	MGZD265	176.1	176.8	0.7	D69241	0.72	0.55	0.385	0.396				Comp B22
60520	MGZD265	176.8	177.5	0.7	D69242	0.78	8.61	6.027	6.7158				Comp B29
60520	MGZD265	177.5	178.2	0.7	D69243	0.66	2.66	1.862	1.7556				Comp B25
60520	MGZD265	178.2	178.9	0.7	D69244	0.73	0.71	0.497	0.5183				Comp B22
60520	MGZD265	178.9	179.6	0.7	D69245	0.74	3.24	2.268	2.3976				Comp B26
60520	MGZD265	179.6	180.3	0.7	D69247	0.81	25.2	17.64	20.412				Comp B31
60520	MGZD265	180.3	181	0.7	D69248	0.81	2.76	1.932	2.2356				Comp B25
60520	MGZD265	181	181.7	0.7	D69249	0.77	3.11	2.177	2.3947				Comp B26
60520	MGZD265	181.7	182.4	0.7	D69250	0.73	2.84	1.988	2.0732				Comp B25
60520	MGZD265	182.4	183.1	0.7	D69251	0.69	5	3.5	3.45				Comp B28
60520	MGZD265	183.1	183.8	0.7	D69252	0.71	0.43	0.301	0.3053				Comp B22
60520	MGZD265	183.8	184.5	0.7	D69253	0.71	27.2	19.04	19.312				Comp B31
60520	MGZD265	184.5	185.2	0.7	D69254	0.7	18.4	12.88	12.88				Comp B31
60520	MGZD265	185.2	185.9	0.7	D69255	0.69	6.85	4.795	4.7265				Comp B28
60520	MGZD265	185.9	186.6	0.7	D69256	0.65	2.42	1.694	1.573				Comp B24
60520	MGZD265	186.6	187.3	0.7	D69257	0.7	0.6	0.42	0.42				Comp B22
60520	MGZD265	187.3	188	0.7	D69259	0.76	7.23	5.061	5.4948				Comp B29
60520	MGZD265	188	188.7	0.7	D69260	0.66	12.5	8.75	8.25				Comp B30
60520	MGZD265	188.7	189.4	0.7	D69261	0.77	2.06	1.442	1.5862				Comp B24
60520	MGZD265	189.4	190.1	0.7	D69262	0.78	3.19	2.233	2.4882				Comp B26
60520	MGZD265	190.1	190.8	0.7	D69263	0.75	5.34	3.738	4.005				Comp B28
60520	MGZD265	190.8	191.5	0.7	D69264	0.83	0.38	0.266	0.3154				Comp B21
60520	MGZD265	191.5	192.2	0.7	D69265	0.82	3.28	2.296	2.6896				Comp B26
60520	MGZD265	192.2	192.9	0.7	D69266	0.83	1.99	1.393	1.6517				Comp B23
60520	MGZD265	192.9	193.6	0.7	D69267	0.84	3.21	2.247	2.6964				Comp B26
60520	MGZD265	193.6	194.3	0.7	D69268	0.73	14.8	10.36	10.804				Comp B30
60520	MGZD265	194.3	195	0.7	D69269	0.77	0.2	0.14	0.154				Comp B21
60520	MGZD265	195	195.7	0.7	D69270	0.72	0.55	0.385	0.396				Comp B22
60520	MGZD265	195.7	196.4	0.7	D69272	0.67	5	3.5	3.35				Comp B28
60520	MGZD265	196.4	197.1	0.7	D69273	0.72	22.2	15.54	15.984				Comp B31
60520	MGZD265	197.1	197.8	0.7	D69274	0.73	1.13	0.791	0.8249				Comp B23
60520	MGZD265	198.5	199.2	0.7	D69277	0.77	3.77	2.639	2.9029				Comp B26
60520	MGZD265	199.2	199.9	0.7	D69279	0.82	3.99	2.793	3.2718	25.2	144.081	5.72	Comp B26
60520	MGZD265	208.3	209	0.7	D69292	0.83	7.48	5.236	6.2084				Comp B29
60520	MGZD265	209	209.7	0.7	D69293	0.83	2.04	1.428	1.6932	1.4	6.664	4.76	Comp B24
60600	MGZD267	173.7	174.4	0.7	D70591	0.79	2.06	1.442	1.6274				Comp B24
60600	MGZD267	174.4	175.1	0.7	D70592	0.83	0.39	0.273	0.3237				Comp B21
60600	MGZD267	175.1	175.8	0.7	D70593	0.84	15	10.5	12.6				Comp B31
60600	MGZD267	175.8	176.5	0.7	D70594	0.86	0.08	0.056	0.0688				Comp B21
60600	MGZD267	176.5	177.2	0.7	D70595	0.85	4.18	2.926	3.553	3.5	15.197	4.34	Comp B27
60600	MGZD267	188.7	189.4	0.7	D70610	0.77	1.29	0.903	0.9933				Comp B23
60600	MGZD267	189.4	190.1	0.7	D70611	0.78	15.1	10.57	11.778				Comp B31
60600	MGZD267	190.1	190.8	0.7	D70612	0.83	9.59	6.713	7.9597				Comp B29
60600	MGZD267	190.8	191.5	0.7	D70613	0.8	2.3	1.61	1.84				Comp B24
60600	MGZD267	191.5	192.2	0.7	D70614	0.83	33.1	23.17	27.473				Comp B32
60600	MGZD267	192.2	192.9	0.7	D70615	0.84	3.76	2.632	3.1584				Comp B26
60600	MGZD267	192.9	193.6	0.7	D70616	0.93	1.14	0.798	1.0602				Comp B23
60600	MGZD267	193.6	194.3	0.7	D70617	0.84	4.21	2.947	3.5364	5.6	49.343	8.81	Comp B27
60600	MGZD277	230.9	231.6	0.7	D73951	0.91	48.1	33.67	43.771				Comp B32
60600	MGZD277	231.6	232.3	0.7	D73952	0.95	1.2	0.84	1.14				Comp B23
60600	MGZD277	232.3	233	0.7	D73953	0.89	3.36	2.352	2.9904	2.1	36.862	17.55	Comp B26
60600	MGZD284	201	202	1	D76676	1.42	1.01	1.01	1.4342	2	90.11	45.06	Comp B23
60600	MGZD284	282.9	283.6	0.7	D76782	0.79	14.4	10.08	11.376				Comp B30

B ZONE HIGH GRADE COMPOSITE (SECTIONS 60440 through 60600)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60600	MGZD284	283.6	284.3	0.7	D76783	0.73	100	70	73				Comp B32
60600	MGZD284	284.3	285	0.7	D76784	0.8	3.14	2.198	2.512				Comp B26
60600	MGZD284	285	286	1	D76785	0.97	2.14	2.14	2.0758	3.1	84.418	27.23	Comp B24
60600	MGZD294	291	292	1	D80176	1.2	2.13	2.13	2.556				Comp B24
60600	MGZD294	292	292.7	0.7	D80177	0.76	2.8	1.96	2.128				Comp B25
60600	MGZD294	292.7	293.4	0.7	D80179	0.82	14.3	10.01	11.726	2.4	14.1	5.87	Comp B30
60600	MGZD306	309	310	1	D85788	1.41	1.32	1.32	1.8612				Comp B23
60600	MGZD306	310	310.7	0.7	D85789	0.84	14.4	10.08	12.096	1.7	11.4	6.71	Comp B30
					0								
Composite grade				500.3	m		8.190477	4098.0231					
(based on (drill core grade x thickness) and meterage, assumes uniform core density)													
Composite grade						589.2	8.01		4718.6				
(based on as-received intercept weights and drill core assays)													

C ZONE LOW GRADE COMPOSITE (SECTIONS 60640 through 60840)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60720	MGZD264	221	222	1	D68900	1	0.29	0.29	0.29				Comp C42
60720	MGZD264	222	223	1	D68902	1.07	0.34	0.34	0.36				Comp C42
60720	MGZD264	223	224	1	D68903	1.05	0.26	0.26	0.27				Comp C42
60720	MGZD264	224	225	1	D68904	1.02	2.18	2.18	2.22				Comp C45
60720	MGZD264	225	226	1	D68905	1.13	0.20	0.20	0.23				Comp C41
60720	MGZD264	226	227	1	D68906	1.09	0.07	0.07	0.08				Comp C41
60720	MGZD264	227	228	1	D68907	1.05	0.04	0.04	0.04				Comp C41
60720	MGZD264	228	229	1	D68908	1.03	0.35	0.35	0.36				Comp C42
60720	MGZD264	229	230	1	D68909	1.1	0.07	0.07	0.08				Comp C41
60720	MGZD264	230	231	1	D68910	0.98	0.43	0.43	0.42				Comp C43
60720	MGZD264	231	232	1	D68911	1.17	0.30	0.30	0.35				Comp C42
60720	MGZD264	232	233	1	D68912	1.15	0.06	0.06	0.07				Comp C41
60720	MGZD264	233	234	1	D68913	1.29	0.40	0.40	0.52				Comp C42
60720	MGZD264	234	235	1	D68914	1.16	0.53	0.53	0.61				Comp C43
60720	MGZD264	235	236	1	D68915	1.01	1.27	1.27	1.28	15	6.790	0.453	Comp C44
60720	MGZD264	251	252	1	D68934	1.12	0.88	0.88	0.99				Comp C44
60720	MGZD264	252	253	1	D68935	1.22	0.35	0.35	0.43				Comp C42
60720	MGZD264	253	254	1	D68936	1.11	0.27	0.27	0.30	3	1.500	0.500	Comp C42
60760	MGZD275	257	257.7	0.7	D73169	0.96	0.43	0.30	0.41				Comp C43
60760	MGZD275	257.7	258.4	0.7	D73171	0.99	0.10	0.07	0.10				Comp C41
60760	MGZD275	258.4	259.1	0.7	D73172	0.88	0.57	0.40	0.50				Comp C43
60760	MGZD275	259.1	260	0.9	D73173	1.15	0.37	0.33	0.43				Comp C42
60760	MGZD275	261	262	1	D73176	1.2	0.44	0.44	0.53				Comp C43
60760	MGZD275	262	263	1	D73177	1.25	1.05	1.05	1.31	6	3.073	0.512	Comp C44
60840	MGZD161	197	198	1	D35353	1.21	0.51	0.51	0.62				Comp C43
60840	MGZD161	198	198.7	0.7	D35354	0.83	0.63	0.44	0.52				Comp C43
60840	MGZD161	198.7	199.4	0.7	D35355	0.8	0.34	0.24	0.27				Comp C42
60840	MGZD161	199.4	200.1	0.7	D35356	0.77	0.25	0.18	0.19				Comp C41
60840	MGZD161	200.1	200.8	0.7	D35357	0.82	0.99	0.69	0.81	3.8	2.057	0.541	Comp C44
60720	MGZD182	140.2	140.9	0.7	D41689	0.89	0.97	0.68	0.86				Comp C44
60720	MGZD182	140.9	141.6	0.7	D41690	0.86	0.09	0.06	0.08				Comp C41
60720	MGZD182	141.6	142.3	0.7	D41691	0.85	0.19	0.13	0.16				Comp C41
60720	MGZD182	142.3	143	0.7	D41692	0.72	0.07	0.05	0.05				Comp C41
60720	MGZD182	143	143.7	0.7	D41693	0.85	1.11	0.78	0.94				Comp C44
60720	MGZD182	143.7	144.4	0.7	D41694	0.82	1.49	1.04	1.22	4.2	2.744	0.653	Comp C45
60760	MGZD046	138.7	139.4	0.7	D04767	0.83	1.66	1.16	1.38				Comp C45
60760	MGZD046	139.4	140.1	0.7	D04769	0.67	0.80	0.56	0.54				Comp C43
60760	MGZD046	140.1	141	0.9	D04770	0.9	0.56	0.50	0.50				Comp C43
60760	MGZD046	141	142	1	D04772	1.04	0.02	0.02	0.02				Comp C41
60760	MGZD046	142	143	1	D04773	1.11	0.45	0.45	0.50				Comp C43
60760	MGZD046	143	144	1	D04774	1.13	0.02	0.02	0.02				Comp C41
60760	MGZD046	144	144.7	0.7	D04775	0.77	1.91	1.34	1.47				Comp C45
60760	MGZD046	144.7	145.4	0.7	D04776	0.81	0.62	0.43	0.50	6.7	4.487	0.670	Comp C43
60800	MGZD160	246.7	247.4	0.7	D35045	0.76	0.67	0.47	0.51				Comp C43
60800	MGZD160	247.4	248.1	0.7	D35047	0.88	0.77	0.54	0.68	1.4	1.008	0.720	Comp C43
60760	MGZD073	182	182.7	0.7	D07864	0.71	1.04	0.73	0.74				Comp C44
60760	MGZD073	182.7	183.4	0.7	D07865	0.8	0.10	0.07	0.08				Comp C41
60760	MGZD073	183.4	184.1	0.7	D07866	0.62	1.03	0.72	0.64				Comp C44
60760	MGZD073	184.1	184.8	0.7	D07867	0.68	0.69	0.48	0.47				Comp C43
60760	MGZD073	184.8	185.5	0.7	D07868	0.65	0.80	0.56	0.52				Comp C43
60760	MGZD073	185.5	186.2	0.7	D07869	0.71	0.77	0.54	0.55				Comp C43
60760	MGZD073	186.2	186.9	0.7	D07870	0.66	1.27	0.89	0.84				Comp C44
60760	MGZD073	186.9	187.6	0.7	D07872	0.74	1.45	1.01	1.07				Comp C45
60760	MGZD073	187.6	188.3	0.7	D07874	0.72	0.34	0.24	0.24				Comp C42
60760	MGZD073	188.3	189	0.7	D07875	0.71	0.37	0.26	0.26				Comp C42
60760	MGZD073	189	189.7	0.7	D07876	0.71	0.25	0.17	0.18				Comp C41
60760	MGZD073	189.7	190.4	0.7	D07877	0.69	0.70	0.49	0.48	8.4	6.167	0.734	Comp C43

C ZONE LOW GRADE COMPOSITE (SECTIONS 60640 through 60840)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60800	MGZD160	214	215	1	D35002	1.15	0.54	0.54	0.62				Comp C43
60800	MGZD160	215	216	1	D35003	1.11	0.36	0.36	0.40				Comp C42
60800	MGZD160	216	217	1	D35004	1.16	0.19	0.19	0.22				Comp C41
60800	MGZD160	217	218	1	D35005	1.22	1.33	1.33	1.62				Comp C45
60800	MGZD160	218	219	1	D35006	1.19	0.36	0.36	0.43				Comp C42
60800	MGZD160	219	220	1	D35007	1.22	0.04	0.04	0.05				Comp C41
60800	MGZD160	220	221	1	D35008	1.15	0.16	0.16	0.18				Comp C41
60800	MGZD160	221	222	1	D35009	1.18	0.09	0.09	0.11				Comp C41
60800	MGZD160	222	222.7	0.7	D35010	0.86	0.30	0.21	0.26				Comp C42
60800	MGZD160	222.7	223.4	0.7	D35011	0.84	0.34	0.24	0.29				Comp C42
60800	MGZD160	223.4	224.1	0.7	D35012	0.88	0.08	0.06	0.07				Comp C41
60800	MGZD160	224.1	224.8	0.7	D35013	0.95	0.04	0.03	0.04				Comp C41
60800	MGZD160	224.8	225.5	0.7	D35014	0.9	2.84	1.99	2.56				Comp C46
60800	MGZD160	225.5	226.2	0.7	D35015	0.85	0.16	0.11	0.14				Comp C41
60800	MGZD160	226.2	226.9	0.7	D35016	0.82	0.08	0.06	0.07				Comp C41
60800	MGZD160	226.9	227.6	0.7	D35017	0.9	0.26	0.18	0.23				Comp C42
60800	MGZD160	227.6	228.3	0.7	D35019	0.84	0.66	0.46	0.55				Comp C43
60800	MGZD160	228.3	229	0.7	D35020	0.76	2.40	1.68	1.82				Comp C45
60800	MGZD160	229	229.7	0.7	D35022	0.84	1.04	0.73	0.87				Comp C44
60800	MGZD160	229.7	230.4	0.7	D35023	0.83	0.97	0.68	0.81				Comp C44
60800	MGZD160	230.4	231.1	0.7	D35024	0.87	0.98	0.69	0.85				Comp C44
60800	MGZD160	231.1	231.8	0.7	D35025	0.79	5.49	3.84	4.34	17.8	14.018	0.788	Comp C47
60720	MGZD196	221.4	222.1	0.7	D44422	0.84	0.65	0.45	0.55				Comp C43
60720	MGZD196	222.1	222.8	0.7	D44423	0.81	0.96	0.67	0.78	1.4	1.127	0.805	Comp C44
60720	MGZD196	213.7	214.4	0.7	D44409	0.84	0.75	0.52	0.63				Comp C43
60720	MGZD196	214.4	215.1	0.7	D44410	0.7	1.53	1.07	1.07				Comp C45
60720	MGZD196	215.1	215.8	0.7	D44411	0.72	0.56	0.39	0.40	2.1	1.988	0.947	Comp C43
60720	MGZD196	157.2	157.9	0.7	D44331	0.62	2.64	1.85	1.64				Comp C46
60720	MGZD196	157.9	158.6	0.7	D44332	0.65	0.57	0.40	0.37				Comp C43
60720	MGZD196	158.6	159.3	0.7	D44333	0.72	0.46	0.32	0.33				Comp C43
60720	MGZD196	159.3	160	0.7	D44334	0.8	0.56	0.39	0.45	2.8	2.961	1.057	Comp C43
60720	MGZD268	274	275	1	D71053	1.17	1.09	1.09	1.28				Comp C44
60720	MGZD268	275	276	1	D71054	1.14	1.25	1.25	1.43	2	2.340	1.170	Comp C44
60680	MGZD218	204	205	1	D51491	1.05	2.26	2.26	2.37				Comp C45
60680	MGZD218	205	206	1	D51492	1.11	0.75	0.75	0.83				Comp C43
60680	MGZD218	206	207	1	D51493	0.97	0.29	0.29	0.28				Comp C42
60680	MGZD218	207	207.7	0.7	D51494	0.75	2.45	1.71	1.84				Comp C46
60680	MGZD218	207.7	208.4	0.7	D51495	0.78	0.63	0.44	0.49	4.4	5.456	1.240	Comp C43
60720	MGZD196	203.1	203.8	0.7	D44394	0.62	0.73	0.51	0.45				Comp C43
60720	MGZD196	203.8	204.5	0.7	D44395	0.75	2.54	1.78	1.91				Comp C46
60720	MGZD196	204.5	205.2	0.7	D44397	0.78	1.64	1.15	1.28				Comp C45
60720	MGZD196	205.2	205.9	0.7	D44399	0.82	0.60	0.42	0.49				Comp C43
60720	MGZD196	205.9	206.6	0.7	D44400	0.76	0.75	0.52	0.57				Comp C43
60720	MGZD196	206.6	207.3	0.7	D44401	0.78	1.43	1.00	1.12	4.2	5.383	1.282	Comp C45
60760	MGZD043	237	237.7	0.7	D04267	0.89	0.32	0.22	0.28				Comp C42
60760	MGZD043	237.7	238.4	0.7	D04268	0.86	1.44	1.01	1.24				Comp C45
60760	MGZD043	238.4	239.1	0.7	D04269	0.78	2.34	1.64	1.83				Comp C45
60760	MGZD043	239.1	240	0.9	D04270	1.02	1.57	1.41	1.60	3	4.283	1.428	Comp C45
60760	MGZD073	140.5	141.2	0.7	D07810	0.55	4.73	3.31	2.60				Comp C47
60760	MGZD073	141.2	141.9	0.7	D07811	0.68	0.12	0.08	0.08				Comp C41
60760	MGZD073	141.9	142.6	0.7	D07812	0.6	0.38	0.27	0.23				Comp C42
60760	MGZD073	142.6	143.3	0.7	D07814	0.82	0.86	0.60	0.71				Comp C44
60760	MGZD073	143.3	144	0.7	D07815	0.74	1.79	1.25	1.32				Comp C45
60760	MGZD073	144	144.7	0.7	D07816	0.69	1.88	1.32	1.30				Comp C45
60760	MGZD073	144.7	145.4	0.7	D07817	0.78	2.16	1.51	1.68				Comp C45
60760	MGZD073	145.4	146.1	0.7	D07818	0.78	0.00	0.00	0.00				Comp C41
60760	MGZD073	146.1	146.8	0.7	D07819	0.07	1.05	0.74	0.07				Comp C44
60760	MGZD073	146.8	147.5	0.7	D07820	0.72	1.00	0.70	0.72				Comp C44
60760	MGZD073	147.5	148.2	0.7	D07822	0.72	3.07	2.15	2.21				Comp C46
60760	MGZD073	148.2	148.9	0.7	D07823	0.74	0.33	0.23	0.24	8.4	12.159	1.447	Comp C42
60640	MGZD246	147.8	148.5	0.7	D63094	0.66	1.64	1.15	1.08				Comp C45

C ZONE LOW GRADE COMPOSITE (SECTIONS 60640 through 60840)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60640	MGZD246	149.2	149.9	0.7	D63097	0.69	1.83	1.28	1.26				Comp C45
60640	MGZD246	149.9	150.6	0.7	D63099	0.66	0.45	0.31	0.30	2.8	4.060	1.450	Comp C43
60720	MGZD097	244	245	1	D12167	1.11	0.36	0.36	0.40				Comp C42
60720	MGZD097	245	245.7	0.7	D12168	0.77	2.38	1.67	1.83				Comp C45
60720	MGZD097	245.7	246.4	0.7	D12169	0.7	4.86	3.40	3.40				Comp C47
60720	MGZD097	246.4	247.1	0.7	D12170	0.64	2.34	1.64	1.50				Comp C45
60720	MGZD097	247.1	247.8	0.7	D12172	0.63	1.39	0.97	0.88				Comp C45
60720	MGZD097	247.8	248.5	0.7	D12173	0.69	1.78	1.25	1.23				Comp C45
60720	MGZD097	248.5	249.2	0.7	D12174	0.71	1.73	1.21	1.23				Comp C45
60720	MGZD097	249.2	249.9	0.7	D12175	0.73	1.55	1.09	1.13				Comp C45
60720	MGZD097	249.9	250.6	0.7	D12176	0.79	1.79	1.25	1.41				Comp C45
60720	MGZD097	250.6	251.3	0.7	D12177	0.73	1.09	0.76	0.80				Comp C44
60720	MGZD097	251.3	252	0.7	D12179	0.62	4.39	3.07	2.72				Comp C47
60720	MGZD097	252	252.7	0.7	D12180	0.74	0.29	0.20	0.21				Comp C42
60720	MGZD097	252.7	253.4	0.7	D12181	0.73	0.03	0.02	0.02				Comp C41
60720	MGZD097	253.4	254.1	0.7	D12182	0.76	0.37	0.26	0.28				Comp C42
60720	MGZD097	254.1	254.8	0.7	D12183	0.72	0.13	0.09	0.09				Comp C41
60720	MGZD097	254.8	255.5	0.7	D12184	0.78	0.24	0.17	0.19				Comp C41
60720	MGZD097	255.5	256.2	0.7	D12185	0.78	1.28	0.90	1.00	12.2	18.308	1.501	Comp C44
60720	MGZD182	152.1	152.8	0.7	D41708	0.88	1.58	1.11	1.39				Comp C45
60720	MGZD182	152.8	153.5	0.7	D41709	0.92	2.60	1.82	2.39				Comp C46
60720	MGZD182	153.5	154.2	0.7	D41710	0.82	1.65	1.15	1.35				Comp C45
60720	MGZD182	154.2	154.9	0.7	D41711	0.94	0.42	0.29	0.39	2.8	4.375	1.563	Comp C43
60640	MGZD181	148	149	1	D40991	1.04	0.73	0.73	0.76				Comp C43
60640	MGZD181	149	150	1	D40992	1.09	2.46	2.46	2.68	2	3.190	1.595	Comp C46
60640	MGZD080	202	203	1	D09141	1.12	2.04	2.04	2.28				Comp C45
60640	MGZD080	203	204	1	D09142	1.15	1.20	1.20	1.38	2	3.240	1.620	Comp C44
60680	MGZD280	282.7	283.4	0.7	D75272	0.82	1.70	1.19	1.39				Comp C45
60680	MGZD280	283.4	284.1	0.7	D75273	0.76	1.97	1.38	1.50				Comp C45
60680	MGZD280	284.8	285.5	0.7	D75276	0.78	1.48	1.04	1.15	2.8	4.634	1.655	Comp C45
60840	MGZD153	222	223	1	D32711	1.37	4.47	4.47	6.12				Comp C47
60840	MGZD153	223	224	1	D32712	1.34	0.12	0.12	0.16				Comp C41
60840	MGZD153	224	225	1	D32713	1.45	0.19	0.19	0.28				Comp C41
60840	MGZD153	225	226	1	D32714	1.29	0.72	0.72	0.93				Comp C43
60840	MGZD153	226	227	1	D32715	1.23	0.16	0.16	0.20				Comp C41
60840	MGZD153	227	227.7	0.7	D32716	0.76	3.47	2.43	2.64				Comp C46
60840	MGZD153	227.7	228.4	0.7	D32717	0.79	3.96	2.77	3.13				Comp C46
60840	MGZD153	228.4	229.1	0.7	D32719	0.81	1.22	0.85	0.99				Comp C44
60840	MGZD153	229.1	229.8	0.7	D32720	0.81	2.37	1.66	1.92				Comp C45
60840	MGZD153	229.8	230.5	0.7	D32722	0.8	1.98	1.39	1.58				Comp C45
60840	MGZD153	230.5	231.2	0.7	D32723	0.86	0.24	0.17	0.21				Comp C41
60840	MGZD153	231.2	231.9	0.7	D32724	0.87	2.32	1.62	2.02	9.9	16.552	1.672	Comp C45
60640	MGZD279	287	288	1	D74833	1.33	0.81	0.81	1.08				Comp C44
60640	MGZD279	288	288.8	0.8	D74834	0.9	2.94	2.35	2.65	1.8	3.162	1.757	Comp C46
60720	MGZD191	139.1	139.8	0.7	D42893	0.72	1.58	1.11	1.14				Comp C45
60720	MGZD191	139.8	140.5	0.7	D42894	0.73	1.98	1.39	1.45	1.4	2.492	1.780	Comp C45
60640	MGZD246	154.8	155.5	0.7	D63106	0.54	2.81	1.97	1.52				Comp C46
60640	MGZD246	155.5	156.2	0.7	D63107	0.75	0.80	0.56	0.60	1.4	2.527	1.805	Comp C43
60720	MGZD196	223.5	224.2	0.7	D44425	0.76	9.04	6.33	6.87				Comp C48
60720	MGZD196	224.2	224.9	0.7	D44426	0.77	1.57	1.10	1.21				Comp C45
60720	MGZD196	224.9	225.6	0.7	D44427	0.81	0.32	0.22	0.26				Comp C42
60720	MGZD196	225.6	226.3	0.7	D44428	0.76	0.08	0.06	0.06				Comp C41
60720	MGZD196	226.3	227	0.7	D44429	0.92	0.09	0.06	0.08				Comp C41
60720	MGZD196	227	227.7	0.7	D44430	0.74	0.29	0.20	0.21				Comp C42
60720	MGZD196	227.7	228.4	0.7	D44431	0.62	1.80	1.26	1.12				Comp C45
60720	MGZD196	228.4	229.1	0.7	D44432	0.65	1.92	1.34	1.25	5.6	10.577	1.889	Comp C45
60640	MGZD181	232	232.7	0.7	D41094	0.91	4.07	2.85	3.70				Comp C47
60640	MGZD181	232.7	233.4	0.7	D41095	0.81	0.29	0.20	0.23				Comp C42
60640	MGZD181	233.4	234.1	0.7	D41097	0.86	2.46	1.72	2.12				Comp C46
60640	MGZD181	234.1	234.8	0.7	D41099	0.84	0.45	0.32	0.38				Comp C43
60640	MGZD181	234.8	235.5	0.7	D41100	0.82	0.35	0.24	0.29				Comp C42

C ZONE LOW GRADE COMPOSITE (SECTIONS 60640 through 60840)

Section	HOLE_ID	Meters From	Meters To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60680	MGZD167	130	131	1	D37206	1.14	2.71	2.71	3.09				Comp C46
60680	MGZD167	131	132	1	D37207	1.12	1.52	1.52	1.70	2	4.230	2.115	Comp C45
60720	MGZD268	210	211	1	D70976	0.93	1.28	1.28	1.19				Comp C44
60720	MGZD268	211	212	1	D70977	1.03	0.06	0.06	0.06				Comp C41
60720	MGZD268	212	213	1	D70979	1.18	8.16	8.16	9.63				Comp C48
60720	MGZD268	213	214	1	D70980	1.22	0.11	0.11	0.13				Comp C41
60720	MGZD268	214	215	1	D70981	1.28	1.05	1.05	1.34	5	10.660	2.132	Comp C44
60720	MGZD268	250	251	1	D71022	1.16	0.38	0.38	0.44				Comp C42
60720	MGZD268	251	252	1	D71023	1.14	1.18	1.18	1.35				Comp C44
60720	MGZD268	252	252.7	0.7	D71024	0.83	0.39	0.27	0.32				Comp C42
60720	MGZD268	252.7	253.4	0.7	D71025	0.78	0.31	0.22	0.24				Comp C42
60720	MGZD268	253.4	254.1	0.7	D71026	0.81	1.31	0.92	1.06				Comp C45
60720	MGZD268	254.1	254.8	0.7	D71027	0.74	2.14	1.50	1.58				Comp C45
60720	MGZD268	254.8	255.5	0.7	D71028	0.84	9.22	6.45	7.74				Comp C48
60720	MGZD268	255.5	256.2	0.7	D71029	0.82	0.42	0.29	0.34				Comp C43
60720	MGZD268	256.2	256.9	0.7	D71030	0.82	1.39	0.97	1.14				Comp C45
60720	MGZD268	256.9	257.6	0.7	D71031	0.82	2.24	1.57	1.84				Comp C45
60720	MGZD268	257.6	258.3	0.7	D71032	0.79	8.21	5.75	6.49				Comp C48
60720	MGZD268	258.3	259	0.7	D71033	0.74	2.37	1.66	1.75				Comp C45
60720	MGZD268	259	260	1	D71034	1.17	0.35	0.35	0.41	10	21.510	2.151	Comp C42
60680	MGZD218	163.8	164.5	0.7	D51437	0.73	1.96	1.37	1.43				Comp C45
60680	MGZD218	164.5	165.2	0.7	D51439	0.68	2.38	1.67	1.62	1.4	3.038	2.170	Comp C45
60680	MGZD266	242	243	1	D69910	1.05	2.19	2.19	2.30	1	2.190	2.190	Comp C45
60680	MGZD272	199	200	1	D71884	1.33	0.38	0.38	0.51				Comp C42
60680	MGZD272	200	201	1	D71885	1.29	4.05	4.05	5.22	2	4.430	2.215	Comp C47
60640	MGZD181	158.7	159.4	0.7	D41004	0.71	3.12	2.18	2.22				Comp C46
60640	MGZD181	159.4	160.1	0.7	D41005	0.73	1.37	0.96	1.00				Comp C45
60640	MGZD181	160.1	160.8	0.7	D41006	0.68	2.18	1.53	1.48	2.1	4.669	2.223	Comp C45
60680	MGZD286	270	271	1	D77423	1.23	2.51	2.51	3.09				Comp C46
60680	MGZD286	271	272	1	D77424	1.27	2.00	2.00	2.54	2	4.510	2.255	Comp C45
60760	MGZD283	225	226	1	D76296	1.1	0.69	0.69	0.76				Comp C43
60760	MGZD283	226	227	1	D76297	1.08	0.48	0.48	0.52				Comp C43
60760	MGZD283	227	228	1	D76299	1.17	0.91	0.91	1.06				Comp C44
60760	MGZD283	228	229	1	D76301	1.13	0.56	0.56	0.63				Comp C43
60760	MGZD283	229	230	1	D76302	1.12	0.15	0.15	0.17				Comp C41
60760	MGZD283	230	231	1	D76303	1.19	0.19	0.19	0.23				Comp C41
60760	MGZD283	231	232	1	D76304	1.1	9.54	9.54	10.49				Comp C48
60760	MGZD283	232	233	1	D76305	1.24	0.13	0.13	0.16				Comp C41
60760	MGZD283	233	234	1	D76306	1.24	0.41	0.41	0.51				Comp C43
60760	MGZD283	234	235	1	D76307	1.17	0.06	0.06	0.07				Comp C41
60760	MGZD283	235	235.8	0.8	D76308	0.83	0.41	0.33	0.34				Comp C43
60760	MGZD283	235.8	236.5	0.7	D76309	1.03	0.89	0.62	0.92				Comp C44
60760	MGZD283	236.5	237.2	0.7	D76311	0.83	12.40	8.68	10.29				Comp C49
60760	MGZD283	237.2	237.9	0.7	D76312	0.77	9.91	6.94	7.63				Comp C48
60760	MGZD283	237.9	238.6	0.7	D76313	0.85	2.43	1.70	2.07	13.6	31.389	2.308	Comp C46
60640	MGZD269	248.4	249.1	0.7	D71399	0.67	3.00	2.10	2.01				Comp C46
60640	MGZD269	249.1	249.8	0.7	D71400	0.65	1.66	1.16	1.08	1.4	3.262	2.330	Comp C45
60640	MGZD246	163.9	164.6	0.7	D63120	0.77	2.37	1.66	1.82	0.7	1.659	2.370	Comp C45
60680	MGZD173	218.2	218.9	0.7	D38734	0.93	0.96	0.67	0.89				Comp C44
60680	MGZD173	218.9	219.6	0.7	D38735	0.79	3.89	2.72	3.07	1.4	3.395	2.425	Comp C46
60840	MGZD077	225.8	226.5	0.7	D08768	0.66	2.19	1.53	1.45				Comp C45
60840	MGZD077	226.5	227.2	0.7	D08769	0.62	1.20	0.84	0.74				Comp C44
60840	MGZD077	227.2	227.9	0.7	D08770	0.73	2.07	1.45	1.51				Comp C45
60840	MGZD077	227.9	228.6	0.7	D08772	0.77	2.41	1.69	1.86				Comp C46
60840	MGZD077	228.6	229.3	0.7	D08773	0.8	2.00	1.40	1.60				Comp C45
60840	MGZD077	229.3	230	0.7	D08774	0.8	0.48	0.34	0.38				Comp C43
60840	MGZD077	230	230.7	0.7	D08775	0.84	0.17	0.12	0.14				Comp C41
60840	MGZD077	230.7	231.4	0.7	D08776	0.8	9.63	6.74	7.70				Comp C48
60840	MGZD077	231.4	232.1	0.7	D08777	0.82	2.83	1.98	2.32				Comp C46
60840	MGZD077	232.1	233	0.9	D08779	1.08	2.80	2.52	3.02	7.2	18.606	2.584	Comp C46
60680	MGZD173	164.9	165.6	0.7	D38669	0.86	1.72	1.20	1.48				Comp C45

C ZONE LOW GRADE COMPOSITE (SECTIONS 60640 through 60840)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60680	MGZD173	166.3	167	0.7	D38672	0.76	3.82	2.67	2.90	2.1	5.495	2.617	Comp C46
60680	MGZD173	237	238	1	D38756	0.98	1.68	1.68	1.65				Comp C45
60680	MGZD173	238	239	1	D38757	1.23	3.60	3.60	4.43	2	5.280	2.640	Comp C46
60720	MGZD264	241	242	1	D68923	1.01	0.29	0.29	0.29				Comp C42
60720	MGZD264	242	243	1	D68924	1.07	1.08	1.08	1.16				Comp C44
60720	MGZD264	243	243.7	0.7	D68925	0.81	0.37	0.26	0.30				Comp C42
60720	MGZD264	243.7	244.4	0.7	D68926	0.73	0.17	0.12	0.12				Comp C41
60720	MGZD264	244.4	245.1	0.7	D68927	0.8	14.20	9.94	11.36				Comp C50
60720	MGZD264	245.1	246	0.9	D68928	0.97	1.98	1.78	1.92	5	13.470	2.694	Comp C45
60680	MGZD257	155.7	156.4	0.7	D66643	0.84	1.76	1.23	1.48				Comp C45
60680	MGZD257	156.4	157.1	0.7	D66644	0.84	3.64	2.55	3.06	1.4	3.780	2.700	Comp C46
60720	MGZD268	238	239	1	D71008	1.12	0.32	0.32	0.36				Comp C42
60720	MGZD268	239	240	1	D71009	1.12	7.10	7.10	7.95				Comp C48
60720	MGZD268	240	241	1	D71010	1.16	0.75	0.75	0.87	3	8.170	2.723	Comp C43
60720	MGZD264	258	258.7	0.7	D68942	0.82	0.60	0.42	0.49				Comp C43
60720	MGZD264	258.7	259.4	0.7	D68943	0.8	4.86	3.40	3.89	1.4	3.822	2.730	Comp C47
60720	MGZD248	159.5	160.2	0.7	D63397	0.76	5.40	3.78	4.10				Comp C47
60720	MGZD248	160.2	160.9	0.7	D63399	0.73	0.40	0.28	0.29				Comp C42
60720	MGZD248	160.9	161.6	0.7	D63400	0.76	0.91	0.64	0.69				Comp C44
60720	MGZD248	161.6	162.3	0.7	D63401	0.65	4.26	2.98	2.77	2.8	7.679	2.743	Comp C47
60680	MGZD178	256.1	256.8	0.7	D39894	0.98	1.77	1.24	1.73				Comp C45
60680	MGZD178	256.8	257.5	0.7	D39895	0.92	3.80	2.66	3.50	1.4	3.899	2.785	Comp C46
60640	MGZD188	305	306	1	D42222	1.21	2.81	2.81	3.40	1	2.812	2.812	Comp C46
60800	MGZD157	229.7	230.4	0.7	D34280	0.81	0.28	0.20	0.23				Comp C42
60800	MGZD157	230.4	231.1	0.7	D34281	0.75	1.04	0.73	0.78				Comp C44
60800	MGZD157	231.1	231.8	0.7	D34282	0.75	0.95	0.67	0.71				Comp C44
60800	MGZD157	231.8	232.5	0.7	D34283	0.82	4.37	3.06	3.58				Comp C47
60800	MGZD157	232.5	233.2	0.7	D34284	0.84	7.44	5.21	6.25	3.5	9.856	2.816	Comp C48
60720	MGZD264	262.2	262.9	0.7	D68949	0.72	3.18	2.23	2.29				Comp C46
60720	MGZD264	262.9	263.6	0.7	D68950	0.71	18.30	12.81	12.99				Comp C50
60720	MGZD264	263.6	264.3	0.7	D68951	0.72	0.28	0.20	0.20				Comp C42
60720	MGZD264	264.3	265	0.7	D68952	0.73	0.20	0.14	0.15				Comp C41
60720	MGZD264	265	266	1	D68953	0.99	0.38	0.38	0.38				Comp C42
60720	MGZD264	266	267	1	D68954	0.91	0.30	0.30	0.27				Comp C42
60720	MGZD264	267	268	1	D68955	1.18	0.80	0.80	0.94	5.8	16.852	2.906	Comp C43
Composite grade				221	m		1.59	351.834					
(based on (drill core grade x thickness) and meterage, assumes uniform core density)													
Composite grade						247.2	1.58		391.1				
(based on as-received intercept weights and drill core assays)													

C ZONE HIGH GRADE COMPOSITE (SECTIONS 60640 through 60840)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60760	MGZD043	149.7	150.4	0.7	D04210	0.76	16.40	11.48	12.46				Comp C50
60760	MGZD043	150.4	151.1	0.7	D04211	0.77	1.98	1.39	1.52	1.4	12.866	9.190	Comp C45
60760	MGZD043	155.7	156.4	0.7	D04218	0.75	0.92	0.64	0.69				Comp C44
60760	MGZD043	149.7	150.4	0.7	D04210	0.76	16.40	11.48	12.46				Comp C50
60760	MGZD043	150.4	151.1	0.7	D04211	0.77	1.98	1.39	1.52	1.4	12.866	9.190	Comp C45
60760	MGZD043	155.7	156.4	0.7	D04218	0.75	0.92	0.64	0.69				Comp C44
60760	MGZD043	156.4	157.1	0.7	D04219	0.84	9.35	6.54	7.85				Comp C48
60760	MGZD043	157.1	157.8	0.7	D04220	0.84	1.14	0.80	0.96				Comp C44
60760	MGZD043	157.8	158.5	0.7	D04222	0.88	1.37	0.96	1.21				Comp C45
60760	MGZD043	158.5	159.2	0.7	D04223	0.78	6.72	4.70	5.24				Comp C48
60760	MGZD043	159.2	159.9	0.7	D04224	0.74	2.65	1.86	1.96	4.2	15.505	3.692	Comp C46
60760	MGZD043	224	225	1	D04251	1.16	2.41	2.41	2.80				Comp C46
60760	MGZD043	225	225.7	0.7	D04252	0.77	1.57	1.10	1.21				Comp C45
60760	MGZD043	225.7	226.4	0.7	D04253	0.68	2.92	2.04	1.99				Comp C46
60760	MGZD043	226.4	227.1	0.7	D04254	0.75	3.91	2.74	2.93				Comp C46
60760	MGZD043	227.1	227.8	0.7	D04255	0.78	6.39	4.47	4.98	3.8	12.763	3.359	Comp C48
60760	MGZD043	247	247.7	0.7	D04280	0.83	25.50	17.85	21.17				Comp C51
60760	MGZD043	247.7	248.4	0.7	D04281	0.81	18.50	12.95	14.99				Comp C50
60760	MGZD043	248.4	249.1	0.7	D04282	0.82	10.60	7.42	8.69				Comp C49
60760	MGZD043	249.1	249.8	0.7	D04283	0.78	4.65	3.26	3.63				Comp C47
60760	MGZD043	249.8	250.5	0.7	D04284	0.82	1.31	0.92	1.07				Comp C45
60760	MGZD043	250.5	251.2	0.7	D04285	0.74	0.53	0.37	0.39				Comp C43
60760	MGZD043	251.2	251.9	0.7	D04286	0.78	1.17	0.82	0.91				Comp C44
60760	MGZD043	251.9	252.6	0.7	D04287	0.74	2.17	1.52	1.61				Comp C45
60760	MGZD043	252.6	253.3	0.7	D04289	0.79	17.90	12.53	14.14				Comp C50
60760	MGZD043	253.3	254	0.7	D04290	0.8	7.45	5.21	5.96				Comp C48
60760	MGZD043	254	254.7	0.7	D04291	0.78	2.35	1.64	1.83				Comp C45
60760	MGZD043	254.7	255.4	0.7	D04292	0.93	24.10	16.87	22.41				Comp C50
60760	MGZD043	255.4	256.1	0.7	D04293	0.84	1.30	0.91	1.09				Comp C44
60760	MGZD043	256.1	257	0.9	D04294	1.04	0.63	0.57	0.66				Comp C43
60760	MGZD043	257	258	1	D04295	1.2	4.11	4.11	4.93	11	86.948	7.904	Comp C47
60760	MGZD043	265.4	266.1	0.7	D04306	0.73	3.54	2.48	2.58				Comp C46
60760	MGZD043	266.1	266.8	0.7	D04307	0.76	4.07	2.85	3.09				Comp C47
60760	MGZD043	266.8	267.5	0.7	D04308	0.77	3.97	2.78	3.06				Comp C46
60760	MGZD043	267.5	268.2	0.7	D04309	0.82	6.11	4.28	5.01	2.8	12.383	4.423	Comp C48
60760	MGZD045	246	247	1	D04579	0.96	3.63	3.63	3.48				Comp C46
60760	MGZD045	247	248	1	D04580	0.92	3.45	3.45	3.17				Comp C46
60760	MGZD045	248	249	1	D04581	1.17	0.23	0.23	0.27				Comp C41
60760	MGZD045	249	249.7	0.7	D04582	0.83	83.30	58.31	69.14				Comp C51
60760	MGZD045	249.7	250.4	0.7	D04583	0.76	28.70	20.09	21.81				Comp C51
60760	MGZD045	250.4	251.1	0.7	D04584	0.73	0.59	0.41	0.43				Comp C43
60760	MGZD045	251.1	252	0.9	D04585	0.96	0.45	0.41	0.43				Comp C43
60760	MGZD045	252	252.7	0.7	D04586	0.73	0.64	0.45	0.47				Comp C43
60760	MGZD045	252.7	253.4	0.7	D04587	0.74	2.83	1.98	2.09				Comp C46
60760	MGZD045	253.4	254.1	0.7	D04589	0.74	16.10	11.27	11.91				Comp C50
60760	MGZD045	254.1	254.8	0.7	D04590	0.81	16.60	11.62	13.45				Comp C50
60760	MGZD045	254.8	255.5	0.7	D04591	0.8	13.30	9.31	10.64				Comp C49
60760	MGZD045	255.5	256.2	0.7	D04592	0.78	0.12	0.08	0.09				Comp C41
60760	MGZD045	256.2	257	0.8	D04593	0.94	2.69	2.15	2.53	11	123.393	11.218	Comp C46
60760	MGZD045	265	266	1	D04603	1.24	8.60	8.60	10.66				Comp C48
60760	MGZD045	266	267	1	D04604	1.3	0.03	0.03	0.04				Comp C41
60760	MGZD045	267	267.7	0.7	D04606	0.91	18.70	13.09	17.02	2.7	21.720	8.044	Comp C50
60760	MGZD073	196	196.7	0.7	D07884	0.57	1.47	1.03	0.84				Comp C45
60760	MGZD073	196.7	197.4	0.7	D07885	0.83	4.84	3.39	4.02				Comp C47
60760	MGZD073	197.4	198.1	0.7	D07886	0.69	8.84	6.19	6.10				Comp C48
60760	MGZD073	198.1	199	0.9	D07887	1.17	0.99	0.89	1.16				Comp C44
60760	MGZD073	199	200	1	D07889	1.33	0.35	0.35	0.47				Comp C42

C ZONE HIGH GRADE COMPOSITE (SECTIONS 60640 through 60840)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60760	MGZD073	200	201	1	D07890	1.16	0.28	0.28	0.32				Comp C42
60760	MGZD073	201	202	1	D07891	1.22	0.39	0.39	0.48				Comp C42
60760	MGZD073	202	203	1	D07892	1.22	1.31	1.31	1.60				Comp C45
60760	MGZD073	203	203.7	0.7	D07893	0.78	182.00	127.40	141.96				
60760	MGZD073	203.7	204.4	0.7	D07894	0.79	190.00	133.00	150.10				
60760	MGZD073	204.4	205.1	0.7	D07895	0.8	7.80	5.46	6.24				Comp C48
60760	MGZD073	205.1	206	0.9	D07897	0.95	0.19	0.17	0.18				Comp C41
60760	MGZD073	206	207	1	D07898	1.13	0.07	0.07	0.08				Comp C41
60760	MGZD073	207	208	1	D07899	1.13	0.88	0.88	0.99				Comp C44
60760	MGZD073	208	209	1	D07900	1.14	0.16	0.16	0.18				Comp C41
60760	MGZD073	209	210	1	D07901	1.1	0.48	0.48	0.53				Comp C43
60760	MGZD073	210	211	1	D07902	1.17	0.41	0.41	0.48				Comp C43
60760	MGZD073	211	211.7	0.7	D07904	0.78	6.37	4.46	4.97				Comp C48
60760	MGZD073	211.7	212.4	0.7	D07905	0.84	2.47	1.73	2.07				Comp C46
60760	MGZD073	212.4	213.1	0.7	D07906	0.88	0.96	0.67	0.84				Comp C44
60760	MGZD073	213.1	214	0.9	D07907	1.04	0.71	0.64	0.74	18	289.356	16.075	Comp C43
60840	MGZD075	187	188	1	D08007	1.16	0.18	0.18	0.21				Comp C41
60840	MGZD075	188	189	1	D08009	1.28	7.81	7.81	10.00	2	7.990	3.995	Comp C48
60840	MGZD075	204	205	1	D08027	1.15	2.45	2.45	2.82				Comp C46
60840	MGZD075	205	206	1	D08028	1.22	1.11	1.11	1.35				Comp C44
60840	MGZD075	206	207	1	D08029	1.23	5.80	5.80	7.13	3	9.360	3.120	Comp C47
60840	MGZD076	213	214	1	D08120	1.13	2.56	2.56	2.89				Comp C46
60840	MGZD076	214	214.7	0.7	D08122	0.79	6.19	4.33	4.89				Comp C48
60840	MGZD076	214.7	215.4	0.7	D08123	0.71	5.20	3.64	3.69				Comp C47
60840	MGZD076	215.4	216.1	0.7	D08124	0.63	1.57	1.10	0.99				Comp C45
60840	MGZD076	216.1	216.8	0.7	D08125	0.75	0.14	0.10	0.11				Comp C41
60840	MGZD076	216.8	217.5	0.7	D08126	0.68	1.37	0.96	0.93				Comp C45
60840	MGZD076	217.5	218.2	0.7	D08127	0.71	7.51	5.26	5.33	5.2	17.946	3.451	Comp C48
60840	MGZD076	223.7	224.4	0.7	D08135	0.67	41.70	29.19	27.94				Comp C51
60840	MGZD076	224.4	225.1	0.7	D08136	0.76	0.94	0.66	0.71				Comp C44
60840	MGZD076	228	228.7	0.7	D08140	0.75	1.59	1.11	1.19				Comp C45
60840	MGZD076	228.7	229.4	0.7	D08141	0.69	12.70	8.89	8.76	2.8	39.851	14.233	Comp C49
60840	MGZD077	214.6	215.3	0.7	D08751	0.79	2.20	1.54	1.74				Comp C45
60840	MGZD077	215.3	216	0.7	D08752	0.81	1.57	1.10	1.27				Comp C45
60840	MGZD077	216	216.7	0.7	D08753	0.77	0.69	0.48	0.53				Comp C43
60840	MGZD077	216.7	217.4	0.7	D08754	0.83	0.19	0.13	0.16				Comp C41
60840	MGZD077	217.4	218.1	0.7	D08755	0.74	0.46	0.32	0.34				Comp C43
60840	MGZD077	218.1	218.8	0.7	D08756	0.76	0.52	0.36	0.40				Comp C43
60840	MGZD077	218.8	219.5	0.7	D08757	0.69	3.92	2.74	2.70				Comp C46
60840	MGZD077	219.5	220.2	0.7	D08759	0.74	14.40	10.08	10.66				Comp C50
60840	MGZD077	220.2	220.9	0.7	D08760	0.66	2.90	2.03	1.91				Comp C46
60840	MGZD077	220.9	221.6	0.7	D08761	0.71	12.30	8.61	8.73				Comp C49
60840	MGZD077	221.6	222.3	0.7	D08762	0.73	4.15	2.91	3.03				Comp C47
60840	MGZD077	222.3	223	0.7	D08763	0.66	2.53	1.77	1.67				Comp C46
60840	MGZD077	223	223.7	0.7	D08764	0.73	4.92	3.44	3.59	9.1	35.525	3.904	Comp C47
60640	MGZD079	229	230	1	D08993	1.15	0.84	0.84	0.97				Comp C44
60640	MGZD079	230	231	1	D08994	1.14	24.50	24.50	27.93	2	25.340	12.670	Comp C50
60640	MGZD079	239	240	1	D09005	1.1	4.14	4.14	4.55				Comp C47
60640	MGZD079	240	240.7	0.7	D09006	0.73	5.14	3.60	3.75				Comp C47
60640	MGZD079	240.7	241.4	0.7	D09007	0.71	2.20	1.54	1.56				Comp C45
60640	MGZD079	241.4	242.1	0.7	D09008	0.71	9.74	6.82	6.92				Comp C48
60640	MGZD079	242.1	243	0.9	D09009	0.97	8.93	8.04	8.66				Comp C48
60640	MGZD079	243	244	1	D09010	1.02	4.52	4.52	4.61				Comp C47
60640	MGZD079	244	245	1	D09011	1.13	3.80	3.80	4.29				Comp C46
60640	MGZD079	245	246	1	D09012	1.09	0.86	0.86	0.94				Comp C44
60640	MGZD079	246	247	1	D09013	1.04	3.75	3.75	3.90				Comp C46
60640	MGZD079	247	248	1	D09014	1.08	2.99	2.99	3.23				Comp C46
60640	MGZD079	248	249	1	D09015	1.07	0.55	0.55	0.59				Comp C43
60640	MGZD079	249	250	1	D09016	1.15	0.91	0.91	1.05				Comp C44
60640	MGZD079	250	251	1	D09017	1.01	5.83	5.83	5.89				Comp C47
60640	MGZD079	251	252	1	D09019	1	32.30	32.30	32.30				Comp C51

C ZONE HIGH GRADE COMPOSITE (SECTIONS 60640 through 60840)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60640	MGZD080	206.1	206.8	0.7	D09147	0.75	2.16	1.51	1.62				Comp C45
60640	MGZD080	206.8	207.5	0.7	D09148	0.72	1.41	0.99	1.02				Comp C45
60640	MGZD080	207.5	208.2	0.7	D09149	0.73	4.89	3.42	3.57				Comp C47
60640	MGZD080	208.2	208.9	0.7	D09150	0.7	3.83	2.68	2.68	2.8	8.603	3.073	Comp C46
60800	MGZD151	194.7	195.4	0.7	D32363	0.82	10.60	7.42	8.69				Comp C49
60800	MGZD151	195.4	196.1	0.7	D32364	0.85	0.81	0.57	0.69	1.4	7.987	5.705	Comp C44
60840	MGZD153	211.7	212.4	0.7	D32699	0.79	2.45	1.72	1.94				Comp C46
60840	MGZD153	212.4	213.1	0.7	D32700	0.75	2.45	1.72	1.84				Comp C46
60840	MGZD153	213.1	213.8	0.7	D32701	0.8	28.40	19.88	22.72	2.1	23.310	11.100	Comp C51
60840	MGZD153	233.3	234	0.7	D32727	0.82	10.70	7.49	8.77				Comp C49
60840	MGZD153	234	234.7	0.7	D32728	0.76	3.58	2.51	2.72				Comp C46
60840	MGZD153	234.7	235.4	0.7	D32729	0.83	23.80	16.66	19.75				Comp C50
60840	MGZD153	235.4	236.1	0.7	D32730	0.84	17.50	12.25	14.70				Comp C50
60840	MGZD153	236.1	236.8	0.7	D32731	0.78	3.67	2.57	2.86				Comp C46
60840	MGZD153	236.8	237.5	0.7	D32732	0.71	8.62	6.03	6.12				Comp C48
60840	MGZD153	237.5	238.2	0.7	D32733	0.79	17.10	11.97	13.51				Comp C50
60840	MGZD153	238.2	238.9	0.7	D32734	0.96	16.90	11.83	16.22	5.6	71.309	12.734	Comp C50
60840	MGZD153	241.7	242.4	0.7	D32740	0.83	2.50	1.75	2.08				Comp C46
60840	MGZD153	242.4	243.1	0.7	D32741	0.86	4.73	3.31	4.07				Comp C47
60840	MGZD153	243.1	243.8	0.7	D32742	0.92	2.42	1.69	2.23				Comp C46
60840	MGZD153	243.8	244.5	0.7	D32743	0.91	3.11	2.18	2.83				Comp C46
60840	MGZD153	244.5	245.2	0.7	D32744	0.94	3.61	2.53	3.39	3.5	11.459	3.274	Comp C46
60800	MGZD154	231.8	232.5	0.7	D33412	0.73	2.43	1.70	1.77				Comp C46
60800	MGZD154	232.5	233.2	0.7	D33413	0.79	2.92	2.04	2.31				Comp C46
60800	MGZD154	233.2	233.9	0.7	D33414	0.82	1.40	0.98	1.15				Comp C45
60800	MGZD154	233.9	234.6	0.7	D33415	0.76	7.19	5.03	5.46	2.8	9.758	3.485	Comp C48
60800	MGZD154	237.4	238.1	0.7	D33422	0.74	2.98	2.09	2.21				Comp C46
60800	MGZD154	238.1	238.8	0.7	D33423	0.76	5.74	4.02	4.36				Comp C47
60800	MGZD154	238.8	239.5	0.7	D33424	0.68	3.48	2.44	2.37				Comp C46
60800	MGZD154	239.5	240.2	0.7	D33425	0.7	14.00	9.80	9.80				Comp C49
60800	MGZD154	240.2	240.9	0.7	D33426	0.74	7.92	5.54	5.86				Comp C48
60800	MGZD154	240.9	241.6	0.7	D33427	0.72	1.40	0.98	1.01	4.2	24.864	5.920	Comp C45
60840	MGZD156	221	221.7	0.7	D33914	0.71	7.55	5.29	5.36				Comp C48
60840	MGZD156	221.7	222.4	0.7	D33915	0.7	3.46	2.42	2.42	1.4	7.707	5.505	Comp C46
60800	MGZD157	236	236.7	0.7	D34289	0.76	3.09	2.16	2.35				Comp C46
60800	MGZD157	236.7	237.4	0.7	D34290	0.79	19.00	13.30	15.01				Comp C50
60800	MGZD157	237.4	238.1	0.7	D34291	0.79	16.40	11.48	12.96	2.1	26.943	12.830	Comp C50
60840	MGZD161	169.7	170.4	0.7	D35317	0.9	16.60	11.62	14.94				Comp C50
60840	MGZD161	170.4	171.1	0.7	D35319	0.77	0.35	0.25	0.27				Comp C42
60840	MGZD161	171.1	171.8	0.7	D35320	0.8	0.31	0.22	0.25				Comp C42
60840	MGZD161	171.8	172.5	0.7	D35322	0.91	1.16	0.81	1.06				Comp C44
60840	MGZD161	172.5	173.2	0.7	D35323	0.94	3.88	2.72	3.65	3.5	15.610	4.460	Comp C46
60840	MGZD161	183	183.7	0.7	D35334	0.96	8.63	6.04	8.28				Comp C48
60840	MGZD161	183.7	184.4	0.7	D35335	0.83	23.70	16.59	19.67				Comp C50
60840	MGZD161	184.4	185.1	0.7	D35336	0.75	10.60	7.42	7.95				Comp C49
60840	MGZD161	185.1	185.8	0.7	D35337	0.81	0.61	0.43	0.49				Comp C43
60840	MGZD161	185.8	186.5	0.7	D35339	0.79	1.46	1.02	1.15				Comp C45
60840	MGZD161	186.5	187.2	0.7	D35340	0.78	2.34	1.64	1.83	4.2	33.138	7.890	Comp C45
60840	MGZD161	215	216	1	D35375	1.26	7.95	7.95	10.02				Comp C48
60840	MGZD161	216	217	1	D35376	1.22	0.20	0.20	0.24	2	8.150	4.075	Comp C41
60840	MGZD161	221	222	1	D35382	1.26	5.97	5.97	7.52				Comp C47
60840	MGZD161	222	223	1	D35383	1.08	0.34	0.34	0.37				Comp C42
60840	MGZD161	223	224	1	D35384	1.1	0.21	0.21	0.23				Comp C41
60840	MGZD161	224	224.7	0.7	D35385	0.77	1.32	0.92	1.02				Comp C45
60840	MGZD161	224.7	225.4	0.7	D35386	0.96	0.28	0.20	0.27				Comp C42
60840	MGZD161	225.4	226.1	0.7	D35387	0.82	19.10	13.37	15.66	5.1	21.010	4.120	Comp C50
60840	MGZD161	233	234	1	D35395	1.14	20.00	20.00	22.80				Comp C50
60840	MGZD161	234	235	1	D35397	1	0.10	0.10	0.10				Comp C41
60840	MGZD161	235	236	1	D35399	0.99	0.07	0.07	0.07				Comp C41
60840	MGZD161	236	237	1	D35400	1.17	0.53	0.53	0.62				Comp C43
60840	MGZD161	237	238	1	D35401	1.19	0.49	0.49	0.58				Comp C43

C ZONE HIGH GRADE COMPOSITE (SECTIONS 60640 through 60840)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60680	MGZD167	137	138	1	D37213	1.01	4.22	4.22	4.26				Comp C47
60680	MGZD167	138	139	1	D37214	0.94	3.75	3.75	3.53	2	7.970	3.985	Comp C46
60680	MGZD178	230	231	1	D39856	1.46	4.30	4.30	6.28				Comp C47
60680	MGZD178	231	232	1	D39857	1.33	2.38	2.38	3.17				Comp C45
60680	MGZD178	232	232.7	0.7	D39859	0.98	0.41	0.29	0.40				Comp C43
60680	MGZD178	232.7	233.4	0.7	D39860	0.78	37.80	26.46	29.48				Comp C51
60680	MGZD178	233.4	234.1	0.7	D39861	0.79	12.20	8.54	9.64				Comp C49
60680	MGZD178	234.1	234.8	0.7	D39862	0.86	41.90	29.33	36.03				Comp C51
60680	MGZD178	234.8	235.5	0.7	D39863	0.83	1.12	0.78	0.93				Comp C44
60680	MGZD178	235.5	236.2	0.7	D39864	0.73	40.20	28.14	29.35				Comp C51
60680	MGZD178	236.2	236.9	0.7	D39865	0.73	3.11	2.18	2.27				Comp C46
60680	MGZD178	236.9	237.6	0.7	D39866	0.72	1.53	1.07	1.10				Comp C45
60680	MGZD178	237.6	238.3	0.7	D39867	0.78	3.36	2.35	2.62	8.3	105.821	12.750	Comp C46
60680	MGZD178	247.7	248.4	0.7	D39882	1.06	7.25	5.08	7.69				Comp C48
60680	MGZD178	248.4	249.1	0.7	D39883	0.95	2.05	1.43	1.95				Comp C45
60680	MGZD178	249.1	249.8	0.7	D39884	0.93	1.34	0.94	1.25				Comp C45
60680	MGZD178	249.8	250.5	0.7	D39885	0.82	4.91	3.44	4.03	2.8	10.885	3.888	Comp C47
60680	MGZD178	254.7	255.4	0.7	D39892	1.02	6.86	4.80	7.00	0.7	4.802	6.860	Comp C48
60680	MGZD178	269.4	270.1	0.7	D39915	0.56	1.17	0.82	0.66				Comp C44
60680	MGZD178	270.1	270.8	0.7	D39916	0.67	59.60	41.72	39.93	1.4	42.539	30.385	Comp C51
60680	MGZD178	277.1	278	0.9	D39928	1.06	8.58	7.72	9.09	0.9	7.722	8.580	Comp C48
60640	MGZD181	178.5	179.2	0.7	D41031	0.9	6.16	4.31	5.54				Comp C48
60640	MGZD181	179.2	179.9	0.7	D41032	0.85	3.13	2.19	2.66				Comp C46
60640	MGZD181	179.9	180.6	0.7	D41033	0.85	4.20	2.94	3.57				Comp C47
60640	MGZD181	180.6	181.3	0.7	D41034	0.8	2.92	2.04	2.34				Comp C46
60640	MGZD181	181.3	182	0.7	D41035	0.76	0.90	0.63	0.68				Comp C44
60640	MGZD181	182	182.7	0.7	D41036	0.71	14.80	10.36	10.51				Comp C50
60640	MGZD181	182.7	183.4	0.7	D41037	0.87	22.00	15.40	19.14				Comp C50
60640	MGZD181	183.4	184.1	0.7	D41039	0.86	7.15	5.00	6.15				Comp C48
60640	MGZD181	184.1	184.8	0.7	D41040	0.85	0.12	0.08	0.10				Comp C41
60640	MGZD181	184.8	185.5	0.7	D41041	0.81	2.47	1.73	2.00	7	44.695	6.385	Comp C46
60640	MGZD181	255	256	1	D41123	1.31	7.59	7.59	9.94	1	7.590	7.590	Comp C48
60640	MGZD188	238.7	239.4	0.7	D42142	0.83	2.81	1.97	2.33				Comp C46
60640	MGZD188	239.4	240.1	0.7	D42143	0.88	38.90	27.23	34.23	1.4	29.197	20.855	Comp C51
60640	MGZD188	245	245.7	0.7	D42152	0.81	4.00	2.80	3.24				Comp C46
60640	MGZD188	245.7	246.4	0.7	D42153	0.8	1.57	1.10	1.26				Comp C45
60640	MGZD188	246.4	247.1	0.7	D42154	0.78	1.79	1.25	1.40				Comp C45
60640	MGZD188	247.1	247.8	0.7	D42155	0.81	5.39	3.77	4.37	2.8	8.925	3.188	Comp C47
60640	MGZD188	254.7	255.4	0.7	D42165	0.8	11.40	7.98	9.12	0.7	7.980	11.400	Comp C49
60720	MGZD191	141.2	141.9	0.7	D42897	0.76	2.78	1.95	2.11				Comp C46
60720	MGZD191	141.9	142.6	0.7	D42899	0.74	6.46	4.52	4.78				Comp C48
60720	MGZD191	142.6	143.3	0.7	D42900	0.73	15.90	11.13	11.61				Comp C50
60720	MGZD191	143.3	144	0.7	D42901	0.68	5.61	3.93	3.81				Comp C47
60720	MGZD191	144	144.7	0.7	D42902	0.66	2.28	1.60	1.50				Comp C45
60720	MGZD191	144.7	145.4	0.7	D42903	0.66	0.88	0.62	0.58				Comp C44
60720	MGZD191	145.4	146.1	0.7	D42904	0.68	0.50	0.35	0.34				Comp C43
60720	MGZD191	146.1	146.8	0.7	D42905	0.71	0.29	0.20	0.21				Comp C42
60720	MGZD191	146.8	147.5	0.7	D42906	0.65	1.25	0.87	0.81				Comp C44
60720	MGZD191	147.5	148.2	0.7	D42907	0.68	0.24	0.17	0.16				Comp C41
60720	MGZD191	148.2	148.9	0.7	D42908	0.86	2.50	1.75	2.15				Comp C46
60720	MGZD191	148.9	149.6	0.7	D42909	0.62	0.75	0.52	0.47				Comp C43
60720	MGZD191	149.6	150.3	0.7	D42910	0.66	3.16	2.21	2.09				Comp C46
60720	MGZD191	150.3	151	0.7	D42911	0.75	0.42	0.29	0.32				Comp C43
60720	MGZD191	151	151.7	0.7	D42912	0.79	0.07	0.05	0.06				Comp C41
60720	MGZD191	151.7	152.4	0.7	D42913	0.67	35.40	24.78	23.72				Comp C51
60720	MGZD191	152.4	153.1	0.7	D42914	0.83	0.46	0.32	0.38	11.9	55.265	4.644	Comp C43
60720	MGZD196	186	187	1	D44368	1.1	0.62	0.62	0.68				Comp C43
60720	MGZD196	187	187.7	0.7	D44369	0.78	0.22	0.15	0.17				Comp C41
60720	MGZD196	187.7	188.4	0.7	D44370	0.71	1.28	0.90	0.91				Comp C44
60720	MGZD196	188.4	189.1	0.7	D44372	0.74	0.22	0.15	0.16				Comp C41
60720	MGZD196	189.1	189.8	0.7	D44373	0.82	7.51	5.26	6.16				Comp C48

C ZONE HIGH GRADE COMPOSITE (SECTIONS 60640 through 60840)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60720	MGZD196	190.5	191.2	0.7	D44375	0.7	1.30	0.91	0.91				Comp C44
60720	MGZD196	191.2	191.9	0.7	D44376	0.66	2.87	2.01	1.89				Comp C46
60720	MGZD196	191.9	192.6	0.7	D44377	0.64	0.91	0.64	0.58				Comp C44
60720	MGZD196	192.6	193.3	0.7	D44379	0.86	19.00	13.30	16.34				Comp C50
60720	MGZD196	193.3	194	0.7	D44380	0.67	15.60	10.92	10.45				Comp C50
60720	MGZD196	194	194.7	0.7	D44381	0.76	2.73	1.91	2.07				Comp C46
60720	MGZD196	194.7	195.4	0.7	D44382	0.77	1.64	1.15	1.26				Comp C45
60720	MGZD196	195.4	196.1	0.7	D44383	0.78	0.36	0.25	0.28				Comp C42
60720	MGZD196	196.1	196.8	0.7	D44384	0.67	5.57	3.90	3.73				Comp C47
60720	MGZD196	196.8	197.5	0.7	D44385	0.72	0.33	0.23	0.24				Comp C42
60720	MGZD196	197.5	198.2	0.7	D44386	0.66	0.49	0.34	0.32				Comp C43
60720	MGZD196	198.2	198.9	0.7	D44387	0.74	1.14	0.80	0.84				Comp C44
60720	MGZD196	198.9	199.6	0.7	D44388	0.81	0.25	0.17	0.20	13.6	50.418	3.707	Comp C41
60720	MGZD203	235.8	236.5	0.7	D46174	0.78	3.36	2.35	2.62				Comp C46
60720	MGZD203	236.5	237.2	0.7	D46175	0.83	17.40	12.18	14.44				Comp C50
60720	MGZD203	237.2	237.9	0.7	D46176	0.76	1.10	0.77	0.84				Comp C44
60720	MGZD203	237.9	238.6	0.7	D46177	0.6	1.40	0.98	0.84				Comp C45
60720	MGZD203	238.6	239.3	0.7	D46179	0.76	1.41	0.99	1.07				Comp C45
60720	MGZD203	239.3	240	0.7	D46180	0.74	0.46	0.32	0.34				Comp C43
60720	MGZD203	240	240.7	0.7	D46181	0.72	2.13	1.49	1.53				Comp C45
60720	MGZD203	240.7	241.4	0.7	D46182	0.77	8.73	6.11	6.72				Comp C48
60720	MGZD203	241.4	242.1	0.7	D46183	0.83	8.73	6.11	7.25				Comp C48
60720	MGZD203	242.1	242.8	0.7	D46184	0.72	17.50	12.25	12.60				Comp C50
60720	MGZD203	242.8	243.5	0.7	D46185	0.73	12.60	8.82	9.20				Comp C49
60720	MGZD203	243.5	244.2	0.7	D46186	0.81	1.93	1.35	1.56				Comp C45
60720	MGZD203	244.2	244.9	0.7	D46187	0.9	10.90	7.63	9.81				Comp C49
60720	MGZD203	244.9	245.6	0.7	D46188	0.81	27.60	19.32	22.36				Comp C51
60720	MGZD203	245.6	246.3	0.7	D46189	0.74	1.39	0.97	1.03				Comp C45
60720	MGZD203	246.3	247	0.7	D46190	0.81	3.50	2.45	2.84				Comp C46
60720	MGZD203	247	247.7	0.7	D46191	0.8	0.30	0.21	0.24				Comp C42
60720	MGZD203	247.7	248.4	0.7	D46192	0.73	3.02	2.11	2.20				Comp C46
60720	MGZD203	248.4	249.1	0.7	D46193	0.72	6.98	4.89	5.03				Comp C48
60720	MGZD203	249.1	249.8	0.7	D46194	0.79	0.78	0.55	0.62				Comp C43
60720	MGZD203	249.8	250.5	0.7	D46195	0.78	28.80	20.16	22.46				Comp C51
60720	MGZD203	250.5	251.2	0.7	D46197	0.81	2.84	1.99	2.30				Comp C46
60720	MGZD203	251.2	251.9	0.7	D46199	0.7	1.91	1.34	1.34				Comp C45
60720	MGZD203	251.9	252.6	0.7	D46200	0.84	0.16	0.11	0.13				Comp C41
60720	MGZD203	252.6	253.3	0.7	D46201	0.83	21.50	15.05	17.85				Comp C50
60720	MGZD203	253.3	254	0.7	D46202	0.79	11.00	7.70	8.69				Comp C49
60720	MGZD203	254	254.7	0.7	D46203	0.82	2.67	1.87	2.19				Comp C46
60720	MGZD203	254.7	255.4	0.7	D46204	0.78	0.34	0.24	0.27				Comp C42
60720	MGZD203	255.4	256.1	0.7	D46205	0.79	0.14	0.10	0.11				Comp C41
60720	MGZD203	256.1	256.8	0.7	D46206	0.82	0.46	0.32	0.38				Comp C43
60720	MGZD203	256.8	257.5	0.7	D46207	0.64	0.10	0.07	0.06				Comp C41
60720	MGZD203	257.5	258.2	0.7	D46208	1	0.85	0.59	0.85				Comp C44
60720	MGZD203	258.2	258.9	0.7	D46209	0.88	0.67	0.47	0.59				Comp C43
60720	MGZD203	258.9	259.6	0.7	D46210	0.89	0.08	0.06	0.07				Comp C41
60720	MGZD203	259.6	260.3	0.7	D46211	0.85	0.06	0.04	0.05				Comp C41
60720	MGZD203	260.3	261	0.7	D46212	0.73	0.43	0.30	0.31				Comp C43
60720	MGZD203	261	261.7	0.7	D46213	0.64	0.12	0.08	0.08				Comp C41
60720	MGZD203	261.7	262.4	0.7	D46214	0.71	0.45	0.31	0.32				Comp C43
60720	MGZD203	262.4	263.1	0.7	D46215	0.7	0.07	0.05	0.05				Comp C41
60720	MGZD203	263.1	263.8	0.7	D46216	0.7	0.05	0.03	0.04				Comp C41
60720	MGZD203	263.8	264.5	0.7	D46217	0.75	1.87	1.31	1.40				Comp C45
60720	MGZD203	264.5	265.2	0.7	D46219	0.83	0.25	0.17	0.21				Comp C41
60720	MGZD203	265.2	265.9	0.7	D46220	0.75	0.35	0.24	0.26				Comp C42
60720	MGZD203	265.9	266.6	0.7	D46222	0.85	0.39	0.27	0.33				Comp C42
60720	MGZD203	266.6	267.3	0.7	D46223	0.85	0.11	0.08	0.09				Comp C41
60720	MGZD203	267.3	268	0.7	D46224	0.85	0.58	0.41	0.49	32.2	145.229	4.510	Comp C43
60680	MGZD218	181.1	181.8	0.7	D51461	0.7	6.01	4.21	4.21				Comp C48
60680	MGZD218	181.8	182.5	0.7	D51462	0.72	2.94	2.06	2.12	0.7	6.265	8.950	Comp C46

C ZONE HIGH GRADE COMPOSITE (SECTIONS 60640 through 60840)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60680	MGZD218	187.4	188.1	0.7	D51470	0.7	71.40	49.98	49.98				Comp C51
60680	MGZD218	188.1	188.8	0.7	D51472	0.64	3.73	2.61	2.39	2.1	58.030	27.633	Comp C46
60680	MGZD218	229.7	230.4	0.7	D51522	0.65	2.64	1.85	1.72				Comp C46
60680	MGZD218	230.4	231.1	0.7	D51523	0.68	14.10	9.87	9.59	1.4	11.718	8.370	Comp C50
60640	MGZD246	152	152.7	0.7	D63102	0.69	3.30	2.31	2.28	0.7	2.310	3.300	Comp C46
60720	MGZD253	241	242	1	D65705	1.13	1.34	1.34	1.51				Comp C45
60720	MGZD253	242	243	1	D65706	1.12	0.56	0.56	0.63				Comp C43
60720	MGZD253	243	244	1	D65707	1.12	0.88	0.88	0.99				Comp C44
60720	MGZD253	244	245	1	D65708	1.11	0.09	0.09	0.10				Comp C41
60720	MGZD253	245	246	1	D65709	1.1	0.24	0.24	0.26				Comp C41
60720	MGZD253	246	247	1	D65710	1.12	0.25	0.25	0.28				Comp C41
60720	MGZD253	247	248	1	D65711	1.14	0.44	0.44	0.50				Comp C43
60720	MGZD253	248	248.7	0.7	D65712	0.84	1.13	0.79	0.95				Comp C44
60720	MGZD253	248.7	249.4	0.7	D65713	0.75	45.70	31.99	34.28				Comp C51
60720	MGZD253	249.4	250.1	0.7	D65714	0.77	2.49	1.74	1.92				Comp C46
60720	MGZD253	250.1	251	0.9	D65715	0.95	0.71	0.64	0.67				Comp C43
60720	MGZD253	251	252	1	D65716	1	0.35	0.35	0.35				Comp C42
60720	MGZD253	252	253	1	D65717	0.98	1.67	1.67	1.64				Comp C45
60720	MGZD253	253	254	1	D65719	1.05	0.35	0.35	0.37				Comp C42
60720	MGZD253	254	254.7	0.7	D65720	0.74	0.15	0.10	0.11				Comp C41
60720	MGZD253	254.7	255.4	0.7	D65722	0.79	2.71	1.90	2.14				Comp C46
60720	MGZD253	255.4	256.1	0.7	D65723	0.83	8.62	6.03	7.15	15.1	49.369	3.269	Comp C48
60640	MGZD258	253	253.7	0.7	D67556	0.91	4.19	2.93	3.81				Comp C47
60640	MGZD258	253.7	254.4	0.7	D67557	0.88	0.25	0.18	0.22				Comp C41
60640	MGZD258	254.4	255.1	0.7	D67559	0.87	12.60	8.82	10.96				Comp C49
60640	MGZD258	255.1	255.8	0.7	D67560	0.81	8.98	6.29	7.27	2.8	18.214	6.505	Comp C48
60640	MGZD258	258.6	259.3	0.7	D67565	0.79	2.25	1.57	1.78				Comp C45
60640	MGZD258	259.3	260	0.7	D67566	0.79	7.00	4.90	5.53	1.4	6.475	4.625	Comp C48
60680	MGZD262	239.2	240	0.8	D68528	0.92	1.91	1.53	1.76				Comp C45
60680	MGZD262	240	241	1	D68529	1.17	5.83	5.83	6.82	1.8	7.358	4.088	Comp C47
60680	MGZD262	259.7	260.4	0.7	D68551	0.8	5.14	3.60	4.11				Comp C47
60680	MGZD262	260.4	261.1	0.7	D68552	0.81	0.32	0.22	0.26				Comp C42
60680	MGZD262	261.1	261.8	0.7	D68553	0.61	3.76	2.63	2.29	2.1	6.454	3.073	Comp C46
60720	MGZD268	264.7	265.4	0.7	D71041	0.82	2.52	1.76	2.07				Comp C46
60720	MGZD268	265.4	266.1	0.7	D71042	0.87	5.35	3.75	4.65				Comp C47
60720	MGZD268	266.1	266.8	0.7	D71043	0.83	0.34	0.24	0.28				Comp C42
60720	MGZD268	266.8	267.5	0.7	D71044	0.86	31.90	22.33	27.43				Comp C51
60720	MGZD268	267.5	268.2	0.7	D71045	0.86	0.38	0.27	0.33	3.5	28.343	8.098	Comp C42
60720	MGZD268	293	294	1	D71074	1.15	0.28	0.28	0.32				Comp C42
60720	MGZD268	295	296	1	D71077	1.18	0.96	0.96	1.13				Comp C44
60720	MGZD268	296	296.7	0.7	D71079	0.91	0.48	0.34	0.44				Comp C43
60720	MGZD268	296.7	297.4	0.7	D71080	0.95	0.35	0.24	0.33				Comp C42
60720	MGZD268	297.4	298.1	0.7	D71081	0.64	33.10	23.17	21.18				Comp C51
60720	MGZD268	298.1	298.8	0.7	D71082	0.77	1.73	1.21	1.33				Comp C45
60720	MGZD268	298.8	299.5	0.7	D71083	0.85	34.90	24.43	29.67				Comp C51
60720	MGZD268	299.5	300.2	0.7	D71084	0.73	0.63	0.44	0.46	7.2	52.373	7.274	Comp C43
60680	MGZD272	212	212.7	0.7	D71899	1.04	13.60	9.52	14.14				Comp C49
60680	MGZD272	213.4	214.1	0.7	D71902	1.01	10.70	7.49	10.81	2.1	17.241	8.210	Comp C49
60680	MGZD272	263	263.7	0.7	D71963	0.73	6.81	4.77	4.97				Comp C48
60680	MGZD272	263.7	264.4	0.7	D71964	0.81	5.00	3.50	4.05	1.4	8.267	5.905	Comp C47
60760	MGZD275	229.7	230.4	0.7	D73123	0.8	0.97	0.68	0.78				Comp C44
60760	MGZD275	230.4	231.1	0.7	D73124	0.83	1.18	0.83	0.98				Comp C44
60760	MGZD275	231.1	231.8	0.7	D73125	0.81	2.41	1.69	1.95				Comp C46
60760	MGZD275	231.8	232.5	0.7	D73126	0.79	8.24	5.77	6.51	2.8	8.960	3.200	Comp C48
60760	MGZD275	236	236.7	0.7	D73133	0.82	1.79	1.25	1.47				Comp C45
60760	MGZD275	236.7	237.4	0.7	D73134	0.8	7.25	5.08	5.80				Comp C48
60760	MGZD275	237.4	238.1	0.7	D73136	0.86	4.47	3.13	3.84				Comp C47
60760	MGZD275	238.1	238.8	0.7	D73137	0.84	0.47	0.33	0.39				Comp C43
60760	MGZD275	238.8	239.5	0.7	D73139	0.77	1.37	0.96	1.05	3.5	10.745	3.070	Comp C45
60760	MGZD275	241.6	242.3	0.7	D73144	0.82	3.33	2.33	2.73				Comp C46
60760	MGZD275	242.3	243	0.7	D73145	0.77	0.29	0.20	0.22				Comp C42

C ZONE HIGH GRADE COMPOSITE (SECTIONS 60640 through 60840)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60760	MGZD275	243.7	244.4	0.7	D73147	0.74	21.80	15.26	16.13				Comp C50
60760	MGZD275	244.4	245.1	0.7	D73148	0.74	4.75	3.32	3.52				Comp C47
60760	MGZD275	245.1	245.8	0.7	D73149	0.85	3.06	2.14	2.60				Comp C46
60760	MGZD275	245.8	246.5	0.7	D73151	0.82	0.69	0.48	0.57				Comp C43
60760	MGZD275	246.5	247.2	0.7	D73152	0.85	1.91	1.34	1.62				Comp C45
60760	MGZD275	247.2	247.9	0.7	D73153	0.82	1.91	1.34	1.57				Comp C45
60760	MGZD275	248.6	249.3	0.7	D73156	0.83	0.22	0.15	0.18				Comp C41
60760	MGZD275	249.3	250	0.7	D73157	0.85	0.05	0.03	0.04				Comp C41
60760	MGZD275	250	250.7	0.7	D73159	0.55	5.61	3.93	3.09				Comp C47
60760	MGZD275	250.7	251.4	0.7	D73161	0.91	0.12	0.08	0.11				Comp C41
60760	MGZD275	251.4	252.1	0.7	D73162	0.83	4.69	3.28	3.89				Comp C47
60760	MGZD275	252.1	252.8	0.7	D73163	0.87	3.81	2.67	3.31				Comp C46
60760	MGZD275	252.8	253.5	0.7	D73164	0.77	12.00	8.40	9.24				Comp C49
60760	MGZD275	253.5	254.2	0.7	D73165	0.82	3.90	2.73	3.20	12.6	51.723	4.105	Comp C46
60640	MGZD276	195	196	1	D73471	1.25	2.62	2.62	3.28				Comp C46
60640	MGZD276	196	196.7	0.7	D73472	0.86	0.92	0.64	0.79				Comp C44
60640	MGZD276	196.7	197.4	0.7	D73473	0.76	1.91	1.34	1.45				Comp C45
60640	MGZD276	198.1	199	0.9	D73476	1.22	2.67	2.40	3.26				Comp C46
60640	MGZD276	199	200	1	D73477	1.45	0.12	0.12	0.17				Comp C41
60640	MGZD276	200	201	1	D73479	1.55	0.33	0.33	0.51				Comp C42
60640	MGZD276	201	202	1	D73481	1.35	16.80	16.80	22.68				Comp C50
60640	MGZD276	202	202.7	0.7	D73482	0.84	0.65	0.45	0.55				Comp C43
60640	MGZD276	202.7	203.4	0.7	D73483	0.79	3.17	2.22	2.50				Comp C46
60640	MGZD276	216	216.7	0.7	D73501	0.89	2.28	1.60	2.03				Comp C45
60640	MGZD276	216.7	217.4	0.7	D73502	0.85	9.76	6.83	8.30				Comp C48
60640	MGZD276	217.4	218.1	0.7	D73503	0.85	0.27	0.19	0.23				Comp C42
60640	MGZD276	218.1	218.8	0.7	D73504	0.99	1.00	0.70	0.99				Comp C44
60640	MGZD276	218.8	219.5	0.7	D73505	0.98	12.40	8.68	12.15	11.9	45.975	3.863	Comp C49
60640	MGZD276	256	257	1	D73553	1.34	3.24	3.24	4.34	1	3.240	3.240	Comp C46
60640	MGZD279	239.7	240.4	0.7	D74768	0.95	1.92	1.34	1.82				Comp C45
60640	MGZD279	240.4	241.2	0.8	D74769	1.01	3.38	2.70	3.41				Comp C46
60640	MGZD279	251.2	251.9	0.7	D74785	0.87	7.39	5.17	6.43				Comp C48
60640	MGZD279	251.9	252.6	0.7	D74786	0.73	1.19	0.83	0.87	2.9	10.054	3.467	Comp C44
60640	MGZD279	260.8	261.5	0.7	D74799	0.86	5.24	3.67	4.51				Comp C47
60640	MGZD279	261.5	262.2	0.7	D74801	0.87	1.86	1.30	1.62	1.4	4.970	3.550	Comp C45
60680	MGZD280	248.9	249.6	0.7	D75226	0.7	14.60	10.22	10.22	0.7	10.220	14.600	Comp C50
60680	MGZD280	255.4	256.1	0.7	D75236	0.75	3.98	2.79	2.99				Comp C46
60680	MGZD280	256.1	256.8	0.7	D75237	0.79	1.83	1.28	1.45	2.1	14.357	6.837	Comp C45
60680	MGZD286	274	275	1	D77427	1.33	5.05	5.05	6.72	1	5.050	5.050	Comp C47
60640	MGZD287	303	304	1	D77907	1.14	7.07	7.07	8.06	1	7.070	7.070	Comp C48
60760	MGZD288	258.4	259.1	0.7	D78291	0.78	39.20	27.44	30.58				Comp C51
60760	MGZD288	259.1	259.8	0.7	D78292	0.84	0.75	0.52	0.63				Comp C43
60760	MGZD288	259.8	260.5	0.7	D78293	0.85	0.20	0.14	0.17				Comp C41
60760	MGZD288	261.2	262	0.8	D78296	0.84	0.26	0.21	0.22				Comp C42
60760	MGZD288	262	262.8	0.8	D78297	0.95	0.04	0.03	0.04				Comp C41
60760	MGZD288	262.8	263.6	0.8	D78299	0.96	0.20	0.16	0.19				Comp C41
60760	MGZD288	263.6	264.3	0.7	D78301	0.68	1.05	0.73	0.71				Comp C44
60760	MGZD288	264.3	265	0.7	D78302	0.72	1.80	1.26	1.30	6.6	30.710	4.653	Comp C45

Composite grade (based on (drill core grade x thickness) and meterage, assumes uniform core density)	314.2 m	6.68	2099.7	
Composite grade (based on as-received intercept weights and drill core assays)	355.2	6.66		2364.5

D ZONE   LOW GRADE COMPOSITE   (SECTIONS 60880 through 61200)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
61120	MGZD018	21.00	21.70	0.70	D01445	0.80	3.26	2.282	2.608				Comp D68
61120	MGZD018	21.70	22.80	1.10	D01447	1.20	1.99	2.189	2.388				Comp D67
61120	MGZD018	22.80	23.70	0.90	D01448	1.00	2.73	2.457	2.730				Comp D68
61120	MGZD018	23.70	24.70	1.00	D01449	1.10	1.39	1.390	1.529	3.70	8.318	2.248	Comp D66
61120	MGZD018	42.00	42.70	0.70	D01470	0.70	1.53	1.071	1.071				Comp D66
61120	MGZD018	42.70	43.40	0.70	D01472	0.80	0.47	0.329	0.376	1.40	1.400	1.000	Comp D62
61120	MGZD018	47.00	48.00	1.00	D01477	1.20	0.47	0.470	0.564				Comp D62
61120	MGZD018	48.00	49.00	1.00	D01478	1.10	1.06	1.060	1.166				Comp D65
61120	MGZD018	49.00	49.70	0.70	D01479	0.80	0.50	0.350	0.400				Comp D62
61120	MGZD018	49.70	50.40	0.70	D01480	0.70	0.89	0.623	0.623	3.40	2.503	0.736	Comp D64
61120	MGZD019	26.70	27.40	0.70	D01526	0.45	1.34	0.938	0.603				Comp D66
61120	MGZD019	27.40	28.10	0.70	D01527	0.74	1.79	1.253	1.325				Comp D67
61120	MGZD019	28.10	29.00	0.90	D01529	0.94	0.44	0.396	0.414				Comp D62
61120	MGZD019	29.00	29.70	0.70	D01530	0.65	0.08	0.056	0.052				Comp D61
61120	MGZD019	29.70	30.40	0.70	D01531	0.72	0.09	0.063	0.065				Comp D61
61120	MGZD019	30.40	31.30	0.90	D01532	1.04	0.08	0.072	0.083				Comp D61
61120	MGZD019	31.30	32.00	0.70	D01533	0.74	2.16	1.512	1.598	5.30	4.290	0.809	Comp D67
61120	MGZD019	36.70	37.40	0.70	D01539	0.65	0.76	0.532	0.494				Comp D64
61120	MGZD019	37.40	38.10	0.70	D01540	0.66	0.56	0.392	0.370				Comp D63
61120	MGZD019	38.10	39.00	0.90	D01541	0.84	0.33	0.297	0.277				Comp D62
61120	MGZD019	39.00	39.70	0.70	D01542	0.74	1.27	0.889	0.940				Comp D65
61120	MGZD019	39.70	40.40	0.70	D01544	0.64	2.01	1.407	1.286				Comp D67
61120	MGZD019	40.40	41.10	0.70	D01545	0.55	0.40	0.280	0.220	4.40	3.797	0.863	Comp D62
61120	MGZD019	82.00	83.00	1.00	D01589	1.20	0.49	0.490	0.588				Comp D62
61120	MGZD019	83.00	84.00	1.00	D01590	1.10	1.97	1.970	2.167				Comp D67
61120	MGZD019	84.00	85.00	1.00	D01591	1.10	1.76	1.760	1.936				Comp D67
61120	MGZD019	85.00	86.00	1.00	D01592	1.40	6.03	6.030	8.442				Comp D70
61120	MGZD019	86.00	87.00	1.00	D01593	1.20	2.00	2.000	2.400				Comp D67
61120	MGZD019	87.00	88.00	1.00	D01594	1.20	0.80	0.800	0.960	6.00	13.050	2.175	Comp D64
61120	MGZD020	63.00	63.70	0.70	D01669	0.75	4.00	2.800	3.000				Comp D69
61120	MGZD020	63.70	64.40	0.70	D01670	0.80	0.07	0.049	0.056	1.40	2.849	2.035	Comp D61
60960	MGZD022	150.00	151.00	1.00	D01863	1.38	0.37	0.370	0.511				Comp D62
60960	MGZD022	151.00	151.70	0.70	D01864	0.74	1.08	0.756	0.799				Comp D65
60960	MGZD022	151.70	152.40	0.70	D01865	0.90	1.24	0.868	1.116				Comp D65
60960	MGZD022	152.40	153.10	0.70	D01866	0.84	1.02	0.714	0.857				Comp D65
60960	MGZD022	153.80	154.50	0.70	D01868	0.89	0.96	0.672	0.854				Comp D64
60960	MGZD022	154.50	155.20	0.70	D01869	0.91	1.44	1.008	1.310				Comp D66
60960	MGZD022	155.20	155.90	0.70	D01870	0.93	0.96	0.672	0.893				Comp D64
60960	MGZD022	155.90	156.60	0.70	D01872	0.90	1.08	0.756	0.972				Comp D65
60960	MGZD022	156.60	157.30	0.70	D01874	0.89	2.49	1.743	2.216				Comp D67
60960	MGZD022	157.30	158.00	0.70	D01875	0.89	0.85	0.595	0.757	8.00	8.777	1.097	Comp D64
61120	MGZD023	22.00	23.00	1.00	D02111	0.90	2.08	2.080	1.872				Comp D67
61120	MGZD023	23.00	24.00	1.00	D02112	1.20	1.09	1.090	1.308				Comp D65
61120	MGZD023	24.00	25.00	1.00	D02114	0.90	1.07	1.070	0.963				Comp D65
61120	MGZD023	25.00	26.00	1.00	D02115	0.90	0.31	0.310	0.279				Comp D62
61120	MGZD023	26.00	26.70	0.70	D02116	0.60	3.22	2.254	1.932				Comp D68
61120	MGZD023	26.70	27.40	0.70	D02117	0.70	1.38	0.966	0.966	5.40	7.770	1.439	Comp D66
61120	MGZD023	32.00	32.70	0.70	D02124	0.70	0.40	0.280	0.280				Comp D62
61120	MGZD023	32.70	33.40	0.70	D02125	0.70	0.97	0.679	0.679				Comp D64
61120	MGZD023	33.40	34.20	0.80	D02126	0.80	2.85	2.280	2.280	2.20	3.239	1.472	Comp D68
61080	MGZD025	41.40	42.40	1.00	D02266	1.10	0.83	0.830	0.913				Comp D64
61080	MGZD025	42.40	43.10	0.70	D02267	0.70	3.15	2.205	2.205				Comp D68
61080	MGZD025	43.10	44.00	0.90	D02268	0.90	0.18	0.162	0.162				Comp D61
61080	MGZD025	44.00	44.70	0.70	D02269	0.70	1.02	0.714	0.714				Comp D65
61080	MGZD025	44.70	45.50	0.80	D02270	0.80	1.86	1.488	1.488				Comp D67
61080	MGZD025	45.50	46.30	0.80	D02272	0.70	0.61	0.488	0.427				Comp D63
61080	MGZD025	46.30	47.00	0.70	D02273	0.70	0.51	0.357	0.357				Comp D63
61080	MGZD025	47.00	47.70	0.70	D02274	0.60	0.55	0.385	0.330	6.30	6.629	1.052	Comp D63
61080	MGZD025	49.80	50.50	0.70	D02279	0.70	1.99	1.393	1.393				Comp D67

D ZONE   LOW GRADE COMPOSITE   (SECTIONS 60880 through 61200)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
61080	MGZD025	50.50	51.20	0.70	D02280	0.70	2.48	1.736	1.736				Comp D67
61080	MGZD025	51.20	51.90	0.70	D02281	0.70	1.56	1.092	1.092				Comp D66
61080	MGZD025	51.90	52.60	0.70	D02282	0.80	5.61	3.927	4.488	2.80	8.148	2.910	Comp D70
61040	MGZD026	86.00	87.00	1.00	D02389	1.20	0.60	0.600	0.720				Comp D63
61040	MGZD026	87.00	87.70	0.70	D02390	0.80	0.24	0.168	0.192				Comp D61
61040	MGZD026	87.70	88.40	0.70	D02391	0.70	1.11	0.777	0.777				Comp D65
61040	MGZD026	88.40	89.10	0.70	D02392	0.80	0.22	0.154	0.176				Comp D61
61040	MGZD026	89.10	89.80	0.70	D02393	0.80	1.59	1.113	1.272				Comp D66
61040	MGZD026	89.80	90.50	0.70	D02394	0.80	1.10	0.770	0.880				Comp D65
61040	MGZD026	90.50	91.20	0.70	D02395	0.80	2.52	1.764	2.016				Comp D68
61040	MGZD026	91.20	92.20	1.00	D02397	1.20	5.51	5.510	6.612	6.20	10.856	1.751	Comp D70
61040	MGZD026	104.00	105.00	1.00	D02412	1.10	4.36	4.360	4.796				Comp D69
61040	MGZD026	105.00	106.00	1.00	D02414	1.20	0.50	0.500	0.600	2.00	4.860	2.430	Comp D62
61040	MGZD027	109.20	109.90	0.70	D02441	0.76	1.55	1.085	1.178				Comp D66
61040	MGZD027	109.90	110.60	0.70	D02442	0.83	0.03	0.021	0.025				Comp D61
61040	MGZD027	110.60	111.30	0.70	D02444	0.86	0.12	0.084	0.103				Comp D61
61040	MGZD027	111.30	112.00	0.70	D02445	0.79	0.46	0.322	0.363				Comp D62
61040	MGZD027	112.00	112.70	0.70	D02447	0.74	1.74	1.218	1.288				Comp D66
61040	MGZD027	112.70	113.40	0.70	D02448	0.79	1.14	0.798	0.901				Comp D65
61040	MGZD027	113.40	114.10	0.70	D02449	0.84	2.49	1.743	2.092				Comp D67
61040	MGZD027	114.10	114.80	0.70	D02450	0.79	3.31	2.317	2.615				Comp D68
61040	MGZD027	114.80	115.50	0.70	D02451	0.74	2.49	1.743	1.843				Comp D67
61040	MGZD027	115.50	116.20	0.70	D02452	0.69	1.78	1.246	1.228				Comp D67
61040	MGZD027	116.20	116.90	0.70	D02453	0.79	2.36	1.652	1.864				Comp D67
61040	MGZD027	116.90	117.60	0.70	D02454	0.85	2.99	2.093	2.542				Comp D68
61040	MGZD027	117.60	118.30	0.70	D02455	0.79	1.43	1.001	1.130				Comp D66
61040	MGZD027	118.30	119.00	0.70	D02456	0.82	2.38	1.666	1.952				Comp D67
61040	MGZD027	119.00	119.70	0.70	D02457	0.82	1.43	1.001	1.173				Comp D66
61040	MGZD027	119.70	120.40	0.70	D02459	0.78	0.72	0.504	0.562				Comp D63
61040	MGZD027	120.40	121.10	0.70	D02460	0.73	0.54	0.378	0.394				Comp D63
61040	MGZD027	121.10	121.80	0.70	D02461	0.81	2.17	1.519	1.758				Comp D67
61040	MGZD027	121.80	122.50	0.70	D02462	1.00	2.88	2.016	2.880				Comp D68
61040	MGZD027	122.50	123.20	0.70	D02463	0.81	4.20	2.940	3.402				Comp D69
61040	MGZD027	123.20	123.90	0.70	D02464	0.88	1.48	1.036	1.302				Comp D66
61040	MGZD027	123.90	124.60	0.70	D02465	0.77	0.82	0.574	0.631				Comp D64
61040	MGZD027	124.60	125.30	0.70	D02466	0.89	1.23	0.861	1.095				Comp D65
61040	MGZD027	125.30	126.00	0.70	D02467	0.83	2.48	1.736	2.058				Comp D67
61040	MGZD027	126.00	126.70	0.70	D02468	0.84	0.83	0.581	0.697	17.50	30.135	1.722	Comp D64
61040	MGZD027	137.70	138.40	0.70	D02483	0.90	3.23	2.261	2.907				Comp D68
61040	MGZD027	138.40	139.10	0.70	D02484	1.00	0.99	0.693	0.990	1.40	2.954	2.110	Comp D64
60960	MGZD028	180.70	181.40	0.70	D02508	0.84	3.14	2.198	2.638				Comp D68
60960	MGZD028	181.40	182.10	0.70	D02509	0.81	1.49	1.043	1.207				Comp D66
60960	MGZD028	182.10	182.80	0.70	D02510	0.94	0.71	0.497	0.667				Comp D63
60960	MGZD028	182.80	183.50	0.70	D02511	0.76	1.08	0.756	0.821				Comp D65
60960	MGZD028	183.50	184.20	0.70	D02512	0.94	4.67	3.269	4.390				Comp D69
60960	MGZD028	184.20	184.90	0.70	D02513	0.83	2.23	1.561	1.851				Comp D67
60960	MGZD028	184.90	185.60	0.70	D02514	1.07	2.24	1.568	2.397				Comp D67
60960	MGZD028	185.60	186.30	0.70	D02515	1.08	0.79	0.553	0.853				Comp D64
60960	MGZD028	186.30	187.00	0.70	D02516	0.85	1.44	1.008	1.224				Comp D66
60960	MGZD028	187.00	187.70	0.70	D02517	0.91	1.30	0.910	1.183				Comp D65
60960	MGZD028	187.70	188.40	0.70	D02519	0.98	8.19	5.733	8.026				Comp D71
60960	MGZD028	188.40	189.10	0.70	D02520	0.83	1.88	1.316	1.560	8.40	20.412	2.430	Comp D67
60960	MGZD029	105.00	106.00	1.00	D02544	1.02	0.13	0.130	0.133				Comp D61
60960	MGZD029	106.00	107.00	1.00	D02545	1.16	0.08	0.080	0.093				Comp D61
60960	MGZD029	107.00	108.00	1.00	D02547	1.02	0.11	0.110	0.112				Comp D61
60960	MGZD029	108.00	108.70	0.70	D02549	0.82	2.15	1.505	1.763				Comp D67
60960	MGZD029	108.70	109.40	0.70	D02550	0.80	2.12	1.484	1.696				Comp D67
60960	MGZD029	109.40	110.10	0.70	D02551	0.79	0.32	0.224	0.253				Comp D62
60960	MGZD029	110.10	111.00	0.90	D02552	1.06	1.00	0.900	1.060				Comp D64
60960	MGZD029	111.00	112.00	1.00	D02553	1.23	0.11	0.110	0.135				Comp D61
60960	MGZD029	112.00	113.00	1.00	D02554	1.36	0.85	0.850	1.156				Comp D64
60960	MGZD029	113.00	114.00	1.00	D02555	1.27	0.71	0.710	0.902				Comp D63
60960	MGZD029	114.00	115.00	1.00	D02556	1.24	1.07	1.070	1.327	12.00	8.823	0.735	Comp D65
61080	MGZD032	49.70	50.40	0.70	D02753	0.70	0.62	0.434	0.434				Comp D63

D ZONE LOW GRADE COMPOSITE (SECTIONS 60880 through 61200)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
61080	MGZD032	50.40	51.10	0.70	D02754	1.80	0.10	0.070	0.180				Comp D61
61080	MGZD032	51.10	52.00	0.90	D02755	1.00	0.42	0.378	0.420				Comp D62
61080	MGZD032	52.00	53.00	1.00	D02756	1.20	1.59	1.590	1.908				Comp D66
61080	MGZD032	53.00	53.70	0.70	D02757	0.80	0.19	0.133	0.152				Comp D61
61080	MGZD032	53.70	54.40	0.70	D02759	0.80	0.80	0.560	0.640				Comp D64
61080	MGZD032	54.40	55.10	0.70	D02760	0.70	0.44	0.308	0.308				Comp D62
61080	MGZD032	55.10	56.00	0.90	D02761	1.00	0.55	0.495	0.550				Comp D63
61080	MGZD032	56.00	57.00	1.00	D02762	1.10	0.42	0.420	0.462				Comp D62
61080	MGZD032	57.00	58.00	1.00	D02763	1.30	0.06	0.060	0.078				Comp D61
61080	MGZD032	58.00	59.00	1.00	D02764	1.40	0.02	0.020	0.028				Comp D61
61080	MGZD032	59.00	60.00	1.00	D02765	1.20	1.18	1.180	1.416				Comp D65
61080	MGZD032	60.00	61.00	1.00	D02766	1.10	1.38	1.380	1.518	11.30	7.028	0.622	Comp D66
61080	MGZD032	73.00	74.00	1.00	D02782	1.07	2.52	2.520	2.696				Comp D68
61080	MGZD032	74.00	74.70	0.70	D02783	0.82	0.36	0.252	0.295				Comp D62
61080	MGZD032	74.70	75.40	0.70	D02784	0.70	0.36	0.252	0.252				Comp D62
61080	MGZD032	75.40	76.10	0.70	D02785	0.81	4.65	3.255	3.767	3.10	6.279	2.025	Comp D69
61080	MGZD032	80.30	81.00	0.70	D02793	0.82	1.29	0.903	1.058				Comp D65
61080	MGZD032	81.00	81.70	0.70	D02794	0.81	3.67	2.569	2.973				Comp D69
61080	MGZD032	81.70	82.40	0.70	D02795	0.74	2.07	1.449	1.532	2.10	4.921	2.343	Comp D67
61120	MGZD033	33.70	34.40	0.70	D02819	1.18	3.77	2.639	4.449				Comp D69
61120	MGZD033	34.40	35.10	0.70	D02820	1.15	0.02	0.014	0.023	1.40	2.653	1.895	Comp D61
61120	MGZD033	42.00	42.70	0.70	D02829	0.76	0.39	0.273	0.296				Comp D62
61120	MGZD033	42.70	43.40	0.70	D02830	0.78	1.08	0.756	0.842				Comp D65
61120	MGZD033	43.40	44.10	0.70	D02831	0.69	1.95	1.365	1.346				Comp D67
61120	MGZD033	44.10	44.80	0.70	D02832	0.74	2.97	2.079	2.198	2.80	4.473	1.598	Comp D68
61160	MGZD034	57.70	58.40	0.70	D02910	0.88	14.80	10.360	13.024				Comp D71
61160	MGZD034	58.40	59.10	0.70	D02911	0.80	0.03	0.021	0.024				Comp D61
61160	MGZD034	59.10	60.00	0.90	D02912	1.05	0.08	0.072	0.084				Comp D61
61160	MGZD034	60.00	61.00	1.00	D02913	1.19	0.12	0.120	0.143				Comp D61
61160	MGZD034	61.00	62.00	1.00	D02914	1.23	1.19	1.190	1.464				Comp D65
61160	MGZD034	62.00	63.00	1.00	D02915	1.33	0.04	0.040	0.053				Comp D61
61160	MGZD034	63.00	64.00	1.00	D02916	1.21	1.21	1.210	1.464	6.30	13.013	2.066	Comp D65
61080	MGZD025	26.00	27.00	1.00	D04082	1.10	0.65	0.650	0.715				Comp D63
61080	MGZD025	27.00	28.00	1.00	D04083	1.10	0.41	0.410	0.451				Comp D62
61080	MGZD025	28.00	29.00	1.00	D04084	1.10	1.51	1.510	1.661	3.00	2.570	0.857	Comp D66
60960	MGZD048	112.00	113.00	1.00	D04666	1.02	1.75	1.750	1.785				Comp D66
60960	MGZD048	113.00	114.00	1.00	D04667	1.09	0.25	0.250	0.273				Comp D61
60960	MGZD048	114.00	114.70	0.70	D04668	0.70	1.99	1.393	1.393				Comp D67
60960	MGZD048	114.70	115.40	0.70	D04669	0.72	5.35	3.745	3.852				Comp D70
60960	MGZD048	115.40	116.10	0.70	D04670	0.74	1.37	0.959	1.014				Comp D66
60960	MGZD048	116.10	117.00	0.90	D04672	0.90	1.95	1.755	1.755				Comp D67
60960	MGZD048	117.00	117.70	0.70	D04673	0.75	1.23	0.861	0.923	5.70	10.713	1.879	Comp D65
60960	MGZD048	137.00	137.70	0.70	D04702	0.71	1.30	0.910	0.923				Comp D65
60960	MGZD048	137.70	138.40	0.70	D04703	0.72	1.19	0.833	0.857				Comp D65
60960	MGZD048	138.40	139.10	0.70	D04704	0.69	1.33	0.931	0.918				Comp D66
60960	MGZD048	139.10	139.80	0.70	D04705	0.71	1.46	1.022	1.037				Comp D66
60960	MGZD048	139.80	140.50	0.70	D04706	0.72	1.66	1.162	1.195				Comp D66
60960	MGZD048	140.50	141.20	0.70	D04707	0.72	1.66	1.162	1.195				Comp D66
60960	MGZD048	141.20	142.00	0.80	D04709	0.83	0.69	0.552	0.573				Comp D63
60960	MGZD048	142.00	143.00	1.00	D04710	1.04	0.40	0.400	0.416				Comp D62
60960	MGZD048	143.00	144.00	1.00	D04711	1.16	0.04	0.040	0.046				Comp D61
60960	MGZD048	144.00	145.00	1.00	D04712	1.15	0.08	0.080	0.092				Comp D61
60960	MGZD048	145.00	146.00	1.00	D04713	1.03	0.17	0.170	0.175				Comp D61
60960	MGZD048	146.00	146.70	0.70	D04714	0.76	1.31	0.917	0.996				Comp D66
60960	MGZD048	146.70	147.40	0.70	D04715	0.72	1.42	0.994	1.022	10.40	9.173	0.882	Comp D66
60960	MGZD048	152.00	153.00	1.00	D04722	1.16	1.63	1.630	1.891				Comp D66
60960	MGZD048	153.00	153.70	0.70	D04724	0.71	2.64	1.848	1.874				Comp D68
60960	MGZD048	153.70	154.40	0.70	D04725	0.63	1.85	1.295	1.166				Comp D67
60960	MGZD048	154.40	155.10	0.70	D04726	0.65	1.64	1.148	1.066				Comp D66
60960	MGZD048	155.10	155.80	0.70	D04727	0.67	2.76	1.932	1.849				Comp D68
60960	MGZD048	155.80	156.50	0.70	D04728	0.66	6.75	4.725	4.455				Comp D70
60960	MGZD048	156.50	157.20	0.70	D04729	0.81	2.42	1.694	1.960				Comp D67
60960	MGZD048	157.20	158.00	0.80	D04730	0.90	0.53	0.424	0.477				Comp D63
60960	MGZD048	158.00	158.70	0.70	D04731	0.83	3.91	2.737	3.245				Comp D69

D ZONE LOW GRADE COMPOSITE (SECTIONS 60880 through 61200)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60960	MGZD048	158.70	159.40	0.70	D04732	0.79	0.66	0.462	0.521				Comp D63
60960	MGZD048	159.40	160.10	0.70	D04733	0.96	0.78	0.546	0.749				Comp D64
60960	MGZD048	160.10	161.00	0.90	D04734	0.93	0.44	0.396	0.409				Comp D62
60960	MGZD048	161.00	162.00	1.00	D04735	1.14	0.34	0.340	0.388				Comp D62
60960	MGZD048	162.00	163.00	1.00	D04736	1.10	0.25	0.250	0.275				Comp D61
60960	MGZD048	163.00	164.00	1.00	D04737	1.30	0.65	0.650	0.845				Comp D63
60960	MGZD048	164.00	165.00	1.00	D04739	1.16	0.40	0.400	0.464				Comp D62
60960	MGZD048	165.00	166.00	1.00	D04740	1.23	0.63	0.630	0.775				Comp D63
60960	MGZD048	166.00	167.00	1.00	D04741	1.18	1.03	1.030	1.215				Comp D65
60960	MGZD048	167.00	168.00	1.00	D04742	1.07	0.74	0.740	0.792				Comp D63
60960	MGZD048	168.00	169.00	1.00	D04743	1.18	0.33	0.330	0.389	17.00	23.207	1.365	Comp D62
61120	MGZD051	19.00	19.70	0.70	D05814	0.84	0.63	0.441	0.529				Comp D63
61120	MGZD051	19.70	20.40	0.70	D05815	0.76	2.26	1.582	1.718	1.40	2.023	1.445	Comp D67
61120	MGZD051	23.00	23.70	0.70	D05820	0.81	2.85	1.995	2.309				Comp D68
61120	MGZD051	23.70	24.40	0.70	D05822	0.75	0.92	0.644	0.690	1.40	2.639	1.885	Comp D64
61120	MGZD051	76.00	77.00	1.00	D05883	1.24	0.54	0.540	0.670				Comp D63
61120	MGZD051	77.00	77.70	0.70	D05884	0.82	1.40	0.980	1.148				Comp D66
61120	MGZD051	77.70	78.40	0.70	D05885	0.85	0.98	0.686	0.833				Comp D64
61120	MGZD051	78.40	79.10	0.70	D05886	0.63	0.40	0.280	0.252				Comp D62
61120	MGZD051	79.10	79.80	0.70	D05887	0.72	0.39	0.273	0.281				Comp D62
61120	MGZD051	79.80	80.50	0.70	D05888	0.90	0.71	0.497	0.639	4.50	3.256	0.724	Comp D63
61160	MGZD056	8.00	8.70	0.70	D05905	0.84	1.10	0.770	0.924				Comp D65
61160	MGZD056	8.70	9.40	0.70	D05906	0.64	1.54	1.078	0.986				Comp D66
61160	MGZD056	9.40	10.10	0.70	D05907	0.77	0.40	0.280	0.308				Comp D62
61160	MGZD056	10.10	10.80	0.70	D05909	0.70	0.38	0.266	0.266				Comp D62
61160	MGZD056	10.80	11.50	0.70	D05910	0.72	1.16	0.812	0.835				Comp D65
61160	MGZD056	11.50	12.20	0.70	D05911	0.76	1.00	0.700	0.760				Comp D64
61160	MGZD056	12.20	13.00	0.80	D05912	0.77	0.65	0.520	0.501	5.00	4.426	0.885	Comp D63
61160	MGZD056	42.00	43.00	1.00	D05948	1.11	1.16	1.160	1.288				Comp D65
61160	MGZD056	43.00	43.70	0.70	D05949	0.76	4.64	3.248	3.526				Comp D69
61160	MGZD056	43.70	44.40	0.70	D05950	0.68	4.75	3.325	3.230				Comp D69
61160	MGZD056	44.40	45.10	0.70	D05951	0.86	9.09	6.363	7.817				Comp D71
61160	MGZD056	45.10	45.80	0.70	D05952	0.80	0.32	0.224	0.256				Comp D62
61160	MGZD056	45.80	46.50	0.70	D05954	0.78	0.05	0.035	0.039				Comp D61
61160	MGZD056	46.50	47.20	0.70	D05955	0.81	0.04	0.028	0.032				Comp D61
61160	MGZD056	47.20	48.00	0.80	D05956	0.90	0.05	0.040	0.045				Comp D61
61160	MGZD056	48.00	48.70	0.70	D05957	0.99	2.72	1.904	2.693				Comp D68
61160	MGZD056	48.70	49.40	0.70	D05958	0.82	4.14	2.898	3.395				Comp D69
61160	MGZD056	49.40	50.10	0.70	D05959	0.83	4.05	2.835	3.362				Comp D69
61160	MGZD056	50.10	51.00	0.90	D05960	0.95	0.68	0.612	0.646				Comp D63
61160	MGZD056	51.00	51.70	0.70	D05961	0.80	2.31	1.617	1.848				Comp D67
61160	MGZD056	51.70	52.40	0.70	D05962	0.69	0.60	0.420	0.414				Comp D63
61160	MGZD056	52.40	53.10	0.70	D05963	0.82	1.04	0.728	0.853	11.10	25.437	2.292	Comp D65
61160	MGZD056	69.00	70.00	1.00	D05984	1.21	0.80	0.800	0.968				Comp D64
61160	MGZD056	70.00	71.00	1.00	D05985	1.31	0.04	0.040	0.052				Comp D61
61160	MGZD056	71.00	72.00	1.00	D05986	1.01	0.36	0.360	0.364				Comp D62
61160	MGZD056	72.00	73.00	1.00	D05987	1.29	0.22	0.220	0.284				Comp D61
61160	MGZD056	73.00	74.00	1.00	D05988	1.09	0.75	0.750	0.818				Comp D63
61160	MGZD056	74.00	75.00	1.00	D05989	1.18	0.63	0.630	0.743				Comp D63
61160	MGZD056	75.00	75.90	0.90	D05990	0.96	0.44	0.396	0.422	6.90	3.196	0.463	Comp D62
61080	MGZD053	31.00	31.70	0.70	D06009	0.64	1.58	1.106	1.011				Comp D66
61080	MGZD053	31.70	32.40	0.70	D06010	0.67	1.09	0.763	0.730				Comp D65
61080	MGZD053	32.40	33.10	0.70	D06011	0.83	0.09	0.063	0.075				Comp D61
61080	MGZD053	33.10	34.00	0.90	D06012	1.00	1.19	1.071	1.190	3.00	3.003	1.001	Comp D65
61080	MGZD053	58.00	58.70	0.70	D06041	0.75	5.74	4.018	4.305				Comp D70
61080	MGZD053	58.70	59.40	0.70	D06043	0.74	0.24	0.168	0.178	1.40	4.186	2.990	Comp D61
61120	MGZD055	24.00	25.00	1.00	D06115	1.27	0.24	0.240	0.305				Comp D61
61120	MGZD055	25.00	25.70	0.70	D06116	0.83	2.79	1.953	2.316				Comp D68
61120	MGZD055	25.70	26.40	0.70	D06117	0.90	1.17	0.819	1.053	2.40	3.012	1.255	Comp D65
61120	MGZD055	32.00	32.70	0.70	D06126	0.84	1.58	1.106	1.327				Comp D66
61120	MGZD055	32.70	33.40	0.70	D06127	0.82	2.97	2.079	2.435				Comp D68
61120	MGZD055	33.40	34.10	0.70	D06128	0.82	1.74	1.218	1.427	2.10	4.403	2.097	Comp D66
61120	MGZD055	36.00	36.70	0.70	D06131	0.78	0.32	0.224	0.250				Comp D62
61120	MGZD055	36.70	37.40	0.70	D06132	0.77	0.97	0.679	0.747				Comp D64

D ZONE LOW GRADE COMPOSITE (SECTIONS 60880 through 61200)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
61120	MGZD055	37.40	38.10	0.70	D06134	0.83	0.82	0.574	0.681	2.10	1.477	0.703	Comp D64
61120	MGZD055	46.00	47.00	1.00	D06144	1.10	0.36	0.360	0.396				Comp D62
61120	MGZD055	47.00	47.70	0.70	D06145	0.82	3.73	2.611	3.059				Comp D69
61120	MGZD055	47.70	48.40	0.70	D06147	0.75	0.99	0.693	0.743	2.40	3.664	1.527	Comp D64
61120	MGZD055	52.00	52.70	0.70	D06153	0.86	3.51	2.457	3.019				Comp D69
61120	MGZD055	52.70	53.40	0.70	D06154	0.73	2.95	2.065	2.154				Comp D68
61120	MGZD055	53.40	54.10	0.70	D06155	0.73	0.64	0.448	0.467				Comp D63
61120	MGZD055	54.10	55.00	0.90	D06156	0.94	0.25	0.225	0.235				Comp D61
61120	MGZD055	55.00	56.00	1.00	D06157	1.20	0.05	0.050	0.060				Comp D61
61120	MGZD055	56.00	56.70	0.70	D06158	0.79	12.50	8.750	9.875	4.70	13.995	2.978	Comp D71
61120	MGZD055	58.10	58.80	0.70	D06161	0.83	0.32	0.224	0.266				Comp D62
61120	MGZD055	58.80	59.50	0.70	D06162	0.85	3.13	2.191	2.661	1.40	2.415	1.725	Comp D68
61120	MGZD055	66.00	66.70	0.70	D06173	0.88	0.65	0.455	0.572				Comp D63
61120	MGZD055	66.70	67.40	0.70	D06174	0.80	4.64	3.248	3.712				Comp D69
61120	MGZD055	67.40	68.10	0.70	D06175	0.95	0.11	0.077	0.105				Comp D61
61120	MGZD055	68.10	69.00	0.90	D06176	1.15	1.86	1.674	2.139				Comp D67
61120	MGZD055	69.00	70.00	1.00	D06177	1.32	0.33	0.330	0.436	4.00	5.784	1.446	Comp D62
61160	MGZD058	1.00	2.00	1.00	D06181	1.00	1.62	1.620	1.620				Comp D66
61160	MGZD058	2.00	3.00	1.00	D06182	1.50	2.46	2.460	3.690	2.00	4.080	2.040	Comp D67
61160	MGZD058	12.70	13.40	0.70	D06195	0.70	1.75	1.225	1.225				Comp D66
61160	MGZD058	13.40	14.10	0.70	D06197	0.70	0.96	0.672	0.672				Comp D64
61160	MGZD058	14.10	14.80	0.70	D06198	0.70	0.24	0.168	0.168				Comp D61
61160	MGZD058	14.80	15.50	0.70	D06199	0.80	0.66	0.462	0.528				Comp D63
61160	MGZD058	15.50	16.20	0.70	D06200	0.80	0.11	0.077	0.088				Comp D61
61160	MGZD058	16.20	17.00	0.80	D06201	0.80	0.50	0.400	0.400	4.30	3.004	0.699	Comp D62
61160	MGZD058	33.00	33.70	0.70	D06219	0.83	1.21	0.847	1.004				Comp D65
61160	MGZD058	33.70	34.40	0.70	D06220	0.77	0.62	0.434	0.477				Comp D63
61160	MGZD058	34.40	35.10	0.70	D06222	0.77	0.67	0.469	0.516				Comp D63
61160	MGZD058	35.10	36.00	0.90	D06224	0.96	0.26	0.234	0.250				Comp D62
61160	MGZD058	36.00	37.00	1.00	D06225	1.01	0.06	0.060	0.061				Comp D61
61160	MGZD058	37.00	38.00	1.00	D06226	1.13	1.00	1.000	1.130				Comp D64
61160	MGZD058	38.00	39.00	1.00	D06227	1.17	0.12	0.120	0.140				Comp D61
61160	MGZD058	39.00	39.70	0.70	D06228	0.76	0.10	0.070	0.076				Comp D61
61160	MGZD058	39.70	40.40	0.70	D06229	0.89	1.75	1.225	1.558	7.40	4.459	0.603	Comp D66
61160	MGZD058	45.40	46.10	0.70	D06236	0.80	4.67	3.269	3.736				Comp D69
61160	MGZD058	46.10	46.80	0.70	D06237	0.80	0.98	0.686	0.784				Comp D64
61160	MGZD058	46.80	47.50	0.70	D06239	0.70	1.34	0.938	0.938				Comp D66
61160	MGZD058	47.50	48.20	0.70	D06240	0.80	0.46	0.322	0.368				Comp D62
61160	MGZD058	48.20	49.00	0.80	D06241	0.90	1.75	1.400	1.575				Comp D66
61160	MGZD058	49.00	50.00	1.00	D06242	1.10	0.58	0.580	0.638	4.60	7.195	1.564	Comp D63
61120	MGZD054	33.70	34.40	0.70	D06320	0.86	2.04	1.428	1.754				Comp D67
61120	MGZD054	34.40	35.10	0.70	D06322	0.85	1.70	1.190	1.445	1.40	2.618	1.870	Comp D66
61120	MGZD054	55.00	55.70	0.70	D06349	0.79	0.95	0.665	0.751				Comp D64
61120	MGZD054	55.70	56.40	0.70	D06350	0.78	8.43	5.901	6.575				Comp D71
61120	MGZD054	56.40	57.10	0.70	D06351	1.02	0.74	0.518	0.755				Comp D63
61120	MGZD054	57.10	58.00	0.90	D06352	0.91	0.65	0.585	0.592	3.00	7.669	2.556	Comp D63
60960	MGZD063	119.00	120.00	1.00	D06386	1.19	5.31	5.310	6.319				Comp D70
60960	MGZD063	120.00	121.00	1.00	D06387	1.07	1.09	1.090	1.166				Comp D65
60960	MGZD063	121.00	121.70	0.70	D06389	0.73	2.29	1.603	1.672				Comp D67
60960	MGZD063	121.70	122.40	0.70	D06390	0.69	2.34	1.638	1.615				Comp D67
60960	MGZD063	122.40	123.10	0.70	D06391	0.78	0.38	0.266	0.296				Comp D62
60960	MGZD063	123.10	123.80	0.70	D06392	0.72	0.45	0.315	0.324				Comp D62
60960	MGZD063	123.80	124.50	0.70	D06393	0.74	0.51	0.357	0.377				Comp D63
60960	MGZD063	124.50	125.20	0.70	D06394	0.68	0.84	0.588	0.571				Comp D64
60960	MGZD063	125.20	126.00	0.80	D06395	0.76	0.44	0.352	0.334				Comp D62
60960	MGZD063	126.00	127.00	1.00	D06397	0.96	0.11	0.110	0.106				Comp D61
60960	MGZD063	127.00	128.00	1.00	D06398	1.03	0.33	0.330	0.340				Comp D62
60960	MGZD063	128.00	129.00	1.00	D06399	0.98	4.89	4.890	4.792				Comp D69
60960	MGZD063	129.00	129.70	0.70	D06400	0.80	0.87	0.609	0.696	10.70	17.458	1.632	Comp D64
60960	MGZD063	137.10	137.80	0.70	D06411	0.73	1.60	1.120	1.168				Comp D66
60960	MGZD063	137.80	138.50	0.70	D06412	0.81	0.92	0.644	0.745				Comp D64
60960	MGZD063	138.50	139.20	0.70	D06413	0.75	0.40	0.280	0.300				Comp D62
60960	MGZD063	139.20	140.00	0.80	D06414	0.83	0.78	0.624	0.647				Comp D64
60960	MGZD063	140.00	141.00	1.00	D06415	1.05	0.23	0.230	0.242				Comp D61

D ZONE   LOW GRADE COMPOSITE   (SECTIONS 60880 through 61200)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60960	MGZD063	141.00	142.00	1.00	D06416	1.12	2.10	2.100	2.352				Comp D67
60960	MGZD063	142.00	143.00	1.00	D06417	1.08	1.32	1.320	1.426				Comp D66
60960	MGZD063	143.00	144.00	1.00	D06419	1.08	2.87	2.870	3.100				Comp D68
60960	MGZD063	144.00	144.70	0.70	D06420	0.75	4.02	2.814	3.015				Comp D69
60960	MGZD063	144.70	145.40	0.70	D06422	0.75	2.21	1.547	1.658				Comp D67
60960	MGZD063	145.40	146.10	0.70	D06423	1.00	0.09	0.063	0.090				Comp D61
60960	MGZD063	146.10	146.80	0.70	D06424	0.73	0.85	0.595	0.621				Comp D64
60960	MGZD063	146.80	147.50	0.70	D06425	0.76	1.32	0.924	1.003				Comp D66
60960	MGZD063	147.50	148.20	0.70	D06426	0.78	1.18	0.826	0.920				Comp D65
60960	MGZD063	148.20	149.20	1.00	D06427	1.06	2.72	2.720	2.883	12.10	18.677	1.544	Comp D68
60960	MGZD062	100.00	101.00	1.00	D06497	1.00	0.36	0.360	0.360				Comp D62
60960	MGZD062	101.00	102.00	1.00	D06498	1.00	0.34	0.340	0.340				Comp D62
60960	MGZD062	102.00	103.00	1.00	D06499	1.20	2.85	2.850	3.420				Comp D68
60960	MGZD062	103.00	104.00	1.00	D06500	1.10	0.09	0.090	0.099				Comp D61
60960	MGZD062	104.00	105.00	1.00	D06501	1.20	0.05	0.050	0.060				Comp D61
60960	MGZD062	105.00	106.00	1.00	D06502	1.10	0.57	0.570	0.627				Comp D63
60960	MGZD062	107.00	108.00	1.00	D06504	1.10	4.55	4.550	5.005				Comp D69
60960	MGZD062	108.00	109.00	1.00	D06505	1.10	0.41	0.410	0.451				Comp D62
60960	MGZD062	109.00	110.00	1.00	D06506	1.10	0.08	0.080	0.088				Comp D61
60960	MGZD062	110.00	111.00	1.00	D06507	1.10	0.20	0.200	0.220				Comp D61
60960	MGZD062	111.00	112.00	1.00	D06509	1.10	1.20	1.200	1.320				Comp D65
60960	MGZD062	112.00	113.00	1.00	D06510	1.00	1.70	1.700	1.700				Comp D66
60960	MGZD062	113.00	114.00	1.00	D06511	1.10	0.52	0.520	0.572	14.00	13.160	0.940	Comp D63
61040	MGZD061	57.00	58.00	1.00	D06681	1.10	2.48	2.480	2.728				Comp D67
61040	MGZD061	58.00	59.00	1.00	D06682	1.10	2.99	2.990	3.289	2.00	5.470	2.735	Comp D68
61040	MGZD059	31.00	32.00	1.00	D07091	1.19	0.75	0.750	0.893				Comp D63
61040	MGZD059	32.00	33.00	1.00	D07092	1.23	1.32	1.320	1.624				Comp D66
61040	MGZD059	33.00	34.00	1.00	D07094	1.21	0.43	0.430	0.520				Comp D62
61040	MGZD059	34.00	35.00	1.00	D07095	1.28	0.46	0.460	0.589	4.00	2.960	0.740	Comp D62
61120	MGZD055	104.00	105.00	1.00	D07223	1.13	1.60	1.600	1.808				Comp D66
61120	MGZD055	105.00	106.00	1.00	D07224	1.14	0.24	0.240	0.274				Comp D61
61120	MGZD055	106.00	107.00	1.00	D07225	1.04	2.44	2.440	2.538	3.00	4.280	1.427	Comp D67
61040	MGZD067	66.00	66.70	0.70	D07277	0.84	0.89	0.623	0.748				Comp D64
61040	MGZD067	66.70	67.40	0.70	D07278	0.71	3.86	2.702	2.741	1.40	3.325	2.375	Comp D69
61040	MGZD067	68.10	69.00	0.90	D07280	1.00	1.01	0.909	1.010				Comp D65
61040	MGZD067	69.00	69.70	0.70	D07281	0.81	0.84	0.588	0.680				Comp D64
61040	MGZD067	69.70	70.40	0.70	D07282	0.80	0.92	0.644	0.736				Comp D64
61040	MGZD067	70.40	71.10	0.70	D07283	0.79	0.73	0.511	0.577				Comp D63
61040	MGZD067	71.10	72.00	0.90	D07284	1.03	1.61	1.449	1.658				Comp D66
61040	MGZD067	72.00	73.00	1.00	D07285	1.08	0.57	0.570	0.616				Comp D63
61040	MGZD067	73.00	74.00	1.00	D07286	1.16	10.50	10.500	12.180				Comp D71
61040	MGZD067	74.00	75.00	1.00	D07287	1.07	1.38	1.380	1.477				Comp D66
61040	MGZD067	75.00	76.00	1.00	D07289	1.02	0.43	0.430	0.439				Comp D62
61040	MGZD067	76.00	77.00	1.00	D07290	1.24	2.28	2.280	2.827				Comp D67
61040	MGZD067	77.00	78.00	1.00	D07291	0.89	1.69	1.690	1.504				Comp D66
61040	MGZD067	78.00	79.00	1.00	D07292	1.15	0.41	0.410	0.472				Comp D62
61040	MGZD067	79.00	80.00	1.00	D07293	1.10	0.11	0.110	0.121				Comp D61
61040	MGZD067	80.00	80.70	0.70	D07294	0.83	1.61	1.127	1.336	12.60	22.598	1.793	Comp D66
61040	MGZD067	119.00	119.70	0.70	D07340	0.86	2.64	1.848	2.270				Comp D68
61040	MGZD067	119.70	120.70	1.00	D07341	1.03	3.10	3.100	3.193				Comp D68
61040	MGZD067	120.70	121.40	0.70	D07342	0.79	2.33	1.631	1.841				Comp D67
61040	MGZD067	121.40	122.10	0.70	D07343	0.81	1.83	1.281	1.482	3.10	7.860	2.535	Comp D67
61040	MGZD069	87.40	88.10	0.70	D07514	0.70	4.89	3.423	3.423				Comp D69
61040	MGZD069	88.10	89.00	0.90	D07515	1.05	0.51	0.459	0.536				Comp D63
61040	MGZD069	89.00	90.00	1.00	D07516	1.19	0.19	0.190	0.226				Comp D61
61040	MGZD069	90.00	91.00	1.00	D07517	1.25	3.21	3.210	4.013	3.60	7.282	2.023	Comp D68
60960	MGZD071	123.10	123.80	0.70	D07642	0.75	3.44	2.408	2.580				Comp D68
60960	MGZD071	123.80	124.50	0.70	D07643	0.71	2.46	1.722	1.747				Comp D67
60960	MGZD071	124.50	125.20	0.70	D07644	0.85	8.53	5.971	7.251				Comp D71
60960	MGZD071	125.20	125.90	0.70	D07645	0.81	0.17	0.119	0.138				Comp D61
60960	MGZD071	125.90	126.60	0.70	D07647	0.83	0.83	0.581	0.689				Comp D64
60960	MGZD071	126.60	127.30	0.70	D07649	0.84	0.08	0.056	0.067				Comp D61
60960	MGZD071	127.30	128.00	0.70	D07650	0.72	0.68	0.476	0.490				Comp D63
60960	MGZD071	128.00	128.70	0.70	D07651	0.82	0.88	0.616	0.722				Comp D64

D ZONE LOW GRADE COMPOSITE (SECTIONS 60880 through 61200)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60960	MGZD071	128.70	129.40	0.70	D07652	0.82	1.06	0.742	0.869				Comp D65
60960	MGZD071	129.40	130.10	0.70	D07653	0.88	9.15	6.405	8.052				Comp D71
60960	MGZD071	130.10	130.80	0.70	D07654	0.93	4.52	3.164	4.204				Comp D69
60960	MGZD071	130.80	131.50	0.70	D07655	0.79	1.05	0.735	0.830				Comp D65
60960	MGZD071	131.50	132.20	0.70	D07656	0.59	1.60	1.120	0.944				Comp D66
60960	MGZD071	132.20	132.90	0.70	D07657	1.04	1.75	1.225	1.820				Comp D66
60960	MGZD071	132.90	133.60	0.70	D07658	0.73	4.17	2.919	3.044	10.50	28.259	2.691	Comp D69
61040	MGZD104	50.80	51.50	0.70	D16897	0.78	0.35	0.245	0.273				Comp D62
61040	MGZD104	51.50	52.20	0.70	D16899	0.63	2.46	1.722	1.550				Comp D67
61040	MGZD104	52.20	52.90	0.70	D16900	0.65	1.38	0.966	0.897				Comp D66
61040	MGZD104	52.90	53.60	0.70	D16901	0.66	0.66	0.462	0.436	2.80	3.395	1.213	Comp D63
61040	MGZD104	63.40	64.10	0.70	D16916	0.58	8.27	5.789	4.797				Comp D71
61040	MGZD104	64.10	64.80	0.70	D16917	0.65	0.19	0.133	0.124				Comp D61
61040	MGZD104	64.80	65.50	0.70	D16919	0.71	4.17	2.919	2.961				Comp D69
61040	MGZD104	65.50	66.20	0.70	D16920	0.66	0.74	0.518	0.488				Comp D63
61040	MGZD104	66.20	66.90	0.70	D16922	0.63	0.92	0.644	0.580				Comp D64
61040	MGZD104	66.90	67.60	0.70	D16923	0.57	3.06	2.142	1.744	4.20	12.145	2.892	Comp D68
61040	MGZD104	90.00	90.70	0.70	D16959	0.84	1.50	1.050	1.260				Comp D66
61040	MGZD104	90.70	91.40	0.70	D16960	0.83	1.95	1.365	1.619				Comp D67
61040	MGZD104	91.40	92.10	0.70	D16961	0.83	0.14	0.098	0.116				Comp D61
61040	MGZD104	92.10	92.80	0.70	D16962	0.82	0.54	0.378	0.443				Comp D63
61040	MGZD104	92.80	93.50	0.70	D16963	0.83	0.09	0.063	0.075				Comp D61
61040	MGZD104	93.50	94.20	0.70	D16964	0.78	0.51	0.357	0.398				Comp D63
61040	MGZD104	94.20	94.90	0.70	D16965	0.79	1.44	1.008	1.138	4.90	4.319	0.881	Comp D66
61080	MGZD106	24.50	25.20	0.70	D18805	0.69	2.31	1.617	1.594				Comp D67
61080	MGZD106	25.20	25.90	0.70	D18806	0.79	2.29	1.603	1.809	1.40	3.220	2.300	Comp D67
61080	MGZD106	34.40	35.10	0.70	D18817	0.76	0.89	0.623	0.676				Comp D64
61080	MGZD106	35.10	35.80	0.70	D18819	0.71	1.21	0.847	0.859				Comp D65
61080	MGZD106	35.80	36.50	0.70	D18820	0.73	1.35	0.945	0.986				Comp D66
61080	MGZD106	36.50	37.20	0.70	D18822	0.86	0.67	0.469	0.576				Comp D63
61080	MGZD106	37.20	37.90	0.70	D18823	0.79	0.09	0.063	0.071				Comp D61
61080	MGZD106	37.90	38.60	0.70	D18824	0.85	1.82	1.274	1.547	4.20	4.221	1.005	Comp D67
61160	MGZD110	9.50	10.20	0.70	D18924	0.68	0.63	0.441	0.428				Comp D63
61160	MGZD110	10.20	10.90	0.70	D18925	0.68	1.65	1.155	1.122				Comp D66
61160	MGZD110	10.90	11.60	0.70	D18926	0.63	1.99	1.393	1.254				Comp D67
61160	MGZD110	11.60	12.30	0.70	D18927	0.64	0.83	0.581	0.531				Comp D64
61160	MGZD110	12.30	13.00	0.70	D18928	0.72	3.47	2.429	2.498				Comp D68
61160	MGZD110	13.00	13.70	0.70	D18929	0.71	0.56	0.392	0.398				Comp D63
61160	MGZD110	13.70	14.40	0.70	D18930	0.71	0.21	0.147	0.149				Comp D61
61160	MGZD110	14.40	15.10	0.70	D18931	0.72	1.09	0.763	0.785				Comp D65
61160	MGZD110	15.10	15.80	0.70	D18932	0.74	2.40	1.680	1.776				Comp D67
61160	MGZD110	15.80	16.50	0.70	D18933	0.66	0.82	0.574	0.541	7.00	9.555	1.365	Comp D64
61080	MGZD105	14.00	14.70	0.70	D19033	1.38	0.73	0.511	1.007				Comp D63
61080	MGZD105	14.70	15.40	0.70	D19034	0.87	0.82	0.574	0.713				Comp D64
61080	MGZD105	15.40	16.10	0.70	D19035	0.69	0.99	0.693	0.683				Comp D64
61080	MGZD105	16.10	16.80	0.70	D19036	0.74	3.13	2.191	2.316				Comp D68
61080	MGZD105	16.80	17.50	0.70	D19037	0.50	3.66	2.562	1.830				Comp D69
61080	MGZD105	17.50	18.20	0.70	D19039	0.65	0.94	0.658	0.611				Comp D64
61080	MGZD105	18.20	18.90	0.70	D19040	0.72	0.76	0.532	0.547				Comp D64
61080	MGZD105	18.90	19.60	0.70	D19041	0.81	1.10	0.770	0.891				Comp D65
61080	MGZD105	19.60	20.30	0.70	D19042	0.85	1.13	0.791	0.961				Comp D65
61080	MGZD105	20.30	21.00	0.70	D19043	0.78	0.59	0.413	0.460				Comp D63
61080	MGZD105	21.00	21.70	0.70	D19044	0.62	0.87	0.609	0.539				Comp D64
61080	MGZD105	21.70	22.40	0.70	D19045	0.75	0.91	0.637	0.683				Comp D64
61080	MGZD105	22.40	23.10	0.70	D19047	0.72	1.01	0.707	0.727	9.10	11.648	1.280	Comp D65
61080	MGZD108	32.40	33.10	0.70	D19174	0.72	3.86	2.702	2.779				Comp D69
61080	MGZD108	33.10	33.80	0.70	D19175	0.78	1.40	0.980	1.092	1.40	3.682	2.630	Comp D66
61080	MGZD108	79.70	80.40	0.70	D19239	0.83	4.11	2.877	3.411				Comp D69
61080	MGZD108	80.40	81.10	0.70	D19240	0.80	0.40	0.280	0.320	1.40	3.157	2.255	Comp D62
61200	MGZD114	14.40	15.10	0.70	D19294	0.79	1.40	0.980	1.106				Comp D66
61200	MGZD114	15.10	15.80	0.70	D19295	0.75	0.43	0.301	0.323				Comp D62
61200	MGZD114	15.80	16.50	0.70	D19297	0.85	1.83	1.281	1.556				Comp D67
61200	MGZD114	16.50	17.20	0.70	D19299	0.70	1.86	1.302	1.302				Comp D67
61200	MGZD114	17.20	17.90	0.70	D19300	0.86	0.86	0.602	0.740	3.50	4.466	1.276	Comp D64

D ZONE LOW GRADE COMPOSITE (SECTIONS 60880 through 61200)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
61200	MGZD114	22.10	22.80	0.70	D19307	0.78	1.20	0.840	0.936				Comp D65
61200	MGZD114	22.80	23.50	0.70	D19308	0.79	0.18	0.126	0.142				Comp D61
61200	MGZD114	23.50	24.20	0.70	D19309	0.78	0.32	0.224	0.250				Comp D62
61200	MGZD114	24.20	24.90	0.70	D19310	0.85	0.54	0.378	0.459				Comp D63
61200	MGZD114	24.90	25.60	0.70	D19311	0.76	2.41	1.687	1.832				Comp D67
61200	MGZD114	25.60	26.30	0.70	D19312	0.67	0.88	0.616	0.590				Comp D64
61200	MGZD114	26.30	27.00	0.70	D19313	0.87	0.71	0.497	0.618				Comp D63
61200	MGZD114	27.00	27.70	0.70	D19314	0.85	0.78	0.546	0.663				Comp D64
61200	MGZD114	27.70	28.40	0.70	D19315	0.90	0.15	0.105	0.135				Comp D61
61200	MGZD114	28.40	29.10	0.70	D19316	0.86	5.14	3.598	4.420				Comp D70
61200	MGZD114	29.10	29.80	0.70	D19317	0.94	0.04	0.028	0.038				Comp D61
61200	MGZD114	29.80	30.50	0.70	D19319	0.87	0.65	0.455	0.566				Comp D63
61200	MGZD114	30.50	31.20	0.70	D19320	0.79	0.76	0.532	0.600				Comp D64
61200	MGZD114	31.20	31.90	0.70	D19322	0.73	0.65	0.455	0.475				Comp D63
61200	MGZD114	31.90	32.60	0.70	D19323	0.82	0.33	0.231	0.271				Comp D62
61200	MGZD114	32.60	33.30	0.70	D19324	0.87	1.43	1.001	1.244	11.20	11.319	1.011	Comp D66
61200	MGZD114	48.70	49.40	0.70	D19349	0.87	1.32	0.924	1.148				Comp D66
61200	MGZD114	49.40	50.10	0.70	D19350	0.53	2.74	1.918	1.452				Comp D68
61200	MGZD114	50.10	50.80	0.70	D19351	0.89	1.59	1.113	1.415				Comp D66
61200	MGZD114	50.80	51.50	0.70	D19352	0.67	1.29	0.903	0.864	2.80	4.858	1.735	Comp D65
61080	MGZD109	51.00	51.70	0.70	D19463	0.98	0.60	0.420	0.588				Comp D63
61080	MGZD109	51.70	52.40	0.70	D19464	0.94	2.30	1.610	2.162				Comp D67
61080	MGZD109	52.40	53.10	0.70	D19465	0.92	0.70	0.490	0.644				Comp D63
61080	MGZD109	53.10	53.80	0.70	D19466	0.92	0.28	0.196	0.258	2.80	2.716	0.970	Comp D62
61160	MGZD111	9.00	10.00	1.00	D19542	0.97	1.02	1.020	0.989				Comp D65
61160	MGZD111	10.00	11.00	1.00	D19543	0.92	0.43	0.430	0.396				Comp D62
61160	MGZD111	11.00	12.00	1.00	D19544	1.16	1.08	1.080	1.253				Comp D65
61160	MGZD111	12.00	13.00	1.00	D19545	1.31	1.28	1.280	1.677				Comp D65
61160	MGZD111	13.00	14.00	1.00	D19547	2.69	1.39	1.390	3.739				Comp D66
61160	MGZD111	14.00	15.00	1.00	D19548	1.74	0.19	0.190	0.331				Comp D61
61160	MGZD111	15.00	16.00	1.00	D19549	1.25	0.78	0.780	0.975				Comp D64
61160	MGZD111	16.00	17.00	1.00	D19550	1.36	0.63	0.630	0.857				Comp D63
61160	MGZD111	17.00	18.00	1.00	D19551	1.28	1.94	1.940	2.483				Comp D67
61160	MGZD111	18.00	19.00	1.00	D19552	1.34	3.75	3.750	5.025				Comp D69
61160	MGZD111	19.00	20.00	1.00	D19553	1.69	1.00	1.000	1.690				Comp D64
61160	MGZD111	20.00	20.70	0.70	D19554	1.37	2.25	1.575	3.083				Comp D67
61160	MGZD111	20.70	21.40	0.70	D19555	1.49	0.10	0.070	0.149				Comp D61
61160	MGZD111	21.40	22.10	0.70	D19556	1.42	0.72	0.504	1.022	13.10	15.639	1.194	Comp D63
61160	MGZD111	27.70	28.40	0.70	D19566	0.81	1.56	1.092	1.264				Comp D66
61160	MGZD111	28.40	29.10	0.70	D19567	0.81	0.16	0.112	0.130				Comp D61
61160	MGZD111	29.10	29.80	0.70	D19568	0.66	0.68	0.476	0.449	2.10	1.680	0.800	Comp D63
61160	MGZD111	32.60	33.30	0.70	D19574	0.75	0.65	0.455	0.488				Comp D63
61160	MGZD111	33.30	34.00	0.70	D19575	0.87	0.53	0.371	0.461				Comp D63
61160	MGZD111	34.00	35.00	1.00	D19576	1.27	1.33	1.330	1.689				Comp D66
61160	MGZD111	35.00	36.00	1.00	D19577	1.21	0.08	0.080	0.097				Comp D61
61160	MGZD111	36.00	36.70	0.70	D19579	0.87	0.21	0.147	0.183				Comp D61
61160	MGZD111	36.70	37.40	0.70	D19580	0.85	5.00	3.500	4.250				Comp D69
61160	MGZD111	37.40	38.10	0.70	D19581	0.79	1.02	0.714	0.806	5.50	6.597	1.199	Comp D65
61200	MGZD112	39.30	40.00	0.70	D19702	0.73	0.41	0.287	0.299				Comp D62
61200	MGZD112	40.00	40.70	0.70	D19703	0.68	0.42	0.294	0.286				Comp D62
61200	MGZD112	40.70	41.40	0.70	D19704	0.82	1.12	0.784	0.918				Comp D65
61200	MGZD112	41.40	42.10	0.70	D19705	0.71	0.31	0.217	0.220				Comp D62
61200	MGZD112	42.10	42.80	0.70	D19706	0.75	0.27	0.189	0.203				Comp D62
61200	MGZD112	42.80	43.50	0.70	D19707	0.69	1.10	0.770	0.759	4.20	2.541	0.605	Comp D65
61200	MGZD113	15.10	15.80	0.70	D19811	0.73	1.04	0.728	0.759				Comp D65
61200	MGZD113	15.80	16.50	0.70	D19812	0.71	0.47	0.329	0.334				Comp D62
61200	MGZD113	16.50	17.20	0.70	D19813	0.78	0.21	0.147	0.164				Comp D61
61200	MGZD113	17.20	17.90	0.70	D19814	0.76	4.68	3.276	3.557	2.80	4.480	1.600	Comp D69
61200	MGZD113	20.70	21.40	0.70	D19820	0.74	2.96	2.072	2.190				Comp D68
61200	MGZD113	21.40	22.10	0.70	D19822	0.82	0.08	0.056	0.066				Comp D61
61200	MGZD113	22.10	22.80	0.70	D19823	0.75	0.16	0.112	0.120				Comp D61
61200	MGZD113	22.80	23.50	0.70	D19824	0.77	1.02	0.714	0.785				Comp D65
61200	MGZD113	23.50	24.20	0.70	D19825	0.71	2.23	1.561	1.583				Comp D67
61200	MGZD113	24.20	24.90	0.70	D19826	0.71	2.62	1.834	1.860				Comp D68
61200	MGZD113	24.90	25.60	0.70	D19827	0.68	1.15	0.805	0.782				Comp D65
61200	MGZD113	25.60	26.30	0.70	D19828	0.70	2.07	1.449	1.449				Comp D67

D ZONE LOW GRADE COMPOSITE (SECTIONS 60880 through 61200)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
61200	MGZD113	26.30	27.00	0.70	D19829	0.74	2.09	1.463	1.547				Comp D67
61200	MGZD113	27.00	27.70	0.70	D19830	0.73	0.74	0.518	0.540				Comp D63
61200	MGZD113	27.70	28.40	0.70	D19831	0.76	2.56	1.792	1.946	7.70	12.376	1.607	Comp D68
61000	MGZD117	100.40	101.10	0.70	D20188	0.67	3.05	2.135	2.044				Comp D68
61000	MGZD117	101.10	101.80	0.70	D20189	0.66	1.17	0.819	0.772	1.40	2.954	2.110	Comp D65
61080	MGZD116	59.00	60.00	1.00	D20361	2.11	0.46	0.460	0.971				Comp D62
61080	MGZD116	60.00	61.00	1.00	D20362	2.19	1.37	1.370	3.000				Comp D66
61080	MGZD116	61.00	62.00	1.00	D20363	2.16	0.66	0.660	1.426				Comp D63
61080	MGZD116	62.00	63.00	1.00	D20364	2.21	0.73	0.730	1.613	4.00	3.220	0.805	Comp D63
61080	MGZD118	43.00	44.00	1.00	D20423	2.18	1.49	1.490	3.248				Comp D66
61080	MGZD118	44.00	45.00	1.00	D20424	2.28	6.08	6.080	13.862				Comp D70
61080	MGZD118	45.00	45.70	0.70	D20425	1.60	1.43	1.001	2.288				Comp D66
61080	MGZD118	45.70	46.40	0.70	D20426	1.58	1.79	1.253	2.828	3.40	9.824	2.889	Comp D67
61080	MGZD118	52.70	53.40	0.70	D20435	1.42	0.44	0.308	0.625				Comp D62
61080	MGZD118	53.40	54.10	0.70	D20436	1.41	0.41	0.287	0.578				Comp D62
61080	MGZD118	54.10	54.80	0.70	D20437	1.24	0.60	0.420	0.744				Comp D63
61080	MGZD118	54.80	55.50	0.70	D20439	1.49	2.10	1.470	3.129				Comp D67
61080	MGZD118	55.50	56.20	0.70	D20440	1.45	0.75	0.525	1.088				Comp D63
61080	MGZD118	56.20	56.90	0.70	D20441	1.42	3.75	2.625	5.325				Comp D69
61080	MGZD118	56.90	57.60	0.70	D20442	1.26	0.14	0.098	0.176				Comp D61
61080	MGZD118	57.60	58.30	0.70	D20443	1.24	0.20	0.140	0.248				Comp D61
61080	MGZD118	58.30	59.00	0.70	D20444	1.31	0.81	0.567	1.061				Comp D64
61080	MGZD118	59.00	59.70	0.70	D20445	1.36	1.91	1.337	2.598	7.00	7.777	1.111	Comp D67
61080	MGZD118	94.00	95.00	1.00	D20494	2.37	1.02	1.020	2.417				Comp D65
61080	MGZD118	95.00	96.00	1.00	D20495	2.24	0.47	0.470	1.053				Comp D62
61080	MGZD118	96.00	96.70	0.70	D20497	1.62	0.23	0.161	0.373				Comp D61
61080	MGZD118	96.70	97.40	0.70	D20499	1.59	0.48	0.336	0.763				Comp D62
61080	MGZD118	97.40	98.10	0.70	D20500	1.34	0.60	0.420	0.804	4.10	2.407	0.587	Comp D63
61000	MGZD119	88.30	89.00	0.70	D20631	0.84	1.04	0.728	0.874				Comp D65
61000	MGZD119	89.00	89.70	0.70	D20632	0.79	5.37	3.759	4.242				Comp D70
61000	MGZD119	89.70	90.40	0.70	D20633	0.75	2.39	1.673	1.793				Comp D67
61000	MGZD119	90.40	91.10	0.70	D20634	0.76	0.10	0.070	0.076				Comp D61
61000	MGZD119	91.10	91.80	0.70	D20635	0.74	1.42	0.994	1.051	3.50	7.224	2.064	Comp D66
61000	MGZD122	110.70	111.40	0.70	D21836	0.69	2.58	1.806	1.780				Comp D68
61000	MGZD122	111.40	112.10	0.70	D21837	0.78	0.46	0.322	0.359				Comp D62
61000	MGZD122	112.10	113.00	0.90	D21839	0.96	2.26	2.034	2.170	2.30	4.162	1.810	Comp D67
61000	MGZD125	93.60	94.30	0.70	D23227	0.69	0.77	0.539	0.531				Comp D64
61000	MGZD125	94.30	95.00	0.70	D23228	0.77	1.04	0.728	0.801				Comp D65
61000	MGZD125	95.00	95.70	0.70	D23229	0.67	0.98	0.686	0.657				Comp D64
61000	MGZD125	95.70	96.40	0.70	D23230	0.70	0.66	0.462	0.462	2.80	2.415	0.863	Comp D63
61000	MGZD125	104.80	105.50	0.70	D23244	0.84	1.78	1.246	1.495				Comp D67
61000	MGZD125	105.50	106.20	0.70	D23245	0.85	0.47	0.329	0.400				Comp D62
61000	MGZD125	106.20	106.90	0.70	D23247	0.79	0.83	0.581	0.656				Comp D64
61000	MGZD125	106.90	107.60	0.70	D23248	0.85	0.65	0.455	0.553				Comp D63
61000	MGZD125	107.60	108.30	0.70	D23249	0.85	0.78	0.546	0.663				Comp D64
61000	MGZD125	108.30	109.00	0.70	D23250	0.77	0.49	0.343	0.377				Comp D62
61000	MGZD125	109.00	109.70	0.70	D23251	0.80	0.61	0.427	0.488				Comp D63
61000	MGZD125	109.70	110.40	0.70	D23252	0.76	0.48	0.336	0.365				Comp D62
61000	MGZD125	110.40	111.10	0.70	D23253	0.79	1.44	1.008	1.138				Comp D66
61000	MGZD125	111.10	111.80	0.70	D23254	0.77	0.62	0.434	0.477				Comp D63
61000	MGZD125	111.80	112.50	0.70	D23255	0.92	2.27	1.589	2.088				Comp D67
61000	MGZD125	112.50	113.20	0.70	D23256	0.72	1.04	0.728	0.749				Comp D65
61000	MGZD125	113.20	113.90	0.70	D23257	0.79	17.70	12.390	13.983				Comp D71
61000	MGZD125	113.90	114.60	0.70	D23259	0.76	13.50	9.450	10.260				Comp D71
61000	MGZD125	114.60	115.30	0.70	D23260	0.81	1.59	1.113	1.288				Comp D66
61000	MGZD125	115.30	116.00	0.70	D23261	0.79	0.84	0.588	0.664				Comp D64
61000	MGZD125	116.00	116.70	0.70	D23262	0.88	1.16	0.812	1.021				Comp D65
61000	MGZD125	116.70	117.40	0.70	D23263	0.83	0.10	0.070	0.083				Comp D61
61000	MGZD125	117.40	118.10	0.70	D23264	0.75	0.53	0.371	0.398				Comp D63
61000	MGZD125	118.10	118.80	0.70	D23265	0.74	0.23	0.161	0.170				Comp D61
61000	MGZD125	118.80	119.50	0.70	D23266	0.79	1.88	1.316	1.485	14.70	34.293	2.333	Comp D67
61040	MGZD026	10.00	11.00	1.00	D24941	1.00	2.27	2.270	2.270				Comp D67

D ZONE   LOW GRADE COMPOSITE   (SECTIONS 60880 through 61200)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
61040	MGZD026	11.00	12.00	1.00	D24942	1.00	1.46	1.460	1.460				Comp D66
61040	MGZD026	12.00	13.00	1.00	D24943	0.80	0.11	0.110	0.088				Comp D61
61040	MGZD026	13.00	14.00	1.00	D24944	1.00	0.65	0.650	0.650	4.00	4.490	1.123	Comp D63
61000	MGZD127	101.60	102.30	0.70	D25356	0.79	0.65	0.455	0.514				Comp D63
61000	MGZD127	102.30	103.00	0.70	D25357	0.70	1.12	0.784	0.784				Comp D65
61000	MGZD127	103.00	104.00	1.00	D25359	1.15	0.79	0.790	0.909				Comp D64
61000	MGZD127	104.00	105.00	1.00	D25360	1.18	0.26	0.260	0.307				Comp D62
61000	MGZD127	105.00	106.00	1.00	D25361	1.12	2.63	2.630	2.946				Comp D68
61000	MGZD127	106.00	107.00	1.00	D25362	1.15	0.81	0.810	0.932				Comp D64
61000	MGZD127	107.00	108.00	1.00	D25363	1.19	0.80	0.800	0.952	6.40	6.529	1.020	Comp D64
61000	MGZD127	111.00	112.00	1.00	D25367	1.10	0.99	0.990	1.089				Comp D64
61000	MGZD127	112.00	113.00	1.00	D25368	1.03	5.65	5.650	5.820				Comp D70
61000	MGZD127	113.00	114.00	1.00	D25369	1.14	0.65	0.650	0.741	3.00	7.290	2.430	Comp D63
60960	MGZD029	103.00	104.00	1.00	D25513	0.95	1.46	1.460	1.387				Comp D66
60960	MGZD029	104.00	105.00	1.00	D25514	0.88	0.19	0.190	0.167				Comp D61
61040	MGZD138	56.40	57.10	0.70	D29107	0.84	1.72	1.204	1.445				Comp D66
61040	MGZD138	57.10	57.80	0.70	D29108	0.83	2.48	1.736	2.058				Comp D67
61040	MGZD138	57.80	58.50	0.70	D29109	0.88	3.99	2.793	3.511	2.10	5.733	2.730	Comp D69
61120	MGZD141	58.00	59.00	1.00	D29573	1.16	0.63	0.630	0.731				Comp D63
61120	MGZD141	59.00	60.00	1.00	D29574	1.29	1.86	1.860	2.399				Comp D67
61120	MGZD141	60.00	61.00	1.00	D29575	1.38	0.61	0.610	0.842				Comp D63
61120	MGZD141	61.00	62.00	1.00	D29576	1.21	0.79	0.790	0.956				Comp D64
61120	MGZD141	62.00	63.00	1.00	D29577	1.33	0.77	0.770	1.024	5.00	4.660	0.932	Comp D64
60920	MGZD142	187.40	188.10	0.70	D29916	0.85	4.04	2.828	3.434				Comp D69
60920	MGZD142	188.10	188.80	0.70	D29917	0.82	3.49	2.443	2.862				Comp D68
60920	MGZD142	188.80	189.50	0.70	D29919	0.81	0.44	0.308	0.356				Comp D62
60920	MGZD142	189.50	190.20	0.70	D29920	0.83	0.08	0.056	0.066				Comp D61
60920	MGZD142	190.20	191.00	0.80	D29922	0.89	2.33	1.864	2.074	3.60	7.499	2.083	Comp D67
60960	MGZD145	94.00	95.00	1.00	D30514	1.23	0.39	0.390	0.480				Comp D62
60960	MGZD145	95.00	96.00	1.00	D30515	1.07	1.34	1.340	1.434				Comp D66
60960	MGZD145	96.00	97.00	1.00	D30516	1.14	0.84	0.840	0.958				Comp D64
60960	MGZD145	97.00	98.00	1.00	D30517	1.25	0.39	0.390	0.488				Comp D62
60960	MGZD145	98.00	99.00	1.00	D30519	1.23	0.57	0.570	0.701	5.00	3.530	0.706	Comp D63
60920	MGZD147	150.70	151.40	0.70	D31813	0.82	1.92	1.344	1.574				Comp D67
60920	MGZD147	151.40	152.10	0.70	D31814	0.81	1.27	0.889	1.029				Comp D65
60920	MGZD147	152.10	152.80	0.70	D31815	0.77	1.85	1.295	1.425				Comp D67
60920	MGZD147	152.80	153.50	0.70	D31816	0.77	3.24	2.268	2.495				Comp D68
60920	MGZD147	153.50	154.20	0.70	D31817	0.72	9.16	6.412	6.595				Comp D71
60920	MGZD147	154.20	154.90	0.70	D31819	0.78	2.34	1.638	1.825				Comp D67
60920	MGZD147	154.90	155.60	0.70	D31820	0.78	2.02	1.414	1.576				Comp D67
60920	MGZD147	155.60	156.30	0.70	D31822	0.75	3.29	2.303	2.468				Comp D68
60920	MGZD147	156.30	157.00	0.70	D31823	0.77	0.90	0.630	0.693				Comp D64
60920	MGZD147	157.00	157.70	0.70	D31824	0.78	1.13	0.791	0.881				Comp D65
60920	MGZD147	157.70	158.40	0.70	D31825	0.81	0.13	0.091	0.105				Comp D61
60920	MGZD147	158.40	159.10	0.70	D31826	0.86	0.66	0.462	0.568	8.40	19.537	2.326	Comp D63
60920	MGZD162	151.00	152.00	1.00	D35628	1.28	3.00	3.000	3.840				Comp D68
60920	MGZD162	152.00	152.70	0.70	D35629	0.93	0.78	0.546	0.725				Comp D64
60920	MGZD162	152.70	153.40	0.70	D35630	0.87	1.60	1.120	1.392				Comp D66
60920	MGZD162	153.40	154.10	0.70	D35631	0.86	0.84	0.588	0.722	3.10	5.254	1.695	Comp D64
60920	MGZD162	161.10	161.80	0.70	D35643	0.76	3.98	2.786	3.025				Comp D69
60920	MGZD162	161.80	162.50	0.70	D35644	0.73	9.17	6.419	6.694				Comp D71
60920	MGZD162	162.50	163.20	0.70	D35645	0.77	0.62	0.434	0.477				Comp D63
60920	MGZD162	163.20	163.90	0.70	D35647	0.80	0.96	0.672	0.768				Comp D64
60920	MGZD162	163.90	164.60	0.70	D35648	0.83	1.46	1.022	1.212				Comp D66
60920	MGZD162	164.60	165.30	0.70	D35649	0.73	0.19	0.133	0.139				Comp D61
60920	MGZD162	165.30	166.00	0.70	D35650	0.77	0.00	0.000	0.000				Comp D61
60920	MGZD162	166.00	167.00	1.00	D35651	1.21	0.00	0.000	0.000				Comp D61
60920	MGZD162	167.00	168.00	1.00	D35652	1.31	4.24	4.240	5.554	6.90	15.706	2.276	Comp D69
60880	MGZD175	174.00	175.00	1.00	D39136	1.10	1.04	1.040	1.144				Comp D65
60880	MGZD175	175.00	176.00	1.00	D39137	1.19	0.12	0.120	0.143				Comp D61
60880	MGZD175	176.00	177.00	1.00	D39139	1.16	0.24	0.240	0.278				Comp D61
60880	MGZD175	177.00	177.70	0.70	D39140	0.84	0.12	0.084	0.101				Comp D61
60880	MGZD175	177.70	178.40	0.70	D39141	0.85	8.72	6.104	7.412	4.40	7.588	1.725	Comp D71

D ZONE   LOW GRADE COMPOSITE   (SECTIONS 60880 through 61200)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60880	MGZD175	184.70	185.40	0.70	D39152	0.79	1.03	0.721	0.814				Comp D65
60880	MGZD175	185.40	186.10	0.70	D39153	0.81	0.54	0.378	0.437				Comp D63
60880	MGZD175	186.10	186.80	0.70	D39154	0.79	0.64	0.448	0.506				Comp D63
60880	MGZD175	186.80	187.50	0.70	D39155	0.76	1.01	0.707	0.768				Comp D65
60880	MGZD175	187.50	188.20	0.70	D39156	0.84	0.08	0.056	0.067				Comp D61
60880	MGZD175	188.20	188.90	0.70	D39157	0.75	0.23	0.161	0.173				Comp D61
60880	MGZD175	188.90	189.60	0.70	D39159	0.85	0.31	0.217	0.264				Comp D62
60880	MGZD175	189.60	190.30	0.70	D39160	0.74	0.71	0.497	0.525				Comp D63
60880	MGZD175	190.30	191.00	0.70	D39161	0.83	0.52	0.364	0.432				Comp D63
60880	MGZD175	191.00	191.70	0.70	D39162	0.78	2.78	1.946	2.168				Comp D68
60880	MGZD175	191.70	192.40	0.70	D39163	0.67	0.10	0.070	0.067				Comp D61
60880	MGZD175	192.40	193.10	0.70	D39164	0.80	0.97	0.679	0.776				Comp D64
60880	MGZD175	195.90	196.60	0.70	D39169	0.71	7.93	5.551	5.630				Comp D70
60880	MGZD175	196.60	197.30	0.70	D39170	0.77	2.99	2.093	2.302	9.80	13.888	1.417	Comp D68
60880	MGZD175	201.00	202.00	1.00	D39176	1.11	2.08	2.080	2.309				Comp D67
60880	MGZD175	202.00	203.00	1.00	D39177	1.22	3.14	3.140	3.831	2.00	5.220	2.610	Comp D68

Composite grade (based on (drill core grade x thickness) and meterage, assumes uniform core density)	511.7 m		1.52	778.46	
Composite grade (based on as-received intercept weights and drill core assays)		598.7	1.51		904.6

D ZONE HIGH GRADE COMPOSITE (SECTIONS 60880 through 61200)

Section	HOLE_ID	Meters From	Meters To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
61120	MGZD019	70.00	70.70	0.70	D01575	0.70	4.57	3.199	3.199				Comp D69
61120	MGZD019	70.70	71.40	0.70	D01576	0.70	2.87	2.009	2.009				Comp D68
61120	MGZD019	71.40	72.10	0.70	D01577	0.80	27.00	18.900	21.600				Comp D71
61120	MGZD019	72.10	73.00	0.90	D01578	1.10	1.77	1.593	1.947	3.00	25.701	8.567	Comp D67
61120	MGZD019	75.00	76.00	1.00	D01581	1.00	1.00	1.000	1.000				Comp D64
61120	MGZD019	76.00	77.00	1.00	D01582	1.00	15.00	15.000	15.000				Comp D71
61120	MGZD019	77.00	78.00	1.00	D01583	1.00	3.56	3.560	3.560				Comp D69
61120	MGZD019	78.00	79.00	1.00	D01584	1.10	0.69	0.690	0.759	4.00	20.250	5.063	Comp D63
61120	MGZD019	100.00	101.00	1.00	D01609	1.04	2.77	2.770	2.881				Comp D68
61120	MGZD019	101.00	102.00	1.00	D01610	1.05	5.52	5.520	5.796				Comp D70
61120	MGZD019	102.00	103.00	1.00	D01611	1.15	0.84	0.840	0.966	3.00	9.130	3.043	Comp D64
61120	MGZD023	54.70	55.40	0.70	D02151	0.80	21.20	14.840	16.960				Comp D71
61120	MGZD023	55.40	56.10	0.70	D02152	0.60	0.21	0.147	0.126				Comp D61
61120	MGZD023	56.10	56.80	0.70	D02153	0.60	0.65	0.455	0.390				Comp D63
61120	MGZD023	56.80	57.50	0.70	D02154	0.70	7.35	5.145	5.145				Comp D70
61120	MGZD023	57.50	58.20	0.70	D02155	0.80	1.97	1.379	1.576	3.50	21.966	6.276	Comp D67
61120	MGZD023	61.40	62.10	0.70	D02161	0.70	12.60	8.820	8.820				Comp D71
61120	MGZD023	62.10	63.10	1.00	D02162	1.00	0.98	0.980	0.980				Comp D64
61120	MGZD023	63.10	63.90	0.80	D02163	0.80	11.00	8.800	8.800	2.50	18.600	7.440	Comp D71
61120	MGZD023	70.00	70.70	0.70	D02170	0.90	3.91	2.737	3.519				Comp D69
61120	MGZD023	70.70	71.40	0.70	D02172	0.70	0.52	0.364	0.364				Comp D63
61120	MGZD023	71.40	72.10	0.70	D02174	0.80	0.87	0.609	0.696				Comp D64
61120	MGZD023	72.10	72.80	0.70	D02175	0.70	0.06	0.042	0.042				Comp D61
61120	MGZD023	72.80	73.50	0.70	D02176	0.90	1.26	0.882	1.134				Comp D65
61120	MGZD023	73.50	74.20	0.70	D02177	0.60	38.50	26.950	23.100				Comp D71
61120	MGZD023	74.20	74.90	0.70	D02178	0.60	2.14	1.498	1.284				Comp D67
61120	MGZD023	74.90	75.60	0.70	D02179	0.80	0.47	0.329	0.376				Comp D62
61120	MGZD023	75.60	76.30	0.70	D02180	0.90	2.75	1.925	2.475	6.30	35.336	5.609	Comp D68
61120	MGZD023	82.00	83.00	1.00	D02187	1.20	24.70	24.700	29.640				Comp D71
61120	MGZD023	83.00	84.00	1.00	D02189	1.20	0.36	0.360	0.432				Comp D62
61120	MGZD023	84.00	85.00	1.00	D02190	1.20	1.72	1.720	2.064	3.00	26.780	8.927	Comp D66
61080	MGZD024	64.40	65.10	0.70	D02219	0.70	2.42	1.694	1.694				Comp D67
61080	MGZD024	65.10	65.80	0.70	D02220	0.70	5.91	4.137	4.137				Comp D70
61080	MGZD024	65.80	66.50	0.70	D02222	0.60	2.20	1.540	1.320				Comp D67
61080	MGZD024	66.50	67.20	0.70	D02223	0.80	13.00	9.100	10.400				Comp D71
61080	MGZD024	67.20	67.90	0.70	D02224	0.70	8.32	5.824	5.824				Comp D71
61080	MGZD024	69.00	70.00	1.00	D02226	1.10	0.28	0.280	0.308				Comp D62
61080	MGZD024	70.00	70.70	0.70	D02227	0.80	0.65	0.455	0.520				Comp D63
61080	MGZD024	70.70	71.40	0.70	D02228	0.80	0.56	0.392	0.448				Comp D63
61080	MGZD024	71.40	72.40	1.00	D02229	1.00	2.53	2.530	2.530	6.90	25.952	3.761	Comp D68
61080	MGZD025	75.00	76.00	1.00	D02309	1.10	5.42	5.420	5.962				Comp D70
61080	MGZD025	76.00	77.00	1.00	D02310	1.00	2.91	2.910	2.910	2.00	8.330	4.165	Comp D68
61080	MGZD025	84.10	85.10	1.00	D02319	1.00	6.67	6.670	6.670				Comp D70
61080	MGZD025	85.10	86.10	1.00	D02320	1.00	12.30	12.300	12.300				Comp D71
61080	MGZD025	86.10	87.00	0.90	D02322	0.90	2.09	1.881	1.881	2.90	20.851	7.190	Comp D67
61040	MGZD027	99.00	100.00	1.00	D02426	1.20	12.20	12.200	14.640				Comp D71
61040	MGZD027	100.00	100.70	0.70	D02427	0.80	0.27	0.189	0.216				Comp D62
61040	MGZD027	100.70	101.40	0.70	D02429	1.00	7.98	5.586	7.980				Comp D70
61040	MGZD027	101.40	102.10	0.70	D02430	0.80	3.34	2.338	2.672				Comp D68
61040	MGZD027	102.10	102.80	0.70	D02431	0.80	5.21	3.647	4.168	3.80	23.960	6.305	Comp D70
61040	MGZD027	105.00	105.70	0.70	D02435	0.80	0.67	0.469	0.536				Comp D63
61040	MGZD027	105.70	106.40	0.70	D02436	0.80	6.84	4.788	5.472	1.40	5.257	3.755	Comp D70
60960	MGZD028	200.00	200.70	0.70	D02534	0.78	13.70	9.590	10.686				Comp D71
60960	MGZD028	200.70	201.40	0.70	D02535	0.87	1.06	0.742	0.922				Comp D65
60960	MGZD028	201.40	202.10	0.70	D02536	0.75	1.99	1.393	1.493	2.10	11.725	5.583	Comp D67
60960	MGZD029	179.10	179.80	0.70	D02591	0.87	12.00	8.400	10.440				Comp D71
60960	MGZD029	179.80	180.50	0.70	D02592	0.87	0.65	0.455	0.566				Comp D63
60960	MGZD029	180.50	181.20	0.70	D02594	0.87	4.54	3.178	3.950				Comp D69

D ZONE HIGH GRADE COMPOSITE (SECTIONS 60880 through 61200)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
60960	MGZD029	181.20	181.90	0.70	D02595	0.79	3.37	2.359	2.662				Comp D68
60960	MGZD029	181.90	182.60	0.70	D02597	0.79	1.07	0.749	0.845	3.50	15.141	4.326	Comp D65
61160	MGZD034	43.00	43.70	0.70	D02890	0.76	1.14	0.798	0.866				Comp D65
61160	MGZD034	43.70	44.40	0.70	D02891	0.81	1.88	1.316	1.523				Comp D67
61160	MGZD034	44.40	45.10	0.70	D02892	0.84	6.44	4.508	5.410				Comp D70
61160	MGZD034	45.10	45.80	0.70	D02894	0.80	9.65	6.755	7.720				Comp D71
61160	MGZD034	45.80	46.50	0.70	D02895	0.89	0.04	0.028	0.036				Comp D61
61160	MGZD034	46.50	47.20	0.70	D02897	0.84	1.76	1.232	1.478				Comp D67
61160	MGZD034	47.20	48.00	0.80	D02898	0.95	2.44	1.952	2.318	5.00	16.589	3.318	Comp D67
60960	MGZD048	109.00	109.70	0.70	D04661	0.75	11.00	7.700	8.250				Comp D71
60960	MGZD048	109.70	110.40	0.70	D04662	0.76	6.33	4.431	4.811				Comp D70
60960	MGZD048	110.40	111.10	0.70	D04664	0.70	6.19	4.333	4.333	2.10	16.464	7.840	Comp D70
60960	MGZD048	121.70	122.40	0.70	D04680	0.72	2.50	1.750	1.800				Comp D67
60960	MGZD048	122.40	123.10	0.70	D04681	0.69	6.62	4.634	4.568				Comp D70
60960	MGZD048	123.10	123.80	0.70	D04682	0.67	3.88	2.716	2.600				Comp D69
60960	MGZD048	123.80	124.50	0.70	D04683	0.68	8.52	5.964	5.794				Comp D71
60960	MGZD048	124.50	125.20	0.70	D04684	0.65	1.51	1.057	0.982				Comp D66
60960	MGZD048	125.20	125.90	0.70	D04685	0.69	3.32	2.324	2.291				Comp D68
60960	MGZD048	125.90	126.60	0.70	D04686	0.80	1.60	1.120	1.280				Comp D66
60960	MGZD048	126.60	127.30	0.70	D04687	0.74	12.30	8.610	9.102				Comp D71
60960	MGZD048	127.30	128.00	0.70	D04688	0.76	3.53	2.471	2.683				Comp D69
60960	MGZD048	128.00	129.00	1.00	D04689	1.03	1.09	1.090	1.123				Comp D65
60960	MGZD048	129.00	129.70	0.70	D04690	0.73	0.83	0.581	0.606				Comp D64
60960	MGZD048	129.70	130.40	0.70	D04691	0.72	1.52	1.064	1.094				Comp D66
60960	MGZD048	130.40	131.10	0.70	D04692	0.72	1.28	0.896	0.922				Comp D65
60960	MGZD048	131.10	131.80	0.70	D04694	0.73	3.85	2.695	2.811				Comp D69
60960	MGZD048	131.80	132.50	0.70	D04695	0.72	1.56	1.092	1.123	10.80	38.064	3.524	Comp D66
61120	MGZD051	14.00	14.70	0.70	D05808	0.89	1.29	0.903	1.148				Comp D65
61120	MGZD051	14.70	15.40	0.70	D05809	0.87	3.97	2.779	3.454				Comp D69
61120	MGZD051	15.40	16.10	0.70	D05810	0.81	4.89	3.423	3.961	2.10	7.105	3.383	Comp D69
61160	MGZD056	65.00	65.70	0.70	D05978	0.86	5.00	3.500	4.300				Comp D69
61160	MGZD056	65.70	66.40	0.70	D05979	0.91	2.82	1.974	2.566	1.40	5.474	3.910	Comp D68
61080	MGZD053	52.00	53.00	1.00	D06035	1.12	11.00	11.000	12.320				Comp D71
61080	MGZD053	53.00	54.00	1.00	D06036	1.22	3.63	3.630	4.429	2.00	14.630	7.315	Comp D69
61080	MGZD053	60.10	60.80	0.70	D06045	0.81	1.80	1.260	1.458				Comp D67
61080	MGZD053	60.80	61.50	0.70	D06047	0.79	2.84	1.988	2.244				Comp D68
61080	MGZD053	61.50	62.20	0.70	D06048	0.78	13.50	9.450	10.530				Comp D71
61080	MGZD053	62.20	63.00	0.80	D06049	0.97	0.52	0.416	0.504				Comp D63
61080	MGZD053	63.00	63.70	0.70	D06050	0.71	16.50	11.550	11.715	3.60	24.664	6.851	Comp D71
61080	MGZD053	67.00	68.00	1.00	D06055	1.12	0.34	0.340	0.381				Comp D62
61080	MGZD053	68.00	68.70	0.70	D06056	0.72	3.18	2.226	2.290				Comp D68
61080	MGZD053	68.70	69.40	0.70	D06057	0.74	1.00	0.700	0.740				Comp D64
61080	MGZD053	69.40	70.10	0.70	D06059	0.57	0.04	0.028	0.023				Comp D61
61080	MGZD053	70.10	70.80	0.70	D06060	0.73	0.36	0.252	0.263				Comp D62
61080	MGZD053	70.80	71.50	0.70	D06061	0.71	1.30	0.910	0.923				Comp D65
61080	MGZD053	71.50	72.20	0.70	D06062	0.84	2.81	1.967	2.360				Comp D68
61080	MGZD053	72.20	73.00	0.80	D06063	0.96	8.87	7.096	8.515				Comp D71
61080	MGZD053	73.00	73.70	0.70	D06064	0.73	4.68	3.276	3.416				Comp D69
61080	MGZD053	73.70	74.40	0.70	D06065	0.64	1.06	0.742	0.678				Comp D65
61080	MGZD053	74.40	75.10	0.70	D06066	0.84	0.18	0.126	0.151				Comp D61
61080	MGZD053	75.10	75.80	0.70	D06067	0.82	0.82	0.574	0.672				Comp D64
61080	MGZD053	75.80	76.50	0.70	D06068	0.75	11.10	7.770	8.325				Comp D71
61080	MGZD053	76.50	77.20	0.70	D06069	0.74	9.34	6.538	6.912				Comp D71
61080	MGZD053	77.20	77.90	0.70	D06070	0.76	2.84	1.988	2.158				Comp D68
61080	MGZD053	77.90	78.60	0.70	D06072	0.84	1.72	1.204	1.445				Comp D66
61080	MGZD053	78.60	79.30	0.70	D06074	0.64	30.20	21.140	19.328				Comp D71
61080	MGZD053	79.30	80.00	0.70	D06075	0.93	2.57	1.799	2.390				Comp D68
61080	MGZD053	80.00	80.70	0.70	D06076	0.84	9.64	6.748	8.098	13.70	65.424	4.775	Comp D71
61160	MGZD052	39.70	40.40	0.70	D06293	0.77	5.34	3.738	4.112				Comp D70
61160	MGZD052	40.40	41.10	0.70	D06294	0.82	18.90	13.230	15.498	1.40	16.968	12.120	Comp D71
61120	MGZD054	68.00	69.00	1.00	D06365	1.33	0.59	0.590	0.785				Comp D63
60960	MGZD063	133.00	134.00	1.00	D06406	1.04	1.08	1.080	1.123				Comp D65
60960	MGZD063	134.00	135.00	1.00	D06407	1.15	11.70	11.700	13.455	2.00	12.780	6.390	Comp D71
61040	MGZD060	82.00	83.00	1.00	D06556	1.00	7.53	7.530	7.530				Comp D70
61040	MGZD060	83.00	84.00	1.00	D06557	1.00	0.13	0.130	0.130	2.00	7.660	3.830	Comp D61
61040	MGZD060	88.70	89.40	0.70	D06563	0.80	12.70	8.890	10.160				Comp D71

D ZONE HIGH GRADE COMPOSITE (SECTIONS 60880 through 61200)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
61040	MGZD060	89.40	90.10	0.70	D06564	0.50	0.57	0.399	0.285	1.40	9.289	6.635	Comp D63
61040	MGZD059	129.00	130.00	1.00	D07150	1.21	26.00	26.000	31.460				Comp D71
61040	MGZD059	130.00	131.00	1.00	D07151	1.27	1.55	1.550	1.969	2.00	27.550	13.775	Comp D66
61120	MGZD054	69.00	70.00	1.00	D07174	1.18	8.75	8.750	10.325	2.00	9.340	4.670	Comp D71
61040	MGZD067	54.70	55.70	1.00	D07263	1.04	2.87	2.870	2.985				Comp D68
61040	MGZD067	55.70	56.40	0.70	D07264	0.78	9.93	6.951	7.745				Comp D71
61040	MGZD067	56.40	57.10	0.70	D07265	0.76	3.76	2.632	2.858				Comp D69
61040	MGZD067	57.10	58.00	0.90	D07266	0.97	3.77	3.393	3.657				Comp D69
61040	MGZD067	58.00	59.00	1.00	D07267	1.02	1.62	1.620	1.652				Comp D66
61040	MGZD067	59.00	60.00	1.00	D07268	1.01	1.32	1.320	1.333				Comp D66
61040	MGZD067	60.00	61.00	1.00	D07269	1.02	1.16	1.160	1.183	6.30	19.946	3.166	Comp D65
61040	MGZD067	86.00	87.00	1.00	D07302	1.22	1.46	1.460	1.781				Comp D66
61040	MGZD067	87.00	88.00	1.00	D07304	1.19	2.55	2.550	3.035				Comp D68
61040	MGZD067	88.00	89.00	1.00	D07305	1.28	6.05	6.050	7.744				Comp D70
61040	MGZD067	89.00	90.00	1.00	D07306	1.26	3.30	3.300	4.158	4.00	13.360	3.340	Comp D68
61040	MGZD067	99.70	100.40	0.70	D07317	0.85	2.42	1.694	2.057				Comp D67
61040	MGZD067	100.40	101.10	0.70	D07319	0.84	4.87	3.409	4.091				Comp D69
61040	MGZD067	101.10	102.00	0.90	D07320	1.17	15.30	13.770	17.901				Comp D71
61040	MGZD067	102.00	103.00	1.00	D07322	1.21	5.57	5.570	6.740	3.30	24.443	7.407	Comp D70
61040	MGZD067	109.00	110.00	1.00	D07329	1.10	10.80	10.800	11.880				Comp D71
61040	MGZD067	110.00	111.00	1.00	D07330	1.10	6.31	6.310	6.941				Comp D70
61040	MGZD067	111.00	112.00	1.00	D07331	0.98	12.20	12.200	11.956	3.00	29.310	9.770	Comp D71
61040	MGZD070	73.00	73.70	0.70	D07608	0.78	8.54	5.978	6.661				Comp D71
61040	MGZD070	73.70	74.40	0.70	D07609	0.78	8.78	6.146	6.848	1.40	12.124	8.660	Comp D71
61160	MGZD110	31.10	31.80	0.70	D18956	0.91	1.54	1.078	1.401				Comp D66
61160	MGZD110	31.80	32.50	0.70	D18957	0.90	0.10	0.070	0.090				Comp D61
61160	MGZD110	32.50	33.20	0.70	D18959	0.81	0.37	0.259	0.300				Comp D62
61160	MGZD110	33.20	33.90	0.70	D18960	0.79	0.59	0.413	0.466				Comp D63
61160	MGZD110	33.90	34.60	0.70	D18961	0.78	0.57	0.399	0.445				Comp D63
61160	MGZD110	34.60	35.30	0.70	D18962	0.83	0.09	0.063	0.075				Comp D61
61160	MGZD110	35.30	36.00	0.70	D18963	0.78	5.40	3.780	4.212				Comp D70
61160	MGZD110	36.00	36.70	0.70	D18964	0.80	0.07	0.049	0.056				Comp D61
61160	MGZD110	36.70	37.40	0.70	D18965	0.78	0.17	0.119	0.133				Comp D61
61160	MGZD110	37.40	38.10	0.70	D18966	0.77	9.71	6.797	7.477				Comp D71
61160	MGZD110	38.10	38.80	0.70	D18967	0.75	0.44	0.308	0.330				Comp D62
61160	MGZD110	38.80	39.50	0.70	D18968	0.78	0.71	0.497	0.554				Comp D63
61160	MGZD110	39.50	40.20	0.70	D18969	0.73	1.58	1.106	1.153				Comp D66
61160	MGZD110	40.20	40.90	0.70	D18970	0.68	2.78	1.946	1.890				Comp D68
61160	MGZD110	40.90	41.60	0.70	D18972	0.79	1.37	0.959	1.082				Comp D66
61160	MGZD110	41.60	42.30	0.70	D18973	0.77	28.10	19.670	21.637	11.20	37.513	3.349	Comp D71
61080	MGZD108	62.30	63.00	0.70	D19215	0.87	5.93	4.151	5.159				Comp D70
61080	MGZD108	63.00	63.70	0.70	D19216	0.57	0.79	0.553	0.450	1.40	4.704	3.360	Comp D64
61000	MGZD117	112.30	113.00	0.70	D20207	0.78	24.30	17.010	18.954				Comp D71
61000	MGZD117	113.70	114.40	0.70	D20209	0.75	0.79	0.553	0.593				Comp D64
61000	MGZD117	114.40	115.10	0.70	D20210	0.85	11.10	7.770	9.435				Comp D71
61000	MGZD117	115.10	115.80	0.70	D20211	0.78	0.80	0.560	0.624				Comp D64
61000	MGZD117	115.80	116.50	0.70	D20212	0.79	0.20	0.140	0.158				Comp D61
61000	MGZD117	116.50	117.20	0.70	D20213	0.83	1.00	0.700	0.830				Comp D64
61000	MGZD117	117.20	117.90	0.70	D20214	0.77	0.19	0.133	0.146				Comp D61
61000	MGZD117	117.90	118.60	0.70	D20215	0.83	0.52	0.364	0.432				Comp D63
61000	MGZD117	118.60	119.30	0.70	D20216	0.84	0.18	0.126	0.151				Comp D61
61000	MGZD117	119.30	120.00	0.70	D20217	0.89	0.27	0.189	0.240				Comp D62
61000	MGZD117	120.00	121.00	1.00	D20219	1.30	1.67	1.670	2.171	8.70	337.215	38.760	Comp D66
61080	MGZD116	67.00	68.00	1.00	D20369	2.06	8.61	8.610	17.737				Comp D71
61080	MGZD116	68.00	69.00	1.00	D20370	2.13	1.67	1.670	3.557	2.00	10.280	5.140	Comp D66
61080	MGZD118	48.50	49.20	0.70	D20430	1.55	0.32	0.224	0.496				Comp D62
61080	MGZD118	49.20	50.00	0.80	D20431	1.73	34.90	27.920	60.377	1.50	28.144	18.763	Comp D71
61080	MGZD118	68.80	69.50	0.70	D20461	1.38	1.46	1.022	2.015				Comp D66
61080	MGZD118	69.50	70.20	0.70	D20462	1.44	8.30	5.810	11.952	1.40	6.832	4.880	Comp D71
61080	MGZD118	73.00	73.70	0.70	D20467	1.60	6.57	4.599	10.512				Comp D70
61080	MGZD118	73.70	74.40	0.70	D20468	1.35	1.87	1.309	2.525				Comp D67
61080	MGZD118	74.40	75.10	0.70	D20469	1.47	1.71	1.197	2.514				Comp D66
61080	MGZD118	75.10	75.80	0.70	D20470	1.50	3.69	2.583	5.535				Comp D69
61080	MGZD118	75.80	76.50	0.70	D20472	1.60	1.31	0.917	2.096	3.50	10.605	3.030	Comp D66
61000	MGZD122	92.40	93.10	0.70	D21813	0.71	4.65	3.255	3.302				Comp D69

D ZONE   HIGH GRADE COMPOSITE   (SECTIONS 60880 through 61200)

Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg	Intercept m	Intercept Sum of g Au/t x m	Average of Intercept Au g/t	Place in Grade Composite
61000	MGZD122	93.10	93.80	0.70	D21814	0.75	2.96	2.072	2.220	1.40	5.327	3.805	Comp D68
61000	MGZD122	116.00	117.00	1.00	D21843	1.20	6.19	6.190	7.428				Comp D70
61000	MGZD122	117.00	118.00	1.00	D21844	1.10	6.35	6.350	6.985	2.00	12.540	6.270	Comp D70
61000	MGZD124	83.00	84.00	1.00	D22267	1.06	24.40	24.400	25.864				Comp D71
61000	MGZD124	84.00	85.00	1.00	D22268	1.10	0.20	0.200	0.220				Comp D61
61000	MGZD124	85.00	86.00	1.00	D22269	0.95	1.15	1.150	1.093	3.00	25.750	8.583	Comp D65
61000	MGZD124	129.50	130.20	0.70	D22329	0.71	1.95	1.365	1.385				Comp D67
61000	MGZD124	130.20	130.90	0.70	D22330	0.69	6.18	4.326	4.264				Comp D70
61000	MGZD124	130.90	131.60	0.70	D22331	0.70	0.56	0.392	0.392				Comp D63
61000	MGZD124	131.60	132.30	0.70	D22332	0.68	7.00	4.900	4.760				Comp D70
61000	MGZD124	132.30	133.00	0.70	D22333	0.74	2.85	1.995	2.109	3.50	12.978	3.708	Comp D68
61000	MGZD124	136.50	137.20	0.70	D22340	0.53	5.88	4.116	3.116				Comp D70
61000	MGZD124	137.20	137.90	0.70	D22341	0.86	0.47	0.329	0.404				Comp D62
61000	MGZD124	137.90	138.60	0.70	D22342	0.78	0.14	0.098	0.109				Comp D61
61000	MGZD124	138.60	139.30	0.70	D22343	0.73	9.82	6.874	7.169	2.80	11.417	4.078	Comp D71
61000	MGZD125	90.10	90.80	0.70	D23222	0.65	4.55	3.185	2.958				Comp D69
61000	MGZD125	90.80	91.50	0.70	D23223	0.67	4.75	3.325	3.183				Comp D69
61000	MGZD125	91.50	92.20	0.70	D23224	0.73	6.96	4.872	5.081	2.10	11.382	5.420	Comp D70
61120	MGZD019	115.00	116.00	1.00	D24562	0.84	6.11	6.110	5.132				Comp D70
61120	MGZD019	116.00	117.00	1.00	D24563	1.05	0.12	0.120	0.126	2.00	6.230	3.115	Comp D61
61040	MGZD138	69.70	70.40	0.70	D29128	0.74	2.94	2.058	2.176				Comp D68
61040	MGZD138	70.40	71.10	0.70	D29129	0.75	4.13	2.891	3.098				Comp D69
61040	MGZD138	71.10	71.80	0.70	D29130	0.80	3.55	2.485	2.840	2.10	7.434	3.540	Comp D69
60920	MGZD147	139.50	140.20	0.70	D31795	0.82	5.91	4.137	4.846				Comp D70
60920	MGZD147	140.20	140.90	0.70	D31797	0.80	1.89	1.323	1.512				Comp D67
60920	MGZD147	140.90	141.60	0.70	D31799	0.80	2.69	1.883	2.152				Comp D68
60920	MGZD147	141.60	142.30	0.70	D31800	0.75	5.45	3.815	4.088				Comp D70
60920	MGZD147	142.30	143.00	0.70	D31801	0.79	3.06	2.142	2.417				Comp D68
60920	MGZD147	143.00	143.70	0.70	D31802	0.74	30.80	21.560	22.792				Comp D71
60920	MGZD147	143.70	144.40	0.70	D31803	0.85	2.81	1.967	2.389				Comp D68
60920	MGZD147	144.40	145.10	0.70	D31804	0.65	2.95	2.065	1.918	5.60	38.892	6.945	Comp D68
60920	MGZD162	156.20	156.90	0.70	D35635	0.76	16.00	11.200	12.160				Comp D71
60920	MGZD162	156.90	157.60	0.70	D35636	0.83	4.90	3.430	4.067				Comp D69
60920	MGZD162	157.60	158.30	0.70	D35637	0.73	5.98	4.186	4.365				Comp D70
60920	MGZD162	158.30	159.00	0.70	D35639	0.73	12.70	8.890	9.271	2.80	27.706	9.895	Comp D71
60880	MGZD164	198.00	199.00	1.00	D36354	1.22	8.18	8.180	9.980				Comp D71
60880	MGZD164	199.00	200.00	1.00	D36355	1.16	0.37	0.370	0.429				Comp D62
60880	MGZD164	200.00	201.00	1.00	D36356	1.17	2.46	2.460	2.878	3.00	11.010	3.670	Comp D67

Composite grade				176.7	m		5.31	938.1					
(based on (drill core grade x thickness) and meterage, assumes uniform core density)													
Composite grade						203.0	5.34		1084.7				
(based on as-received intercept weights and drill core assays)													

Appendix D

Zone A to D Sample Listing

	Au Grade Range of Constituents From	To	Weight, kg	Au Grade, g Au/t Calculated from As-Received Weight and drill core assays
GRADE COMPOSITE A1	0.20	0.50	26.85	0.28
GRADE COMPOSITE A2	0.50	0.80	28.50	0.65
GRADE COMPOSITE A3	0.80	1.20	30.68	1.00
GRADE COMPOSITE A4	1.20	1.60	27.67	1.39
GRADE COMPOSITE A5	1.60	2.00	28.43	1.78
GRADE COMPOSITE A6	2.00	2.40	24.29	2.20
GRADE COMPOSITE A7	2.40	3.00	19.49	2.71
GRADE COMPOSITE A8	3.00	4.00	30.02	3.42
GRADE COMPOSITE A9	4.00	6.00	19.52	5.04
GRADE COMPOSITE A10	6.00	8.00	9.81	6.98
GRADE COMPOSITE A11	8.00	12.00	12.76	9.33
GRADE COMPOSITE A12	12.00	25.00	11.91	17.71
GRADE COMPOSITE A13	25.00		8.96	43.63
GRADE COMPOSITE B21	0.00	0.40	30.64	0.21
GRADE COMPOSITE B22	0.40	1.00	42.03	0.66
GRADE COMPOSITE B23	1.00	2.00	57.51	1.48
GRADE COMPOSITE B24	2.00	2.50	40.49	2.23
GRADE COMPOSITE B25	2.50	3.00	31.98	2.77
GRADE COMPOSITE B26	3.00	4.00	43.41	3.43
GRADE COMPOSITE B27	4.00	5.00	23.08	4.45
GRADE COMPOSITE B28	5.00	7.00	34.19	5.84
GRADE COMPOSITE B29	7.00	10.00	36.92	8.22
GRADE COMPOSITE B30	10.00	15.00	24.02	12.40
GRADE COMPOSITE B31	15.00	30.00	27.34	20.72
GRADE COMPOSITE B32	30.00		11.20	58.23
GRADE COMPOSITE C41	0.00	0.25	39.39	0.13
GRADE COMPOSITE C42	0.25	0.40	30.98	0.33
GRADE COMPOSITE C43	0.40	0.80	37.38	0.58
GRADE COMPOSITE C44	0.80	1.30	30.37	1.04
GRADE COMPOSITE C45	1.30	2.40	46.79	1.82
GRADE COMPOSITE C46	2.40	4.00	42.03	3.07
GRADE COMPOSITE C47	4.00	6.00	20.25	4.87
GRADE COMPOSITE C48	6.00	10.00	23.47	7.89
GRADE COMPOSITE C49	10.00	14.00	7.81	11.91
GRADE COMPOSITE C50	14.00	25.00	14.14	18.34
GRADE COMPOSITE C51	25.00		7.83	39.98
GRADE COMPOSITE D61	0.00	0.25	51.16	0.13
GRADE COMPOSITE D62	0.25	0.50	43.04	0.39
GRADE COMPOSITE D63	0.50	0.75	46.69	0.63
GRADE COMPOSITE D64	0.75	1.00	36.01	0.87
GRADE COMPOSITE D65	1.00	1.30	34.92	1.13
GRADE COMPOSITE D66	1.30	1.75	44.39	1.51
GRADE COMPOSITE D67	1.75	2.50	41.87	2.13
GRADE COMPOSITE D68	2.50	3.50	30.32	2.93
GRADE COMPOSITE D69	3.50	5.00	24.52	4.19
GRADE COMPOSITE D70	5.00	8.00	19.61	6.12
GRADE COMPOSITE D71	8.00		28.38	14.20

A ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp A1	60240	MGZD189	60.7	61.4	0.7	D42667	1.06	0.39	0.27	0.41
Comp A1	60240	MGZD198	137.4	138.1	0.7	D45284	1.17	0.24	0.17	0.28
Comp A1	60240	MGZD198	138.1	138.8	0.7	D45285	1.14	0.27	0.19	0.31
Comp A1	60240	MGZD199	47.0	48.0	1.0	D48473	1.74	0.34	0.34	0.59
Comp A1	60240	MGZD199	162.4	163.1	0.7	D48603	1.13	0.05	0.04	0.06
Comp A1	60240	MGZD214	1.0	2.0	1.0	D49989	0.81	0.39	0.39	0.32
Comp A1	60240	MGZD221	0.0	1.0	1.0	D52283	0.95	0.31	0.31	0.29
Comp A1	60240	MGZD221	3.0	4.0	1.0	D52286	0.97	0.37	0.37	0.36
Comp A1	60240	MGZD255	52.0	53.0	1.0	D66223	1.9	0.39	0.39	0.74
Comp A1	60240	MGZD255	53.0	54.0	1.0	D66224	1.78	0.46	0.46	0.82
Comp A1	60240	MGZD255	54.0	55.0	1.0	D66225	1.85	0.47	0.47	0.87
Comp A1	60280	MGZD094	90.0	91.0	1.0	D16228	0.94	0.48	0.48	0.45
Comp A1	60280	MGZD200	98.0	99.0	1.0	D45783	1.72	0.40	0.40	0.69
Comp A1	60280	MGZD200	99.0	100.0	1.0	D45784	1.52	0.29	0.29	0.44
Comp A1	60280	MGZD200	100.0	100.7	0.7	D45785	1.1	0.43	0.30	0.47
Comp A1	60280	MGZD213	217.0	218.0	1.0	D49944	1.84	0.03	0.03	0.05
Comp A1	60280	MGZD213	218.0	219.0	1.0	D49945	1.8	0.04	0.04	0.06
Comp A1	60280	MGZD282	80.0	81.0	1.0	D75876	1.7	0.21	0.21	0.36
Comp A1	60320	MGZD009	87.5	88.8	1.3	D00722	1.56	0.42	0.55	0.66
Comp A1	60320	MGZD014	24.0	25.0	1.0	D01373	2.16	0.03	0.03	0.06
Comp A1	60320	MGZD014	27.0	28.0	1.0	D01376	1.12	0.05	0.05	0.06
Comp A1	60320	MGZD014	28.0	29.0	1.0	D01377	1.13	0.24	0.24	0.27
Comp A1	60320	MGZD017	86.0	87.0	1.0	D01331	1.26	0.41	0.41	0.52
Comp A1	60320	MGZD017	91.0	92.0	1.0	D01337	1.13	0.39	0.39	0.44
Comp A1	60320	MGZD123	40.0	40.7	0.7	D21983	0.82	0.27	0.19	0.22
Comp A1	60320	MGZD123	78.0	79.0	1.0	D22027	1.16	0.05	0.05	0.06
Comp A1	60320	MGZD126	155.4	156.1	0.7	D24024	0.89	0.31	0.22	0.28
Comp A1	60320	MGZD209	124.0	125.0	1.0	D47616	1.76	0.22	0.22	0.39
Comp A1	60320	MGZD271	64.0	64.7	0.7	D71582	1.21	0.44	0.31	0.53
Comp A1	60320	MGZD271	100.3	101.0	0.7	D71629	1.13	0.39	0.27	0.44
Comp A1	60320	MGZD273	47.9	48.6	0.7	D72110	1.23	0.18	0.13	0.22
Comp A1	60360	MGZD005	166.0	167.0	1.0	D00377	1.03	0.14	0.14	0.14
Comp A1	60360	MGZD016	141.4	142.1	0.7	D01220	0.94	0.42	0.29	0.39
Comp A1	60360	MGZD040	104.0	105.0	1.0	D03338	1.07	0.26	0.26	0.28
Comp A1	60400	MGZD010	84.0	85.0	1.0	D08352	1.14	0.22	0.22	0.25
Comp A1	60400	MGZD010	85.0	86.0	1.0	D08353	1.06	0.24	0.24	0.25
Comp A1	60400	MGZD039	160.0	160.7	0.7	D03241	1.12	0.33	0.23	0.37
Comp A1	60400	MGZD039	247.1	247.8	0.7	D03312	0.72	0.43	0.30	0.31
Comp A1	60400	MGZD101	241.8	242.5	0.7	D16003	1.04	0.32	0.22	0.33
Comp A1	60400	MGZD254	256.7	257.4	0.7	D66100	1.44	0.42	0.29	0.60
Comp A1	60400	MGZD254	258.8	259.5	0.7	D66103	1.26	0.11	0.08	0.14
Comp A1	60400	MGZD254	259.5	260.2	0.7	D66104	1.2	0.37	0.26	0.44
Comp A2	60240	MGZD189	61.4	62.1	0.7	D42668	1.04	0.57	0.40	0.59
Comp A2	60240	MGZD198	136.7	137.4	0.7	D45283	1.1	0.56	0.39	0.62
Comp A2	60240	MGZD199	48.0	49.0	1.0	D48474	1.59	0.69	0.69	1.10
Comp A2	60240	MGZD199	163.1	164.0	0.9	D48604	1.62	0.79	0.71	1.29
Comp A2	60240	MGZD214	2.0	3.0	1.0	D49990	0.97	0.74	0.74	0.72
Comp A2	60240	MGZD247	38.0	39.0	1.0	D64009	1.46	0.59	0.59	0.86
Comp A2	60240	MGZD255	51.0	52.0	1.0	D66222	1.92	0.56	0.56	1.08
Comp A2	60240	MGZD255	55.0	56.0	1.0	D66226	1.87	0.73	0.73	1.37
Comp A2	60280	MGZD200	102.8	103.5	0.7	D45789	1.12	0.56	0.39	0.63
Comp A2	60280	MGZD200	186.0	187.0	1.0	D45883	1.64	0.64	0.64	1.04
Comp A2	60280	MGZD217	124.0	125.0	1.0	D51099	1.66	0.75	0.75	1.25
Comp A2	60280	MGZD217	125.0	126.0	1.0	D51100	1	0.52	0.52	0.52

A ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp A2	60280	MGZD217	130.0	131.0	1.0	D51106	1.75	0.53	0.53	0.93
Comp A2	60280	MGZD282	81.0	82.0	1.0	D75877	1.62	0.68	0.68	1.10
Comp A2	60320	MGZD009	90.0	90.7	0.7	D00724	0.84	0.61	0.43	0.51
Comp A2	60320	MGZD014	26.0	27.0	1.0	D01375	1.87	0.58	0.58	1.08
Comp A2	60320	MGZD017	88.0	89.0	1.0	D01334	0.88	0.62	0.62	0.55
Comp A2	60320	MGZD017	89.0	90.0	1.0	D01335	1.23	0.69	0.69	0.85
Comp A2	60320	MGZD017	90.0	91.0	1.0	D01336	1.14	0.71	0.71	0.81
Comp A2	60320	MGZD017	92.0	93.0	1.0	D01338	1.1	0.74	0.74	0.81
Comp A2	60320	MGZD017	93.0	94.0	1.0	D01339	1.31	0.68	0.68	0.89
Comp A2	60320	MGZD123	24.0	25.0	1.0	D21963	1.04	0.70	0.70	0.73
Comp A2	60320	MGZD123	100.1	100.8	0.7	D22052	0.77	0.71	0.50	0.55
Comp A2	60320	MGZD209	125.0	126.0	1.0	D47617	1.9	0.67	0.67	1.27
Comp A2	60320	MGZD271	62.0	63.0	1.0	D71580	1.99	0.56	0.56	1.11
Comp A2	60320	MGZD271	63.0	64.0	1.0	D71581	1.91	0.77	0.77	1.47
Comp A2	60320	MGZD271	101.0	101.7	0.7	D71630	1.04	0.55	0.39	0.57
Comp A2	60320	MGZD273	43.0	43.7	0.7	D72103	1.35	0.68	0.48	0.92
Comp A2	60320	MGZD273	43.7	44.4	0.7	D72104	1.24	0.58	0.41	0.72
Comp A2	60320	MGZD273	47.2	47.9	0.7	D72109	1.19	0.76	0.53	0.90
Comp A2	60320	MGZD273	48.6	49.3	0.7	D72111	1.07	0.57	0.40	0.61
Comp A2	60360	MGZD015	208.0	209.0	1.0	D01178	1.09	0.65	0.65	0.71
Comp A2	60360	MGZD016	140.0	140.7	0.7	D01218	0.67	0.71	0.50	0.48
Comp A2	60360	MGZD016	143.0	144.0	1.0	D01223	1.42	0.57	0.57	0.81
Comp A2	60360	MGZD040	105.0	106.0	1.0	D03339	1.04	0.50	0.50	0.52
Comp A2	60360	MGZD040	106.7	107.4	0.7	D03341	0.75	0.62	0.43	0.47
Comp A2	60360	MGZD207	141.9	142.6	0.7	D47289	0.56	0.60	0.42	0.34
Comp A2	60360	MGZD207	144.7	145.4	0.7	D47293	0.87	0.51	0.36	0.44
Comp A2	60360	MGZD215	228.9	229.6	0.7	D50580	0.89	0.78	0.55	0.69
Comp A2	60400	MGZD010	82.0	83.0	1.0	D08350	1.03	0.75	0.75	0.77
Comp A2	60400	MGZD038	219.0	219.7	0.7	D03173	0.8	0.57	0.40	0.46
Comp A2	60400	MGZD039	235.4	236.1	0.7	D03299	0.78	0.53	0.37	0.41
Comp A2	60400	MGZD039	236.1	237.0	0.9	D03300	1.15	0.56	0.50	0.64
Comp A2	60400	MGZD087	209.8	210.5	0.7	D10924	0.82	0.72	0.50	0.59
Comp A2	60400	MGZD254	157.0	158.0	1.0	D65984	1.78	0.78	0.78	1.39
Comp A2	60400	MGZD254	187.1	187.8	0.7	D66019	1.11	0.68	0.48	0.75
Comp A3	60240	MGZD195	74.4	75.1	0.7	D44667	1.07	0.81	0.57	0.87
Comp A3	60240	MGZD199	46.0	47.0	1.0	D48472	1.63	1.17	1.17	1.91
Comp A3	60240	MGZD214	0.0	1.0	1.0	D49988	1.67	0.83	0.83	1.38
Comp A3	60240	MGZD221	1.0	2.0	1.0	D52284	0.43	0.85	0.85	0.37
Comp A3	60240	MGZD270	85.0	86.0	1.0	D72322	1.81	1.17	1.17	2.12
Comp A3	60240	MGZD289	44.4	45.1	0.7	D78437	1.35	1.01	0.71	1.36
Comp A3	60280	MGZD155	66.5	67.2	0.7	D33566	0.89	1.07	0.75	0.95
Comp A3	60280	MGZD200	101.4	102.1	0.7	D45787	1.07	0.95	0.66	1.02
Comp A3	60280	MGZD213	216.0	217.0	1.0	D49943	1.84	1.08	1.08	1.99
Comp A3	60280	MGZD213	219.0	220.0	1.0	D49947	1.56	0.99	0.99	1.54
Comp A3	60280	MGZD223	50.0	51.0	1.0	D53907	1.47	0.93	0.93	1.37
Comp A3	60280	MGZD223	51.0	52.0	1.0	D53908	1.55	0.94	0.94	1.46
Comp A3	60280	MGZD282	78.0	79.0	1.0	D75873	1.62	0.93	0.93	1.51
Comp A3	60320	MGZD008	20.0	21.0	1.0	D01886	0.98	1.00	1.00	0.98
Comp A3	60320	MGZD008	56.0	57.0	1.0	D01927	1.18	0.91	0.91	1.07
Comp A3	60320	MGZD008	57.0	58.0	1.0	D01928	1.2	0.84	0.84	1.01
Comp A3	60320	MGZD009	64.0	65.0	1.0	D01979	1.23	0.80	0.80	0.98
Comp A3	60320	MGZD014	29.0	30.0	1.0	D01379	1.11	0.98	0.98	1.09
Comp A3	60320	MGZD014	30.0	31.0	1.0	D01380	1.26	1.17	1.17	1.47
Comp A3	60320	MGZD014	43.0	44.0	1.0	D02075	1.2	1.03	1.03	1.24
Comp A3	60320	MGZD014	44.0	45.0	1.0	D02076	1.2	1.04	1.04	1.25
Comp A3	60320	MGZD014	61.0	62.0	1.0	D01388	1.27	0.87	0.87	1.10
Comp A3	60320	MGZD014	170.0	171.0	1.0	D03541	1.37	1.19	1.19	1.63
Comp A3	60320	MGZD083	261.0	262.0	1.0	D09772	1.27	0.88	0.88	1.12

A ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp A3	60320	MGZD123	40.7	41.4	0.7	D21984	0.86	0.86	0.60	0.74
Comp A3	60320	MGZD126	36.0	37.0	1.0	D23891	1.29	1.01	1.01	1.30
Comp A3	60320	MGZD209	121.0	122.0	1.0	D47613	1.62	0.94	0.94	1.52
Comp A3	60320	MGZD209	122.0	123.0	1.0	D47614	1.46	1.07	1.07	1.57
Comp A3	60320	MGZD209	123.0	124.0	1.0	D47615	1.54	0.96	0.96	1.48
Comp A3	60320	MGZD261	120.8	121.5	0.7	D68022	1.34	1.04	0.73	1.39
Comp A3	60320	MGZD273	0.0	1.0	1.0	D72053	1.2	0.94	0.94	1.13
Comp A3	60320	MGZD273	44.4	45.1	0.7	D72105	1.31	0.81	0.57	1.06
Comp A3	60320	MGZD273	45.1	45.8	0.7	D72106	1.34	1.01	0.71	1.35
Comp A3	60320	MGZD273	56.3	57.0	0.7	D72124	1.21	1.18	0.83	1.43
Comp A3	60320	MGZD290	233.0	234.0	1.0	D78829	1.55	1.15	1.15	1.78
Comp A3	60360	MGZD015	153.0	154.0	1.0	D01116	1.26	1.09	1.09	1.37
Comp A3	60360	MGZD015	185.0	186.0	1.0	D01152	1.17	1.10	1.10	1.29
Comp A3	60360	MGZD016	140.7	141.4	0.7	D01219	0.91	0.81	0.57	0.74
Comp A3	60360	MGZD016	142.1	143.0	0.9	D01222	1.19	1.04	0.94	1.24
Comp A3	60360	MGZD016	170.0	171.0	1.0	D01229	1.14	1.11	1.11	1.27
Comp A3	60360	MGZD040	113.4	114.1	0.7	D03352	0.73	1.17	0.82	0.85
Comp A3	60360	MGZD040	135.2	135.9	0.7	D03379	0.65	1.00	0.70	0.65
Comp A3	60360	MGZD207	124.3	125.0	0.7	D47261	0.86	0.93	0.65	0.80
Comp A3	60360	MGZD207	140.5	141.2	0.7	D47287	0.57	1.06	0.74	0.60
Comp A3	60360	MGZD207	145.4	146.1	0.7	D47294	0.84	0.81	0.57	0.68
Comp A3	60360	MGZD215	225.4	226.1	0.7	D50573	0.84	1.19	0.83	1.00
Comp A3	60400	MGZD041	195.0	196.0	1.0	D05137	1.21	1.16	1.16	1.40
Comp A3	60400	MGZD087	199.0	200.0	1.0	D10909	1.25	0.81	0.81	1.01
Comp A3	60400	MGZD254	262.3	263.0	0.7	D66108	1.1	1.02	0.71	1.12
Comp A3	60400	MGZD260	176.2	177.0	0.8	D70227	0.61	1.05	0.84	0.64
Comp A4	60240	MGZD195	73.7	74.4	0.7	D44666	1	1.55	1.09	1.55
Comp A4	60240	MGZD195	116.0	117.0	1.0	D44713	1.6	1.44	1.44	2.30
Comp A4	60240	MGZD198	139.5	140.2	0.7	D45287	1.04	1.26	0.88	1.31
Comp A4	60240	MGZD199	154.0	155.0	1.0	D48592	1.81	1.24	1.24	2.24
Comp A4	60240	MGZD199	155.0	156.0	1.0	D48593	1.81	1.43	1.43	2.59
Comp A4	60240	MGZD199	161.7	162.4	0.7	D48602	1.07	1.39	0.97	1.49
Comp A4	60240	MGZD199	164.0	165.0	1.0	D48605	1.82	1.41	1.41	2.56
Comp A4	60240	MGZD247	39.0	40.0	1.0	D64010	1.64	1.47	1.47	2.41
Comp A4	60240	MGZD289	27.0	28.0	1.0	D78414	1.71	1.41	1.41	2.41
Comp A4	60280	MGZD094	221.4	222.1	0.7	D11916	0.72	1.37	0.96	0.99
Comp A4	60280	MGZD159	41.0	42.0	1.0	D34641	1.6	1.38	1.38	2.21
Comp A4	60280	MGZD200	100.7	101.4	0.7	D45786	1.07	1.56	1.09	1.67
Comp A4	60280	MGZD200	102.1	102.8	0.7	D45788	1.07	1.30	0.91	1.39
Comp A4	60280	MGZD213	55.0	56.0	1.0	D49764	1.57	1.32	1.32	2.08
Comp A4	60280	MGZD213	56.0	57.0	1.0	D49765	1.53	1.42	1.42	2.17
Comp A4	60280	MGZD217	131.0	132.0	1.0	D51107	1.75	1.21	1.21	2.11
Comp A4	60280	MGZD217	253.0	254.0	1.0	D51242	1.8	1.52	1.52	2.74
Comp A4	60280	MGZD223	44.0	45.0	1.0	D53901	1.69	1.46	1.46	2.46
Comp A4	60320	MGZD008	121.0	122.3	1.3	D00678	1.45	1.57	2.04	2.28
Comp A4	60320	MGZD009	88.8	90.0	1.2	D00723	1.4	1.40	1.68	1.96
Comp A4	60320	MGZD014	45.0	46.0	1.0	D02077	1.24	1.44	1.44	1.79
Comp A4	60320	MGZD017	94.0	95.0	1.0	D01340	1.22	1.32	1.32	1.61
Comp A4	60320	MGZD017	99.0	100.0	1.0	D01345	1.26	1.26	1.26	1.59
Comp A4	60320	MGZD123	37.0	37.7	0.7	D21979	0.82	1.21	0.85	0.99
Comp A4	60320	MGZD123	57.7	58.4	0.7	D22004	0.94	1.28	0.90	1.20
Comp A4	60320	MGZD123	102.2	102.9	0.7	D22055	0.74	1.20	0.84	0.89
Comp A4	60320	MGZD123	156.0	156.7	0.7	D22119	0.83	1.48	1.04	1.23
Comp A4	60320	MGZD126	35.0	36.0	1.0	D23890	1.26	1.53	1.53	1.93
Comp A4	60320	MGZD126	48.0	49.0	1.0	D23905	1.24	1.27	1.27	1.57
Comp A4	60320	MGZD126	69.0	70.0	1.0	D23928	1.4	1.53	1.53	2.14
Comp A4	60320	MGZD126	176.4	177.1	0.7	D24049	0.9	1.44	1.01	1.30
Comp A4	60320	MGZD126	185.0	186.0	1.0	D24059	1.19	1.27	1.27	1.51

A ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp A4	60320	MGZD271	64.7	65.4	0.7	D71583	1	1.32	0.92	1.32
Comp A4	60320	MGZD273	16.8	17.5	0.7	D72073	1.16	1.37	0.96	1.59
Comp A4	60360	MGZD015	151.0	152.0	1.0	D01114	1.23	1.28	1.28	1.57
Comp A4	60360	MGZD040	107.4	108.1	0.7	D03342	0.76	1.55	1.08	1.18
Comp A4	60360	MGZD190	128.4	129.1	0.7	D43985	0.82	1.53	1.07	1.25
Comp A4	60360	MGZD207	125.7	126.4	0.7	D47263	0.88	1.52	1.06	1.34
Comp A4	60360	MGZD210	176.8	177.5	0.7	D48383	0.74	1.32	0.92	0.98
Comp A4	60360	MGZD210	178.2	178.9	0.7	D48385	0.73	1.28	0.90	0.93
Comp A4	60360	MGZD215	224.7	225.4	0.7	D50572	0.88	1.56	1.09	1.37
Comp A4	60400	MGZD010	81.0	82.0	1.0	D08349	0.99	1.34	1.34	1.33
Comp A4	60400	MGZD039	199.0	199.7	0.7	D03251	0.92	1.41	0.99	1.30
Comp A4	60400	MGZD101	297.5	298.2	0.7	D16068	0.94	1.41	0.99	1.33
Comp A4	60400	MGZD254	258.1	258.8	0.7	D66102	1.22	1.27	0.89	1.55
Comp A4	60400	MGZD260	185.0	186.0	1.0	D70236	0.88	1.30	1.30	1.14
Comp A5	60240	MGZD198	136.0	136.7	0.7	D45282	1.17	1.67	1.17	1.95
Comp A5	60240	MGZD255	56.0	57.0	1.0	D66227	1.83	1.87	1.87	3.42
Comp A5	60280	MGZD094	120.0	121.0	1.0	D11804	1.36	1.82	1.82	2.48
Comp A5	60280	MGZD094	220.7	221.4	0.7	D11915	0.74	1.63	1.14	1.21
Comp A5	60280	MGZD155	63.0	63.7	0.7	D33561	1.13	1.66	1.16	1.88
Comp A5	60280	MGZD155	63.7	64.4	0.7	D33562	1.42	1.61	1.13	2.29
Comp A5	60280	MGZD159	51.0	51.7	0.7	D34652	1.34	1.95	1.37	2.61
Comp A5	60280	MGZD200	116.0	117.0	1.0	D45805	1.6	1.75	1.75	2.80
Comp A5	60280	MGZD200	117.0	118.0	1.0	D45806	1.73	1.81	1.81	3.13
Comp A5	60280	MGZD200	185.0	186.0	1.0	D45882	1.69	1.76	1.76	2.98
Comp A5	60280	MGZD223	49.0	50.0	1.0	D53906	1.6	1.76	1.76	2.81
Comp A5	60280	MGZD282	77.0	78.0	1.0	D75872	1.72	1.66	1.66	2.86
Comp A5	60320	MGZD008	33.0	34.0	1.0	D01901	1.12	1.73	1.73	1.94
Comp A5	60320	MGZD008	34.0	35.0	1.0	D01902	1.18	1.72	1.72	2.03
Comp A5	60320	MGZD008	66.0	67.0	1.0	D01938	1.31	1.95	1.95	2.55
Comp A5	60320	MGZD014	23.0	24.0	1.0	D01372	1.96	1.88	1.88	3.68
Comp A5	60320	MGZD014	25.0	26.0	1.0	D01374	1.96	1.83	1.83	3.59
Comp A5	60320	MGZD014	41.0	42.0	1.0	D02073	1.16	1.75	1.75	2.03
Comp A5	60320	MGZD017	87.0	88.0	1.0	D01332	1.1	1.85	1.85	2.04
Comp A5	60320	MGZD083	260.0	261.0	1.0	D09770	1.27	1.66	1.66	2.11
Comp A5	60320	MGZD126	37.0	38.0	1.0	D23892	1.26	1.82	1.82	2.29
Comp A5	60320	MGZD209	59.0	60.0	1.0	D47544	1.46	1.80	1.80	2.62
Comp A5	60320	MGZD271	99.6	100.3	0.7	D71628	1.15	1.81	1.27	2.08
Comp A5	60360	MGZD005	137.0	138.0	1.0	D00354	1.25	1.95	1.95	2.44
Comp A5	60360	MGZD015	201.0	202.0	1.0	D01170	0.99	1.60	1.60	1.58
Comp A5	60360	MGZD015	202.0	203.0	1.0	D01172	1.06	1.75	1.75	1.86
Comp A5	60360	MGZD015	207.0	208.0	1.0	D01177	1.15	1.68	1.68	1.93
Comp A5	60360	MGZD016	79.3	80.0	0.7	D01197	0.76	1.90	1.33	1.44
Comp A5	60360	MGZD016	124.0	125.0	1.0	D05310	1.19	1.68	1.68	2.00
Comp A5	60360	MGZD016	125.0	126.0	1.0	D05311	1.18	1.70	1.70	2.01
Comp A5	60360	MGZD016	237.4	238.1	0.7	D01274	0.86	1.60	1.12	1.38
Comp A5	60360	MGZD040	103.0	104.0	1.0	D03337	1.19	1.80	1.80	2.14
Comp A5	60360	MGZD040	114.1	115.0	0.9	D03353	0.92	1.60	1.44	1.47
Comp A5	60360	MGZD207	118.7	119.4	0.7	D47252	0.89	1.98	1.39	1.76
Comp A5	60360	MGZD210	171.9	172.6	0.7	D48375	0.81	1.68	1.18	1.36
Comp A5	60360	MGZD215	227.5	228.2	0.7	D50577	0.92	1.62	1.13	1.49
Comp A5	60400	MGZD038	225.0	225.7	0.7	D03181	0.69	1.97	1.38	1.36
Comp A5	60400	MGZD038	230.6	231.3	0.7	D03189	0.68	1.89	1.32	1.29
Comp A5	60400	MGZD039	234.0	234.7	0.7	D03295	0.82	1.97	1.38	1.62
Comp A5	60400	MGZD041	279.4	280.1	0.7	D04482	0.74	1.97	1.38	1.46
Comp A5	60400	MGZD101	153.0	154.0	1.0	D22904	1.02	1.74	1.74	1.77
Comp A5	60400	MGZD101	241.1	241.8	0.7	D16002	1.07	1.87	1.31	2.00
Comp A5	60400	MGZD254	256.0	256.7	0.7	D66099	1.27	1.65	1.15	2.10
Comp A5	60400	MGZD254	257.4	258.1	0.7	D66101	1.09	1.75	1.23	1.91

A ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp A5	60400	MGZD254	260.2	260.9	0.7	D66105	1.08	1.81	1.27	1.95
Comp A5	60400	MGZD254	261.6	262.3	0.7	D66107	0.98	1.87	1.31	1.83
Comp A5	60400	MGZD254	265.1	265.8	0.7	D66112	0.95	1.63	1.14	1.55
Comp A5	60400	MGZD254	269.3	270.0	0.7	D66119	1.03	1.88	1.32	1.94
Comp A6	60240	MGZD189	60.0	60.7	0.7	D42666	1.13	2.01	1.41	2.27
Comp A6	60240	MGZD193	175.0	176.0	1.0	D43752	1.55	2.39	2.39	3.70
Comp A6	60240	MGZD195	117.0	118.0	1.0	D44714	1.61	2.37	2.37	3.81
Comp A6	60240	MGZD195	119.0	120.0	1.0	D44716	1.53	2.09	2.09	3.19
Comp A6	60240	MGZD198	144.4	145.1	0.7	D45293	1.17	2.06	1.44	2.41
Comp A6	60240	MGZD270	86.0	87.0	1.0	D72323	1.86	2.12	2.12	3.94
Comp A6	60240	MGZD289	43.7	44.4	0.7	D78436	1.27	2.29	1.60	2.91
Comp A6	60280	MGZD200	123.0	124.0	1.0	D45812	1.73	2.30	2.30	3.98
Comp A6	60320	MGZD008	55.0	56.0	1.0	D01926	1.22	2.00	2.00	2.44
Comp A6	60320	MGZD008	58.0	59.0	1.0	D01929	1.46	2.08	2.08	3.04
Comp A6	60320	MGZD009	222.0	223.0	1.0	D04049	1.07	2.17	2.17	2.32
Comp A6	60320	MGZD014	42.0	43.0	1.0	D02074	1.31	2.38	2.38	3.12
Comp A6	60320	MGZD017	175.0	176.0	1.0	D16322	1.41	2.24	2.24	3.16
Comp A6	60320	MGZD083	130.0	131.0	1.0	D09628	1.33	2.00	2.00	2.66
Comp A6	60320	MGZD123	23.0	24.0	1.0	D21962	1.08	2.20	2.20	2.38
Comp A6	60320	MGZD123	41.4	42.1	0.7	D21985	0.84	2.11	1.48	1.77
Comp A6	60320	MGZD123	53.0	54.0	1.0	D21999	1.2	2.14	2.14	2.57
Comp A6	60320	MGZD123	58.4	59.1	0.7	D22005	0.96	2.36	1.65	2.27
Comp A6	60320	MGZD123	67.0	68.0	1.0	D22014	1.17	2.01	2.01	2.35
Comp A6	60320	MGZD123	77.0	78.0	1.0	D22026	1.23	2.32	2.32	2.85
Comp A6	60320	MGZD123	106.7	107.4	0.7	D22062	0.84	2.07	1.45	1.74
Comp A6	60320	MGZD123	124.0	125.0	1.0	D22082	1.27	2.15	2.15	2.73
Comp A6	60320	MGZD126	68.0	69.0	1.0	D23927	1.17	2.14	2.14	2.50
Comp A6	60320	MGZD126	138.0	139.0	1.0	D24004	1.43	2.36	2.36	3.37
Comp A6	60320	MGZD271	22.7	23.4	0.7	D71530	1.25	2.28	1.60	2.85
Comp A6	60320	MGZD273	45.8	46.5	0.7	D72107	1.22	2.33	1.63	2.84
Comp A6	60320	MGZD273	46.5	47.2	0.7	D72108	1.12	2.19	1.53	2.45
Comp A6	60320	MGZD273	49.3	50.0	0.7	D72112	1.07	2.22	1.55	2.38
Comp A6	60360	MGZD016	139.3	140.0	0.7	D01217	0.68	2.32	1.62	1.58
Comp A6	60360	MGZD040	132.4	133.1	0.7	D03375	0.7	2.07	1.45	1.45
Comp A6	60360	MGZD078	274.4	275.1	0.7	D08948	0.8	2.03	1.42	1.62
Comp A6	60360	MGZD202	268.4	269.1	0.7	D46560	0.55	2.09	1.46	1.15
Comp A6	60360	MGZD210	178.9	179.6	0.7	D48386	0.76	2.18	1.53	1.66
Comp A6	60360	MGZD215	233.1	233.8	0.7	D50586	0.9	2.19	1.53	1.97
Comp A6	60360	MGZD215	233.8	234.5	0.7	D50587	0.94	2.39	1.67	2.25
Comp A6	60400	MGZD010	83.0	84.0	1.0	D08351	1.03	2.27	2.27	2.34
Comp A6	60400	MGZD039	233.3	234.0	0.7	D03294	0.9	2.15	1.50	1.94
Comp A6	60400	MGZD254	156.0	157.0	1.0	D65983	1.64	2.31	2.31	3.79
Comp A6	60400	MGZD254	187.8	188.5	0.7	D66020	1.03	2.31	1.62	2.38
Comp A6	60400	MGZD254	263.0	263.7	0.7	D66109	1.02	2.03	1.42	2.07
Comp A6	60400	MGZD254	265.8	266.5	0.7	D66113	0.99	2.19	1.53	2.17
Comp A6	60400	MGZD254	268.6	269.3	0.7	D66117	1.14	2.03	1.42	2.31
Comp A7	60240	MGZD189	103.0	104.0	1.0	D42714	1.53	2.77	2.77	4.24
Comp A7	60240	MGZD221	205.0	206.0	1.0	D52511	1.53	2.90	2.90	4.44
Comp A7	60280	MGZD094	119.0	120.0	1.0	D11803	1.35	2.77	2.77	3.74
Comp A7	60280	MGZD155	64.4	65.1	0.7	D33563	1.23	2.57	1.80	3.16
Comp A7	60280	MGZD200	140.0	141.0	1.0	D45831	1.58	2.77	2.77	4.38
Comp A7	60320	MGZD009	158.0	159.0	1.0	D00755	1.18	2.79	2.79	3.29
Comp A7	60320	MGZD014	60.0	61.0	1.0	D01387	1.23	2.46	2.46	3.03
Comp A7	60320	MGZD014	119.0	120.0	1.0	D01417	1.25	2.95	2.95	3.69
Comp A7	60320	MGZD017	96.0	97.0	1.0	D01342	1.19	2.43	2.43	2.89
Comp A7	60320	MGZD123	100.8	101.5	0.7	D22053	0.78	2.86	2.00	2.23
Comp A7	60320	MGZD123	103.6	104.3	0.7	D22057	0.78	2.68	1.88	2.09
Comp A7	60320	MGZD123	156.7	157.4	0.7	D22120	0.75	2.57	1.80	1.93

A ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp A7	60320	MGZD271	90.6	91.3	0.7	D71616	1.17	2.97	2.08	3.47
Comp A7	60320	MGZD273	16.1	16.8	0.7	D72072	1.23	2.40	1.68	2.95
Comp A7	60320	MGZD273	76.2	76.9	0.7	D72150	0.98	2.73	1.91	2.68
Comp A7	60320	MGZD273	76.9	77.6	0.7	D72151	1.04	2.54	1.78	2.64
Comp A7	60360	MGZD007	100.0	101.0	1.0	D05579	0.9	2.43	2.43	2.19
Comp A7	60360	MGZD015	205.0	206.0	1.0	D01175	0.84	2.82	2.82	2.37
Comp A7	60360	MGZD016	217.0	218.0	1.0	D04024	1.24	2.68	2.68	3.32
Comp A7	60360	MGZD016	228.0	229.0	1.0	D01260	1.16	2.64	2.64	3.06
Comp A7	60360	MGZD016	236.7	237.4	0.7	D01272	0.84	2.81	1.97	2.36
Comp A7	60360	MGZD016	242.8	243.5	0.7	D01281	0.8	2.95	2.06	2.36
Comp A7	60360	MGZD016	243.5	244.2	0.7	D01282	0.83	2.98	2.09	2.47
Comp A7	60360	MGZD040	106.0	106.7	0.7	D03340	0.77	2.70	1.89	2.08
Comp A7	60360	MGZD040	119.0	120.0	1.0	D03359	1.13	2.71	2.71	3.06
Comp A7	60360	MGZD040	135.9	136.6	0.7	D03380	0.8	2.63	1.84	2.10
Comp A7	60360	MGZD163	124.0	125.0	1.0	D35933	1.41	2.77	2.77	3.91
Comp A7	60360	MGZD207	123.6	124.3	0.7	D47260	0.88	2.85	2.00	2.51
Comp A7	60360	MGZD207	146.1	146.8	0.7	D47295	0.78	2.72	1.90	2.12
Comp A7	60360	MGZD210	152.6	153.3	0.7	D48350	0.8	2.56	1.79	2.05
Comp A7	60360	MGZD210	153.3	154.0	0.7	D48351	0.74	2.45	1.71	1.81
Comp A7	60360	MGZD215	170.4	171.1	0.7	D50507	0.81	2.96	2.07	2.40
Comp A7	60400	MGZD010	86.0	87.0	1.0	D08354	0.99	2.83	2.83	2.80
Comp A7	60400	MGZD039	160.7	161.4	0.7	D03242	0.98	2.50	1.75	2.45
Comp A7	60400	MGZD227	297.0	298.0	1.0	D56668	1.76	2.69	2.69	4.73
Comp A7	60400	MGZD254	260.9	261.6	0.7	D66106	1.08	2.79	1.95	3.01
Comp A7	60400	MGZD260	172.7	173.4	0.7	D70222	0.63	2.77	1.94	1.75
Comp A8	60240	MGZD189	102.0	103.0	1.0	D42713	1.46	3.69	3.69	5.38
Comp A8	60280	MGZD094	89.0	90.0	1.0	D16227	1.04	3.05	3.05	3.17
Comp A8	60280	MGZD130	70.0	71.0	1.0	D26033	1.39	3.05	3.05	4.24
Comp A8	60280	MGZD155	65.1	65.8	0.7	D33564	1.1	3.35	2.35	3.69
Comp A8	60280	MGZD155	65.8	66.5	0.7	D33565	1.76	3.66	2.56	6.44
Comp A8	60280	MGZD155	67.9	68.6	0.7	D33568	1.25	3.91	2.74	4.89
Comp A8	60280	MGZD213	77.0	78.0	1.0	D49788	1.56	3.72	3.72	5.80
Comp A8	60280	MGZD217	254.0	255.0	1.0	D51243	1.72	3.16	3.16	5.44
Comp A8	60280	MGZD282	76.3	77.0	0.7	D75871	1.16	3.84	2.69	4.45
Comp A8	60320	MGZD008	69.0	70.0	1.0	D01941	1.23	3.43	3.43	4.22
Comp A8	60320	MGZD008	70.0	71.0	1.0	D01942	1.03	3.85	3.85	3.97
Comp A8	60320	MGZD009	31.0	32.0	1.0	D05625	1.04	3.98	3.98	4.14
Comp A8	60320	MGZD009	153.0	153.7	0.7	D00748	0.78	3.33	2.36	2.60
Comp A8	60320	MGZD009	216.0	217.0	1.0	D04041	1.27	3.09	3.09	3.92
Comp A8	60320	MGZD009	217.0	218.0	1.0	D04042	1.29	3.74	3.74	4.82
Comp A8	60320	MGZD017	95.0	96.0	1.0	D01341	1.24	3.00	3.00	3.72
Comp A8	60320	MGZD017	98.0	99.0	1.0	D01344	1.3	3.60	3.60	4.68
Comp A8	60320	MGZD017	223.0	224.0	1.0	D08561	1.25	3.00	3.00	3.75
Comp A8	60320	MGZD123	79.0	80.0	1.0	D22028	1.22	3.04	3.04	3.71
Comp A8	60320	MGZD126	175.7	176.4	0.7	D24048	0.76	3.00	2.10	2.28
Comp A8	60320	MGZD271	22.0	22.7	0.7	D71529	1.23	3.08	2.16	3.79
Comp A8	60320	MGZD271	24.1	24.8	0.7	D71532	1.35	3.77	2.64	5.09
Comp A8	60320	MGZD271	85.7	86.4	0.7	D71609	0.85	3.40	2.38	2.89
Comp A8	60320	MGZD273	1.0	2.0	1.0	D72054	1.45	3.52	3.52	5.10
Comp A8	60320	MGZD290	103.0	104.0	1.0	D78664	1.73	3.97	3.97	6.87
Comp A8	60360	MGZD015	200.0	201.0	1.0	D01169	1.14	3.43	3.43	3.91
Comp A8	60360	MGZD015	203.0	204.0	1.0	D01173	1.21	3.87	3.87	4.68
Comp A8	60360	MGZD015	206.0	207.0	1.0	D01176	1.08	3.15	3.15	3.40
Comp A8	60360	MGZD015	209.0	210.0	1.0	D01179	1.13	3.41	3.41	3.85
Comp A8	60360	MGZD016	80.0	80.7	0.7	D01199	0.77	3.30	2.31	2.54
Comp A8	60360	MGZD016	171.0	172.0	1.0	D01230	1.21	3.15	3.15	3.81
Comp A8	60360	MGZD016	242.1	242.8	0.7	D01280	0.83	3.91	2.74	3.25
Comp A8	60360	MGZD190	127.7	128.4	0.7	D43984	0.85	3.27	2.29	2.78

A ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp A8	60360	MGZD202	267.7	268.4	0.7	D46559	0.8	3.16	2.21	2.53
Comp A8	60360	MGZD207	119.4	120.1	0.7	D47253	0.91	3.02	2.11	2.75
Comp A8	60360	MGZD207	120.1	120.8	0.7	D47254	0.91	3.11	2.18	2.83
Comp A8	60360	MGZD207	137.0	137.7	0.7	D47282	0.79	3.06	2.14	2.42
Comp A8	60360	MGZD207	139.8	140.5	0.7	D47286	0.6	3.68	2.58	2.21
Comp A8	60360	MGZD207	142.6	143.3	0.7	D47290	0.52	3.67	2.57	1.91
Comp A8	60360	MGZD207	143.3	144.0	0.7	D47291	0.64	3.54	2.48	2.27
Comp A8	60360	MGZD210	149.1	149.8	0.7	D48344	0.8	3.03	2.12	2.42
Comp A8	60360	MGZD210	150.5	151.2	0.7	D48347	0.84	3.05	2.13	2.56
Comp A8	60360	MGZD210	171.2	171.9	0.7	D48374	0.79	3.85	2.70	3.04
Comp A8	60360	MGZD210	172.6	173.3	0.7	D48376	0.8	3.73	2.61	2.98
Comp A8	60360	MGZD210	173.3	174.0	0.7	D48377	0.77	3.48	2.44	2.68
Comp A8	60360	MGZD215	103.7	104.4	0.7	D50430	0.82	3.39	2.37	2.78
Comp A8	60360	MGZD215	104.4	105.1	0.7	D50431	0.86	3.74	2.62	3.22
Comp A8	60400	MGZD039	245.0	245.7	0.7	D03309	0.76	3.28	2.30	2.49
Comp A8	60400	MGZD039	246.4	247.1	0.7	D03311	0.82	3.02	2.11	2.48
Comp A8	60400	MGZD039	247.8	248.5	0.7	D03314	0.72	3.28	2.30	2.36
Comp A8	60400	MGZD039	248.5	249.2	0.7	D03315	0.77	3.08	2.16	2.37
Comp A8	60400	MGZD041	233.0	233.7	0.7	D04464	0.86	3.79	2.65	3.26
Comp A8	60400	MGZD041	278.0	278.7	0.7	D04480	0.81	3.12	2.18	2.53
Comp A8	60400	MGZD041	278.7	279.4	0.7	D04481	0.8	3.46	2.42	2.77
Comp A8	60400	MGZD087	208.4	209.1	0.7	D10922	0.85	3.53	2.47	3.00
Comp A8	60400	MGZD087	209.1	209.8	0.7	D10923	0.83	3.14	2.20	2.61
Comp A8	60400	MGZD254	266.5	267.2	0.7	D66114	1.05	3.09	2.16	3.24
Comp A8	60400	MGZD260	172.0	172.7	0.7	D70220	0.66	3.31	2.32	2.18
Comp A8	60400	MGZD260	286.0	286.7	0.7	D70353	0.58	3.97	2.78	2.30
Comp A9	60240	MGZD199	161.0	161.7	0.7	D48601	1.19	4.97	3.48	5.92
Comp A9	60280	MGZD155	67.2	67.9	0.7	D33567	1.18	5.18	3.63	6.11
Comp A9	60280	MGZD159	67.7	68.4	0.7	D34672	1.31	4.12	2.88	5.40
Comp A9	60320	MGZD008	120.3	121.0	0.7	D00677	0.94	4.56	3.28	4.29
Comp A9	60320	MGZD009	63.0	64.0	1.0	D01977	1.29	5.60	5.60	7.22
Comp A9	60320	MGZD017	97.0	98.0	1.0	D01343	1.19	4.98	4.98	5.93
Comp A9	60320	MGZD123	25.0	25.7	0.7	D21964	0.77	5.02	3.51	3.87
Comp A9	60320	MGZD123	102.9	103.6	0.7	D22056	0.79	5.70	3.99	4.50
Comp A9	60320	MGZD126	156.1	156.8	0.7	D24025	0.93	5.07	3.55	4.72
Comp A9	60320	MGZD209	58.0	59.0	1.0	D47543	1.41	5.77	5.77	8.13
Comp A9	60320	MGZD271	85.0	85.7	0.7	D71608	1.02	4.10	2.87	4.18
Comp A9	60320	MGZD271	98.9	99.6	0.7	D71627	0.95	5.13	3.59	4.87
Comp A9	60320	MGZD271	101.7	102.4	0.7	D71631	1.15	4.30	3.01	4.95
Comp A9	60320	MGZD271	113.0	114.0	1.0	D71645	1.52	5.15	5.15	7.83
Comp A9	60320	MGZD290	40.0	41.0	1.0	D78583	1.41	4.51	4.51	6.36
Comp A9	60320	MGZD290	214.0	215.0	1.0	D78806	1.64	5.82	5.82	9.54
Comp A9	60360	MGZD005	128.0	129.0	1.0	D00346	1.37	4.40	4.40	6.03
Comp A9	60360	MGZD005	138.0	138.7	0.7	D00355	0.71	5.42	3.79	3.85
Comp A9	60360	MGZD005	164.0	165.0	1.0	D00374	0.98	5.21	5.21	5.11
Comp A9	60360	MGZD005	165.0	166.0	1.0	D00376	0.95	5.86	5.86	5.57
Comp A9	60360	MGZD015	152.0	153.0	1.0	D01115	1.1	5.06	5.06	5.57
Comp A9	60360	MGZD015	186.0	187.0	1.0	D01154	1.14	5.60	5.60	6.38
Comp A9	60360	MGZD015	204.0	205.0	1.0	D01174	1.06	5.20	5.20	5.51
Comp A9	60360	MGZD015	216.0	217.0	1.0	D01187	1.17	4.67	4.67	5.46
Comp A9	60360	MGZD016	240.7	241.4	0.7	D01278	0.81	5.25	3.68	4.25
Comp A9	60360	MGZD040	108.1	108.8	0.7	D03344	0.71	5.56	3.89	3.95
Comp A9	60360	MGZD202	269.1	269.8	0.7	D46561	0.72	4.47	3.13	3.22
Comp A9	60360	MGZD207	144.0	144.7	0.7	D47292	0.45	4.31	3.02	1.94
Comp A9	60360	MGZD215	103.0	103.7	0.7	D50429	0.81	5.50	3.85	4.46
Comp A9	60360	MGZD215	224.0	224.7	0.7	D50570	0.83	4.29	3.00	3.56
Comp A9	60360	MGZD215	229.6	230.3	0.7	D50581	0.97	5.12	3.58	4.97
Comp A9	60360	MGZD215	238.7	239.4	0.7	D50594	0.88	4.72	3.30	4.15

A ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp A9	60400	MGZD038	229.9	230.6	0.7	D03188	0.67	5.62	3.93	3.77
Comp A9	60400	MGZD038	231.3	232.0	0.7	D03190	0.81	4.71	3.30	3.82
Comp A9	60400	MGZD039	199.7	200.4	0.7	D03252	0.78	5.41	3.79	4.22
Comp A9	60400	MGZD039	245.7	246.4	0.7	D03310	0.76	5.60	3.92	4.26
Comp A9	60400	MGZD087	210.5	211.2	0.7	D10925	0.85	4.49	3.14	3.82
Comp A9	60400	MGZD101	298.2	298.9	0.7	D16069	0.91	4.11	2.88	3.74
Comp A9	60400	MGZD254	263.7	264.4	0.7	D66110	0.91	5.71	4.00	5.20
Comp A10	60320	MGZD008	62.0	63.0	1.0	D01934	1.14	6.70	6.70	7.64
Comp A10	60320	MGZD008	136.0	136.7	0.7	D00694	0.83	7.27	5.09	6.03
Comp A10	60320	MGZD014	160.0	161.0	1.0	D03530	1.2	7.55	7.55	9.06
Comp A10	60320	MGZD017	222.0	223.0	1.0	D08560	1.18	6.85	6.85	8.08
Comp A10	60320	MGZD126	154.0	154.7	0.7	D24022	0.87	7.85	5.49	6.83
Comp A10	60320	MGZD271	91.3	92.0	0.7	D71617	1.31	6.09	4.26	7.98
Comp A10	60320	MGZD271	102.4	103.1	0.7	D71632	1.12	6.54	4.58	7.32
Comp A10	60320	MGZD273	17.5	18.2	0.7	D72074	1.02	7.29	5.10	7.44
Comp A10	60360	MGZD040	212.7	213.4	0.7	D03423	0.9	7.35	5.15	6.62
Comp A10	60360	MGZD078	143.0	144.0	1.0	D16807	1.04	7.30	7.30	7.59
Comp A10	60360	MGZD078	144.0	145.0	1.0	D16808	0.96	7.59	7.59	7.29
Comp A10	60360	MGZD210	167.7	168.4	0.7	D48368	0.79	6.85	4.80	5.41
Comp A10	60360	MGZD215	217.7	218.4	0.7	D50561	0.75	6.05	4.24	4.54
Comp A10	60400	MGZD039	237.0	238.0	1.0	D03301	1.18	6.10	6.10	7.20
Comp A10	60400	MGZD087	211.2	212.0	0.8	D10926	0.97	6.96	5.57	6.75
Comp A10	60400	MGZD089	209.4	210.1	0.7	D11193	0.79	7.63	5.34	6.03
Comp A10	60400	MGZD101	263.0	263.7	0.7	D16028	0.78	7.08	4.96	5.52
Comp A10	60400	MGZD254	264.4	265.1	0.7	D66111	0.95	7.91	5.54	7.51
Comp A10	60400	MGZD254	267.2	267.9	0.7	D66115	0.97	7.03	4.92	6.82
Comp A10	60400	MGZD260	186.0	187.0	1.0	D70237	0.87	6.09	6.09	5.30
Comp A11	60240	MGZD195	100.0	101.0	1.0	D44695	1.6	10.00	10.00	16.00
Comp A11	60240	MGZD195	118.0	119.0	1.0	D44715	1.53	8.62	8.62	13.18
Comp A11	60240	MGZD198	138.8	139.5	0.7	D45286	1.12	8.00	5.60	8.96
Comp A11	60280	MGZD159	67.0	67.7	0.7	D34670	1.26	8.60	6.02	10.84
Comp A11	60320	MGZD009	176.0	176.7	0.7	D00775	0.78	9.81	6.87	7.65
Comp A11	60320	MGZD009	226.0	226.7	0.7	D09454	0.8	8.59	6.01	6.87
Comp A11	60320	MGZD123	98.7	99.4	0.7	D22050	0.78	8.90	6.23	6.94
Comp A11	60320	MGZD123	101.5	102.2	0.7	D22054	0.7	8.08	5.66	5.66
Comp A11	60320	MGZD271	23.4	24.1	0.7	D71531	1.19	10.30	7.21	12.26
Comp A11	60320	MGZD271	66.1	66.8	0.7	D71585	1.1	8.80	6.16	9.68
Comp A11	60320	MGZD273	55.6	56.3	0.7	D72123	1.3	9.10	6.37	11.83
Comp A11	60320	MGZD273	85.0	86.0	1.0	D72161	1.85	8.00	8.00	14.80
Comp A11	60360	MGZD005	162.0	163.0	1.0	D00372	0.99	10.50	10.50	10.40
Comp A11	60360	MGZD016	130.0	130.7	0.7	D01206	0.84	8.76	6.13	7.36
Comp A11	60360	MGZD207	132.8	133.5	0.7	D47274	0.76	8.26	5.78	6.28
Comp A11	60360	MGZD207	134.9	135.6	0.7	D47279	0.78	9.84	6.89	7.68
Comp A11	60360	MGZD207	141.2	141.9	0.7	D47288	0.57	10.00	7.00	5.70
Comp A11	60360	MGZD210	179.6	180.3	0.7	D48387	0.85	11.80	8.26	10.03
Comp A11	60360	MGZD215	226.1	226.8	0.7	D50574	0.9	9.97	6.98	8.97
Comp A11	60400	MGZD038	219.7	220.4	0.7	D03174	0.77	8.41	5.89	6.48
Comp A11	60400	MGZD038	225.7	226.4	0.7	D03182	0.8	10.10	7.07	8.08
Comp A11	60400	MGZD039	234.7	235.4	0.7	D03297	0.8	9.24	6.47	7.39
Comp A11	60400	MGZD087	198.0	199.0	1.0	D10908	1.27	9.96	9.96	12.65
Comp A11	60400	MGZD101	242.5	243.2	0.7	D16004	1.02	8.78	6.15	8.96
Comp A11	60400	MGZD254	267.9	268.6	0.7	D66116	1.16	11.60	8.12	13.46
Comp A12	60240	MGZD198	143.7	144.4	0.7	D45292	1.02	21.70	15.19	22.13
Comp A12	60320	MGZD008	92.4	93.6	1.2	D00647	1.6	15.60	19.19	24.96
Comp A12	60320	MGZD009	176.7	177.7	1.0	D00776	1.24	22.40	22.40	27.78
Comp A12	60320	MGZD123	57.0	57.7	0.7	D22003	0.94	19.20	13.44	18.05
Comp A12	60320	MGZD123	76.0	77.0	1.0	D22025	1.19	12.40	12.40	14.76
Comp A12	60320	MGZD123	99.4	100.1	0.7	D22051	0.81	19.50	13.65	15.80

A ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp A12	60320	MGZD209	109.0	110.0	1.0	D47601	1.48	19.30	19.30	28.56
Comp A12	60320	MGZD273	15.4	16.1	0.7	D72070	1.23	15.10	10.57	18.57
Comp A12	60360	MGZD005	167.0	168.0	1.0	D00378	1.12	12.40	12.40	13.89
Comp A12	60360	MGZD016	135.0	136.0	1.0	D01212	1.29	22.60	22.60	29.15
Comp A12	60360	MGZD040	214.1	214.8	0.7	D03425	0.93	23.70	16.59	22.04
Comp A12	60360	MGZD207	125.0	125.7	0.7	D47262	0.87	21.60	15.12	18.79
Comp A12	60360	MGZD207	132.1	132.8	0.7	D47273	0.79	20.90	14.63	16.51
Comp A12	60360	MGZD207	146.8	147.5	0.7	D47297	0.96	16.90	11.83	16.22
Comp A12	60360	MGZD210	176.1	176.8	0.7	D48382	0.78	16.80	11.76	13.10
Comp A12	60360	MGZD210	177.5	178.2	0.7	D48384	0.75	13.00	9.10	9.75
Comp A12	60400	MGZD089	208.7	209.4	0.7	D11192	0.66	14.60	10.22	9.64
Comp A12	60400	MGZD101	152.0	153.0	1.0	D22903	1.15	14.60	14.60	16.79
Comp A12	60400	MGZD101	298.9	299.6	0.7	D16070	0.87	13.60	9.52	11.83
Comp A12	60400	MGZD227	283.0	284.0	1.0	D56653	1.62	20.40	20.40	33.05
Comp A12	60400	MGZD254	270.0	270.7	0.7	D66120	1.12	15.60	10.92	17.47
Comp A12	60400	MGZD260	175.5	176.2	0.7	D70226	0.68	16.90	11.83	11.49
Comp A12	60400	MGZD260	255.7	256.4	0.7	D70316	0.71	16.10	11.27	11.43
Comp A13	60240	MGZD214	192.0	193.0	1.0	D50203	1.81	51.40	51.40	93.03
Comp A13	60320	MGZD126	154.7	155.4	0.7	D24023	0.82	39.40	27.58	32.31
Comp A13	60320	MGZD209	110.0	111.0	1.0	D47602	1.48	45.50	45.50	67.34
Comp A13	60320	MGZD271	21.3	22.0	0.7	D71528	1.17	36.00	25.20	42.12
Comp A13	60360	MGZD005	135.4	137.0	1.6	D00353	0.76	25.00	40.00	19.00
Comp A13	60360	MGZD005	163.0	164.0	1.0	D00373	1.04	38.10	38.10	39.62
Comp A13	60360	MGZD016	241.4	242.1	0.7	D01279	0.82	26.40	18.48	21.65
Comp A13	60360	MGZD040	108.8	109.5	0.7	D03345	0.76	28.10	19.67	21.36
Comp A13	60360	MGZD040	213.4	214.1	0.7	D03424	0.94	75.50	52.85	70.97
Comp A13	60360	MGZD163	257.0	258.0	1.0	D36081	1.76	89.60	89.60	157.70
Comp A13	60360	MGZD190	265.0	266.0	1.0	D44136	1.07	33.80	33.80	36.17
Comp A13	60360	MGZD202	137.0	138.0	1.0	D46412	1.08	41.20	41.20	44.50
Comp A13	60360	MGZD202	138.0	139.0	1.0	D46413	1.09	32.70	32.70	35.64
Comp A13	60360	MGZD210	149.8	150.5	0.7	D48345	0.37	25.60	17.92	9.47
Comp A13	60360	MGZD215	228.2	228.9	0.7	D50579	0.85	32.40	22.68	27.54
Comp A13	60400	MGZD041	196.0	197.0	1.0	D05138	1.2	28.60	28.60	34.32
Comp A13	60400	MGZD101	296.8	297.5	0.7	D16067	0.89	32.30	22.61	28.75

B ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp B21	60440	MGZD002	256	257	1.0	D00206	1.29	0.32	0.32	0.4128
Comp B21	60440	MGZD002	260	261	1.0	D00211	1.18	0.28	0.28	0.3304
Comp B21	60440	MGZD086	223	224	1.0	D10362	1.22	0.08	0.08	0.0976
Comp B21	60440	MGZD132	290	290.7	0.7	D27407	1.07	0.19	0.133	0.2033
Comp B21	60440	MGZD144	154.2	154.9	0.7	D30392	1.44	0.24	0.168	0.3456
Comp B21	60440	MGZD152	88	89	1.0	D32050	1.59	0.32	0.32	0.5088
Comp B21	60440	MGZD152	89	90	1.0	D32051	1.79	0.35	0.35	0.6265
Comp B21	60440	MGZD152	103.1	103.8	0.7	D32068	0.89	0.3	0.21	0.267
Comp B21	60440	MGZD201	184.4	185.1	0.7	D45517	0.75	0.36	0.252	0.27
Comp B21	60480	MGZD011	138	139	1.0	D00806	1.2	0.25	0.25	0.3
Comp B21	60480	MGZD011	169	170	1.0	D00842	1.09	0.06	0.06	0.0654
Comp B21	60480	MGZD011	170	170.6	0.6	D00843	0.65	0.09	0.054	0.0585
Comp B21	60480	MGZD011	173.3	174.3	1.0	D00848	1	0.07	0.07	0.07
Comp B21	60480	MGZD011	177	177.7	0.7	D00852	0.81	0.13	0.091	0.1053
Comp B21	60480	MGZD012	218	219	1.0	D01049	1.16	0.04	0.04	0.0464
Comp B21	60480	MGZD012	221	222	1.0	D01052	1.26	0.08	0.08	0.1008
Comp B21	60480	MGZD012	222	223	1.0	D01053	1.25	0.03	0.03	0.0375
Comp B21	60480	MGZD096	152	153	1.0	D12308	1.05	0.38	0.38	0.399
Comp B21	60480	MGZD096	178.4	179.1	0.7	D12342	0.71	0.31	0.217	0.2201
Comp B21	60480	MGZD096	179.1	179.8	0.7	D12343	0.69	0.22	0.154	0.1518
Comp B21	60480	MGZD128	241.1	241.8	0.7	D25905	0.73	0.38	0.266	0.2774
Comp B21	60480	MGZD131	130	131	1.0	D26868	1.06	0.37	0.37	0.3922
Comp B21	60480	MGZD131	201.1	201.8	0.7	D26950	0.8	0.06	0.042	0.048
Comp B21	60480	MGZD172	42.6	43.3	0.7	D38426	1.07	0.3	0.21	0.321
Comp B21	60480	MGZD172	58.8	59.5	0.7	D38449	1.17	0.2	0.14	0.234
Comp B21	60480	MGZD172	59.5	60.2	0.7	D38450	1.21	0.11	0.077	0.1331
Comp B21	60480	MGZD172	61.6	62.3	0.7	D38453	1.27	0.2	0.14	0.254
Comp B21	60480	MGZD222	287.9	288.6	0.7	D53809	1.02	0.249	0.1743	0.25398
Comp B21	60480	MGZD238	301.7	302.4	0.7	D60107	0.81	0.23	0.161	0.1863
Comp B21	60520	MGZD006	25	26	1.0	D23622	1.19	0.01	0.01	0.0119
Comp B21	60520	MGZD006	159.35	160.06	0.7	D00469	0.69	0.17	0.1207	0.1173
Comp B21	60520	MGZD036	204	204.7	0.7	D03081	0.76	0.13	0.091	0.0988
Comp B21	60520	MGZD036	205.7	206.7	1.0	D03083	1.12	0.08	0.08	0.0896
Comp B21	60520	MGZD098	210.2	210.9	0.7	D14941	0.9	0.19	0.133	0.171
Comp B21	60520	MGZD098	214.4	215.1	0.7	D14948	0.86	0.17	0.119	0.1462
Comp B21	60520	MGZD098	215.1	215.8	0.7	D14949	0.92	0.17	0.119	0.1564
Comp B21	60520	MGZD098	216.5	217.2	0.7	D14951	0.88	0.29	0.203	0.2552
Comp B21	60520	MGZD098	223.5	224.2	0.7	D14962	0.87	0.2	0.14	0.174
Comp B21	60520	MGZD106	37.2	37.9	0.7	D18823	0.79	0.09	0.063	0.0711
Comp B21	60520	MGZD107	232	232.7	0.7	D18724	0.77	0.36	0.252	0.2772
Comp B21	60520	MGZD107	250.9	251.6	0.7	D18753	0.93	0.21	0.147	0.1953
Comp B21	60520	MGZD134	198.5	199.2	0.7	D27931	0.86	0.15	0.105	0.129
Comp B21	60520	MGZD136	260.4	261.1	0.7	D28800	0.78	0.13	0.091	0.1014
Comp B21	60520	MGZD136	293.2	294	0.8	D28839	0.91	0.35	0.28	0.3185
Comp B21	60520	MGZD225	283.1	283.8	0.7	D55212	0.89	0.31	0.217	0.2759
Comp B21	60520	MGZD231	169	170	1.0	D56907	1.17	0.33	0.33	0.3861
Comp B21	60520	MGZD265	157.9	158.6	0.7	D69212	0.64	0.29	0.203	0.1856
Comp B21	60520	MGZD265	190.8	191.5	0.7	D69264	0.83	0.38	0.266	0.3154
Comp B21	60520	MGZD265	194.3	195	0.7	D69269	0.77	0.2	0.14	0.154
Comp B21	60560	MGZD042	233	234	1.0	D04407	1.1	0.32	0.32	0.352
Comp B21	60560	MGZD066	265	266	1.0	D06908	0.85	0.06	0.06	0.051
Comp B21	60560	MGZD099	223	224	1.0	D15852	1.22	0.23	0.23	0.2806
Comp B21	60560	MGZD224	217.4	218.1	0.7	D54797	0.76	0.06	0.042	0.0456

B ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp B21	60560	MGZD237	265	266	1.0	D59690	1.32	0.22	0.22	0.2904
Comp B21	60600	MGZD084	230.8	231.5	0.7	D10136	0.76	0.07	0.049	0.0532
Comp B21	60600	MGZD084	236	237	1.0	D10144	1.2	0.23	0.23	0.276
Comp B21	60600	MGZD084	251	252	1.0	D10161	1.17	0.33	0.33	0.3861
Comp B21	60600	MGZD088	234.9	235.6	0.7	D10594	0.84	0.07	0.049	0.0588
Comp B21	60600	MGZD088	273.1	273.8	0.7	D10642	0.78	0.09	0.063	0.0702
Comp B21	60600	MGZD090	268.5	269.2	0.7	D11447	0.82	0.32	0.224	0.2624
Comp B21	60600	MGZD267	174.4	175.1	0.7	D70592	0.83	0.39	0.273	0.3237
Comp B21	60600	MGZD267	175.8	176.5	0.7	D70594	0.86	0.08	0.056	0.0688
Comp B22	60440	MGZD086	219	220	1.0	D10357	1.21	0.46	0.46	0.5566
Comp B22	60440	MGZD144	85.5	86.2	0.7	D30312	1.08	0.89	0.623	0.9612
Comp B22	60440	MGZD149	69.8	70.5	0.7	D31176	0.88	0.68	0.476	0.5984
Comp B22	60440	MGZD149	77.5	78.2	0.7	D31188	1.02	0.69	0.483	0.7038
Comp B22	60440	MGZD149	78.2	78.9	0.7	D31189	1.15	0.58	0.406	0.667
Comp B22	60440	MGZD149	81.7	82.4	0.7	D31194	1.19	0.45	0.315	0.5355
Comp B22	60440	MGZD152	81	82	1.0	D32042	1.35	0.49	0.49	0.6615
Comp B22	60440	MGZD152	91	92	1.0	D32053	1.7	0.62	0.62	1.054
Comp B22	60440	MGZD152	103.8	104.5	0.7	D32069	1.06	0.53	0.371	0.5618
Comp B22	60440	MGZD152	115	115.7	0.7	D32087	1.05	0.64	0.448	0.672
Comp B22	60440	MGZD197	287.1	287.8	0.7	D45087	0.92	0.95	0.665	0.874
Comp B22	60440	MGZD201	187.9	188.6	0.7	D45524	0.85	0.69	0.483	0.5865
Comp B22	60440	MGZD201	191.4	192.1	0.7	D45529	0.9	0.57	0.399	0.513
Comp B22	60480	MGZD011	166	167	1.0	D00838	1.11	0.46	0.46	0.5106
Comp B22	60480	MGZD011	176.3	177	0.7	D00851	0.79	0.83	0.581	0.6557
Comp B22	60480	MGZD012	176	177	1.0	D00999	1.07	0.59	0.59	0.6313
Comp B22	60480	MGZD012	177	178	1.0	D01000	1.08	0.44	0.44	0.4752
Comp B22	60480	MGZD012	179.4	180.1	0.7	D01004	0.79	0.58	0.406	0.4582
Comp B22	60480	MGZD012	223	224	1.0	D01054	1.23	0.88	0.88	1.0824
Comp B22	60480	MGZD013	132	133	1.0	D02013	1.12	0.94	0.94	1.0528
Comp B22	60480	MGZD013	229	230	1.0	D01074	1.16	0.47	0.47	0.5452
Comp B22	60480	MGZD013	231	232	1.0	D01076	0.99	0.42	0.42	0.4158
Comp B22	60480	MGZD096	173.5	174.2	0.7	D12334	0.87	0.85	0.595	0.7395
Comp B22	60480	MGZD096	177	177.7	0.7	D12340	0.7	0.96	0.672	0.672
Comp B22	60480	MGZD096	183.3	184	0.7	D12350	0.66	0.62	0.434	0.4092
Comp B22	60480	MGZD103	143	144	1.0	D18379	1.03	0.49	0.49	0.5047
Comp B22	60480	MGZD103	178.3	179	0.7	D18420	0.9	0.96	0.672	0.864
Comp B22	60480	MGZD103	190.4	191.1	0.7	D18436	0.7	0.44	0.308	0.308
Comp B22	60480	MGZD103	209.4	210.1	0.7	D18459	0.67	0.88	0.616	0.5896
Comp B22	60480	MGZD103	220.6	221.3	0.7	D18476	0.96	0.72	0.504	0.6912
Comp B22	60480	MGZD128	239.7	240.4	0.7	D25903	0.71	0.64	0.448	0.4544
Comp B22	60480	MGZD131	127	128	1.0	D26865	1.15	0.69	0.69	0.7935
Comp B22	60480	MGZD131	129	130	1.0	D26867	0.89	0.56	0.56	0.4984
Comp B22	60480	MGZD131	131	132	1.0	D26869	1.17	0.55	0.55	0.6435
Comp B22	60480	MGZD131	209	210	1.0	D26960	1.33	0.47	0.47	0.6251
Comp B22	60480	MGZD131	271.7	272.4	0.7	D27030	0.74	0.49	0.343	0.3626
Comp B22	60480	MGZD172	24.4	25.1	0.7	D38397	1.17	0.67	0.469	0.7839
Comp B22	60480	MGZD172	39.8	40.5	0.7	D38422	0.94	0.45	0.315	0.423
Comp B22	60480	MGZD172	40.5	41.2	0.7	D38423	1.03	0.87	0.609	0.8961
Comp B22	60480	MGZD211	235.7	236.4	0.7	D48937	0.86	0.95	0.665	0.817
Comp B22	60480	MGZD211	237.8	238.5	0.7	D48941	0.77	0.64	0.448	0.4928
Comp B22	60480	MGZD216	123	124	1.0	D50740	0.98	0.576	0.576	0.56448
Comp B22	60480	MGZD216	124	125	1.0	D50741	1.02	0.972	0.972	0.99144
Comp B22	60480	MGZD216	126	127	1.0	D50743	1.02	0.744	0.744	0.75888
Comp B22	60480	MGZD216	127	128	1.0	D50744	0.97	0.648	0.648	0.62856
Comp B22	60480	MGZD216	128	129	1.0	D50745	1.06	0.414	0.414	0.43884
Comp B22	60480	MGZD222	211.4	212.1	0.7	D53715	0.91	0.509	0.3563	0.46319

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Comp B22	60480	MGZD222	215	216	1.0	D53722	1.09	0.628	0.628	0.68452
Comp B22	60480	MGZD222	287.2	287.9	0.7	D53808	1.05	0.494	0.3458	0.5187
Comp B22	60480	MGZD230	260.4	261.1	0.7	D57769	0.74	0.96	0.672	0.7104
Comp B22	60480	MGZD230	262.5	263.2	0.7	D57773	0.79	0.77	0.539	0.6083
Comp B22	60520	MGZD035	138	139	1.0	D13822	1.12	0.89	0.89	0.9968
Comp B22	60520	MGZD035	204.1	205	0.9	D03004	1.02	0.59	0.531	0.6018
Comp B22	60520	MGZD035	213	214	1.0	D03017	1.14	0.51	0.51	0.5814
Comp B22	60520	MGZD036	223	224	1.0	D03104	1.15	0.8	0.8	0.92
Comp B22	60520	MGZD082	144	145	1.0	D22715	1.15	0.92	0.92	1.058
Comp B22	60520	MGZD098	252.9	253.6	0.7	D15008	0.7	0.48	0.336	0.336
Comp B22	60520	MGZD106	34.4	35.1	0.7	D18817	0.76	0.89	0.623	0.6764
Comp B22	60520	MGZD106	36.5	37.2	0.7	D18822	0.86	0.67	0.469	0.5762
Comp B22	60520	MGZD107	232.7	233.4	0.7	D18725	0.8	0.59	0.413	0.472
Comp B22	60520	MGZD134	197.1	197.8	0.7	D27929	0.79	0.99	0.693	0.7821
Comp B22	60520	MGZD134	199.2	199.9	0.7	D27932	0.81	0.62	0.434	0.5022
Comp B22	60520	MGZD134	222.3	223	0.7	D27964	0.86	0.81	0.567	0.6966
Comp B22	60520	MGZD136	197	198	1.0	D28725	1.36	0.84	0.84	1.1424
Comp B22	60520	MGZD136	237.9	238.6	0.7	D28772	0.85	0.54	0.378	0.459
Comp B22	60520	MGZD265	176.1	176.8	0.7	D69241	0.72	0.55	0.385	0.396
Comp B22	60520	MGZD265	178.2	178.9	0.7	D69244	0.73	0.71	0.497	0.5183
Comp B22	60520	MGZD265	183.1	183.8	0.7	D69252	0.71	0.43	0.301	0.3053
Comp B22	60520	MGZD265	186.6	187.3	0.7	D69257	0.7	0.6	0.42	0.42
Comp B22	60520	MGZD265	195	195.7	0.7	D69270	0.72	0.55	0.385	0.396
Comp B22	60560	MGZD042	185	186	1.0	D04345	1.24	0.74	0.74	0.9176
Comp B22	60560	MGZD042	234	235	1.0	D04409	1.09	0.7	0.7	0.763
Comp B22	60560	MGZD042	235	236	1.0	D04410	1.01	0.56	0.56	0.5656
Comp B22	60560	MGZD042	236	237	1.0	D04411	1.04	0.76	0.76	0.7904
Comp B22	60560	MGZD044	262.1	262.8	0.7	D04512	0.67	0.9	0.63	0.603
Comp B22	60560	MGZD064	257.7	258.4	0.7	D06728	0.75	0.68	0.476	0.51
Comp B22	60560	MGZD066	260	261	1.0	D06903	1.18	0.46	0.46	0.5428
Comp B22	60560	MGZD066	285	286	1.0	D06931	1.35	0.65	0.65	0.8775
Comp B22	60560	MGZD133	231.7	232.4	0.7	D27709	0.75	0.75	0.525	0.5625
Comp B22	60560	MGZD135	144.9	145.6	0.7	D28270	0.61	0.67	0.469	0.4087
Comp B22	60560	MGZD224	206	207	1.0	D54784	1.09	0.52	0.52	0.5668
Comp B22	60560	MGZD224	255.1	256	0.9	D54841	1.12	0.8	0.72	0.896
Comp B22	60560	MGZD232	205.7	206.4	0.7	D57308	0.89	0.98	0.686	0.8722
Comp B22	60600	MGZD093	225.5	226.2	0.7	D11714	0.83	0.48	0.336	0.3984
Comp B22	60600	MGZD095	143	144	1.0	D11974	0.95	0.41	0.41	0.3895
Comp B22	60600	MGZD095	162.5	163.2	0.7	D11997	0.69	0.67	0.469	0.4623
Comp B22	60600	MGZD294	266	267	1.0	D80145	1.27	0.48	0.48	0.6096
Comp B23	60440	MGZD002	266.6	267.6	1.0	D00218	1.1	1.61	1.61	1.771
Comp B23	60440	MGZD086	153.5	154.2	0.7	D10284	0.73	1.69	1.183	1.2337
Comp B23	60440	MGZD129	257.4	258.1	0.7	D26615	0.66	1.98	1.386	1.3068
Comp B23	60440	MGZD149	69.1	69.8	0.7	D31175	1.09	1.48	1.036	1.6132
Comp B23	60440	MGZD149	71.9	72.6	0.7	D31180	1.01	1.47	1.029	1.4847
Comp B23	60440	MGZD149	75.4	76.1	0.7	D31185	0.93	1.46	1.022	1.3578
Comp B23	60440	MGZD149	76.1	76.8	0.7	D31186	0.95	1.27	0.889	1.2065
Comp B23	60440	MGZD149	81	81.7	0.7	D31193	1.12	1.08	0.756	1.2096
Comp B23	60440	MGZD152	79	80	1.0	D32040	1.54	1.69	1.69	2.6026
Comp B23	60440	MGZD152	80	81	1.0	D32041	1.5	1.45	1.45	2.175
Comp B23	60440	MGZD152	84	85	1.0	D32045	1.37	1.33	1.33	1.8221
Comp B23	60440	MGZD152	85	86	1.0	D32047	1.38	1.52	1.52	2.0976
Comp B23	60440	MGZD152	95	96	1.0	D32057	1.44	1.21	1.21	1.7424
Comp B23	60440	MGZD152	101.7	102.4	0.7	D32066	1	1.92	1.344	1.92
Comp B23	60440	MGZD197	172	173	1.0	D44937	1.11	1.36	1.36	1.5096
Comp B23	60440	MGZD201	192.8	193.5	0.7	D45531	0.88	1.87	1.309	1.6456

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Comp B23	60440	MGZD245	261.8	262.5	0.7	D62885	0.76	1.76	1.232	1.3376
Comp B23	60480	MGZD011	144.8	146	1.2	D00814	1.42	1.81	2.172	2.5702
Comp B23	60480	MGZD011	168	169	1.0	D00841	1.02	1.16	1.16	1.1832
Comp B23	60480	MGZD012	171.5	172.2	0.7	D00993	0.69	1.52	1.064	1.0488
Comp B23	60480	MGZD012	174	175	1.0	D00997	1.01	1.85	1.85	1.8685
Comp B23	60480	MGZD012	180.1	180.8	0.7	D01005	0.79	1.5	1.05	1.185
Comp B23	60480	MGZD012	182.2	183	0.8	D01008	0.7	1.35	1.08	0.945
Comp B23	60480	MGZD012	196	197	1.0	D01024	1.09	1	1	1.09
Comp B23	60480	MGZD012	212	213	1.0	D01041	1.11	1.4	1.4	1.554
Comp B23	60480	MGZD012	219	220	1.0	D01050	1.24	1.28	1.28	1.5872
Comp B23	60480	MGZD013	133	134	1.0	D02014	1.1	1.83	1.83	2.013
Comp B23	60480	MGZD013	177	178	1.0	D02043	1.25	1.24	1.24	1.55
Comp B23	60480	MGZD013	230	231	1.0	D01075	1.02	1.61	1.61	1.6422
Comp B23	60480	MGZD013	232	233	1.0	D01077	1.06	1.03	1.03	1.0918
Comp B23	60480	MGZD096	141	141.7	0.7	D12292	0.73	1.14	0.798	0.8322
Comp B23	60480	MGZD096	174.2	174.9	0.7	D12335	0.7	1.69	1.183	1.183
Comp B23	60480	MGZD096	176.3	177	0.7	D12339	0.66	1.35	0.945	0.891
Comp B23	60480	MGZD096	184	184.7	0.7	D12351	0.75	1.9	1.33	1.425
Comp B23	60480	MGZD103	221.3	222	0.7	D18477	0.95	1.47	1.029	1.3965
Comp B23	60480	MGZD128	239	239.7	0.7	D25902	0.68	1.02	0.714	0.6936
Comp B23	60480	MGZD131	128	129	1.0	D26866	1.27	1.6	1.6	2.032
Comp B23	60480	MGZD131	132	133	1.0	D26870	1.1	1.59	1.59	1.749
Comp B23	60480	MGZD131	200.4	201.1	0.7	D26949	0.88	1.07	0.749	0.9416
Comp B23	60480	MGZD131	201.8	202.5	0.7	D26951	1	1.91	1.337	1.91
Comp B23	60480	MGZD131	270	271	1.0	D27028	1.18	1.93	1.93	2.2774
Comp B23	60480	MGZD131	271	271.7	0.7	D27029	0.79	1.59	1.113	1.2561
Comp B23	60480	MGZD172	25.1	25.8	0.7	D38398	1.13	1.48	1.036	1.6724
Comp B23	60480	MGZD172	27.9	28.6	0.7	D38402	1.08	1.33	0.931	1.4364
Comp B23	60480	MGZD172	35.6	36.3	0.7	D38414	0.93	1.91	1.337	1.7763
Comp B23	60480	MGZD172	36.3	37	0.7	D38415	0.89	1.46	1.022	1.2994
Comp B23	60480	MGZD172	37	37.7	0.7	D38416	0.93	1.47	1.029	1.3671
Comp B23	60480	MGZD172	39.1	39.8	0.7	D38420	0.89	1.32	0.924	1.1748
Comp B23	60480	MGZD172	44	45	1.0	D38428	1.6	1.71	1.71	2.736
Comp B23	60480	MGZD172	50.4	51.1	0.7	D38435	1.08	1.75	1.225	1.89
Comp B23	60480	MGZD172	56	56.7	0.7	D38444	1.21	1	0.7	1.21
Comp B23	60480	MGZD211	235	235.7	0.7	D48936	0.87	1.38	0.966	1.2006
Comp B23	60480	MGZD211	246.4	247.1	0.7	D48952	0.78	1.56	1.092	1.2168
Comp B23	60480	MGZD222	285.1	285.8	0.7	D53805	1.06	1.33	0.931	1.4098
Comp B23	60480	MGZD230	245.7	246.4	0.7	D57751	0.75	1.77	1.239	1.3275
Comp B23	60480	MGZD230	261.1	261.8	0.7	D57770	0.78	1.14	0.798	0.8892
Comp B23	60480	MGZD230	261.8	262.5	0.7	D57772	0.84	1.17	0.819	0.9828
Comp B23	60520	MGZD006	160.06	160.76	0.7	D00470	0.75	1.88	1.316	1.41
Comp B23	60520	MGZD035	167.4	168.1	0.7	D02957	0.81	1.56	1.092	1.2636
Comp B23	60520	MGZD035	214	214.7	0.7	D03018	0.73	1.75	1.225	1.2775
Comp B23	60520	MGZD082	143	144	1.0	D22714	1.13	1.56	1.56	1.7628
Comp B23	60520	MGZD082	266	266.7	0.7	D09414	0.79	1.3	0.91	1.027
Comp B23	60520	MGZD098	222.1	222.8	0.7	D14960	0.84	1.65	1.155	1.386
Comp B23	60520	MGZD098	245.9	246.6	0.7	D14997	0.94	1.24	0.868	1.1656
Comp B23	60520	MGZD098	246.6	247.3	0.7	D14999	0.64	1.33	0.931	0.8512
Comp B23	60520	MGZD098	247.3	248	0.7	D15000	0.74	1.61	1.127	1.1914
Comp B23	60520	MGZD106	35.1	35.8	0.7	D18819	0.71	1.21	0.847	0.8591
Comp B23	60520	MGZD106	35.8	36.5	0.7	D18820	0.73	1.35	0.945	0.9855
Comp B23	60520	MGZD106	37.9	38.6	0.7	D18824	0.85	1.82	1.274	1.547
Comp B23	60520	MGZD107	204	204.7	0.7	D18680	0.85	1.34	0.938	1.139
Comp B23	60520	MGZD107	217.3	218	0.7	D18701	0.8	1.62	1.134	1.296
Comp B23	60520	MGZD107	218	218.7	0.7	D18702	0.75	1.26	0.882	0.945

B ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp B23	60520	MGZD107	218.7	219.4	0.7	D18703	0.78	1.58	1.106	1.2324
Comp B23	60520	MGZD107	220.1	220.8	0.7	D18705	0.75	1.23	0.861	0.9225
Comp B23	60520	MGZD107	246.7	247.4	0.7	D18747	0.87	1.6	1.12	1.392
Comp B23	60520	MGZD134	197.8	198.5	0.7	D27930	0.84	1.87	1.309	1.5708
Comp B23	60520	MGZD134	200.6	201.3	0.7	D27934	0.83	1.97	1.379	1.6351
Comp B23	60520	MGZD134	272.4	273.1	0.7	D28025	0.81	1.88	1.316	1.5228
Comp B23	60520	MGZD225	281.7	282.4	0.7	D55210	0.95	1.38	0.966	1.311
Comp B23	60520	MGZD234	294	294.7	0.7	D58627	0.8	1.82	1.274	1.456
Comp B23	60520	MGZD265	164.9	165.6	0.7	D69224	0.86	1.48	1.036	1.2728
Comp B23	60520	MGZD265	166.3	167	0.7	D69226	0.76	1.79	1.253	1.3604
Comp B23	60520	MGZD265	175.4	176.1	0.7	D69240	0.73	1.31	0.917	0.9563
Comp B23	60520	MGZD265	192.2	192.9	0.7	D69266	0.83	1.99	1.393	1.6517
Comp B23	60520	MGZD265	197.1	197.8	0.7	D69274	0.73	1.13	0.791	0.8249
Comp B23	60560	MGZD042	180.1	180.8	0.7	D04339	0.78	1.4	0.98	1.092
Comp B23	60560	MGZD042	204	205	1.0	D04370	1.19	1.94	1.94	2.3086
Comp B23	60560	MGZD042	231.6	232.3	0.7	D04405	0.77	1	0.7	0.77
Comp B23	60560	MGZD042	232.3	233	0.7	D04406	0.83	1.28	0.896	1.0624
Comp B23	60560	MGZD044	265.7	266.4	0.7	D04518	0.72	1.56	1.092	1.1232
Comp B23	60560	MGZD044	269.4	270.1	0.7	D04524	0.7	1.85	1.295	1.295
Comp B23	60560	MGZD064	269	270	1.0	D06741	1.08	1.17	1.17	1.2636
Comp B23	60560	MGZD066	155	156	1.0	D14473	1.07	1.03	1.03	1.1021
Comp B23	60560	MGZD066	247	248	1.0	D06888	1.07	1.66	1.66	1.7762
Comp B23	60560	MGZD066	255	256	1.0	D06897	1.2	1.76	1.76	2.112
Comp B23	60560	MGZD066	263	264	1.0	D06906	1.02	1.14	1.14	1.1628
Comp B23	60560	MGZD099	181	181.7	0.7	D15804	0.79	1.55	1.085	1.2245
Comp B23	60560	MGZD099	181.7	182.4	0.7	D15805	0.75	1.25	0.875	0.9375
Comp B23	60560	MGZD099	182.4	183.1	0.7	D15806	0.81	1.05	0.735	0.8505
Comp B23	60560	MGZD099	231.4	232.1	0.7	D15862	0.79	1.07	0.749	0.8453
Comp B23	60560	MGZD099	263.1	263.8	0.7	D15902	0.83	1.6	1.12	1.328
Comp B23	60560	MGZD133	222.7	223.4	0.7	D27697	0.92	1.58	1.106	1.4536
Comp B23	60560	MGZD224	141	142	1.0	D54708	0.97	1.47	1.47	1.4259
Comp B23	60560	MGZD224	143	144	1.0	D54710	1.1	1.19	1.19	1.309
Comp B23	60560	MGZD224	147	148	1.0	D54714	1.04	1.605	1.605	1.6692
Comp B23	60560	MGZD224	272.1	272.8	0.7	D54863	0.83	1.44	1.008	1.1952
Comp B23	60560	MGZD224	277.4	278.1	0.7	D54870	0.86	1.91	1.337	1.6426
Comp B23	60560	MGZD232	278	279	1.0	D57394	1.21	1.21	1.21	1.4641
Comp B23	60600	MGZD084	269	270	1.0	D10181	1.24	1.68	1.68	2.0832
Comp B23	60600	MGZD088	223	223.7	0.7	D10576	0.95	1.86	1.302	1.767
Comp B23	60600	MGZD088	223.7	224.4	0.7	D10577	0.72	1.53	1.071	1.1016
Comp B23	60600	MGZD088	264	264.7	0.7	D10628	0.82	1.5	1.05	1.23
Comp B23	60600	MGZD088	271.7	272.4	0.7	D10640	0.79	1.2	0.84	0.948
Comp B23	60600	MGZD093	207.3	208	0.7	D11686	0.71	1.99	1.393	1.4129
Comp B23	60600	MGZD093	213.6	214.3	0.7	D11695	0.85	1.97	1.379	1.6745
Comp B23	60600	MGZD093	217.8	218.5	0.7	D11703	1.1	1.04	0.728	1.144
Comp B23	60600	MGZD093	234.6	235.3	0.7	D11729	0.85	1.76	1.232	1.496
Comp B23	60600	MGZD267	188.7	189.4	0.7	D70610	0.77	1.29	0.903	0.9933
Comp B23	60600	MGZD267	192.9	193.6	0.7	D70616	0.93	1.14	0.798	1.0602
Comp B23	60600	MGZD277	231.6	232.3	0.7	D73952	0.95	1.2	0.84	1.14
Comp B23	60600	MGZD284	201	202	1.0	D76676	1.42	1.01	1.01	1.4342
Comp B23	60600	MGZD306	309	310	1.0	D85788	1.41	1.32	1.32	1.8612
Comp B24	60440	MGZD086	150	150.7	0.7	D10279	0.9	2.05	1.435	1.845
Comp B24	60440	MGZD129	256.7	257.4	0.7	D26614	0.94	2.05	1.435	1.927
Comp B24	60440	MGZD129	299.8	300.5	0.7	D26665	0.76	2.49	1.743	1.8924
Comp B24	60440	MGZD149	67.7	68.4	0.7	D31173	1.06	2.46	1.722	2.6076
Comp B24	60440	MGZD149	85.2	85.9	0.7	D31201	1.15	2.4	1.68	2.76
Comp B24	60440	MGZD152	74.1	75	0.9	D32034	1.15	2.11	1.899	2.4265

B ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp B24	60440	MGZD152	75	76	1.0	D32035	1.43	2.08	2.08	2.9744
Comp B24	60440	MGZD152	83	84	1.0	D32044	1.48	2.46	2.46	3.6408
Comp B24	60440	MGZD152	86	87	1.0	D32048	1.66	2.18	2.18	3.6188
Comp B24	60440	MGZD152	94	95	1.0	D32056	1.29	2.17	2.17	2.7993
Comp B24	60440	MGZD197	260.3	261	0.7	D45052	0.89	2.03	1.421	1.8067
Comp B24	60480	MGZD011	139	140	1.0	D00807	1.2	2.45	2.45	2.94
Comp B24	60480	MGZD011	157.3	158	0.7	D00828	0.74	2.29	1.603	1.6946
Comp B24	60480	MGZD011	180.4	181.1	0.7	D00857	0.72	2.24	1.568	1.6128
Comp B24	60480	MGZD012	79	80	1.0	D12705	1.13	2.21	2.21	2.4973
Comp B24	60480	MGZD012	188	189	1.0	D01014	1.02	2.42	2.42	2.4684
Comp B24	60480	MGZD013	176	177	1.0	D02042	0.99	2.23	2.23	2.2077
Comp B24	60480	MGZD096	141.7	142.4	0.7	D12293	0.77	2.02	1.414	1.5554
Comp B24	60480	MGZD103	130	131	1.0	D18364	1.11	2.08	2.08	2.3088
Comp B24	60480	MGZD103	182.1	182.8	0.7	D18426	0.84	2.09	1.463	1.7556
Comp B24	60480	MGZD103	222	222.7	0.7	D18479	0.87	2.2	1.54	1.914
Comp B24	60480	MGZD128	238	239	1.0	D25901	0.35	2.47	2.47	0.8645
Comp B24	60480	MGZD131	273.8	274.5	0.7	D27033	0.69	2.43	1.701	1.6767
Comp B24	60480	MGZD131	274.5	275.2	0.7	D27034	0.7	2.02	1.414	1.414
Comp B24	60480	MGZD172	28.6	29.3	0.7	D38403	1.14	2.37	1.659	2.7018
Comp B24	60480	MGZD172	32.1	32.8	0.7	D38409	0.99	2.45	1.715	2.4255
Comp B24	60480	MGZD172	38.4	39.1	0.7	D38419	0.93	2.43	1.701	2.2599
Comp B24	60480	MGZD172	45	46	1.0	D38429	1.76	2.07	2.07	3.6432
Comp B24	60480	MGZD172	51.1	51.8	0.7	D38436	1.06	2.21	1.547	2.3426
Comp B24	60480	MGZD211	122	123	1.0	D48810	1	2.257	2.257	2.257
Comp B24	60480	MGZD216	125	126	1.0	D50742	1.01	2.21	2.21	2.2321
Comp B24	60480	MGZD222	214.2	215	0.8	D53720	1.22	2.12	1.696	2.5864
Comp B24	60480	MGZD222	289.3	290	0.7	D53811	1	2.02	1.414	2.02
Comp B24	60480	MGZD238	319	320	1.0	D60128	1.15	2.44	2.44	2.806
Comp B24	60520	MGZD006	24	25	1.0	D23620	1.22	2	2	2.44
Comp B24	60520	MGZD006	201.4	202	0.6	D00517	0.81	2.19	1.314	1.7739
Comp B24	60520	MGZD035	137	138	1.0	D13820	1.09	2.48	2.48	2.7032
Comp B24	60520	MGZD035	166.7	167.4	0.7	D02956	0.78	2.16	1.512	1.6848
Comp B24	60520	MGZD035	212.3	213	0.7	D03016	0.79	2.2	1.54	1.738
Comp B24	60520	MGZD035	227.4	228.1	0.7	D03035	0.85	2.14	1.498	1.819
Comp B24	60520	MGZD036	230	231	1.0	D03111	1.15	2.22	2.22	2.553
Comp B24	60520	MGZD082	258.8	259.5	0.7	D09405	0.65	2.16	1.512	1.404
Comp B24	60520	MGZD082	262.4	263.1	0.7	D09410	0.68	2.22	1.554	1.5096
Comp B24	60520	MGZD098	203.9	204.6	0.7	D14931	0.68	2.19	1.533	1.4892
Comp B24	60520	MGZD098	217.9	218.6	0.7	D14953	0.75	2.26	1.582	1.695
Comp B24	60520	MGZD098	224.9	225.6	0.7	D14964	0.72	2.2	1.54	1.584
Comp B24	60520	MGZD098	231.9	232.6	0.7	D14975	0.85	2	1.4	1.7
Comp B24	60520	MGZD098	232.6	233.3	0.7	D14976	0.75	2.18	1.526	1.635
Comp B24	60520	MGZD106	24.5	25.2	0.7	D18805	0.69	2.31	1.617	1.5939
Comp B24	60520	MGZD106	25.2	25.9	0.7	D18806	0.79	2.29	1.603	1.8091
Comp B24	60520	MGZD107	210.3	211	0.7	D18689	0.79	2	1.4	1.58
Comp B24	60520	MGZD107	211	211.7	0.7	D18690	0.81	2.38	1.666	1.9278
Comp B24	60520	MGZD107	233.4	234.1	0.7	D18726	0.8	2.31	1.617	1.848
Comp B24	60520	MGZD107	243.9	244.6	0.7	D18742	0.87	2.29	1.603	1.9923
Comp B24	60520	MGZD134	206.1	206.8	0.7	D27942	0.82	2.45	1.715	2.009
Comp B24	60520	MGZD134	217.4	218.1	0.7	D27956	0.92	2.28	1.596	2.0976
Comp B24	60520	MGZD136	245.4	246.1	0.7	D28782	0.76	2.43	1.701	1.8468
Comp B24	60520	MGZD220	139	140	1.0	D52105	1.09	2.39	2.39	2.6051
Comp B24	60520	MGZD225	284.5	285.2	0.7	D55214	0.89	2.47	1.729	2.1983
Comp B24	60520	MGZD225	285.2	285.9	0.7	D55215	0.87	2.02	1.414	1.7574
Comp B24	60520	MGZD265	174.7	175.4	0.7	D69239	0.81	2.23	1.561	1.8063
Comp B24	60520	MGZD265	185.9	186.6	0.7	D69256	0.65	2.42	1.694	1.573

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Comp B24	60520	MGZD265	209	209.7	0.7	D69293	0.83	2.04	1.428	1.6932
Comp B24	60560	MGZD044	265	265.7	0.7	D04517	0.84	2.26	1.582	1.8984
Comp B24	60560	MGZD066	156	157	1.0	D14474	1.01	2.19	2.19	2.2119
Comp B24	60560	MGZD099	183.8	184.5	0.7	D15808	0.88	2.08	1.456	1.8304
Comp B24	60560	MGZD133	223.4	224.1	0.7	D27699	0.79	2.22	1.554	1.7538
Comp B24	60560	MGZD133	224.1	224.8	0.7	D27700	0.89	2.43	1.701	2.1627
Comp B24	60560	MGZD133	224.8	225.5	0.7	D27701	0.87	2.22	1.554	1.9314
Comp B24	60560	MGZD224	145	146	1.0	D54712	1	2.23	2.23	2.23
Comp B24	60560	MGZD224	146	147	1.0	D54713	0.98	2.47	2.47	2.4206
Comp B24	60560	MGZD224	270.7	271.4	0.7	D54861	0.89	2.08	1.456	1.8512
Comp B24	60560	MGZD232	284.4	285.1	0.7	D57403	0.76	2.33	1.631	1.7708
Comp B24	60560	MGZD237	256.1	256.8	0.7	D59679	0.8	2.35	1.645	1.88
Comp B24	60600	MGZD084	232.2	232.9	0.7	D10139	0.75	2.31	1.617	1.7325
Comp B24	60600	MGZD084	250	251	1.0	D10160	1.18	2.22	2.22	2.6196
Comp B24	60600	MGZD088	234.2	234.9	0.7	D10593	0.73	2.32	1.624	1.6936
Comp B24	60600	MGZD088	268.2	268.9	0.7	D10634	0.72	2.07	1.449	1.4904
Comp B24	60600	MGZD088	272.4	273.1	0.7	D10641	0.76	2.16	1.512	1.6416
Comp B24	60600	MGZD093	214.3	215	0.7	D11697	0.95	2.31	1.617	2.1945
Comp B24	60600	MGZD249	250	251	1.0	D63839	1.19	2.06	2.06	2.4514
Comp B24	60600	MGZD267	173.7	174.4	0.7	D70591	0.79	2.06	1.442	1.6274
Comp B24	60600	MGZD267	190.8	191.5	0.7	D70613	0.8	2.3	1.61	1.84
Comp B24	60600	MGZD284	285	286	1.0	D76785	0.97	2.14	2.14	2.0758
Comp B24	60600	MGZD294	267	268	1.0	D80146	1.2	2.32	2.32	2.784
Comp B24	60600	MGZD294	291	292	1.0	D80176	1.2	2.13	2.13	2.556
Comp B25	60440	MGZD002	255	256	1.0	D00205	1.29	2.75	2.75	3.5475
Comp B25	60440	MGZD002	267.6	268.6	1.0	D00219	1.04	2.99	2.99	3.1096
Comp B25	60440	MGZD086	218	219	1.0	D10356	1.29	2.7	2.7	3.483
Comp B25	60440	MGZD144	82.7	83.4	0.7	D30308	1.09	2.83	1.981	3.0847
Comp B25	60440	MGZD144	87.6	88.3	0.7	D30315	1	2.69	1.883	2.69
Comp B25	60440	MGZD149	79.6	80.3	0.7	D31191	1.21	2.68	1.876	3.2428
Comp B25	60440	MGZD152	72.7	73.4	0.7	D32032	0.96	2.92	2.044	2.8032
Comp B25	60440	MGZD152	73.4	74.1	0.7	D32033	0.96	2.92	2.044	2.8032
Comp B25	60440	MGZD152	82	83	1.0	D32043	1.42	2.76	2.76	3.9192
Comp B25	60440	MGZD152	97	98	1.0	D32060	1.51	2.73	2.73	4.1223
Comp B25	60440	MGZD152	104.5	105.2	0.7	D32070	1.05	2.91	2.037	3.0555
Comp B25	60440	MGZD245	245.5	246.2	0.7	D62863	0.83	2.81	1.967	2.3323
Comp B25	60440	MGZD251	241.5	242.2	0.7	D65019	0.54	2.67	1.869	1.4418
Comp B25	60480	MGZD011	158	158.7	0.7	D00829	0.75	2.96	2.072	2.22
Comp B25	60480	MGZD011	177.7	178.7	1.0	D00853	1.04	2.6	2.6	2.704
Comp B25	60480	MGZD011	178.7	179.4	0.7	D00854	0.72	2.74	1.918	1.9728
Comp B25	60480	MGZD012	225	226	1.0	D01056	1.17	2.97	2.97	3.4749
Comp B25	60480	MGZD096	122	123	1.0	D12272	0.93	2.88	2.88	2.6784
Comp B25	60480	MGZD096	148.4	149.1	0.7	D12303	0.78	2.5	1.75	1.95
Comp B25	60480	MGZD096	151.2	152	0.8	D12307	0.9	2.99	2.392	2.691
Comp B25	60480	MGZD096	177.7	178.4	0.7	D12341	0.68	2.89	2.023	1.9652
Comp B25	60480	MGZD131	280	281	1.0	D27041	1.1	2.87	2.87	3.157
Comp B25	60480	MGZD172	32.8	33.5	0.7	D38410	1.22	2.56	1.792	3.1232
Comp B25	60480	MGZD172	51.8	52.5	0.7	D38437	1.2	2.85	1.995	3.42
Comp B25	60480	MGZD211	237.1	237.8	0.7	D48940	0.72	2.71	1.897	1.9512
Comp B25	60480	MGZD211	259.7	260.4	0.7	D48968	0.76	2.89	2.023	2.1964
Comp B25	60480	MGZD222	192.1	192.8	0.7	D53692	0.98	2.84	1.988	2.7832
Comp B25	60480	MGZD222	210.7	211.4	0.7	D53714	0.86	2.67	1.869	2.2962
Comp B25	60480	MGZD222	213.5	214.2	0.7	D53719	0.8	2.65	1.855	2.12
Comp B25	60480	MGZD222	264	265	1.0	D53779	1.31	2.77	2.77	3.6287
Comp B25	60520	MGZD035	168.8	169.5	0.7	D02959	0.74	2.65	1.855	1.961
Comp B25	60520	MGZD035	211.6	212.3	0.7	D03015	0.67	2.97	2.079	1.9899

B ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp B25	60520	MGZD036	253.3	254.04	0.7	D03141	0.74	2.5	1.85	1.85
Comp B25	60520	MGZD037	133	134	1.0	D13274	1.11	2.66	2.66	2.9526
Comp B25	60520	MGZD082	258.1	258.8	0.7	D09404	0.65	2.97	2.079	1.9305
Comp B25	60520	MGZD082	270.2	270.9	0.7	D09422	0.82	2.58	1.806	2.1156
Comp B25	60520	MGZD098	217.2	217.9	0.7	D14952	0.84	2.84	1.988	2.3856
Comp B25	60520	MGZD098	234	234.7	0.7	D14979	0.72	2.91	2.037	2.0952
Comp B25	60520	MGZD098	239.6	240.3	0.7	D14987	0.62	2.5	1.75	1.55
Comp B25	60520	MGZD098	240.3	241	0.7	D14988	0.78	2.97	2.079	2.3166
Comp B25	60520	MGZD107	221.5	222.2	0.7	D18707	0.83	2.84	1.988	2.3572
Comp B25	60520	MGZD107	223.6	224.3	0.7	D18710	0.81	2.88	2.016	2.3328
Comp B25	60520	MGZD107	227.1	227.8	0.7	D18715	0.94	2.76	1.932	2.5944
Comp B25	60520	MGZD134	199.9	200.6	0.7	D27933	0.79	2.95	2.065	2.3305
Comp B25	60520	MGZD134	216.7	217.4	0.7	D27955	0.85	2.97	2.079	2.5245
Comp B25	60520	MGZD136	237.2	237.9	0.7	D28770	0.78	2.97	2.079	2.3166
Comp B25	60520	MGZD184	76.5	77.2	0.7	D40531	1.19	2.54	1.778	3.0226
Comp B25	60520	MGZD225	282.4	283.1	0.7	D55211	0.86	2.78	1.946	2.3908
Comp B25	60520	MGZD225	283.8	284.5	0.7	D55213	0.85	2.68	1.876	2.278
Comp B25	60520	MGZD265	156.5	157.2	0.7	D69210	0.98	2.69	1.883	2.6362
Comp B25	60520	MGZD265	177.5	178.2	0.7	D69243	0.66	2.66	1.862	1.7556
Comp B25	60520	MGZD265	180.3	181	0.7	D69248	0.81	2.76	1.932	2.2356
Comp B25	60520	MGZD265	181.7	182.4	0.7	D69250	0.73	2.84	1.988	2.0732
Comp B25	60560	MGZD042	186	186.7	0.7	D04347	0.81	2.64	1.848	2.1384
Comp B25	60560	MGZD042	228.1	228.8	0.7	D04400	0.71	2.51	1.757	1.7821
Comp B25	60560	MGZD044	271.5	272.2	0.7	D04527	0.78	2.61	1.827	2.0358
Comp B25	60560	MGZD064	270	270.7	0.7	D06742	0.72	2.64	1.848	1.9008
Comp B25	60560	MGZD066	230	231	1.0	D06869	0.98	2.63	2.63	2.5774
Comp B25	60560	MGZD099	236.3	237	0.7	D15869	0.83	2.68	1.876	2.2244
Comp B25	60560	MGZD224	254.4	255.1	0.7	D54840	0.92	2.78	1.946	2.5576
Comp B25	60560	MGZD232	196.1	196.8	0.7	D57295	0.96	2.79	1.953	2.6784
Comp B25	60560	MGZD232	259.7	260.4	0.7	D57373	0.92	2.68	1.876	2.4656
Comp B25	60560	MGZD232	283	283.7	0.7	D57401	0.81	2.57	1.799	2.0817
Comp B25	60560	MGZD237	264	265	1.0	D59689	1.19	2.64	2.64	3.1416
Comp B25	60600	MGZD088	236.3	237	0.7	D10597	0.78	2.91	2.037	2.2698
Comp B25	60600	MGZD093	217.1	217.8	0.7	D11702	1	2.82	1.974	2.82
Comp B25	60600	MGZD095	161.8	162.5	0.7	D11995	0.67	2.92	2.044	1.9564
Comp B25	60600	MGZD294	191.2	192	0.8	D80051	1.12	2.66	2.128	2.9792
Comp B25	60600	MGZD294	292	292.7	0.7	D80177	0.76	2.8	1.96	2.128
Comp B26	60440	MGZD001	116	117	1.0	D12528	1.15	3.04	3.04	3.496
Comp B26	60440	MGZD002	239	240	1.0	D00187	1.23	3.11	3.11	3.8253
Comp B26	60440	MGZD002	259	260	1.0	D00209	1.27	3.47	3.47	4.4069
Comp B26	60440	MGZD086	152.8	153.5	0.7	D10283	0.82	3.45	2.415	2.829
Comp B26	60440	MGZD086	222	223	1.0	D10361	1.19	3.43	3.43	4.0817
Comp B26	60440	MGZD144	86.9	87.6	0.7	D30314	1.07	3.09	2.163	3.3063
Comp B26	60440	MGZD144	154.9	155.6	0.7	D30393	1.21	3.68	2.576	4.4528
Comp B26	60440	MGZD149	71.2	71.9	0.7	D31179	0.74	3.97	2.779	2.9378
Comp B26	60440	MGZD149	72.6	73.3	0.7	D31181	0.94	3.96	2.772	3.7224
Comp B26	60440	MGZD149	74.7	75.4	0.7	D31184	0.9	3.35	2.345	3.015
Comp B26	60440	MGZD149	83.1	83.8	0.7	D31197	0.89	3.6	2.52	3.204
Comp B26	60440	MGZD149	85.9	86.6	0.7	D31202	1.04	3.98	2.786	4.1392
Comp B26	60440	MGZD152	102.4	103.1	0.7	D32067	0.7	3.67	2.569	2.569
Comp B26	60440	MGZD152	115.7	116.4	0.7	D32088	1.29	3.52	2.464	4.5408
Comp B26	60440	MGZD201	188.6	189.3	0.7	D45525	0.79	3.65	2.555	2.8835
Comp B26	60440	MGZD245	244.8	245.5	0.7	D62862	0.97	3.79	2.653	3.6763
Comp B26	60480	MGZD011	143.6	144.8	1.2	D00813	1.42	3.85	4.62	5.467
Comp B26	60480	MGZD011	165	166	1.0	D00837	1.1	3.08	3.08	3.388
Comp B26	60480	MGZD012	172.2	173	0.8	D00994	0.84	3.2	2.56	2.688

B ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp B26	60480	MGZD012	184	185	1.0	D01010	1.06	3.07	3.07	3.2542
Comp B26	60480	MGZD012	185	186	1.0	D01011	0.99	3.47	3.47	3.4353
Comp B26	60480	MGZD012	186	187	1.0	D01012	1.02	3.03	3.03	3.0906
Comp B26	60480	MGZD012	197	198	1.0	D01025	1.01	3.01	3.01	3.0401
Comp B26	60480	MGZD012	211	212	1.0	D01040	1.1	3.43	3.43	3.773
Comp B26	60480	MGZD096	172.8	173.5	0.7	D12333	0.85	3.06	2.142	2.601
Comp B26	60480	MGZD096	179.8	180.5	0.7	D12344	0.73	3.5	2.45	2.555
Comp B26	60480	MGZD103	189	189.7	0.7	D18434	0.73	3.15	2.205	2.2995
Comp B26	60480	MGZD128	240.4	241.1	0.7	D25904	0.75	3.7	2.59	2.775
Comp B26	60480	MGZD128	241.8	242.5	0.7	D25906	0.75	3.26	2.282	2.445
Comp B26	60480	MGZD128	257	257.7	0.7	D25925	0.83	3.28	2.296	2.7224
Comp B26	60480	MGZD131	210	211	1.0	D26961	1.17	3.42	3.42	4.0014
Comp B26	60480	MGZD172	31.4	32.1	0.7	D38408	1.11	3.69	2.583	4.0959
Comp B26	60480	MGZD172	34.9	35.6	0.7	D38413	1.06	3.5	2.45	3.71
Comp B26	60480	MGZD172	37.7	38.4	0.7	D38417	0.88	3.16	2.212	2.7808
Comp B26	60480	MGZD172	41.9	42.6	0.7	D38425	1.03	3.07	2.149	3.1621
Comp B26	60480	MGZD172	60.2	60.9	0.7	D38451	1.02	3.01	2.107	3.0702
Comp B26	60480	MGZD172	60.9	61.6	0.7	D38452	1.19	3.04	2.128	3.6176
Comp B26	60480	MGZD211	236.4	237.1	0.7	D48939	0.81	3.02	2.114	2.4462
Comp B26	60480	MGZD211	245	245.7	0.7	D48950	0.75	3.36	2.352	2.52
Comp B26	60480	MGZD211	294.2	294.9	0.7	D49010	0.76	3.75	2.625	2.85
Comp B26	60480	MGZD222	246	247	1.0	D53759	1.12	3.46	3.46	3.8752
Comp B26	60520	MGZD006	158.6	159.35	0.8	D00468	0.83	3.18	2.385	2.6394
Comp B26	60520	MGZD006	200.7	201.4	0.7	D00516	0.82	3.74	2.618	3.0668
Comp B26	60520	MGZD035	169.5	170.2	0.7	D02960	0.77	3.4	2.38	2.618
Comp B26	60520	MGZD035	203.4	204.1	0.7	D03003	0.81	3.5	2.45	2.835
Comp B26	60520	MGZD035	210.2	210.9	0.7	D03012	0.64	3.32	2.324	2.1248
Comp B26	60520	MGZD036	224	225	1.0	D03105	1.28	3.86	3.86	4.9408
Comp B26	60520	MGZD082	257.4	258.1	0.7	D09403	0.65	3.1	2.17	2.015
Comp B26	60520	MGZD098	220	220.7	0.7	D14956	0.78	3.74	2.618	2.9172
Comp B26	60520	MGZD098	244.5	245.2	0.7	D14994	0.73	3.03	2.121	2.2119
Comp B26	60520	MGZD098	245.2	245.9	0.7	D14995	0.78	3.3	2.31	2.574
Comp B26	60520	MGZD098	249.4	250.1	0.7	D15003	0.77	3.57	2.499	2.7489
Comp B26	60520	MGZD098	252.2	252.9	0.7	D15007	0.83	3.68	2.576	3.0544
Comp B26	60520	MGZD107	213.8	214.5	0.7	D18694	0.76	3.92	2.744	2.9792
Comp B26	60520	MGZD107	244.6	245.3	0.7	D18743	0.82	3.6	2.52	2.952
Comp B26	60520	MGZD134	218.8	219.5	0.7	D27959	0.94	3.16	2.212	2.9704
Comp B26	60520	MGZD134	224.4	225.1	0.7	D27967	0.92	3.25	2.275	2.99
Comp B26	60520	MGZD134	225.8	226.5	0.7	D27969	0.92	3.3	2.31	3.036
Comp B26	60520	MGZD134	273.1	273.8	0.7	D28026	0.83	3.7	2.59	3.071
Comp B26	60520	MGZD136	196	197	1.0	D28724	1.47	3.62	3.62	5.3214
Comp B26	60520	MGZD136	244.7	245.4	0.7	D28781	0.76	3.32	2.324	2.5232
Comp B26	60520	MGZD136	259.7	260.4	0.7	D28799	0.76	3.73	2.611	2.8348
Comp B26	60520	MGZD136	261.1	261.8	0.7	D28801	0.8	3.16	2.212	2.528
Comp B26	60520	MGZD136	292.5	293.2	0.7	D28837	0.77	3.82	2.674	2.9414
Comp B26	60520	MGZD184	73	73.7	0.7	D40526	1.08	3	2.1	3.24
Comp B26	60520	MGZD220	137	138	1.0	D52103	1.27	3.17	3.17	4.0259
Comp B26	60520	MGZD231	170	171	1.0	D56908	1.19	3.75	3.75	4.4625
Comp B26	60520	MGZD265	157.2	157.9	0.7	D69211	0.62	3.09	2.163	1.9158
Comp B26	60520	MGZD265	165.6	166.3	0.7	D69225	0.79	3.35	2.345	2.6465
Comp B26	60520	MGZD265	167	167.7	0.7	D69227	0.77	3.61	2.527	2.7797
Comp B26	60520	MGZD265	178.9	179.6	0.7	D69245	0.74	3.24	2.268	2.3976
Comp B26	60520	MGZD265	181	181.7	0.7	D69249	0.77	3.11	2.177	2.3947
Comp B26	60520	MGZD265	189.4	190.1	0.7	D69262	0.78	3.19	2.233	2.4882
Comp B26	60520	MGZD265	191.5	192.2	0.7	D69265	0.82	3.28	2.296	2.6896
Comp B26	60520	MGZD265	192.9	193.6	0.7	D69267	0.84	3.21	2.247	2.6964

B ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp B26	60520	MGZD265	199.2	199.9	0.7	D69279	0.82	3.99	2.793	3.2718
Comp B26	60560	MGZD042	229.5	230.2	0.7	D04402	0.72	3.87	2.709	2.7864
Comp B26	60560	MGZD044	156	157	1.0	D20840	1	3.39	3.39	3.39
Comp B26	60560	MGZD044	270.1	270.8	0.7	D04525	0.68	3.96	2.772	2.6928
Comp B26	60560	MGZD044	270.8	271.5	0.7	D04526	0.78	3.93	2.751	3.0654
Comp B26	60560	MGZD044	272.2	272.9	0.7	D04529	0.81	3.11	2.177	2.5191
Comp B26	60560	MGZD064	257	257.7	0.7	D06727	0.69	3.67	2.569	2.5323
Comp B26	60560	MGZD066	231	232	1.0	D06870	1.01	3.31	3.31	3.3431
Comp B26	60560	MGZD066	244	245	1.0	D06885	1.17	3.12	3.12	3.6504
Comp B26	60560	MGZD066	286	287	1.0	D06932	1.26	3	3	3.78
Comp B26	60560	MGZD133	232.4	233.15	0.8	D27710	1.02	3.83	2.8725	3.9066
Comp B26	60560	MGZD135	140.7	141.4	0.7	D28264	0.68	3.12	2.184	2.1216
Comp B26	60560	MGZD232	279	280	1.0	D57395	1.2	3.78	3.78	4.536
Comp B26	60600	MGZD084	229.4	230.1	0.7	D10134	0.79	3.75	2.625	2.9625
Comp B26	60600	MGZD088	271	271.7	0.7	D10639	0.81	3.51	2.457	2.8431
Comp B26	60600	MGZD267	192.2	192.9	0.7	D70615	0.84	3.76	2.632	3.1584
Comp B26	60600	MGZD277	232.3	233	0.7	D73953	0.89	3.36	2.352	2.9904
Comp B26	60600	MGZD284	284.3	285	0.7	D76784	0.8	3.14	2.198	2.512
Comp B27	60440	MGZD001	113	114	1.0	D12525	1.08	4.64	4.64	5.0112
Comp B27	60440	MGZD003	218.2	219.2	1.0	D00254	1.08	4.8	4.8	5.184
Comp B27	60440	MGZD086	150.7	151.4	0.7	D10280	0.75	4.8	3.36	3.6
Comp B27	60440	MGZD086	151.4	152.1	0.7	D10281	0.8	4.92	3.444	3.936
Comp B27	60440	MGZD132	289	290	1.0	D27406	1.44	4.12	4.12	5.9328
Comp B27	60440	MGZD144	84.8	85.5	0.7	D30311	1.14	4.02	2.814	4.5828
Comp B27	60440	MGZD144	86.2	86.9	0.7	D30313	1.24	4.48	3.136	5.5552
Comp B27	60440	MGZD197	173	174	1.0	D44939	1.13	4.643	4.643	5.24659
Comp B27	60440	MGZD245	238.5	239.2	0.7	D62852	0.81	4.86	3.402	3.9366
Comp B27	60440	MGZD245	255	256	1.0	D62876	1.19	4.39	4.39	5.2241
Comp B27	60440	MGZD245	261.1	261.8	0.7	D62884	0.66	4.78	3.346	3.1548
Comp B27	60480	MGZD011	170.6	171.3	0.7	D00844	0.71	4.49	3.143	3.1879
Comp B27	60480	MGZD012	183	184	1.0	D01009	1.26	4.18	4.18	5.2668
Comp B27	60480	MGZD012	220	221	1.0	D01051	1.22	4.54	4.54	5.5388
Comp B27	60480	MGZD103	177.6	178.3	0.7	D18419	0.88	4.52	3.164	3.9776
Comp B27	60480	MGZD103	189.7	190.4	0.7	D18435	0.77	4.81	3.367	3.7037
Comp B27	60480	MGZD172	23.7	24.4	0.7	D38395	1	4.02	2.814	4.02
Comp B27	60480	MGZD172	25.8	26.5	0.7	D38399	1.12	4.19	2.933	4.6928
Comp B27	60480	MGZD172	62.3	63	0.7	D38454	1.16	4.87	3.409	5.6492
Comp B27	60480	MGZD205	129	130	1.0	D46890	0.8	4.253	4.253	3.4024
Comp B27	60520	MGZD035	168.1	168.8	0.7	D02958	0.78	4.8	3.36	3.744
Comp B27	60520	MGZD035	173	173.7	0.7	D02965	0.89	4.04	2.828	3.5956
Comp B27	60520	MGZD035	173.7	174.4	0.7	D02966	0.97	4.12	2.884	3.9964
Comp B27	60520	MGZD035	214.7	215.4	0.7	D03019	0.81	4.27	2.989	3.4587
Comp B27	60520	MGZD035	226.7	227.4	0.7	D03034	0.82	4.68	3.276	3.8376
Comp B27	60520	MGZD036	203	204	1.0	D03080	1.12	4.17	4.17	4.6704
Comp B27	60520	MGZD082	260.2	261	0.8	D09407	0.79	4.65	3.72	3.6735
Comp B27	60520	MGZD098	250.1	250.8	0.7	D15004	0.85	4.59	3.213	3.9015
Comp B27	60520	MGZD098	255	255.7	0.7	D15011	0.71	4.24	2.968	3.0104
Comp B27	60520	MGZD107	212.4	213.1	0.7	D18692	0.76	4.25	2.975	3.23
Comp B27	60520	MGZD107	219.4	220.1	0.7	D18704	0.79	4.38	3.066	3.4602
Comp B27	60520	MGZD107	241.1	241.8	0.7	D18737	0.8	4.83	3.381	3.864
Comp B27	60520	MGZD134	227.9	228.6	0.7	D27973	0.9	4.99	3.493	4.491
Comp B27	60520	MGZD231	240	241	1.0	D56986	1.09	4.57	4.57	4.9813
Comp B27	60560	MGZD042	179.4	180.1	0.7	D04338	0.75	4.78	3.346	3.585
Comp B27	60560	MGZD066	232	233	1.0	D06872	0.96	4.16	4.16	3.9936
Comp B27	60560	MGZD066	246	247	1.0	D06887	0.96	4.13	4.13	3.9648
Comp B27	60560	MGZD099	234.9	235.6	0.7	D15867	0.96	4.4	3.08	4.224

B ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp B27	60560	MGZD099	261.7	262.4	0.7	D15900	0.79	4.7	3.29	3.713
Comp B27	60560	MGZD224	148	149	1.0	D54715	1	4.36	4.36	4.36
Comp B27	60560	MGZD224	205.3	206	0.7	D54783	0.87	4.15	2.905	3.6105
Comp B27	60560	MGZD232	196.8	197.5	0.7	D57297	0.78	4.39	3.073	3.4242
Comp B27	60600	MGZD084	230.1	230.8	0.7	D10135	0.71	4.93	3.451	3.5003
Comp B27	60600	MGZD084	231.5	232.2	0.7	D10137	0.78	4.33	3.031	3.3774
Comp B27	60600	MGZD084	235	236	1.0	D10143	1.24	4.38	4.38	5.4312
Comp B27	60600	MGZD090	265.7	266.4	0.7	D11442	0.74	4.05	2.835	2.997
Comp B27	60600	MGZD090	269.2	269.9	0.7	D11448	0.82	4.33	3.031	3.5506
Comp B27	60600	MGZD093	212.2	212.9	0.7	D11693	0.79	4.66	3.262	3.6814
Comp B27	60600	MGZD267	176.5	177.2	0.7	D70595	0.85	4.18	2.926	3.553
Comp B27	60600	MGZD267	193.6	194.3	0.7	D70617	0.84	4.21	2.947	3.5364
Comp B28	60440	MGZD149	68.4	69.1	0.7	D31174	1.19	6.53	4.571	7.7707
Comp B28	60440	MGZD149	73.3	74	0.7	D31182	0.97	5.71	3.997	5.5387
Comp B28	60440	MGZD149	74	74.7	0.7	D31183	1.16	5.17	3.619	5.9972
Comp B28	60440	MGZD149	76.8	77.5	0.7	D31187	0.85	5.88	4.116	4.998
Comp B28	60440	MGZD149	80.3	81	0.7	D31192	0.91	5.28	3.696	4.8048
Comp B28	60440	MGZD152	77	78	1.0	D32037	1.61	5.98	5.98	9.6278
Comp B28	60440	MGZD152	87	88	1.0	D32049	1.75	5.93	5.93	10.3775
Comp B28	60440	MGZD152	93	94	1.0	D32055	1.38	5.4	5.4	7.452
Comp B28	60440	MGZD152	114.3	115	0.7	D32086	1.03	5.2	3.64	5.356
Comp B28	60440	MGZD152	116.4	117.1	0.7	D32089	0.95	5.65	3.955	5.3675
Comp B28	60440	MGZD152	129	129.7	0.7	D32109	1.16	5.53	3.871	6.4148
Comp B28	60440	MGZD245	210	211	1.0	D62814	1.15	5.84	5.84	6.716
Comp B28	60440	MGZD245	258	259	1.0	D62880	1.21	5.05	5.05	6.1105
Comp B28	60440	MGZD251	240.8	241.5	0.7	D65017	0.71	6.01	4.207	4.2671
Comp B28	60480	MGZD011	167	168	1.0	D00839	1.08	5.77	5.77	6.2316
Comp B28	60480	MGZD011	174.3	175.6	1.3	D00849	1.35	5.44	7.072	7.344
Comp B28	60480	MGZD012	210	211	1.0	D01039	1.2	5.98	5.98	7.176
Comp B28	60480	MGZD012	213	214	1.0	D01042	1.03	6.28	6.28	6.4684
Comp B28	60480	MGZD012	216	217	1.0	D01045	1.09	5.02	5.02	5.4718
Comp B28	60480	MGZD096	147.7	148.4	0.7	D12302	0.65	5.6	3.92	3.64
Comp B28	60480	MGZD096	174.9	175.6	0.7	D12336	0.67	5.23	3.661	3.5041
Comp B28	60480	MGZD096	175.6	176.3	0.7	D12337	0.65	5.05	3.535	3.2825
Comp B28	60480	MGZD096	182.6	183.3	0.7	D12349	0.77	6.71	4.697	5.1667
Comp B28	60480	MGZD096	185.4	186.1	0.7	D12353	0.51	5.44	3.808	2.7744
Comp B28	60480	MGZD103	191.1	192	0.9	D18437	0.99	6.52	5.868	6.4548
Comp B28	60480	MGZD103	208.7	209.4	0.7	D18457	0.73	6.23	4.361	4.5479
Comp B28	60480	MGZD131	272.4	273.1	0.7	D27031	0.77	6.02	4.214	4.6354
Comp B28	60480	MGZD172	26.5	27.2	0.7	D38400	1.14	6.18	4.326	7.0452
Comp B28	60480	MGZD172	27.2	27.9	0.7	D38401	1.07	5.65	3.955	6.0455
Comp B28	60480	MGZD172	43.3	44	0.7	D38427	1.2	5.19	3.633	6.228
Comp B28	60480	MGZD172	55.3	56	0.7	D38443	1.26	6.36	4.452	8.0136
Comp B28	60480	MGZD222	283.7	284.4	0.7	D53803	0.99	5.56	3.892	5.5044
Comp B28	60480	MGZD222	285.8	286.5	0.7	D53806	1.12	5.7	3.99	6.384
Comp B28	60480	MGZD222	288.6	289.3	0.7	D53810	0.98	5.94	4.158	5.8212
Comp B28	60480	MGZD238	292.7	293.4	0.7	D60095	0.79	5.35	3.745	4.2265
Comp B28	60520	MGZD035	207.4	208.1	0.7	D03008	0.75	6.23	4.361	4.6725
Comp B28	60520	MGZD035	210.9	211.6	0.7	D03014	0.68	6.29	4.403	4.2772
Comp B28	60520	MGZD036	251.2	251.9	0.7	D03138	0.75	5.79	4.053	4.3425
Comp B28	60520	MGZD082	259.5	260.2	0.7	D09406	0.72	5.78	4.046	4.1616
Comp B28	60520	MGZD082	261.7	262.4	0.7	D09409	0.65	6.03	4.221	3.9195
Comp B28	60520	MGZD098	220.7	221.4	0.7	D14957	0.78	6.41	4.487	4.9998
Comp B28	60520	MGZD098	221.4	222.1	0.7	D14959	0.85	5.94	4.158	5.049
Comp B28	60520	MGZD098	236.1	236.8	0.7	D14982	0.68	6.48	4.536	4.4064
Comp B28	60520	MGZD098	237.5	238.2	0.7	D14984	0.69	6.08	4.256	4.1952

B ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp B28	60520	MGZD098	243.8	244.5	0.7	D14993	0.8	6.14	4.298	4.912
Comp B28	60520	MGZD098	248	248.7	0.7	D15001	0.69	5.09	3.563	3.5121
Comp B28	60520	MGZD098	248.7	249.4	0.7	D15002	0.84	6.61	4.627	5.5524
Comp B28	60520	MGZD098	253.6	254.3	0.7	D15009	0.79	6.65	4.655	5.2535
Comp B28	60520	MGZD107	206.1	206.8	0.7	D18683	0.86	6.21	4.347	5.3406
Comp B28	60520	MGZD107	211.7	212.4	0.7	D18691	0.82	6.37	4.459	5.2234
Comp B28	60520	MGZD107	216.6	217.3	0.7	D18700	0.76	5.17	3.619	3.9292
Comp B28	60520	MGZD107	250.2	250.9	0.7	D18752	0.87	6.03	4.221	5.2461
Comp B28	60520	MGZD134	221.6	222.3	0.7	D27963	0.89	5	3.5	4.45
Comp B28	60520	MGZD136	289.7	290.4	0.7	D28833	0.76	5.58	3.906	4.2408
Comp B28	60520	MGZD220	138	139	1.0	D52104	0.98	6.04	6.04	5.9192
Comp B28	60520	MGZD220	261.7	262.4	0.7	D52245	0.76	5.4	3.78	4.104
Comp B28	60520	MGZD265	182.4	183.1	0.7	D69251	0.69	5	3.5	3.45
Comp B28	60520	MGZD265	185.2	185.9	0.7	D69255	0.69	6.85	4.795	4.7265
Comp B28	60520	MGZD265	190.1	190.8	0.7	D69263	0.75	5.34	3.738	4.005
Comp B28	60520	MGZD265	195.7	196.4	0.7	D69272	0.67	5	3.5	3.35
Comp B28	60560	MGZD042	178.7	179.4	0.7	D04337	0.78	6.23	4.361	4.8594
Comp B28	60560	MGZD044	155	156	1.0	D20839	1.07	5.54	5.54	5.9278
Comp B28	60560	MGZD044	268.7	269.4	0.7	D04523	0.7	5.95	4.165	4.165
Comp B28	60560	MGZD066	261	262	1.0	D06904	0.81	5.62	5.62	4.5522
Comp B28	60560	MGZD135	142.1	142.8	0.7	D28266	0.71	6.72	4.704	4.7712
Comp B28	60560	MGZD135	145.6	146.3	0.7	D28272	0.7	5.78	4.046	4.046
Comp B28	60560	MGZD224	271.4	272.1	0.7	D54862	0.83	5.95	4.165	4.9385
Comp B28	60560	MGZD224	276.7	277.4	0.7	D54869	0.79	5.08	3.556	4.0132
Comp B28	60560	MGZD237	256.8	257.5	0.7	D59680	0.6	6.65	4.655	3.99
Comp B28	60600	MGZD084	252	253	1.0	D10162	1.18	6.17	6.17	7.2806
Comp B28	60600	MGZD088	264.7	265.4	0.7	D10629	0.79	6.78	4.746	5.3562
Comp B28	60600	MGZD088	265.4	266.1	0.7	D10630	0.8	6.59	4.613	5.272
Comp B28	60600	MGZD088	266.8	267.5	0.7	D10632	0.86	6.08	4.256	5.2288
Comp B28	60600	MGZD093	224.8	225.5	0.7	D11713	0.79	6.98	4.886	5.5142
Comp B28	60600	MGZD093	226.2	226.9	0.7	D11715	0.76	5.36	3.752	4.0736
Comp B28	60600	MGZD095	142	143	1.0	D11973	0.96	5.27	5.27	5.0592
Comp B29	60440	MGZD132	290.7	291.4	0.7	D27408	0.91	7.45	5.215	6.7795
Comp B29	60440	MGZD144	82	82.7	0.7	D30307	1.11	9.2	6.44	10.212
Comp B29	60440	MGZD149	82.4	83.1	0.7	D31195	1.24	8.95	6.265	11.098
Comp B29	60440	MGZD149	83.8	84.5	0.7	D31199	0.99	7.74	5.418	7.6626
Comp B29	60440	MGZD149	84.5	85.2	0.7	D31200	0.99	9.85	6.895	9.7515
Comp B29	60440	MGZD152	96	97	1.0	D32059	1.41	7.73	7.73	10.8993
Comp B29	60440	MGZD197	248.5	249.2	0.7	D45034	0.77	7.14	4.998	5.4978
Comp B29	60440	MGZD201	185.1	185.8	0.7	D45519	0.71	7.43	5.201	5.2753
Comp B29	60480	MGZD011	171.3	172.3	1.0	D00845	1.07	7.78	7.78	8.3246
Comp B29	60480	MGZD011	172.3	173.3	1.0	D00847	1.1	9.19	9.19	10.109
Comp B29	60480	MGZD012	187	188	1.0	D01013	1.07	9.93	9.93	10.6251
Comp B29	60480	MGZD012	204	205	1.0	D01032	1.07	8.76	8.76	9.3732
Comp B29	60480	MGZD012	205	206	1.0	D01034	1.06	9.28	9.28	9.8368
Comp B29	60480	MGZD096	147	147.7	0.7	D12301	0.74	8.7	6.09	6.438
Comp B29	60480	MGZD096	184.7	185.4	0.7	D12352	0.73	7.21	5.047	5.2633
Comp B29	60480	MGZD096	186.8	187.5	0.7	D12355	0.75	9.21	6.447	6.9075
Comp B29	60480	MGZD096	188.2	188.9	0.7	D12357	0.7	9.75	6.825	6.825
Comp B29	60480	MGZD103	142	143	1.0	D18377	1.17	7.69	7.69	8.9973
Comp B29	60480	MGZD128	242.5	243.2	0.7	D25907	0.71	7.82	5.474	5.5522
Comp B29	60480	MGZD172	23	23.7	0.7	D38394	1.09	8.05	5.635	8.7745
Comp B29	60480	MGZD172	41.2	41.9	0.7	D38424	1.12	8.26	5.782	9.2512
Comp B29	60480	MGZD172	58.1	58.8	0.7	D38448	1.23	7.79	5.453	9.5817
Comp B29	60480	MGZD211	245.7	246.4	0.7	D48951	0.8	8.15	5.705	6.52
Comp B29	60480	MGZD222	191.4	192.1	0.7	D53691	0.9	9.14	6.398	8.226

B ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp B29	60480	MGZD222	268	269	1.0	D53783	1.45	7.11	7.11	10.3095
Comp B29	60480	MGZD222	284.4	285.1	0.7	D53804	1.05	9.04	6.328	9.492
Comp B29	60480	MGZD222	286.5	287.2	0.7	D53807	1.01	8.15	5.705	8.2315
Comp B29	60480	MGZD230	244.3	245	0.7	D57749	0.83	8.36	5.852	6.9388
Comp B29	60520	MGZD035	172.3	173	0.7	D02964	0.8	7.41	5.187	5.928
Comp B29	60520	MGZD035	206.7	207.4	0.7	D03007	0.76	7.43	5.201	5.6468
Comp B29	60520	MGZD035	209.5	210.2	0.7	D03011	0.76	9.89	6.923	7.5164
Comp B29	60520	MGZD035	215.4	216.1	0.7	D03020	0.8	8.6	6.02	6.88
Comp B29	60520	MGZD036	202	203	1.0	D03079	0.76	9.2	9.2	6.992
Comp B29	60520	MGZD036	204.7	205.7	1.0	D03082	1.05	8.72	8.72	9.156
Comp B29	60520	MGZD036	206.7	207.4	0.7	D03084	0.84	7.57	5.299	6.3588
Comp B29	60520	MGZD036	247.7	248.4	0.7	D03132	0.75	8.22	5.754	6.165
Comp B29	60520	MGZD098	204.6	205.3	0.7	D14932	0.65	7.26	5.082	4.719
Comp B29	60520	MGZD098	213.7	214.4	0.7	D14947	0.84	7.66	5.362	6.4344
Comp B29	60520	MGZD098	222.8	223.5	0.7	D14961	0.84	8.14	5.698	6.8376
Comp B29	60520	MGZD098	224.2	224.9	0.7	D14963	0.88	7.73	5.411	6.8024
Comp B29	60520	MGZD098	229.1	229.8	0.7	D14970	0.84	7.08	4.956	5.9472
Comp B29	60520	MGZD098	235.4	236.1	0.7	D14981	0.7	7.37	5.159	5.159
Comp B29	60520	MGZD098	238.9	239.6	0.7	D14986	0.78	8.71	6.097	6.7938
Comp B29	60520	MGZD098	241	241.7	0.7	D14989	0.78	7.09	4.963	5.5302
Comp B29	60520	MGZD098	243.1	243.8	0.7	D14992	0.8	8.69	6.083	6.952
Comp B29	60520	MGZD098	250.8	251.5	0.7	D15005	0.78	8.11	5.677	6.3258
Comp B29	60520	MGZD098	251.5	252.2	0.7	D15006	0.83	8.16	5.712	6.7728
Comp B29	60520	MGZD107	220.8	221.5	0.7	D18706	0.74	8.79	6.153	6.5046
Comp B29	60520	MGZD107	224.3	225	0.7	D18711	0.79	7.04	4.928	5.5616
Comp B29	60520	MGZD107	231.3	232	0.7	D18723	0.75	7.57	5.299	5.6775
Comp B29	60520	MGZD134	21	22	1.0	D27734	1.18	8.44	8.44	9.9592
Comp B29	60520	MGZD134	226.5	227.2	0.7	D27970	0.93	7.63	5.341	7.0959
Comp B29	60520	MGZD136	290.4	291.1	0.7	D28834	0.86	9.43	6.601	8.1098
Comp B29	60520	MGZD225	256	257	1.0	D55181	1.26	9.48	9.48	11.9448
Comp B29	60520	MGZD234	295.4	296.1	0.7	D58629	0.94	7.21	5.047	6.7774
Comp B29	60520	MGZD265	158.6	159.3	0.7	D69213	0.7	7	4.9	4.9
Comp B29	60520	MGZD265	176.8	177.5	0.7	D69242	0.78	8.61	6.027	6.7158
Comp B29	60520	MGZD265	187.3	188	0.7	D69259	0.76	7.23	5.061	5.4948
Comp B29	60520	MGZD265	208.3	209	0.7	D69292	0.83	7.48	5.236	6.2084
Comp B29	60560	MGZD042	180.8	181.5	0.7	D04340	0.85	8.39	5.873	7.1315
Comp B29	60560	MGZD042	181.5	182.2	0.7	D04341	0.77	7.68	5.376	5.9136
Comp B29	60560	MGZD042	182.2	183	0.8	D04342	0.97	9.62	7.696	9.3314
Comp B29	60560	MGZD042	228.8	229.5	0.7	D04401	0.74	7.6	5.32	5.624
Comp B29	60560	MGZD044	280	281	1.0	D04538	1.29	8.35	8.35	10.7715
Comp B29	60560	MGZD066	233	234	1.0	D06873	1.01	7.03	7.03	7.1003
Comp B29	60560	MGZD066	257	258	1.0	D06900	0.91	7.88	7.88	7.1708
Comp B29	60560	MGZD066	258	259	1.0	D06901	1.31	7.63	7.63	9.9953
Comp B29	60560	MGZD099	183.1	183.8	0.7	D15807	0.83	9.17	6.419	7.6111
Comp B29	60560	MGZD135	142.8	143.5	0.7	D28267	0.63	7.84	5.488	4.9392
Comp B29	60560	MGZD135	143.5	144.2	0.7	D28268	0.7	8.97	6.279	6.279
Comp B29	60560	MGZD224	144	145	1.0	D54711	0.99	7.85	7.85	7.7715
Comp B29	60560	MGZD224	216.7	217.4	0.7	D54795	0.8	9.71	6.797	7.768
Comp B29	60560	MGZD224	218.1	218.8	0.7	D54799	0.8	7.72	5.404	6.176
Comp B29	60560	MGZD232	283.7	284.4	0.7	D57402	0.73	8.47	5.929	6.1831
Comp B29	60600	MGZD088	225.1	225.8	0.7	D10580	0.79	8.77	6.139	6.9283
Comp B29	60600	MGZD088	266.1	266.8	0.7	D10631	0.83	7.97	5.579	6.6151
Comp B29	60600	MGZD088	267.5	268.2	0.7	D10633	0.78	7.44	5.208	5.8032
Comp B29	60600	MGZD090	266.4	267.1	0.7	D11443	0.7	8.32	5.824	5.824
Comp B29	60600	MGZD093	208	208.7	0.7	D11687	0.74	7.1	4.97	5.254
Comp B29	60600	MGZD093	212.9	213.6	0.7	D11694	0.84	7.03	4.921	5.9052

B ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp B29	60600	MGZD249	253	254	1.0	D63842	1.46	8.28	8.28	12.0888
Comp B29	60600	MGZD267	190.1	190.8	0.7	D70612	0.83	9.59	6.713	7.9597
Comp B30	60440	MGZD149	70.5	71.2	0.7	D31177	1.24	13	9.1	16.12
Comp B30	60440	MGZD149	78.9	79.6	0.7	D31190	1.05	10.2	7.14	10.71
Comp B30	60440	MGZD152	76	77	1.0	D32036	1.39	11.2	11.2	15.568
Comp B30	60440	MGZD152	78	79	1.0	D32039	1.5	11.2	11.2	16.8
Comp B30	60440	MGZD197	247.1	247.8	0.7	D45032	0.77	12.6	8.82	9.702
Comp B30	60440	MGZD226	290.5	291.2	0.7	D55569	0.79	11.4	7.98	9.006
Comp B30	60480	MGZD011	175.6	176.3	0.7	D00850	0.73	10	7	7.3
Comp B30	60480	MGZD011	179.4	180.4	1.0	D00856	0.91	13.8	13.8	12.558
Comp B30	60480	MGZD012	170.8	171.5	0.7	D00992	0.7	11.9	8.33	8.33
Comp B30	60480	MGZD012	175	176	1.0	D00998	1.05	13.6	13.6	14.28
Comp B30	60480	MGZD012	209	210	1.0	D01038	1.27	10.3	10.3	13.081
Comp B30	60480	MGZD012	214	215	1.0	D01043	1.1	14.6	14.6	16.06
Comp B30	60480	MGZD012	215	216	1.0	D01044	1.22	12.2	12.2	14.884
Comp B30	60480	MGZD012	224	225	1.0	D01055	1.25	13.5	13.5	16.875
Comp B30	60480	MGZD096	181.9	182.6	0.7	D12348	0.73	13.5	9.45	9.855
Comp B30	60480	MGZD128	261.2	261.9	0.7	D25931	0.82	11.9	8.33	9.758
Comp B30	60480	MGZD172	56.7	57.4	0.7	D38445	1.02	12.1	8.47	12.342
Comp B30	60480	MGZD205	128	129	1.0	D46889	0.94	10	10	9.4
Comp B30	60480	MGZD211	183	184	1.0	D48879	1.01	10	10	10.1
Comp B30	60480	MGZD230	245	245.7	0.7	D57750	0.79	14.5	10.15	11.455
Comp B30	60480	MGZD238	293.4	294.1	0.7	D60097	0.77	10.9	7.63	8.393
Comp B30	60480	MGZD238	301	301.7	0.7	D60106	0.71	10.4	7.28	7.384
Comp B30	60520	MGZD036	240.4	241.1	0.7	D03124	0.76	14	9.8	10.64
Comp B30	60520	MGZD036	252.6	253.3	0.7	D03140	0.74	13.6	9.52	10.064
Comp B30	60520	MGZD036	266	267	1.0	D03159	1.29	11.2	11.2	14.448
Comp B30	60520	MGZD082	261	261.7	0.7	D09408	0.67	11.5	8.05	7.705
Comp B30	60520	MGZD098	228.4	229.1	0.7	D14969	0.84	14.1	9.87	11.844
Comp B30	60520	MGZD098	231.2	231.9	0.7	D14974	0.73	10.3	7.21	7.519
Comp B30	60520	MGZD098	234.7	235.4	0.7	D14980	0.6	14	9.8	8.4
Comp B30	60520	MGZD098	236.8	237.5	0.7	D14983	0.71	10.4	7.28	7.384
Comp B30	60520	MGZD098	254.3	255	0.7	D15010	0.66	12.8	8.96	8.448
Comp B30	60520	MGZD107	204.7	205.4	0.7	D18681	0.82	11	7.7	9.02
Comp B30	60520	MGZD107	213.1	213.8	0.7	D18693	0.75	13	9.1	9.75
Comp B30	60520	MGZD107	247.4	248.1	0.7	D18748	0.82	14.4	10.08	11.808
Comp B30	60520	MGZD134	227.2	227.9	0.7	D27972	0.85	13.4	9.38	11.39
Comp B30	60520	MGZD184	75.8	76.5	0.7	D40530	1.08	12.5	8.75	13.5
Comp B30	60520	MGZD265	188	188.7	0.7	D69260	0.66	12.5	8.75	8.25
Comp B30	60520	MGZD265	193.6	194.3	0.7	D69268	0.73	14.8	10.36	10.804
Comp B30	60560	MGZD066	245	246	1.0	D06886	0.89	11.4	11.4	10.146
Comp B30	60560	MGZD066	249	250	1.0	D06890	0.85	14.8	14.8	12.58
Comp B30	60560	MGZD066	264	265	1.0	D06907	0.94	12.9	12.9	12.126
Comp B30	60560	MGZD066	266	267	1.0	D06909	1.04	12.2	12.2	12.688
Comp B30	60560	MGZD066	276	277	1.0	D06920	1.32	14.1	14.1	18.612
Comp B30	60560	MGZD099	224	225	1.0	D15853	1.09	13.3	13.3	14.497
Comp B30	60560	MGZD099	235.6	236.3	0.7	D15868	0.97	11.6	8.12	11.252
Comp B30	60560	MGZD099	262.4	263.1	0.7	D15901	0.83	10.9	7.63	9.047
Comp B30	60560	MGZD135	141.4	142.1	0.7	D28265	0.7	12.5	8.75	8.75
Comp B30	60560	MGZD224	142	143	1.0	D54709	0.98	11.25	11.25	11.025
Comp B30	60600	MGZD093	233.9	234.6	0.7	D11728	0.79	13.8	9.66	10.902
Comp B30	60600	MGZD095	163.2	163.9	0.7	D11999	0.71	10.9	7.63	7.739
Comp B30	60600	MGZD284	282.9	283.6	0.7	D76782	0.79	14.4	10.08	11.376
Comp B30	60600	MGZD294	292.7	293.4	0.7	D80179	0.82	14.3	10.01	11.726
Comp B30	60600	MGZD306	310	310.7	0.7	D85789	0.84	14.4	10.08	12.096

B ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp B31	60440	MGZD086	152.1	152.8	0.7	D10282	0.73	20.4	14.28	14.892
Comp B31	60440	MGZD129	299.1	299.8	0.7	D26664	0.75	20.8	14.56	15.6
Comp B31	60440	MGZD152	90	91	1.0	D32052	1.8	19.4	19.4	34.92
Comp B31	60440	MGZD152	92	93	1.0	D32054	1.39	19.1	19.1	26.549
Comp B31	60440	MGZD197	161	162	1.0	D44926	1.05	17.5	17.5	18.375
Comp B31	60440	MGZD197	247.8	248.5	0.7	D45033	0.86	25.4	17.78	21.844
Comp B31	60440	MGZD197	261	261.7	0.7	D45053	0.83	23.5	16.45	19.505
Comp B31	60440	MGZD197	287.8	288.5	0.7	D45088	0.9	19	13.3	17.1
Comp B31	60440	MGZD197	293.4	294.1	0.7	D45097	0.93	16.8	11.76	15.624
Comp B31	60440	MGZD201	193.5	194.2	0.7	D45532	0.77	23.9	16.73	18.403
Comp B31	60480	MGZD011	164	165	1.0	D00836	1	20.6	20.6	20.6
Comp B31	60480	MGZD012	178	178.7	0.7	D01001	0.92	26	18.2	23.92
Comp B31	60480	MGZD012	207	208	1.0	D01036	1.07	20.3	20.3	21.721
Comp B31	60480	MGZD012	217	218	1.0	D01047	1.25	17.4	17.4	21.75
Comp B31	60480	MGZD096	180.5	181.2	0.7	D12345	0.81	27.4	19.18	22.194
Comp B31	60480	MGZD096	181.2	181.9	0.7	D12347	0.73	26.8	18.76	19.564
Comp B31	60480	MGZD096	187.5	188.2	0.7	D12356	0.84	22.3	15.61	18.732
Comp B31	60480	MGZD131	273.1	273.8	0.7	D27032	0.7	18.8	13.16	13.16
Comp B31	60480	MGZD131	316	317	1.0	D27081	1.17	18.9	18.9	22.113
Comp B31	60480	MGZD172	49.7	50.4	0.7	D38434	0.97	16.8	11.76	16.296
Comp B31	60480	MGZD172	57.4	58.1	0.7	D38447	1.14	15.1	10.57	17.214
Comp B31	60520	MGZD035	208.8	209.5	0.7	D03010	0.74	22.1	15.47	16.354
Comp B31	60520	MGZD036	228	229	1.0	D03109	1.22	20.6	20.6	25.132
Comp B31	60520	MGZD036	229	230	1.0	D03110	1.04	16.4	16.4	17.056
Comp B31	60520	MGZD036	247	247.7	0.7	D03131	0.73	20.8	14.56	15.184
Comp B31	60520	MGZD036	251.9	252.6	0.7	D03139	0.77	20	14	15.4
Comp B31	60520	MGZD098	142	143	1.0	D14861	0.92	19.8	19.8	18.216
Comp B31	60520	MGZD098	209.5	210.2	0.7	D14940	0.87	23.8	16.66	20.706
Comp B31	60520	MGZD098	233.3	234	0.7	D14977	0.71	16.7	11.69	11.857
Comp B31	60520	MGZD098	238.2	238.9	0.7	D14985	0.73	18	12.6	13.14
Comp B31	60520	MGZD098	242.4	243.1	0.7	D14991	0.87	29.8	20.86	25.926
Comp B31	60520	MGZD107	205.4	206.1	0.7	D18682	0.81	25.7	17.99	20.817
Comp B31	60520	MGZD107	230.6	231.3	0.7	D18722	0.83	15.5	10.85	12.865
Comp B31	60520	MGZD107	238.3	239	0.7	D18733	0.77	19.7	13.79	15.169
Comp B31	60520	MGZD107	241.8	242.5	0.7	D18739	0.88	27.4	19.18	24.112
Comp B31	60520	MGZD134	225.1	225.8	0.7	D27968	0.88	27.4	19.18	24.112
Comp B31	60520	MGZD220	262.4	263.1	0.7	D52247	0.95	29.3	20.51	27.835
Comp B31	60520	MGZD234	294.7	295.4	0.7	D58628	0.92	20.7	14.49	19.044
Comp B31	60520	MGZD265	179.6	180.3	0.7	D69247	0.81	25.2	17.64	20.412
Comp B31	60520	MGZD265	183.8	184.5	0.7	D69253	0.71	27.2	19.04	19.312
Comp B31	60520	MGZD265	184.5	185.2	0.7	D69254	0.7	18.4	12.88	12.88
Comp B31	60520	MGZD265	196.4	197.1	0.7	D69273	0.72	22.2	15.54	15.984
Comp B31	60560	MGZD042	200.1	200.8	0.7	D04365	0.74	20.3	14.21	15.022
Comp B31	60560	MGZD042	227.4	228.1	0.7	D04399	0.81	17.3	12.11	14.013
Comp B31	60560	MGZD044	261.4	262.1	0.7	D04511	0.74	22.5	15.75	16.65
Comp B31	60560	MGZD066	256	257	1.0	D06899	1.34	16.2	16.2	21.708
Comp B31	60560	MGZD066	259	260	1.0	D06902	0.92	17.2	17.2	15.824
Comp B31	60560	MGZD066	262	263	1.0	D06905	0.9	20	20	18
Comp B31	60560	MGZD099	232.1	232.8	0.7	D15863	0.8	25.3	17.71	20.24
Comp B31	60560	MGZD224	199.8	200.5	0.7	D54774	0.84	17.6	12.32	14.784
Comp B31	60560	MGZD224	213	214	1.0	D54791	1.13	23.6	23.6	26.668
Comp B31	60560	MGZD224	216	216.7	0.7	D54794	0.88	18.2	12.74	16.016
Comp B31	60560	MGZD224	218.8	219.5	0.7	D54800	0.94	20	14	18.8
Comp B31	60560	MGZD232	206.4	207.1	0.7	D57309	0.9	15.5	10.85	13.95
Comp B31	60600	MGZD088	224.4	225.1	0.7	D10579	0.85	29.3	20.51	24.905
Comp B31	60600	MGZD088	233.5	234.2	0.7	D10592	0.8	20.9	14.63	16.72

B ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp B31	60600	MGZD088	235.6	236.3	0.7	D10595	0.82	18.5	12.95	15.17
Comp B31	60600	MGZD088	273.8	274.5	0.7	D10643	0.79	17.4	12.18	13.746
Comp B31	60600	MGZD090	267.1	267.8	0.7	D11444	0.67	22	15.4	14.74
Comp B31	60600	MGZD267	175.1	175.8	0.7	D70593	0.84	15	10.5	12.6
Comp B31	60600	MGZD267	189.4	190.1	0.7	D70611	0.78	15.1	10.57	11.778
Comp B32	60440	MGZD129	283	284	1.0	D26645	1.06	46.6	46.6	49.396
Comp B32	60440	MGZD129	297.7	298.4	0.7	D26662	0.72	45.1	31.57	32.472
Comp B32	60440	MGZD129	298.4	299.1	0.7	D26663	0.83	38.8	27.16	32.204
Comp B32	60440	MGZD152	72	72.7	0.7	D32031	1.01	33.1	23.17	33.431
Comp B32	60440	MGZD201	190.7	191.4	0.7	D45528	0.95	51.6	36.12	49.02
Comp B32	60480	MGZD012	178.7	179.4	0.7	D01002	0.6	36.6	25.62	21.96
Comp B32	60480	MGZD012	180.8	181.5	0.7	D01006	0.73	56.8	39.76	41.464
Comp B32	60480	MGZD012	208	209	1.0	D01037	1.17	30.4	30.4	35.568
Comp B32	60480	MGZD096	186.1	186.8	0.7	D12354	0.75	100	70	75
Comp B32	60480	MGZD211	278	279	1.0	D48989	1.23	48.1	48.1	59.163
Comp B32	60520	MGZD035	208.1	208.8	0.7	D03009	0.77	39.6	27.72	30.492
Comp B32	60520	MGZD082	266.7	267.4	0.7	D09415	0.89	31.9	22.33	28.391
Comp B32	60520	MGZD082	270.9	271.6	0.7	D09423	0.78	69.1	48.37	53.898
Comp B32	60520	MGZD098	215.8	216.5	0.7	D14950	0.78	33.2	23.24	25.896
Comp B32	60520	MGZD098	241.7	242.4	0.7	D14990	0.81	100	70	81
Comp B32	60520	MGZD107	236.9	237.6	0.7	D18731	0.78	54.8	38.36	42.744
Comp B32	60520	MGZD107	237.6	238.3	0.7	D18732	0.69	100	70	69
Comp B32	60560	MGZD042	205	205.7	0.7	D04372	0.7	33	23.1	23.1
Comp B32	60560	MGZD066	248	249	1.0	D06889	0.89	100	100	89
Comp B32	60560	MGZD099	230.7	231.4	0.7	D15861	0.83	82.5	57.75	68.475
Comp B32	60560	MGZD224	253	253.7	0.7	D54837	0.82	55.5	38.85	45.51
Comp B32	60560	MGZD232	259	259.7	0.7	D57372	0.89	53.8	37.66	47.882
Comp B32	60600	MGZD084	270	271	1.0	D10182	1.25	100	100	125
Comp B32	60600	MGZD267	191.5	192.2	0.7	D70614	0.83	33.1	23.17	27.473
Comp B32	60600	MGZD277	230.9	231.6	0.7	D73951	0.91	48.1	33.67	43.771
Comp B32	60600	MGZD284	283.6	284.3	0.7	D76783	0.73	100	70	73

C ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp C41	60640	MGZD181	184.1	184.8	0.7	D41040	0.85	0.12	0.08	0.10
Comp C41	60640	MGZD258	253.7	254.4	0.7	D67557	0.88	0.25	0.18	0.22
Comp C41	60640	MGZD276	199	200	1.0	D73477	1.45	0.12	0.12	0.17
Comp C41	60720	MGZD097	252.7	253.4	0.7	D12181	0.73	0.03	0.02	0.02
Comp C41	60720	MGZD097	254.1	254.8	0.7	D12183	0.72	0.13	0.09	0.09
Comp C41	60720	MGZD097	254.8	255.5	0.7	D12184	0.78	0.24	0.17	0.19
Comp C41	60720	MGZD182	140.9	141.6	0.7	D41690	0.86	0.09	0.06	0.08
Comp C41	60720	MGZD182	141.6	142.3	0.7	D41691	0.85	0.19	0.13	0.16
Comp C41	60720	MGZD182	142.3	143	0.7	D41692	0.72	0.07	0.05	0.05
Comp C41	60720	MGZD191	147.5	148.2	0.7	D42907	0.68	0.24	0.17	0.16
Comp C41	60720	MGZD191	151	151.7	0.7	D42912	0.79	0.07	0.05	0.06
Comp C41	60720	MGZD196	187	187.7	0.7	D44369	0.78	0.22	0.15	0.17
Comp C41	60720	MGZD196	188.4	189.1	0.7	D44372	0.74	0.22	0.15	0.16
Comp C41	60720	MGZD196	198.9	199.6	0.7	D44388	0.81	0.25	0.17	0.20
Comp C41	60720	MGZD196	225.6	226.3	0.7	D44428	0.76	0.08	0.06	0.06
Comp C41	60720	MGZD196	226.3	227	0.7	D44429	0.92	0.09	0.06	0.08
Comp C41	60720	MGZD203	251.9	252.6	0.7	D46200	0.84	0.16	0.11	0.13
Comp C41	60720	MGZD203	255.4	256.1	0.7	D46205	0.79	0.14	0.10	0.11
Comp C41	60720	MGZD203	256.8	257.5	0.7	D46207	0.64	0.10	0.07	0.06
Comp C41	60720	MGZD203	258.9	259.6	0.7	D46210	0.89	0.08	0.06	0.07
Comp C41	60720	MGZD203	259.6	260.3	0.7	D46211	0.85	0.06	0.04	0.05
Comp C41	60720	MGZD203	261	261.7	0.7	D46213	0.64	0.12	0.08	0.08
Comp C41	60720	MGZD203	262.4	263.1	0.7	D46215	0.7	0.07	0.05	0.05
Comp C41	60720	MGZD203	263.1	263.8	0.7	D46216	0.7	0.05	0.03	0.04
Comp C41	60720	MGZD203	264.5	265.2	0.7	D46219	0.83	0.25	0.17	0.21
Comp C41	60720	MGZD203	266.6	267.3	0.7	D46223	0.85	0.11	0.08	0.09
Comp C41	60720	MGZD253	244	245	1.0	D65708	1.11	0.09	0.09	0.10
Comp C41	60720	MGZD253	245	246	1.0	D65709	1.1	0.24	0.24	0.26
Comp C41	60720	MGZD253	246	247	1.0	D65710	1.12	0.25	0.25	0.28
Comp C41	60720	MGZD253	254	254.7	0.7	D65720	0.74	0.15	0.10	0.11
Comp C41	60720	MGZD264	225	226	1.0	D68905	1.13	0.20	0.20	0.23
Comp C41	60720	MGZD264	226	227	1.0	D68906	1.09	0.07	0.07	0.08
Comp C41	60720	MGZD264	227	228	1.0	D68907	1.05	0.04	0.04	0.04
Comp C41	60720	MGZD264	229	230	1.0	D68909	1.1	0.07	0.07	0.08
Comp C41	60720	MGZD264	232	233	1.0	D68912	1.15	0.06	0.06	0.07
Comp C41	60720	MGZD264	243.7	244.4	0.7	D68926	0.73	0.17	0.12	0.12
Comp C41	60720	MGZD264	264.3	265	0.7	D68952	0.73	0.20	0.14	0.15
Comp C41	60720	MGZD268	211	212	1.0	D70977	1.03	0.06	0.06	0.06
Comp C41	60720	MGZD268	213	214	1.0	D70980	1.22	0.11	0.11	0.13
Comp C41	60760	MGZD045	248	249	1.0	D04581	1.17	0.23	0.23	0.27
Comp C41	60760	MGZD045	255.5	256.2	0.7	D04592	0.78	0.12	0.08	0.09
Comp C41	60760	MGZD045	266	267	1.0	D04604	1.3	0.03	0.03	0.04
Comp C41	60760	MGZD046	141	142	1.0	D04772	1.04	0.02	0.02	0.02
Comp C41	60760	MGZD046	143	144	1.0	D04774	1.13	0.02	0.02	0.02
Comp C41	60760	MGZD073	141.2	141.9	0.7	D07811	0.68	0.12	0.08	0.08
Comp C41	60760	MGZD073	145.4	146.1	0.7	D07818	0.78	0.00	0.00	0.00
Comp C41	60760	MGZD073	182.7	183.4	0.7	D07865	0.8	0.10	0.07	0.08
Comp C41	60760	MGZD073	189	189.7	0.7	D07876	0.71	0.25	0.17	0.18
Comp C41	60760	MGZD073	205.1	206	0.9	D07897	0.95	0.19	0.17	0.18
Comp C41	60760	MGZD073	206	207	1.0	D07898	1.13	0.07	0.07	0.08
Comp C41	60760	MGZD073	208	209	1.0	D07900	1.14	0.16	0.16	0.18

C ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp C41	60760	MGZD275	248.6	249.3	0.7	D73156	0.83	0.22	0.15	0.18
Comp C41	60760	MGZD275	249.3	250	0.7	D73157	0.85	0.05	0.03	0.04
Comp C41	60760	MGZD275	250.7	251.4	0.7	D73161	0.91	0.12	0.08	0.11
Comp C41	60760	MGZD275	257.7	258.4	0.7	D73171	0.99	0.10	0.07	0.10
Comp C41	60760	MGZD283	229	230	1.0	D76302	1.12	0.15	0.15	0.17
Comp C41	60760	MGZD283	230	231	1.0	D76303	1.19	0.19	0.19	0.23
Comp C41	60760	MGZD283	232	233	1.0	D76305	1.24	0.13	0.13	0.16
Comp C41	60760	MGZD283	234	235	1.0	D76307	1.17	0.06	0.06	0.07
Comp C41	60760	MGZD288	259.8	260.5	0.7	D78293	0.85	0.20	0.14	0.17
Comp C41	60760	MGZD288	262	262.8	0.8	D78297	0.95	0.04	0.03	0.04
Comp C41	60760	MGZD288	262.8	263.6	0.8	D78299	0.96	0.20	0.16	0.19
Comp C41	60800	MGZD160	216	217	1.0	D35004	1.16	0.19	0.19	0.22
Comp C41	60800	MGZD160	219	220	1.0	D35007	1.22	0.04	0.04	0.05
Comp C41	60800	MGZD160	220	221	1.0	D35008	1.15	0.16	0.16	0.18
Comp C41	60800	MGZD160	221	222	1.0	D35009	1.18	0.09	0.09	0.11
Comp C41	60800	MGZD160	223.4	224.1	0.7	D35012	0.88	0.08	0.06	0.07
Comp C41	60800	MGZD160	224.1	224.8	0.7	D35013	0.95	0.04	0.03	0.04
Comp C41	60800	MGZD160	225.5	226.2	0.7	D35015	0.85	0.16	0.11	0.14
Comp C41	60800	MGZD160	226.2	226.9	0.7	D35016	0.82	0.08	0.06	0.07
Comp C41	60840	MGZD075	187	188	1.0	D08007	1.16	0.18	0.18	0.21
Comp C41	60840	MGZD076	216.1	216.8	0.7	D08125	0.75	0.14	0.10	0.11
Comp C41	60840	MGZD077	216.7	217.4	0.7	D08754	0.83	0.19	0.13	0.16
Comp C41	60840	MGZD077	230	230.7	0.7	D08775	0.84	0.17	0.12	0.14
Comp C41	60840	MGZD153	223	224	1.0	D32712	1.34	0.12	0.12	0.16
Comp C41	60840	MGZD153	224	225	1.0	D32713	1.45	0.19	0.19	0.28
Comp C41	60840	MGZD153	226	227	1.0	D32715	1.23	0.16	0.16	0.20
Comp C41	60840	MGZD153	230.5	231.2	0.7	D32723	0.86	0.24	0.17	0.21
Comp C41	60840	MGZD161	199.4	200.1	0.7	D35356	0.77	0.25	0.18	0.19
Comp C41	60840	MGZD161	216	217	1.0	D35376	1.22	0.20	0.20	0.24
Comp C41	60840	MGZD161	223	224	1.0	D35384	1.1	0.21	0.21	0.23
Comp C41	60840	MGZD161	234	235	1.0	D35397	1	0.10	0.10	0.10
Comp C41	60840	MGZD161	235	236	1.0	D35399	0.99	0.07	0.07	0.07
Comp C42	60640	MGZD181	232.7	233.4	0.7	D41095	0.81	0.29	0.20	0.23
Comp C42	60640	MGZD181	234.8	235.5	0.7	D41100	0.82	0.35	0.24	0.29
Comp C42	60640	MGZD276	200	201	1.0	D73479	1.55	0.33	0.33	0.51
Comp C42	60640	MGZD276	217.4	218.1	0.7	D73503	0.85	0.27	0.19	0.23
Comp C42	60680	MGZD218	206	207	1.0	D51493	0.97	0.29	0.29	0.28
Comp C42	60680	MGZD262	260.4	261.1	0.7	D68552	0.81	0.32	0.22	0.26
Comp C42	60680	MGZD272	199	200	1.0	D71884	1.33	0.38	0.38	0.51
Comp C42	60720	MGZD097	244	245	1.0	D12167	1.11	0.36	0.36	0.40
Comp C42	60720	MGZD097	252	252.7	0.7	D12180	0.74	0.29	0.20	0.21
Comp C42	60720	MGZD097	253.4	254.1	0.7	D12182	0.76	0.37	0.26	0.28
Comp C42	60720	MGZD191	146.1	146.8	0.7	D42905	0.71	0.29	0.20	0.21
Comp C42	60720	MGZD196	195.4	196.1	0.7	D44383	0.78	0.36	0.25	0.28
Comp C42	60720	MGZD196	196.8	197.5	0.7	D44385	0.72	0.33	0.23	0.24
Comp C42	60720	MGZD196	224.9	225.6	0.7	D44427	0.81	0.32	0.22	0.26
Comp C42	60720	MGZD196	227	227.7	0.7	D44430	0.74	0.29	0.20	0.21
Comp C42	60720	MGZD203	247	247.7	0.7	D46191	0.8	0.30	0.21	0.24
Comp C42	60720	MGZD203	254.7	255.4	0.7	D46204	0.78	0.34	0.24	0.27
Comp C42	60720	MGZD203	265.2	265.9	0.7	D46220	0.75	0.35	0.24	0.26
Comp C42	60720	MGZD203	265.9	266.6	0.7	D46222	0.85	0.39	0.27	0.33
Comp C42	60720	MGZD248	160.2	160.9	0.7	D63399	0.73	0.40	0.28	0.29
Comp C42	60720	MGZD253	251	252	1.0	D65716	1	0.35	0.35	0.35
Comp C42	60720	MGZD253	253	254	1.0	D65719	1.05	0.35	0.35	0.37
Comp C42	60720	MGZD264	221	222	1.0	D68900	1	0.29	0.29	0.29

C ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp C42	60720	MGZD264	222	223	1.0	D68902	1.07	0.34	0.34	0.36
Comp C42	60720	MGZD264	223	224	1.0	D68903	1.05	0.26	0.26	0.27
Comp C42	60720	MGZD264	228	229	1.0	D68908	1.03	0.35	0.35	0.36
Comp C42	60720	MGZD264	231	232	1.0	D68911	1.17	0.30	0.30	0.35
Comp C42	60720	MGZD264	233	234	1.0	D68913	1.29	0.40	0.40	0.52
Comp C42	60720	MGZD264	241	242	1.0	D68923	1.01	0.29	0.29	0.29
Comp C42	60720	MGZD264	243	243.7	0.7	D68925	0.81	0.37	0.26	0.30
Comp C42	60720	MGZD264	252	253	1.0	D68935	1.22	0.35	0.35	0.43
Comp C42	60720	MGZD264	253	254	1.0	D68936	1.11	0.27	0.27	0.30
Comp C42	60720	MGZD264	263.6	264.3	0.7	D68951	0.72	0.28	0.20	0.20
Comp C42	60720	MGZD264	265	266	1.0	D68953	0.99	0.38	0.38	0.38
Comp C42	60720	MGZD264	266	267	1.0	D68954	0.91	0.30	0.30	0.27
Comp C42	60720	MGZD268	238	239	1.0	D71008	1.12	0.32	0.32	0.36
Comp C42	60720	MGZD268	250	251	1.0	D71022	1.16	0.38	0.38	0.44
Comp C42	60720	MGZD268	252	252.7	0.7	D71024	0.83	0.39	0.27	0.32
Comp C42	60720	MGZD268	252.7	253.4	0.7	D71025	0.78	0.31	0.22	0.24
Comp C42	60720	MGZD268	259	260	1.0	D71034	1.17	0.35	0.35	0.41
Comp C42	60720	MGZD268	266.1	266.8	0.7	D71043	0.83	0.34	0.24	0.28
Comp C42	60720	MGZD268	267.5	268.2	0.7	D71045	0.86	0.38	0.27	0.33
Comp C42	60720	MGZD268	293	294	1.0	D71074	1.15	0.28	0.28	0.32
Comp C42	60720	MGZD268	296.7	297.4	0.7	D71080	0.95	0.35	0.24	0.33
Comp C42	60760	MGZD043	237	237.7	0.7	D04267	0.89	0.32	0.22	0.28
Comp C42	60760	MGZD073	141.9	142.6	0.7	D07812	0.6	0.38	0.27	0.23
Comp C42	60760	MGZD073	148.2	148.9	0.7	D07823	0.74	0.33	0.23	0.24
Comp C42	60760	MGZD073	187.6	188.3	0.7	D07874	0.72	0.34	0.24	0.24
Comp C42	60760	MGZD073	188.3	189	0.7	D07875	0.71	0.37	0.26	0.26
Comp C42	60760	MGZD073	199	200	1.0	D07889	1.33	0.35	0.35	0.47
Comp C42	60760	MGZD073	200	201	1.0	D07890	1.16	0.28	0.28	0.32
Comp C42	60760	MGZD073	201	202	1.0	D07891	1.22	0.39	0.39	0.48
Comp C42	60760	MGZD275	242.3	243	0.7	D73145	0.77	0.29	0.20	0.22
Comp C42	60760	MGZD275	259.1	260	0.9	D73173	1.15	0.37	0.33	0.43
Comp C42	60760	MGZD288	261.2	262	0.8	D78296	0.84	0.26	0.21	0.22
Comp C42	60800	MGZD157	229.7	230.4	0.7	D34280	0.81	0.28	0.20	0.23
Comp C42	60800	MGZD160	215	216	1.0	D35003	1.11	0.36	0.36	0.40
Comp C42	60800	MGZD160	218	219	1.0	D35006	1.19	0.36	0.36	0.43
Comp C42	60800	MGZD160	222	222.7	0.7	D35010	0.86	0.30	0.21	0.26
Comp C42	60800	MGZD160	222.7	223.4	0.7	D35011	0.84	0.34	0.24	0.29
Comp C42	60800	MGZD160	226.9	227.6	0.7	D35017	0.9	0.26	0.18	0.23
Comp C42	60840	MGZD161	170.4	171.1	0.7	D35319	0.77	0.35	0.25	0.27
Comp C42	60840	MGZD161	171.1	171.8	0.7	D35320	0.8	0.31	0.22	0.25
Comp C42	60840	MGZD161	198.7	199.4	0.7	D35355	0.8	0.34	0.24	0.27
Comp C42	60840	MGZD161	222	223	1.0	D35383	1.08	0.34	0.34	0.37
Comp C42	60840	MGZD161	224.7	225.4	0.7	D35386	0.96	0.28	0.20	0.27
Comp C43	60640	MGZD079	248	249	1.0	D09015	1.07	0.55	0.55	0.59
Comp C43	60640	MGZD181	148	149	1.0	D40991	1.04	0.73	0.73	0.76
Comp C43	60640	MGZD181	234.1	234.8	0.7	D41099	0.84	0.45	0.32	0.38
Comp C43	60640	MGZD246	149.9	150.6	0.7	D63099	0.66	0.45	0.31	0.30
Comp C43	60640	MGZD246	155.5	156.2	0.7	D63107	0.75	0.80	0.56	0.60
Comp C43	60640	MGZD276	202	202.7	0.7	D73482	0.84	0.65	0.45	0.55
Comp C43	60680	MGZD178	232	232.7	0.7	D39859	0.98	0.41	0.29	0.40
Comp C43	60680	MGZD218	205	206	1.0	D51492	1.11	0.75	0.75	0.83
Comp C43	60680	MGZD218	207.7	208.4	0.7	D51495	0.78	0.63	0.44	0.49
Comp C43	60720	MGZD182	154.2	154.9	0.7	D41711	0.94	0.42	0.29	0.39
Comp C43	60720	MGZD191	145.4	146.1	0.7	D42904	0.68	0.50	0.35	0.34
Comp C43	60720	MGZD191	148.9	149.6	0.7	D42909	0.62	0.75	0.52	0.47

C ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp C43	60720	MGZD191	150.3	151	0.7	D42911	0.75	0.42	0.29	0.32
Comp C43	60720	MGZD191	152.4	153.1	0.7	D42914	0.83	0.46	0.32	0.38
Comp C43	60720	MGZD196	157.9	158.6	0.7	D44332	0.65	0.57	0.40	0.37
Comp C43	60720	MGZD196	158.6	159.3	0.7	D44333	0.72	0.46	0.32	0.33
Comp C43	60720	MGZD196	159.3	160	0.7	D44334	0.8	0.56	0.39	0.45
Comp C43	60720	MGZD196	186	187	1.0	D44368	1.1	0.62	0.62	0.68
Comp C43	60720	MGZD196	197.5	198.2	0.7	D44386	0.66	0.49	0.34	0.32
Comp C43	60720	MGZD196	203.1	203.8	0.7	D44394	0.62	0.73	0.51	0.45
Comp C43	60720	MGZD196	205.2	205.9	0.7	D44399	0.82	0.60	0.42	0.49
Comp C43	60720	MGZD196	205.9	206.6	0.7	D44400	0.76	0.75	0.52	0.57
Comp C43	60720	MGZD196	213.7	214.4	0.7	D44409	0.84	0.75	0.52	0.63
Comp C43	60720	MGZD196	215.1	215.8	0.7	D44411	0.72	0.56	0.39	0.40
Comp C43	60720	MGZD196	221.4	222.1	0.7	D44422	0.84	0.65	0.45	0.55
Comp C43	60720	MGZD203	239.3	240	0.7	D46180	0.74	0.46	0.32	0.34
Comp C43	60720	MGZD203	249.1	249.8	0.7	D46194	0.79	0.78	0.55	0.62
Comp C43	60720	MGZD203	256.1	256.8	0.7	D46206	0.82	0.46	0.32	0.38
Comp C43	60720	MGZD203	258.2	258.9	0.7	D46209	0.88	0.67	0.47	0.59
Comp C43	60720	MGZD203	260.3	261	0.7	D46212	0.73	0.43	0.30	0.31
Comp C43	60720	MGZD203	261.7	262.4	0.7	D46214	0.71	0.45	0.31	0.32
Comp C43	60720	MGZD203	267.3	268	0.7	D46224	0.85	0.58	0.41	0.49
Comp C43	60720	MGZD253	242	243	1.0	D65706	1.12	0.56	0.56	0.63
Comp C43	60720	MGZD253	247	248	1.0	D65711	1.14	0.44	0.44	0.50
Comp C43	60720	MGZD253	250.1	251	0.9	D65715	0.95	0.71	0.64	0.67
Comp C43	60720	MGZD264	230	231	1.0	D68910	0.98	0.43	0.43	0.42
Comp C43	60720	MGZD264	234	235	1.0	D68914	1.16	0.53	0.53	0.61
Comp C43	60720	MGZD264	258	258.7	0.7	D68942	0.82	0.60	0.42	0.49
Comp C43	60720	MGZD264	267	268	1.0	D68955	1.18	0.80	0.80	0.94
Comp C43	60720	MGZD268	240	241	1.0	D71010	1.16	0.75	0.75	0.87
Comp C43	60720	MGZD268	255.5	256.2	0.7	D71029	0.82	0.42	0.29	0.34
Comp C43	60720	MGZD268	296	296.7	0.7	D71079	0.91	0.48	0.34	0.44
Comp C43	60720	MGZD268	299.5	300.2	0.7	D71084	0.73	0.63	0.44	0.46
Comp C43	60760	MGZD043	250.5	251.2	0.7	D04285	0.74	0.53	0.37	0.39
Comp C43	60760	MGZD043	256.1	257	0.9	D04294	1.04	0.63	0.57	0.66
Comp C43	60760	MGZD045	250.4	251.1	0.7	D04584	0.73	0.59	0.41	0.43
Comp C43	60760	MGZD045	251.1	252	0.9	D04585	0.96	0.45	0.41	0.43
Comp C43	60760	MGZD045	252	252.7	0.7	D04586	0.73	0.64	0.45	0.47
Comp C43	60760	MGZD046	139.4	140.1	0.7	D04769	0.67	0.80	0.56	0.54
Comp C43	60760	MGZD046	140.1	141	0.9	D04770	0.9	0.56	0.50	0.50
Comp C43	60760	MGZD046	142	143	1.0	D04773	1.11	0.45	0.45	0.50
Comp C43	60760	MGZD046	144.7	145.4	0.7	D04776	0.81	0.62	0.43	0.50
Comp C43	60760	MGZD073	184.1	184.8	0.7	D07867	0.68	0.69	0.48	0.47
Comp C43	60760	MGZD073	184.8	185.5	0.7	D07868	0.65	0.80	0.56	0.52
Comp C43	60760	MGZD073	185.5	186.2	0.7	D07869	0.71	0.77	0.54	0.55
Comp C43	60760	MGZD073	189.7	190.4	0.7	D07877	0.69	0.70	0.49	0.48
Comp C43	60760	MGZD073	209	210	1.0	D07901	1.1	0.48	0.48	0.53
Comp C43	60760	MGZD073	210	211	1.0	D07902	1.17	0.41	0.41	0.48
Comp C43	60760	MGZD073	213.1	214	0.9	D07907	1.04	0.71	0.64	0.74
Comp C43	60760	MGZD275	238.1	238.8	0.7	D73137	0.84	0.47	0.33	0.39
Comp C43	60760	MGZD275	245.8	246.5	0.7	D73151	0.82	0.69	0.48	0.57
Comp C43	60760	MGZD275	257	257.7	0.7	D73169	0.96	0.43	0.30	0.41
Comp C43	60760	MGZD275	258.4	259.1	0.7	D73172	0.88	0.57	0.40	0.50
Comp C43	60760	MGZD275	261	262	1.0	D73176	1.2	0.44	0.44	0.53
Comp C43	60760	MGZD283	225	226	1.0	D76296	1.1	0.69	0.69	0.76
Comp C43	60760	MGZD283	226	227	1.0	D76297	1.08	0.48	0.48	0.52
Comp C43	60760	MGZD283	228	229	1.0	D76301	1.13	0.56	0.56	0.63

C ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp C43	60760	MGZD283	233	234	1.0	D76306	1.24	0.41	0.41	0.51
Comp C43	60760	MGZD283	235	235.8	0.8	D76308	0.83	0.41	0.33	0.34
Comp C43	60760	MGZD288	259.1	259.8	0.7	D78292	0.84	0.75	0.52	0.63
Comp C43	60800	MGZD160	214	215	1.0	D35002	1.15	0.54	0.54	0.62
Comp C43	60800	MGZD160	227.6	228.3	0.7	D35019	0.84	0.66	0.46	0.55
Comp C43	60800	MGZD160	246.7	247.4	0.7	D35045	0.76	0.67	0.47	0.51
Comp C43	60800	MGZD160	247.4	248.1	0.7	D35047	0.88	0.77	0.54	0.68
Comp C43	60840	MGZD077	216	216.7	0.7	D08753	0.77	0.69	0.48	0.53
Comp C43	60840	MGZD077	217.4	218.1	0.7	D08755	0.74	0.46	0.32	0.34
Comp C43	60840	MGZD077	218.1	218.8	0.7	D08756	0.76	0.52	0.36	0.40
Comp C43	60840	MGZD077	229.3	230	0.7	D08774	0.8	0.48	0.34	0.38
Comp C43	60840	MGZD153	225	226	1.0	D32714	1.29	0.72	0.72	0.93
Comp C43	60840	MGZD161	185.1	185.8	0.7	D35337	0.81	0.61	0.43	0.49
Comp C43	60840	MGZD161	197	198	1.0	D35353	1.21	0.51	0.51	0.62
Comp C43	60840	MGZD161	198	198.7	0.7	D35354	0.83	0.63	0.44	0.52
Comp C43	60840	MGZD161	236	237	1.0	D35400	1.17	0.53	0.53	0.62
Comp C43	60840	MGZD161	237	238	1.0	D35401	1.19	0.49	0.49	0.58
Comp C44	60640	MGZD079	229	230	1.0	D08993	1.15	0.84	0.84	0.97
Comp C44	60640	MGZD079	245	246	1.0	D09012	1.09	0.86	0.86	0.94
Comp C44	60640	MGZD079	249	250	1.0	D09016	1.15	0.91	0.91	1.05
Comp C44	60640	MGZD080	203	204	1.0	D09142	1.15	1.20	1.20	1.38
Comp C44	60640	MGZD181	181.3	182	0.7	D41035	0.76	0.90	0.63	0.68
Comp C44	60640	MGZD276	196	196.7	0.7	D73472	0.86	0.92	0.64	0.79
Comp C44	60640	MGZD276	218.1	218.8	0.7	D73504	0.99	1.00	0.70	0.99
Comp C44	60640	MGZD279	251.9	252.6	0.7	D74786	0.73	1.19	0.83	0.87
Comp C44	60640	MGZD279	287	288	1.0	D74833	1.33	0.81	0.81	1.08
Comp C44	60680	MGZD173	218.2	218.9	0.7	D38734	0.93	0.96	0.67	0.89
Comp C44	60680	MGZD178	234.8	235.5	0.7	D39863	0.83	1.12	0.78	0.93
Comp C44	60680	MGZD178	269.4	270.1	0.7	D39915	0.56	1.17	0.82	0.66
Comp C44	60720	MGZD097	250.6	251.3	0.7	D12177	0.73	1.09	0.76	0.80
Comp C44	60720	MGZD097	255.5	256.2	0.7	D12185	0.78	1.28	0.90	1.00
Comp C44	60720	MGZD182	140.2	140.9	0.7	D41689	0.89	0.97	0.68	0.86
Comp C44	60720	MGZD182	143	143.7	0.7	D41693	0.85	1.11	0.78	0.94
Comp C44	60720	MGZD191	144.7	145.4	0.7	D42903	0.66	0.88	0.62	0.58
Comp C44	60720	MGZD191	146.8	147.5	0.7	D42906	0.65	1.25	0.87	0.81
Comp C44	60720	MGZD196	187.7	188.4	0.7	D44370	0.71	1.28	0.90	0.91
Comp C44	60720	MGZD196	190.5	191.2	0.7	D44375	0.7	1.30	0.91	0.91
Comp C44	60720	MGZD196	191.9	192.6	0.7	D44377	0.64	0.91	0.64	0.58
Comp C44	60720	MGZD196	198.2	198.9	0.7	D44387	0.74	1.14	0.80	0.84
Comp C44	60720	MGZD196	222.1	222.8	0.7	D44423	0.81	0.96	0.67	0.78
Comp C44	60720	MGZD203	237.2	237.9	0.7	D46176	0.76	1.10	0.77	0.84
Comp C44	60720	MGZD203	257.5	258.2	0.7	D46208	1	0.85	0.59	0.85
Comp C44	60720	MGZD248	160.9	161.6	0.7	D63400	0.76	0.91	0.64	0.69
Comp C44	60720	MGZD253	243	244	1.0	D65707	1.12	0.88	0.88	0.99
Comp C44	60720	MGZD253	248	248.7	0.7	D65712	0.84	1.13	0.79	0.95
Comp C44	60720	MGZD264	235	236	1.0	D68915	1.01	1.27	1.27	1.28
Comp C44	60720	MGZD264	242	243	1.0	D68924	1.07	1.08	1.08	1.16
Comp C44	60720	MGZD264	251	252	1.0	D68934	1.12	0.88	0.88	0.99
Comp C44	60720	MGZD268	210	211	1.0	D70976	0.93	1.28	1.28	1.19
Comp C44	60720	MGZD268	214	215	1.0	D70981	1.28	1.05	1.05	1.34
Comp C44	60720	MGZD268	251	252	1.0	D71023	1.14	1.18	1.18	1.35
Comp C44	60720	MGZD268	274	275	1.0	D71053	1.17	1.09	1.09	1.28
Comp C44	60720	MGZD268	275	276	1.0	D71054	1.14	1.25	1.25	1.43
Comp C44	60720	MGZD268	295	296	1.0	D71077	1.18	0.96	0.96	1.13
Comp C44	60760	MGZD043	155.7	156.4	0.7	D04218	0.75	0.92	0.64	0.69

C ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp C44	60760	MGZD043	155.7	156.4	0.7	D04218	0.75	0.92	0.64	0.69
Comp C44	60760	MGZD043	157.1	157.8	0.7	D04220	0.84	1.14	0.80	0.96
Comp C44	60760	MGZD043	251.2	251.9	0.7	D04286	0.78	1.17	0.82	0.91
Comp C44	60760	MGZD043	255.4	256.1	0.7	D04293	0.84	1.30	0.91	1.09
Comp C44	60760	MGZD073	142.6	143.3	0.7	D07814	0.82	0.86	0.60	0.71
Comp C44	60760	MGZD073	146.1	146.8	0.7	D07819	0.07	1.05	0.74	0.07
Comp C44	60760	MGZD073	146.8	147.5	0.7	D07820	0.72	1.00	0.70	0.72
Comp C44	60760	MGZD073	182	182.7	0.7	D07864	0.71	1.04	0.73	0.74
Comp C44	60760	MGZD073	183.4	184.1	0.7	D07866	0.62	1.03	0.72	0.64
Comp C44	60760	MGZD073	186.2	186.9	0.7	D07870	0.66	1.27	0.89	0.84
Comp C44	60760	MGZD073	198.1	199	0.9	D07887	1.17	0.99	0.89	1.16
Comp C44	60760	MGZD073	207	208	1.0	D07899	1.13	0.88	0.88	0.99
Comp C44	60760	MGZD073	212.4	213.1	0.7	D07906	0.88	0.96	0.67	0.84
Comp C44	60760	MGZD275	229.7	230.4	0.7	D73123	0.8	0.97	0.68	0.78
Comp C44	60760	MGZD275	230.4	231.1	0.7	D73124	0.83	1.18	0.83	0.98
Comp C44	60760	MGZD275	262	263	1.0	D73177	1.25	1.05	1.05	1.31
Comp C44	60760	MGZD283	227	228	1.0	D76299	1.17	0.91	0.91	1.06
Comp C44	60760	MGZD283	235.8	236.5	0.7	D76309	1.03	0.89	0.62	0.92
Comp C44	60760	MGZD288	263.6	264.3	0.7	D78301	0.68	1.05	0.73	0.71
Comp C44	60800	MGZD151	195.4	196.1	0.7	D32364	0.85	0.81	0.57	0.69
Comp C44	60800	MGZD157	230.4	231.1	0.7	D34281	0.75	1.04	0.73	0.78
Comp C44	60800	MGZD157	231.1	231.8	0.7	D34282	0.75	0.95	0.67	0.71
Comp C44	60800	MGZD160	229	229.7	0.7	D35022	0.84	1.04	0.73	0.87
Comp C44	60800	MGZD160	229.7	230.4	0.7	D35023	0.83	0.97	0.68	0.81
Comp C44	60800	MGZD160	230.4	231.1	0.7	D35024	0.87	0.98	0.69	0.85
Comp C44	60840	MGZD075	205	206	1.0	D08028	1.22	1.11	1.11	1.35
Comp C44	60840	MGZD076	224.4	225.1	0.7	D08136	0.76	0.94	0.66	0.71
Comp C44	60840	MGZD077	226.5	227.2	0.7	D08769	0.62	1.20	0.84	0.74
Comp C44	60840	MGZD153	228.4	229.1	0.7	D32719	0.81	1.22	0.85	0.99
Comp C44	60840	MGZD161	171.8	172.5	0.7	D35322	0.91	1.16	0.81	1.06
Comp C44	60840	MGZD161	200.1	200.8	0.7	D35357	0.82	0.99	0.69	0.81
Comp C45	60640	MGZD079	240.7	241.4	0.7	D09007	0.71	2.20	1.54	1.56
Comp C45	60640	MGZD080	202	203	1.0	D09141	1.12	2.04	2.04	2.28
Comp C45	60640	MGZD080	206.1	206.8	0.7	D09147	0.75	2.16	1.51	1.62
Comp C45	60640	MGZD080	206.8	207.5	0.7	D09148	0.72	1.41	0.99	1.02
Comp C45	60640	MGZD181	159.4	160.1	0.7	D41005	0.73	1.37	0.96	1.00
Comp C45	60640	MGZD181	160.1	160.8	0.7	D41006	0.68	2.18	1.53	1.48
Comp C45	60640	MGZD188	245.7	246.4	0.7	D42153	0.8	1.57	1.10	1.26
Comp C45	60640	MGZD188	246.4	247.1	0.7	D42154	0.78	1.79	1.25	1.40
Comp C45	60640	MGZD246	147.8	148.5	0.7	D63094	0.66	1.64	1.15	1.08
Comp C45	60640	MGZD246	148.5	149.2	0.7	D63095	0.72	1.88	1.32	1.35
Comp C45	60640	MGZD246	149.2	149.9	0.7	D63097	0.69	1.83	1.28	1.26
Comp C45	60640	MGZD246	163.9	164.6	0.7	D63120	0.77	2.37	1.66	1.82
Comp C45	60640	MGZD258	258.6	259.3	0.7	D67565	0.79	2.25	1.57	1.78
Comp C45	60640	MGZD269	249.1	249.8	0.7	D71400	0.65	1.66	1.16	1.08
Comp C45	60640	MGZD276	196.7	197.4	0.7	D73473	0.76	1.91	1.34	1.45
Comp C45	60640	MGZD276	216	216.7	0.7	D73501	0.89	2.28	1.60	2.03
Comp C45	60640	MGZD279	239.7	240.4	0.7	D74768	0.95	1.92	1.34	1.82
Comp C45	60640	MGZD279	261.5	262.2	0.7	D74801	0.87	1.86	1.30	1.62
Comp C45	60680	MGZD167	131	132	1.0	D37207	1.12	1.52	1.52	1.70
Comp C45	60680	MGZD173	164.9	165.6	0.7	D38669	0.86	1.72	1.20	1.48
Comp C45	60680	MGZD173	165.6	166.3	0.7	D38670	0.73	2.31	1.62	1.69
Comp C45	60680	MGZD173	237	238	1.0	D38756	0.98	1.68	1.68	1.65
Comp C45	60680	MGZD178	231	232	1.0	D39857	1.33	2.38	2.38	3.17
Comp C45	60680	MGZD178	236.9	237.6	0.7	D39866	0.72	1.53	1.07	1.10

C ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp C45	60680	MGZD178	248.4	249.1	0.7	D39883	0.95	2.05	1.43	1.95
Comp C45	60680	MGZD178	249.1	249.8	0.7	D39884	0.93	1.34	0.94	1.25
Comp C45	60680	MGZD178	256.1	256.8	0.7	D39894	0.98	1.77	1.24	1.73
Comp C45	60680	MGZD218	163.8	164.5	0.7	D51437	0.73	1.96	1.37	1.43
Comp C45	60680	MGZD218	164.5	165.2	0.7	D51439	0.68	2.38	1.67	1.62
Comp C45	60680	MGZD218	204	205	1.0	D51491	1.05	2.26	2.26	2.37
Comp C45	60680	MGZD257	155.7	156.4	0.7	D66643	0.84	1.76	1.23	1.48
Comp C45	60680	MGZD262	239.2	240	0.8	D68528	0.92	1.91	1.53	1.76
Comp C45	60680	MGZD266	242	243	1.0	D69910	1.05	2.19	2.19	2.30
Comp C45	60680	MGZD280	256.1	256.8	0.7	D75237	0.79	1.83	1.28	1.45
Comp C45	60680	MGZD280	282.7	283.4	0.7	D75272	0.82	1.70	1.19	1.39
Comp C45	60680	MGZD280	283.4	284.1	0.7	D75273	0.76	1.97	1.38	1.50
Comp C45	60680	MGZD280	284.8	285.5	0.7	D75276	0.78	1.48	1.04	1.15
Comp C45	60680	MGZD286	271	272	1.0	D77424	1.27	2.00	2.00	2.54
Comp C45	60720	MGZD097	245	245.7	0.7	D12168	0.77	2.38	1.67	1.83
Comp C45	60720	MGZD097	246.4	247.1	0.7	D12170	0.64	2.34	1.64	1.50
Comp C45	60720	MGZD097	247.1	247.8	0.7	D12172	0.63	1.39	0.97	0.88
Comp C45	60720	MGZD097	247.8	248.5	0.7	D12173	0.69	1.78	1.25	1.23
Comp C45	60720	MGZD097	248.5	249.2	0.7	D12174	0.71	1.73	1.21	1.23
Comp C45	60720	MGZD097	249.2	249.9	0.7	D12175	0.73	1.55	1.09	1.13
Comp C45	60720	MGZD097	249.9	250.6	0.7	D12176	0.79	1.79	1.25	1.41
Comp C45	60720	MGZD182	143.7	144.4	0.7	D41694	0.82	1.49	1.04	1.22
Comp C45	60720	MGZD182	152.1	152.8	0.7	D41708	0.88	1.58	1.11	1.39
Comp C45	60720	MGZD182	153.5	154.2	0.7	D41710	0.82	1.65	1.15	1.35
Comp C45	60720	MGZD191	139.1	139.8	0.7	D42893	0.72	1.58	1.11	1.14
Comp C45	60720	MGZD191	139.8	140.5	0.7	D42894	0.73	1.98	1.39	1.45
Comp C45	60720	MGZD191	144	144.7	0.7	D42902	0.66	2.28	1.60	1.50
Comp C45	60720	MGZD196	194.7	195.4	0.7	D44382	0.77	1.64	1.15	1.26
Comp C45	60720	MGZD196	204.5	205.2	0.7	D44397	0.78	1.64	1.15	1.28
Comp C45	60720	MGZD196	206.6	207.3	0.7	D44401	0.78	1.43	1.00	1.12
Comp C45	60720	MGZD196	214.4	215.1	0.7	D44410	0.7	1.53	1.07	1.07
Comp C45	60720	MGZD196	224.2	224.9	0.7	D44426	0.77	1.57	1.10	1.21
Comp C45	60720	MGZD196	227.7	228.4	0.7	D44431	0.62	1.80	1.26	1.12
Comp C45	60720	MGZD196	228.4	229.1	0.7	D44432	0.65	1.92	1.34	1.25
Comp C45	60720	MGZD203	237.9	238.6	0.7	D46177	0.6	1.40	0.98	0.84
Comp C45	60720	MGZD203	238.6	239.3	0.7	D46179	0.76	1.41	0.99	1.07
Comp C45	60720	MGZD203	240	240.7	0.7	D46181	0.72	2.13	1.49	1.53
Comp C45	60720	MGZD203	243.5	244.2	0.7	D46186	0.81	1.93	1.35	1.56
Comp C45	60720	MGZD203	245.6	246.3	0.7	D46189	0.74	1.39	0.97	1.03
Comp C45	60720	MGZD203	251.2	251.9	0.7	D46199	0.7	1.91	1.34	1.34
Comp C45	60720	MGZD203	263.8	264.5	0.7	D46217	0.75	1.87	1.31	1.40
Comp C45	60720	MGZD253	241	242	1.0	D65705	1.13	1.34	1.34	1.51
Comp C45	60720	MGZD253	252	253	1.0	D65717	0.98	1.67	1.67	1.64
Comp C45	60720	MGZD264	224	225	1.0	D68904	1.02	2.18	2.18	2.22
Comp C45	60720	MGZD264	245.1	246	0.9	D68928	0.97	1.98	1.78	1.92
Comp C45	60720	MGZD268	253.4	254.1	0.7	D71026	0.81	1.31	0.92	1.06
Comp C45	60720	MGZD268	254.1	254.8	0.7	D71027	0.74	2.14	1.50	1.58
Comp C45	60720	MGZD268	256.2	256.9	0.7	D71030	0.82	1.39	0.97	1.14
Comp C45	60720	MGZD268	256.9	257.6	0.7	D71031	0.82	2.24	1.57	1.84
Comp C45	60720	MGZD268	258.3	259	0.7	D71033	0.74	2.37	1.66	1.75
Comp C45	60720	MGZD268	298.1	298.8	0.7	D71082	0.77	1.73	1.21	1.33
Comp C45	60760	MGZD043	150.4	151.1	0.7	D04211	0.77	1.98	1.39	1.52
Comp C45	60760	MGZD043	150.4	151.1	0.7	D04211	0.77	1.98	1.39	1.52
Comp C45	60760	MGZD043	157.8	158.5	0.7	D04222	0.88	1.37	0.96	1.21
Comp C45	60760	MGZD043	225	225.7	0.7	D04252	0.77	1.57	1.10	1.21

C ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp C45	60760	MGZD043	237.7	238.4	0.7	D04268	0.86	1.44	1.01	1.24
Comp C45	60760	MGZD043	238.4	239.1	0.7	D04269	0.78	2.34	1.64	1.83
Comp C45	60760	MGZD043	239.1	240	0.9	D04270	1.02	1.57	1.41	1.60
Comp C45	60760	MGZD043	249.8	250.5	0.7	D04284	0.82	1.31	0.92	1.07
Comp C45	60760	MGZD043	251.9	252.6	0.7	D04287	0.74	2.17	1.52	1.61
Comp C45	60760	MGZD043	254	254.7	0.7	D04291	0.78	2.35	1.64	1.83
Comp C45	60760	MGZD046	138.7	139.4	0.7	D04767	0.83	1.66	1.16	1.38
Comp C45	60760	MGZD046	144	144.7	0.7	D04775	0.77	1.91	1.34	1.47
Comp C45	60760	MGZD073	143.3	144	0.7	D07815	0.74	1.79	1.25	1.32
Comp C45	60760	MGZD073	144	144.7	0.7	D07816	0.69	1.88	1.32	1.30
Comp C45	60760	MGZD073	144.7	145.4	0.7	D07817	0.78	2.16	1.51	1.68
Comp C45	60760	MGZD073	186.9	187.6	0.7	D07872	0.74	1.45	1.01	1.07
Comp C45	60760	MGZD073	196	196.7	0.7	D07884	0.57	1.47	1.03	0.84
Comp C45	60760	MGZD073	202	203	1.0	D07892	1.22	1.31	1.31	1.60
Comp C45	60760	MGZD275	236	236.7	0.7	D73133	0.82	1.79	1.25	1.47
Comp C45	60760	MGZD275	238.8	239.5	0.7	D73139	0.77	1.37	0.96	1.05
Comp C45	60760	MGZD275	246.5	247.2	0.7	D73152	0.85	1.91	1.34	1.62
Comp C45	60760	MGZD275	247.2	247.9	0.7	D73153	0.82	1.91	1.34	1.57
Comp C45	60760	MGZD288	264.3	265	0.7	D78302	0.72	1.80	1.26	1.30
Comp C45	60800	MGZD154	233.2	233.9	0.7	D33414	0.82	1.40	0.98	1.15
Comp C45	60800	MGZD154	240.9	241.6	0.7	D33427	0.72	1.40	0.98	1.01
Comp C45	60800	MGZD160	217	218	1.0	D35005	1.22	1.33	1.33	1.62
Comp C45	60800	MGZD160	228.3	229	0.7	D35020	0.76	2.40	1.68	1.82
Comp C45	60840	MGZD076	215.4	216.1	0.7	D08124	0.63	1.57	1.10	0.99
Comp C45	60840	MGZD076	216.8	217.5	0.7	D08126	0.68	1.37	0.96	0.93
Comp C45	60840	MGZD076	228	228.7	0.7	D08140	0.75	1.59	1.11	1.19
Comp C45	60840	MGZD077	214.6	215.3	0.7	D08751	0.79	2.20	1.54	1.74
Comp C45	60840	MGZD077	215.3	216	0.7	D08752	0.81	1.57	1.10	1.27
Comp C45	60840	MGZD077	225.8	226.5	0.7	D08768	0.66	2.19	1.53	1.45
Comp C45	60840	MGZD077	227.2	227.9	0.7	D08770	0.73	2.07	1.45	1.51
Comp C45	60840	MGZD077	228.6	229.3	0.7	D08773	0.8	2.00	1.40	1.60
Comp C45	60840	MGZD153	229.1	229.8	0.7	D32720	0.81	2.37	1.66	1.92
Comp C45	60840	MGZD153	229.8	230.5	0.7	D32722	0.8	1.98	1.39	1.58
Comp C45	60840	MGZD153	231.2	231.9	0.7	D32724	0.87	2.32	1.62	2.02
Comp C45	60840	MGZD161	185.8	186.5	0.7	D35339	0.79	1.46	1.02	1.15
Comp C45	60840	MGZD161	186.5	187.2	0.7	D35340	0.78	2.34	1.64	1.83
Comp C45	60840	MGZD161	224	224.7	0.7	D35385	0.77	1.32	0.92	1.02
Comp C46	60640	MGZD079	244	245	1.0	D09011	1.13	3.80	3.80	4.29
Comp C46	60640	MGZD079	246	247	1.0	D09013	1.04	3.75	3.75	3.90
Comp C46	60640	MGZD079	247	248	1.0	D09014	1.08	2.99	2.99	3.23
Comp C46	60640	MGZD080	208.2	208.9	0.7	D09150	0.7	3.83	2.68	2.68
Comp C46	60640	MGZD181	149	150	1.0	D40992	1.09	2.46	2.46	2.68
Comp C46	60640	MGZD181	158.7	159.4	0.7	D41004	0.71	3.12	2.18	2.22
Comp C46	60640	MGZD181	179.2	179.9	0.7	D41032	0.85	3.13	2.19	2.66
Comp C46	60640	MGZD181	180.6	181.3	0.7	D41034	0.8	2.92	2.04	2.34
Comp C46	60640	MGZD181	184.8	185.5	0.7	D41041	0.81	2.47	1.73	2.00
Comp C46	60640	MGZD181	233.4	234.1	0.7	D41097	0.86	2.46	1.72	2.12
Comp C46	60640	MGZD181	235.5	236.2	0.7	D41101	0.8	3.84	2.69	3.07
Comp C46	60640	MGZD188	238.7	239.4	0.7	D42142	0.83	2.81	1.97	2.33
Comp C46	60640	MGZD188	245	245.7	0.7	D42152	0.81	4.00	2.80	3.24
Comp C46	60640	MGZD188	305	306	1.0	D42222	1.21	2.81	2.81	3.40
Comp C46	60640	MGZD246	152	152.7	0.7	D63102	0.69	3.30	2.31	2.28
Comp C46	60640	MGZD246	154.8	155.5	0.7	D63106	0.54	2.81	1.97	1.52
Comp C46	60640	MGZD269	248.4	249.1	0.7	D71399	0.67	3.00	2.10	2.01
Comp C46	60640	MGZD276	195	196	1.0	D73471	1.25	2.62	2.62	3.28

C ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp C46	60640	MGZD276	198.1	199	0.9	D73476	1.22	2.67	2.40	3.26
Comp C46	60640	MGZD276	202.7	203.4	0.7	D73483	0.79	3.17	2.22	2.50
Comp C46	60640	MGZD276	256	257	1.0	D73553	1.34	3.24	3.24	4.34
Comp C46	60640	MGZD279	240.4	241.2	0.8	D74769	1.01	3.38	2.70	3.41
Comp C46	60640	MGZD279	288	288.8	0.8	D74834	0.9	2.94	2.35	2.65
Comp C46	60680	MGZD167	130	131	1.0	D37206	1.14	2.71	2.71	3.09
Comp C46	60680	MGZD167	138	139	1.0	D37214	0.94	3.75	3.75	3.53
Comp C46	60680	MGZD173	166.3	167	0.7	D38672	0.76	3.82	2.67	2.90
Comp C46	60680	MGZD173	218.9	219.6	0.7	D38735	0.79	3.89	2.72	3.07
Comp C46	60680	MGZD173	238	239	1.0	D38757	1.23	3.60	3.60	4.43
Comp C46	60680	MGZD178	236.2	236.9	0.7	D39865	0.73	3.11	2.18	2.27
Comp C46	60680	MGZD178	237.6	238.3	0.7	D39867	0.78	3.36	2.35	2.62
Comp C46	60680	MGZD178	256.8	257.5	0.7	D39895	0.92	3.80	2.66	3.50
Comp C46	60680	MGZD218	181.8	182.5	0.7	D51462	0.72	2.94	2.06	2.12
Comp C46	60680	MGZD218	188.1	188.8	0.7	D51472	0.64	3.73	2.61	2.39
Comp C46	60680	MGZD218	207	207.7	0.7	D51494	0.75	2.45	1.71	1.84
Comp C46	60680	MGZD218	229.7	230.4	0.7	D51522	0.65	2.64	1.85	1.72
Comp C46	60680	MGZD257	156.4	157.1	0.7	D66644	0.84	3.64	2.55	3.06
Comp C46	60680	MGZD262	261.1	261.8	0.7	D68553	0.61	3.76	2.63	2.29
Comp C46	60680	MGZD280	255.4	256.1	0.7	D75236	0.75	3.98	2.79	2.99
Comp C46	60680	MGZD286	270	271	1.0	D77423	1.23	2.51	2.51	3.09
Comp C46	60720	MGZD182	152.8	153.5	0.7	D41709	0.92	2.60	1.82	2.39
Comp C46	60720	MGZD191	141.2	141.9	0.7	D42897	0.76	2.78	1.95	2.11
Comp C46	60720	MGZD191	148.2	148.9	0.7	D42908	0.86	2.50	1.75	2.15
Comp C46	60720	MGZD191	149.6	150.3	0.7	D42910	0.66	3.16	2.21	2.09
Comp C46	60720	MGZD196	157.2	157.9	0.7	D44331	0.62	2.64	1.85	1.64
Comp C46	60720	MGZD196	191.2	191.9	0.7	D44376	0.66	2.87	2.01	1.89
Comp C46	60720	MGZD196	194	194.7	0.7	D44381	0.76	2.73	1.91	2.07
Comp C46	60720	MGZD196	203.8	204.5	0.7	D44395	0.75	2.54	1.78	1.91
Comp C46	60720	MGZD203	235.8	236.5	0.7	D46174	0.78	3.36	2.35	2.62
Comp C46	60720	MGZD203	246.3	247	0.7	D46190	0.81	3.50	2.45	2.84
Comp C46	60720	MGZD203	247.7	248.4	0.7	D46192	0.73	3.02	2.11	2.20
Comp C46	60720	MGZD203	250.5	251.2	0.7	D46197	0.81	2.84	1.99	2.30
Comp C46	60720	MGZD203	254	254.7	0.7	D46203	0.82	2.67	1.87	2.19
Comp C46	60720	MGZD253	249.4	250.1	0.7	D65714	0.77	2.49	1.74	1.92
Comp C46	60720	MGZD253	254.7	255.4	0.7	D65722	0.79	2.71	1.90	2.14
Comp C46	60720	MGZD264	262.2	262.9	0.7	D68949	0.72	3.18	2.23	2.29
Comp C46	60720	MGZD268	264.7	265.4	0.7	D71041	0.82	2.52	1.76	2.07
Comp C46	60760	MGZD043	159.2	159.9	0.7	D04224	0.74	2.65	1.86	1.96
Comp C46	60760	MGZD043	224	225	1.0	D04251	1.16	2.41	2.41	2.80
Comp C46	60760	MGZD043	225.7	226.4	0.7	D04253	0.68	2.92	2.04	1.99
Comp C46	60760	MGZD043	226.4	227.1	0.7	D04254	0.75	3.91	2.74	2.93
Comp C46	60760	MGZD043	265.4	266.1	0.7	D04306	0.73	3.54	2.48	2.58
Comp C46	60760	MGZD043	266.8	267.5	0.7	D04308	0.77	3.97	2.78	3.06
Comp C46	60760	MGZD045	246	247	1.0	D04579	0.96	3.63	3.63	3.48
Comp C46	60760	MGZD045	247	248	1.0	D04580	0.92	3.45	3.45	3.17
Comp C46	60760	MGZD045	252.7	253.4	0.7	D04587	0.74	2.83	1.98	2.09
Comp C46	60760	MGZD045	256.2	257	0.8	D04593	0.94	2.69	2.15	2.53
Comp C46	60760	MGZD073	147.5	148.2	0.7	D07822	0.72	3.07	2.15	2.21
Comp C46	60760	MGZD073	211.7	212.4	0.7	D07905	0.84	2.47	1.73	2.07
Comp C46	60760	MGZD275	231.1	231.8	0.7	D73125	0.81	2.41	1.69	1.95
Comp C46	60760	MGZD275	241.6	242.3	0.7	D73144	0.82	3.33	2.33	2.73
Comp C46	60760	MGZD275	245.1	245.8	0.7	D73149	0.85	3.06	2.14	2.60
Comp C46	60760	MGZD275	252.1	252.8	0.7	D73163	0.87	3.81	2.67	3.31
Comp C46	60760	MGZD275	253.5	254.2	0.7	D73165	0.82	3.90	2.73	3.20

C ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp C46	60760	MGZD283	237.9	238.6	0.7	D76313	0.85	2.43	1.70	2.07
Comp C46	60800	MGZD154	231.8	232.5	0.7	D33412	0.73	2.43	1.70	1.77
Comp C46	60800	MGZD154	232.5	233.2	0.7	D33413	0.79	2.92	2.04	2.31
Comp C46	60800	MGZD154	237.4	238.1	0.7	D33422	0.74	2.98	2.09	2.21
Comp C46	60800	MGZD154	238.8	239.5	0.7	D33424	0.68	3.48	2.44	2.37
Comp C46	60800	MGZD157	236	236.7	0.7	D34289	0.76	3.09	2.16	2.35
Comp C46	60800	MGZD160	224.8	225.5	0.7	D35014	0.9	2.84	1.99	2.56
Comp C46	60840	MGZD075	204	205	1.0	D08027	1.15	2.45	2.45	2.82
Comp C46	60840	MGZD076	213	214	1.0	D08120	1.13	2.56	2.56	2.89
Comp C46	60840	MGZD077	218.8	219.5	0.7	D08757	0.69	3.92	2.74	2.70
Comp C46	60840	MGZD077	220.2	220.9	0.7	D08760	0.66	2.90	2.03	1.91
Comp C46	60840	MGZD077	222.3	223	0.7	D08763	0.66	2.53	1.77	1.67
Comp C46	60840	MGZD077	227.9	228.6	0.7	D08772	0.77	2.41	1.69	1.86
Comp C46	60840	MGZD077	231.4	232.1	0.7	D08777	0.82	2.83	1.98	2.32
Comp C46	60840	MGZD077	232.1	233	0.9	D08779	1.08	2.80	2.52	3.02
Comp C46	60840	MGZD153	211.7	212.4	0.7	D32699	0.79	2.45	1.72	1.94
Comp C46	60840	MGZD153	212.4	213.1	0.7	D32700	0.75	2.45	1.72	1.84
Comp C46	60840	MGZD153	227	227.7	0.7	D32716	0.76	3.47	2.43	2.64
Comp C46	60840	MGZD153	227.7	228.4	0.7	D32717	0.79	3.96	2.77	3.13
Comp C46	60840	MGZD153	234	234.7	0.7	D32728	0.76	3.58	2.51	2.72
Comp C46	60840	MGZD153	236.1	236.8	0.7	D32731	0.78	3.67	2.57	2.86
Comp C46	60840	MGZD153	241.7	242.4	0.7	D32740	0.83	2.50	1.75	2.08
Comp C46	60840	MGZD153	243.1	243.8	0.7	D32742	0.92	2.42	1.69	2.23
Comp C46	60840	MGZD153	243.8	244.5	0.7	D32743	0.91	3.11	2.18	2.83
Comp C46	60840	MGZD153	244.5	245.2	0.7	D32744	0.94	3.61	2.53	3.39
Comp C46	60840	MGZD156	221.7	222.4	0.7	D33915	0.7	3.46	2.42	2.42
Comp C46	60840	MGZD161	172.5	173.2	0.7	D35323	0.94	3.88	2.72	3.65
Comp C47	60640	MGZD079	239	240	1.0	D09005	1.1	4.14	4.14	4.55
Comp C47	60640	MGZD079	240	240.7	0.7	D09006	0.73	5.14	3.60	3.75
Comp C47	60640	MGZD079	243	244	1.0	D09010	1.02	4.52	4.52	4.61
Comp C47	60640	MGZD079	250	251	1.0	D09017	1.01	5.83	5.83	5.89
Comp C47	60640	MGZD080	207.5	208.2	0.7	D09149	0.73	4.89	3.42	3.57
Comp C47	60640	MGZD181	179.9	180.6	0.7	D41033	0.85	4.20	2.94	3.57
Comp C47	60640	MGZD181	232	232.7	0.7	D41094	0.91	4.07	2.85	3.70
Comp C47	60640	MGZD188	247.1	247.8	0.7	D42155	0.81	5.39	3.77	4.37
Comp C47	60640	MGZD258	253	253.7	0.7	D67556	0.91	4.19	2.93	3.81
Comp C47	60640	MGZD279	260.8	261.5	0.7	D74799	0.86	5.24	3.67	4.51
Comp C47	60680	MGZD167	137	138	1.0	D37213	1.01	4.22	4.22	4.26
Comp C47	60680	MGZD178	230	231	1.0	D39856	1.46	4.30	4.30	6.28
Comp C47	60680	MGZD178	249.8	250.5	0.7	D39885	0.82	4.91	3.44	4.03
Comp C47	60680	MGZD262	240	241	1.0	D68529	1.17	5.83	5.83	6.82
Comp C47	60680	MGZD262	259.7	260.4	0.7	D68551	0.8	5.14	3.60	4.11
Comp C47	60680	MGZD272	200	201	1.0	D71885	1.29	4.05	4.05	5.22
Comp C47	60680	MGZD272	263.7	264.4	0.7	D71964	0.81	5.00	3.50	4.05
Comp C47	60680	MGZD286	274	275	1.0	D77427	1.33	5.05	5.05	6.72
Comp C47	60720	MGZD097	245.7	246.4	0.7	D12169	0.7	4.86	3.40	3.40
Comp C47	60720	MGZD097	251.3	252	0.7	D12179	0.62	4.39	3.07	2.72
Comp C47	60720	MGZD191	143.3	144	0.7	D42901	0.68	5.61	3.93	3.81
Comp C47	60720	MGZD196	196.1	196.8	0.7	D44384	0.67	5.57	3.90	3.73
Comp C47	60720	MGZD248	159.5	160.2	0.7	D63397	0.76	5.40	3.78	4.10
Comp C47	60720	MGZD248	161.6	162.3	0.7	D63401	0.65	4.26	2.98	2.77
Comp C47	60720	MGZD264	258.7	259.4	0.7	D68943	0.8	4.86	3.40	3.89
Comp C47	60720	MGZD268	265.4	266.1	0.7	D71042	0.87	5.35	3.75	4.65
Comp C47	60760	MGZD043	249.1	249.8	0.7	D04283	0.78	4.65	3.26	3.63
Comp C47	60760	MGZD043	257	258	1.0	D04295	1.2	4.11	4.11	4.93

C ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp C47	60760	MGZD043	266.1	266.8	0.7	D04307	0.76	4.07	2.85	3.09
Comp C47	60760	MGZD073	140.5	141.2	0.7	D07810	0.55	4.73	3.31	2.60
Comp C47	60760	MGZD073	196.7	197.4	0.7	D07885	0.83	4.84	3.39	4.02
Comp C47	60760	MGZD275	237.4	238.1	0.7	D73136	0.86	4.47	3.13	3.84
Comp C47	60760	MGZD275	243	243.7	0.7	D73146	0.76	5.63	3.94	4.28
Comp C47	60760	MGZD275	244.4	245.1	0.7	D73148	0.74	4.75	3.32	3.52
Comp C47	60760	MGZD275	250	250.7	0.7	D73159	0.55	5.61	3.93	3.09
Comp C47	60760	MGZD275	251.4	252.1	0.7	D73162	0.83	4.69	3.28	3.89
Comp C47	60800	MGZD154	238.1	238.8	0.7	D33423	0.76	5.74	4.02	4.36
Comp C47	60800	MGZD157	231.8	232.5	0.7	D34283	0.82	4.37	3.06	3.58
Comp C47	60800	MGZD160	231.1	231.8	0.7	D35025	0.79	5.49	3.84	4.34
Comp C47	60840	MGZD075	206	207	1.0	D08029	1.23	5.80	5.80	7.13
Comp C47	60840	MGZD076	214.7	215.4	0.7	D08123	0.71	5.20	3.64	3.69
Comp C47	60840	MGZD077	221.6	222.3	0.7	D08762	0.73	4.15	2.91	3.03
Comp C47	60840	MGZD077	223	223.7	0.7	D08764	0.73	4.92	3.44	3.59
Comp C47	60840	MGZD153	222	223	1.0	D32711	1.37	4.47	4.47	6.12
Comp C47	60840	MGZD153	242.4	243.1	0.7	D32741	0.86	4.73	3.31	4.07
Comp C47	60840	MGZD161	221	222	1.0	D35382	1.26	5.97	5.97	7.52
Comp C48	60640	MGZD079	241.4	242.1	0.7	D09008	0.71	9.74	6.82	6.92
Comp C48	60640	MGZD079	242.1	243	0.9	D09009	0.97	8.93	8.04	8.66
Comp C48	60640	MGZD079	252	253	1.0	D09020	1.06	7.31	7.31	7.75
Comp C48	60640	MGZD181	178.5	179.2	0.7	D41031	0.9	6.16	4.31	5.54
Comp C48	60640	MGZD181	183.4	184.1	0.7	D41039	0.86	7.15	5.00	6.15
Comp C48	60640	MGZD181	255	256	1.0	D41123	1.31	7.59	7.59	9.94
Comp C48	60640	MGZD258	255.1	255.8	0.7	D67560	0.81	8.98	6.29	7.27
Comp C48	60640	MGZD258	259.3	260	0.7	D67566	0.79	7.00	4.90	5.53
Comp C48	60640	MGZD276	216.7	217.4	0.7	D73502	0.85	9.76	6.83	8.30
Comp C48	60640	MGZD279	251.2	251.9	0.7	D74785	0.87	7.39	5.17	6.43
Comp C48	60640	MGZD287	303	304	1.0	D77907	1.14	7.07	7.07	8.06
Comp C48	60680	MGZD178	247.7	248.4	0.7	D39882	1.06	7.25	5.08	7.69
Comp C48	60680	MGZD178	254.7	255.4	0.7	D39892	1.02	6.86	4.80	7.00
Comp C48	60680	MGZD178	277.1	278	0.9	D39928	1.06	8.58	7.72	9.09
Comp C48	60680	MGZD218	181.1	181.8	0.7	D51461	0.7	6.01	4.21	4.21
Comp C48	60680	MGZD218	186.7	187.4	0.7	D51469	0.64	7.77	5.44	4.97
Comp C48	60680	MGZD272	263	263.7	0.7	D71963	0.73	6.81	4.77	4.97
Comp C48	60720	MGZD191	141.9	142.6	0.7	D42899	0.74	6.46	4.52	4.78
Comp C48	60720	MGZD196	189.1	189.8	0.7	D44373	0.82	7.51	5.26	6.16
Comp C48	60720	MGZD196	189.8	190.5	0.7	D44374	0.6	9.72	6.80	5.83
Comp C48	60720	MGZD196	223.5	224.2	0.7	D44425	0.76	9.04	6.33	6.87
Comp C48	60720	MGZD203	240.7	241.4	0.7	D46182	0.77	8.73	6.11	6.72
Comp C48	60720	MGZD203	241.4	242.1	0.7	D46183	0.83	8.73	6.11	7.25
Comp C48	60720	MGZD203	248.4	249.1	0.7	D46193	0.72	6.98	4.89	5.03
Comp C48	60720	MGZD253	255.4	256.1	0.7	D65723	0.83	8.62	6.03	7.15
Comp C48	60720	MGZD268	212	213	1.0	D70979	1.18	8.16	8.16	9.63
Comp C48	60720	MGZD268	239	240	1.0	D71009	1.12	7.10	7.10	7.95
Comp C48	60720	MGZD268	254.8	255.5	0.7	D71028	0.84	9.22	6.45	7.74
Comp C48	60720	MGZD268	257.6	258.3	0.7	D71032	0.79	8.21	5.75	6.49
Comp C48	60760	MGZD043	156.4	157.1	0.7	D04219	0.84	9.35	6.54	7.85
Comp C48	60760	MGZD043	158.5	159.2	0.7	D04223	0.78	6.72	4.70	5.24
Comp C48	60760	MGZD043	227.1	227.8	0.7	D04255	0.78	6.39	4.47	4.98
Comp C48	60760	MGZD043	253.3	254	0.7	D04290	0.8	7.45	5.21	5.96
Comp C48	60760	MGZD043	267.5	268.2	0.7	D04309	0.82	6.11	4.28	5.01
Comp C48	60760	MGZD045	265	266	1.0	D04603	1.24	8.60	8.60	10.66
Comp C48	60760	MGZD073	197.4	198.1	0.7	D07886	0.69	8.84	6.19	6.10
Comp C48	60760	MGZD073	204.4	205.1	0.7	D07895	0.8	7.80	5.46	6.24

C ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp C48	60760	MGZD073	211	211.7	0.7	D07904	0.78	6.37	4.46	4.97
Comp C48	60760	MGZD275	231.8	232.5	0.7	D73126	0.79	8.24	5.77	6.51
Comp C48	60760	MGZD275	236.7	237.4	0.7	D73134	0.8	7.25	5.08	5.80
Comp C48	60760	MGZD283	231	232	1.0	D76304	1.1	9.54	9.54	10.49
Comp C48	60760	MGZD283	237.2	237.9	0.7	D76312	0.77	9.91	6.94	7.63
Comp C48	60800	MGZD154	233.9	234.6	0.7	D33415	0.76	7.19	5.03	5.46
Comp C48	60800	MGZD154	240.2	240.9	0.7	D33426	0.74	7.92	5.54	5.86
Comp C48	60800	MGZD157	232.5	233.2	0.7	D34284	0.84	7.44	5.21	6.25
Comp C48	60840	MGZD075	188	189	1.0	D08009	1.28	7.81	7.81	10.00
Comp C48	60840	MGZD076	214	214.7	0.7	D08122	0.79	6.19	4.33	4.89
Comp C48	60840	MGZD076	217.5	218.2	0.7	D08127	0.71	7.51	5.26	5.33
Comp C48	60840	MGZD077	230.7	231.4	0.7	D08776	0.8	9.63	6.74	7.70
Comp C48	60840	MGZD153	236.8	237.5	0.7	D32732	0.71	8.62	6.03	6.12
Comp C48	60840	MGZD156	221	221.7	0.7	D33914	0.71	7.55	5.29	5.36
Comp C48	60840	MGZD161	183	183.7	0.7	D35334	0.96	8.63	6.04	8.28
Comp C48	60840	MGZD161	215	216	1.0	D35375	1.26	7.95	7.95	10.02
Comp C48	60840	MGZD161	238	238.7	0.7	D35402	0.9	8.46	5.92	7.61
Comp C49	60640	MGZD188	254.7	255.4	0.7	D42165	0.8	11.40	7.98	9.12
Comp C49	60640	MGZD258	254.4	255.1	0.7	D67559	0.87	12.60	8.82	10.96
Comp C49	60640	MGZD276	218.8	219.5	0.7	D73505	0.98	12.40	8.68	12.15
Comp C49	60680	MGZD178	233.4	234.1	0.7	D39861	0.79	12.20	8.54	9.64
Comp C49	60680	MGZD272	212	212.7	0.7	D71899	1.04	13.60	9.52	14.14
Comp C49	60680	MGZD272	213.4	214.1	0.7	D71902	1.01	10.70	7.49	10.81
Comp C49	60720	MGZD203	242.8	243.5	0.7	D46185	0.73	12.60	8.82	9.20
Comp C49	60720	MGZD203	244.2	244.9	0.7	D46187	0.9	10.90	7.63	9.81
Comp C49	60720	MGZD203	253.3	254	0.7	D46202	0.79	11.00	7.70	8.69
Comp C49	60760	MGZD043	248.4	249.1	0.7	D04282	0.82	10.60	7.42	8.69
Comp C49	60760	MGZD045	254.8	255.5	0.7	D04591	0.8	13.30	9.31	10.64
Comp C49	60760	MGZD275	252.8	253.5	0.7	D73164	0.77	12.00	8.40	9.24
Comp C49	60760	MGZD283	236.5	237.2	0.7	D76311	0.83	12.40	8.68	10.29
Comp C49	60800	MGZD151	194.7	195.4	0.7	D32363	0.82	10.60	7.42	8.69
Comp C49	60800	MGZD154	239.5	240.2	0.7	D33425	0.7	14.00	9.80	9.80
Comp C49	60840	MGZD076	228.7	229.4	0.7	D08141	0.69	12.70	8.89	8.76
Comp C49	60840	MGZD077	220.9	221.6	0.7	D08761	0.71	12.30	8.61	8.73
Comp C49	60840	MGZD153	233.3	234	0.7	D32727	0.82	10.70	7.49	8.77
Comp C49	60840	MGZD161	184.4	185.1	0.7	D35336	0.75	10.60	7.42	7.95
Comp C50	60640	MGZD079	230	231	1.0	D08994	1.14	24.50	24.50	27.93
Comp C50	60640	MGZD181	182	182.7	0.7	D41036	0.71	14.80	10.36	10.51
Comp C50	60640	MGZD181	182.7	183.4	0.7	D41037	0.87	22.00	15.40	19.14
Comp C50	60640	MGZD276	201	202	1.0	D73481	1.35	16.80	16.80	22.68
Comp C50	60680	MGZD218	230.4	231.1	0.7	D51523	0.68	14.10	9.87	9.59
Comp C50	60680	MGZD280	248.9	249.6	0.7	D75226	0.7	14.60	10.22	10.22
Comp C50	60720	MGZD191	142.6	143.3	0.7	D42900	0.73	15.90	11.13	11.61
Comp C50	60720	MGZD196	192.6	193.3	0.7	D44379	0.86	19.00	13.30	16.34
Comp C50	60720	MGZD196	193.3	194	0.7	D44380	0.67	15.60	10.92	10.45
Comp C50	60720	MGZD203	236.5	237.2	0.7	D46175	0.83	17.40	12.18	14.44
Comp C50	60720	MGZD203	242.1	242.8	0.7	D46184	0.72	17.50	12.25	12.60
Comp C50	60720	MGZD203	252.6	253.3	0.7	D46201	0.83	21.50	15.05	17.85
Comp C50	60720	MGZD264	244.4	245.1	0.7	D68927	0.8	14.20	9.94	11.36
Comp C50	60720	MGZD264	262.9	263.6	0.7	D68950	0.71	18.30	12.81	12.99
Comp C50	60760	MGZD043	149.7	150.4	0.7	D04210	0.76	16.40	11.48	12.46
Comp C50	60760	MGZD043	149.7	150.4	0.7	D04210	0.76	16.40	11.48	12.46
Comp C50	60760	MGZD043	247.7	248.4	0.7	D04281	0.81	18.50	12.95	14.99
Comp C50	60760	MGZD043	252.6	253.3	0.7	D04289	0.79	17.90	12.53	14.14
Comp C50	60760	MGZD043	254.7	255.4	0.7	D04292	0.93	24.10	16.87	22.41

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Comp C50	60760	MGZD045	253.4	254.1	0.7	D04589	0.74	16.10	11.27	11.91
Comp C50	60760	MGZD045	254.1	254.8	0.7	D04590	0.81	16.60	11.62	13.45
Comp C50	60760	MGZD045	267	267.7	0.7	D04606	0.91	18.70	13.09	17.02
Comp C50	60760	MGZD275	243.7	244.4	0.7	D73147	0.74	21.80	15.26	16.13
Comp C50	60800	MGZD157	236.7	237.4	0.7	D34290	0.79	19.00	13.30	15.01
Comp C50	60800	MGZD157	237.4	238.1	0.7	D34291	0.79	16.40	11.48	12.96
Comp C50	60840	MGZD077	219.5	220.2	0.7	D08759	0.74	14.40	10.08	10.66
Comp C50	60840	MGZD153	234.7	235.4	0.7	D32729	0.83	23.80	16.66	19.75
Comp C50	60840	MGZD153	235.4	236.1	0.7	D32730	0.84	17.50	12.25	14.70
Comp C50	60840	MGZD153	237.5	238.2	0.7	D32733	0.79	17.10	11.97	13.51
Comp C50	60840	MGZD153	238.2	238.9	0.7	D32734	0.96	16.90	11.83	16.22
Comp C50	60840	MGZD161	169.7	170.4	0.7	D35317	0.9	16.60	11.62	14.94
Comp C50	60840	MGZD161	183.7	184.4	0.7	D35335	0.83	23.70	16.59	19.67
Comp C50	60840	MGZD161	225.4	226.1	0.7	D35387	0.82	19.10	13.37	15.66
Comp C50	60840	MGZD161	233	234	1.0	D35395	1.14	20.00	20.00	22.80
Comp C51	60640	MGZD079	251	252	1.0	D09019	1	32.30	32.30	32.30
Comp C51	60640	MGZD188	239.4	240.1	0.7	D42143	0.88	38.90	27.23	34.23
Comp C51	60680	MGZD178	232.7	233.4	0.7	D39860	0.78	37.80	26.46	29.48
Comp C51	60680	MGZD178	234.1	234.8	0.7	D39862	0.86	41.90	29.33	36.03
Comp C51	60680	MGZD178	235.5	236.2	0.7	D39864	0.73	40.20	28.14	29.35
Comp C51	60680	MGZD178	270.1	270.8	0.7	D39916	0.67	59.60	41.72	39.93
Comp C51	60680	MGZD218	187.4	188.1	0.7	D51470	0.7	71.40	49.98	49.98
Comp C51	60720	MGZD191	151.7	152.4	0.7	D42913	0.67	35.40	24.78	23.72
Comp C51	60720	MGZD203	244.9	245.6	0.7	D46188	0.81	27.60	19.32	22.36
Comp C51	60720	MGZD203	249.8	250.5	0.7	D46195	0.78	28.80	20.16	22.46
Comp C51	60720	MGZD253	248.7	249.4	0.7	D65713	0.75	45.70	31.99	34.28
Comp C51	60720	MGZD268	266.8	267.5	0.7	D71044	0.86	31.90	22.33	27.43
Comp C51	60720	MGZD268	297.4	298.1	0.7	D71081	0.64	33.10	23.17	21.18
Comp C51	60720	MGZD268	298.8	299.5	0.7	D71083	0.85	34.90	24.43	29.67
Comp C51	60760	MGZD043	247	247.7	0.7	D04280	0.83	25.50	17.85	21.17
Comp C51	60760	MGZD045	249	249.7	0.7	D04582	0.83	83.30	58.31	69.14
Comp C51	60760	MGZD045	249.7	250.4	0.7	D04583	0.76	28.70	20.09	21.81
Comp C51	60760	MGZD288	258.4	259.1	0.7	D78291	0.78	39.20	27.44	30.58
Comp C51	60840	MGZD076	223.7	224.4	0.7	D08135	0.67	41.70	29.19	27.94
Comp C51	60840	MGZD153	213.1	213.8	0.7	D32701	0.8	28.40	19.88	22.72

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Comp D61	60880	MGZD175	175	176	1.0	D39137	1.19	0.12	0.12	0.1428
Comp D61	60880	MGZD175	176	177	1.0	D39139	1.16	0.24	0.24	0.2784
Comp D61	60880	MGZD175	177	177.7	0.7	D39140	0.84	0.12	0.084	0.1008
Comp D61	60880	MGZD175	187.5	188.2	0.7	D39156	0.84	0.08	0.056	0.0672
Comp D61	60880	MGZD175	188.2	188.9	0.7	D39157	0.75	0.23	0.161	0.1725
Comp D61	60880	MGZD175	191.7	192.4	0.7	D39163	0.67	0.1	0.07	0.067
Comp D61	60920	MGZD142	189.5	190.2	0.7	D29920	0.83	0.08	0.056	0.0664
Comp D61	60920	MGZD147	157.7	158.4	0.7	D31825	0.81	0.13	0.091	0.1053
Comp D61	60920	MGZD162	164.6	165.3	0.7	D35649	0.73	0.19	0.133	0.1387
Comp D61	60920	MGZD162	165.3	166	0.7	D35650	0.77	0	0	0
Comp D61	60920	MGZD162	166	167	1.0	D35651	1.21	0	0	0
Comp D61	60960	MGZD029	104	105	1.0	D25514	0.88	0.19	0.19	0.1672
Comp D61	60960	MGZD029	105	106	1.0	D02544	1.02	0.13	0.13	0.1326
Comp D61	60960	MGZD029	106	107	1.0	D02545	1.16	0.08	0.08	0.0928
Comp D61	60960	MGZD029	107	108	1.0	D02547	1.02	0.11	0.11	0.1122
Comp D61	60960	MGZD029	111	112	1.0	D02553	1.23	0.11	0.11	0.1353
Comp D61	60960	MGZD048	113	114	1.0	D04667	1.09	0.25	0.25	0.2725
Comp D61	60960	MGZD048	143	144	1.0	D04711	1.16	0.04	0.04	0.0464
Comp D61	60960	MGZD048	144	145	1.0	D04712	1.15	0.08	0.08	0.092
Comp D61	60960	MGZD048	145	146	1.0	D04713	1.03	0.17	0.17	0.1751
Comp D61	60960	MGZD048	162	163	1.0	D04736	1.1	0.25	0.25	0.275
Comp D61	60960	MGZD062	103	104	1.0	D06500	1.1	0.09	0.09	0.099
Comp D61	60960	MGZD062	104	105	1.0	D06501	1.2	0.05	0.05	0.06
Comp D61	60960	MGZD062	109	110	1.0	D06506	1.1	0.08	0.08	0.088
Comp D61	60960	MGZD062	110	111	1.0	D06507	1.1	0.2	0.2	0.22
Comp D61	60960	MGZD063	126	127	1.0	D06397	0.96	0.11	0.11	0.1056
Comp D61	60960	MGZD063	140	141	1.0	D06415	1.05	0.23	0.23	0.2415
Comp D61	60960	MGZD063	145.4	146.1	0.7	D06423	1	0.09	0.063	0.09
Comp D61	60960	MGZD071	125.2	125.9	0.7	D07645	0.81	0.17	0.119	0.1377
Comp D61	60960	MGZD071	126.6	127.3	0.7	D07649	0.84	0.08	0.056	0.0672
Comp D61	61000	MGZD117	115.8	116.5	0.7	D20212	0.79	0.2	0.14	0.158
Comp D61	61000	MGZD117	117.2	117.9	0.7	D20214	0.77	0.19	0.133	0.1463
Comp D61	61000	MGZD117	118.6	119.3	0.7	D20216	0.84	0.18	0.126	0.1512
Comp D61	61000	MGZD119	90.4	91.1	0.7	D20634	0.76	0.1	0.07	0.076
Comp D61	61000	MGZD124	84	85	1.0	D22268	1.1	0.2	0.2	0.22
Comp D61	61000	MGZD124	137.9	138.6	0.7	D22342	0.78	0.14	0.098	0.1092
Comp D61	61000	MGZD125	116.7	117.4	0.7	D23263	0.83	0.1	0.07	0.083
Comp D61	61000	MGZD125	118.1	118.8	0.7	D23265	0.74	0.23	0.161	0.1702
Comp D61	61040	MGZD026	12	13	1.0	D24943	0.8	0.11	0.11	0.088
Comp D61	61040	MGZD026	87	87.7	0.7	D02390	0.8	0.24	0.168	0.192
Comp D61	61040	MGZD026	88.4	89.1	0.7	D02392	0.8	0.22	0.154	0.176
Comp D61	61040	MGZD027	109.9	110.6	0.7	D02442	0.83	0.03	0.021	0.0249
Comp D61	61040	MGZD027	110.6	111.3	0.7	D02444	0.86	0.12	0.084	0.1032
Comp D61	61040	MGZD060	83	84	1.0	D06557	1	0.13	0.13	0.13
Comp D61	61040	MGZD067	79	80	1.0	D07293	1.1	0.11	0.11	0.121
Comp D61	61040	MGZD069	89	90	1.0	D07516	1.19	0.19	0.19	0.2261
Comp D61	61040	MGZD104	64.1	64.8	0.7	D16917	0.65	0.19	0.133	0.1235
Comp D61	61040	MGZD104	91.4	92.1	0.7	D16961	0.83	0.14	0.098	0.1162
Comp D61	61040	MGZD104	92.8	93.5	0.7	D16963	0.83	0.09	0.063	0.0747
Comp D61	61080	MGZD025	43.1	44	0.9	D02268	0.9	0.18	0.162	0.162
Comp D61	61080	MGZD032	50.4	51.1	0.7	D02754	1.8	0.1	0.07	0.18

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Comp D61	61080	MGZD032	53	53.7	0.7	D02757	0.8	0.19	0.133	0.152
Comp D61	61080	MGZD032	57	58	1.0	D02763	1.3	0.06	0.06	0.078
Comp D61	61080	MGZD032	58	59	1.0	D02764	1.4	0.02	0.02	0.028
Comp D61	61080	MGZD053	32.4	33.1	0.7	D06011	0.83	0.09	0.063	0.0747
Comp D61	61080	MGZD053	58.7	59.4	0.7	D06043	0.74	0.24	0.168	0.1776
Comp D61	61080	MGZD053	69.4	70.1	0.7	D06059	0.57	0.04	0.028	0.0228
Comp D61	61080	MGZD053	74.4	75.1	0.7	D06066	0.84	0.18	0.126	0.1512
Comp D61	61080	MGZD106	37.2	37.9	0.7	D18823	0.79	0.09	0.063	0.0711
Comp D61	61080	MGZD118	56.9	57.6	0.7	D20442	1.26	0.14	0.098	0.1764
Comp D61	61080	MGZD118	57.6	58.3	0.7	D20443	1.24	0.2	0.14	0.248
Comp D61	61080	MGZD118	96	96.7	0.7	D20497	1.62	0.23	0.161	0.3726
Comp D61	61120	MGZD019	29	29.7	0.7	D01530	0.65	0.08	0.056	0.052
Comp D61	61120	MGZD019	29.7	30.4	0.7	D01531	0.72	0.09	0.063	0.0648
Comp D61	61120	MGZD019	30.4	31.3	0.9	D01532	1.04	0.08	0.072	0.0832
Comp D61	61120	MGZD019	116	117	1.0	D24563	1.05	0.12	0.12	0.126
Comp D61	61120	MGZD020	63.7	64.4	0.7	D01670	0.8	0.07	0.049	0.056
Comp D61	61120	MGZD023	55.4	56.1	0.7	D02152	0.6	0.21	0.147	0.126
Comp D61	61120	MGZD023	72.1	72.8	0.7	D02175	0.7	0.06	0.042	0.042
Comp D61	61120	MGZD033	34.4	35.1	0.7	D02820	1.15	0.02	0.014	0.023
Comp D61	61120	MGZD055	24	25	1.0	D06115	1.27	0.24	0.24	0.3048
Comp D61	61120	MGZD055	54.1	55	0.9	D06156	0.94	0.25	0.225	0.235
Comp D61	61120	MGZD055	55	56	1.0	D06157	1.2	0.05	0.05	0.06
Comp D61	61120	MGZD055	67.4	68.1	0.7	D06175	0.95	0.11	0.077	0.1045
Comp D61	61120	MGZD055	105	106	1.0	D07224	1.14	0.24	0.24	0.2736
Comp D61	61160	MGZD034	45.8	46.5	0.7	D02895	0.89	0.04	0.028	0.0356
Comp D61	61160	MGZD034	58.4	59.1	0.7	D02911	0.8	0.03	0.021	0.024
Comp D61	61160	MGZD034	59.1	60	0.9	D02912	1.05	0.08	0.072	0.084
Comp D61	61160	MGZD034	60	61	1.0	D02913	1.19	0.12	0.12	0.1428
Comp D61	61160	MGZD034	62	63	1.0	D02915	1.33	0.04	0.04	0.0532
Comp D61	61160	MGZD056	45.8	46.5	0.7	D05954	0.78	0.05	0.035	0.039
Comp D61	61160	MGZD056	46.5	47.2	0.7	D05955	0.81	0.04	0.028	0.0324
Comp D61	61160	MGZD056	47.2	48	0.8	D05956	0.9	0.05	0.04	0.045
Comp D61	61160	MGZD056	70	71	1.0	D05985	1.31	0.04	0.04	0.0524
Comp D61	61160	MGZD056	72	73	1.0	D05987	1.29	0.22	0.22	0.2838
Comp D61	61160	MGZD058	14.1	14.8	0.7	D06198	0.7	0.24	0.168	0.168
Comp D61	61160	MGZD058	15.5	16.2	0.7	D06200	0.8	0.11	0.077	0.088
Comp D61	61160	MGZD058	36	37	1.0	D06225	1.01	0.06	0.06	0.0606
Comp D61	61160	MGZD058	38	39	1.0	D06227	1.17	0.12	0.12	0.1404
Comp D61	61160	MGZD058	39	39.7	0.7	D06228	0.76	0.1	0.07	0.076
Comp D61	61160	MGZD110	13.7	14.4	0.7	D18930	0.71	0.21	0.147	0.1491
Comp D61	61160	MGZD110	31.8	32.5	0.7	D18957	0.9	0.1	0.07	0.09
Comp D61	61160	MGZD110	34.6	35.3	0.7	D18962	0.83	0.09	0.063	0.0747
Comp D61	61160	MGZD110	36	36.7	0.7	D18964	0.8	0.07	0.049	0.056
Comp D61	61160	MGZD110	36.7	37.4	0.7	D18965	0.78	0.17	0.119	0.1326
Comp D61	61160	MGZD111	14	15	1.0	D19548	1.74	0.19	0.19	0.3306
Comp D61	61160	MGZD111	20.7	21.4	0.7	D19555	1.49	0.1	0.07	0.149
Comp D61	61160	MGZD111	28.4	29.1	0.7	D19567	0.81	0.16	0.112	0.1296
Comp D61	61160	MGZD111	35	36	1.0	D19577	1.21	0.08	0.08	0.0968
Comp D61	61160	MGZD111	36	36.7	0.7	D19579	0.87	0.21	0.147	0.1827
Comp D61	61200	MGZD113	16.5	17.2	0.7	D19813	0.78	0.21	0.147	0.1638
Comp D61	61200	MGZD113	21.4	22.1	0.7	D19822	0.82	0.08	0.056	0.0656
Comp D61	61200	MGZD113	22.1	22.8	0.7	D19823	0.75	0.16	0.112	0.12
Comp D61	61200	MGZD114	22.8	23.5	0.7	D19308	0.79	0.18	0.126	0.1422
Comp D61	61200	MGZD114	27.7	28.4	0.7	D19315	0.9	0.15	0.105	0.135
Comp D61	61200	MGZD114	29.1	29.8	0.7	D19317	0.94	0.04	0.028	0.0376

D ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp D62	60880	MGZD164	199	200	1.0	D36355	1.16	0.37	0.37	0.4292
Comp D62	60880	MGZD175	188.9	189.6	0.7	D39159	0.85	0.31	0.217	0.2635
Comp D62	60920	MGZD142	188.8	189.5	0.7	D29919	0.81	0.44	0.308	0.3564
Comp D62	60960	MGZD022	150	151	1.0	D01863	1.38	0.37	0.37	0.5106
Comp D62	60960	MGZD029	109.4	110.1	0.7	D02551	0.79	0.32	0.224	0.2528
Comp D62	60960	MGZD048	142	143	1.0	D04710	1.04	0.4	0.4	0.416
Comp D62	60960	MGZD048	160.1	161	0.9	D04734	0.93	0.44	0.396	0.4092
Comp D62	60960	MGZD048	161	162	1.0	D04735	1.14	0.34	0.34	0.3876
Comp D62	60960	MGZD048	164	165	1.0	D04739	1.16	0.4	0.4	0.464
Comp D62	60960	MGZD048	168	169	1.0	D04743	1.18	0.33	0.33	0.3894
Comp D62	60960	MGZD062	100	101	1.0	D06497	1	0.36	0.36	0.36
Comp D62	60960	MGZD062	101	102	1.0	D06498	1	0.34	0.34	0.34
Comp D62	60960	MGZD062	108	109	1.0	D06505	1.1	0.41	0.41	0.451
Comp D62	60960	MGZD063	122.4	123.1	0.7	D06391	0.78	0.38	0.266	0.2964
Comp D62	60960	MGZD063	123.1	123.8	0.7	D06392	0.72	0.45	0.315	0.324
Comp D62	60960	MGZD063	125.2	126	0.8	D06395	0.76	0.44	0.352	0.3344
Comp D62	60960	MGZD063	127	128	1.0	D06398	1.03	0.33	0.33	0.3399
Comp D62	60960	MGZD063	138.5	139.2	0.7	D06413	0.75	0.4	0.28	0.3
Comp D62	60960	MGZD145	94	95	1.0	D30514	1.23	0.39	0.39	0.4797
Comp D62	60960	MGZD145	97	98	1.0	D30517	1.25	0.39	0.39	0.4875
Comp D62	61000	MGZD117	119.3	120	0.7	D20217	0.89	0.27	0.189	0.2403
Comp D62	61000	MGZD122	111.4	112.1	0.7	D21837	0.78	0.46	0.322	0.3588
Comp D62	61000	MGZD124	137.2	137.9	0.7	D22341	0.86	0.47	0.329	0.4042
Comp D62	61000	MGZD125	105.5	106.2	0.7	D23245	0.85	0.47	0.329	0.3995
Comp D62	61000	MGZD125	108.3	109	0.7	D23250	0.77	0.49	0.343	0.3773
Comp D62	61000	MGZD125	109.7	110.4	0.7	D23252	0.76	0.48	0.336	0.3648
Comp D62	61000	MGZD127	104	105	1.0	D25360	1.18	0.26	0.26	0.3068
Comp D62	61040	MGZD026	105	106	1.0	D02414	1.2	0.5	0.5	0.6
Comp D62	61040	MGZD027	100	100.7	0.7	D02427	0.8	0.27	0.189	0.216
Comp D62	61040	MGZD027	111.3	112	0.7	D02445	0.79	0.46	0.322	0.3634
Comp D62	61040	MGZD059	33	34	1.0	D07094	1.21	0.43	0.43	0.5203
Comp D62	61040	MGZD059	34	35	1.0	D07095	1.28	0.46	0.46	0.5888
Comp D62	61040	MGZD067	75	76	1.0	D07289	1.02	0.43	0.43	0.4386
Comp D62	61040	MGZD067	78	79	1.0	D07292	1.15	0.41	0.41	0.4715
Comp D62	61040	MGZD104	50.8	51.5	0.7	D16897	0.78	0.35	0.245	0.273
Comp D62	61080	MGZD024	69	70	1.0	D02226	1.1	0.28	0.28	0.308
Comp D62	61080	MGZD025	27	28	1.0	D04083	1.1	0.41	0.41	0.451
Comp D62	61080	MGZD032	51.1	52	0.9	D02755	1	0.42	0.378	0.42
Comp D62	61080	MGZD032	54.4	55.1	0.7	D02760	0.7	0.44	0.308	0.308
Comp D62	61080	MGZD032	56	57	1.0	D02762	1.1	0.42	0.42	0.462
Comp D62	61080	MGZD032	74	74.7	0.7	D02783	0.82	0.36	0.252	0.2952
Comp D62	61080	MGZD032	74.7	75.4	0.7	D02784	0.7	0.36	0.252	0.252
Comp D62	61080	MGZD053	67	68	1.0	D06055	1.12	0.34	0.34	0.3808
Comp D62	61080	MGZD053	70.1	70.8	0.7	D06060	0.73	0.36	0.252	0.2628
Comp D62	61080	MGZD108	80.4	81.1	0.7	D19240	0.8	0.4	0.28	0.32
Comp D62	61080	MGZD109	53.1	53.8	0.7	D19466	0.92	0.28	0.196	0.2576
Comp D62	61080	MGZD116	59	60	1.0	D20361	2.11	0.46	0.46	0.9706
Comp D62	61080	MGZD118	48.5	49.2	0.7	D20430	1.55	0.32	0.224	0.496
Comp D62	61080	MGZD118	52.7	53.4	0.7	D20435	1.42	0.44	0.308	0.6248
Comp D62	61080	MGZD118	53.4	54.1	0.7	D20436	1.41	0.41	0.287	0.5781
Comp D62	61080	MGZD118	95	96	1.0	D20495	2.24	0.47	0.47	1.0528
Comp D62	61080	MGZD118	96.7	97.4	0.7	D20499	1.59	0.48	0.336	0.7632
Comp D62	61120	MGZD018	42.7	43.4	0.7	D01472	0.8	0.47	0.329	0.376
Comp D62	61120	MGZD018	47	48	1.0	D01477	1.2	0.47	0.47	0.564
Comp D62	61120	MGZD018	49	49.7	0.7	D01479	0.8	0.5	0.35	0.4
Comp D62	61120	MGZD019	28.1	29	0.9	D01529	0.94	0.44	0.396	0.4136
Comp D62	61120	MGZD019	38.1	39	0.9	D01541	0.84	0.33	0.297	0.2772
Comp D62	61120	MGZD019	40.4	41.1	0.7	D01545	0.55	0.4	0.28	0.22
Comp D62	61120	MGZD019	82	83	1.0	D01589	1.2	0.49	0.49	0.588

D ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp D62	61120	MGZD023	25	26	1.0	D02115	0.9	0.31	0.31	0.279
Comp D62	61120	MGZD023	32	32.7	0.7	D02124	0.7	0.4	0.28	0.28
Comp D62	61120	MGZD023	74.9	75.6	0.7	D02179	0.8	0.47	0.329	0.376
Comp D62	61120	MGZD023	83	84	1.0	D02189	1.2	0.36	0.36	0.432
Comp D62	61120	MGZD033	42	42.7	0.7	D02829	0.76	0.39	0.273	0.2964
Comp D62	61120	MGZD051	78.4	79.1	0.7	D05886	0.63	0.4	0.28	0.252
Comp D62	61120	MGZD051	79.1	79.8	0.7	D05887	0.72	0.39	0.273	0.2808
Comp D62	61120	MGZD055	36	36.7	0.7	D06131	0.78	0.32	0.224	0.2496
Comp D62	61120	MGZD055	46	47	1.0	D06144	1.1	0.36	0.36	0.396
Comp D62	61120	MGZD055	58.1	58.8	0.7	D06161	0.83	0.32	0.224	0.2656
Comp D62	61120	MGZD055	69	70	1.0	D06177	1.32	0.33	0.33	0.4356
Comp D62	61160	MGZD056	9.4	10.1	0.7	D05907	0.77	0.4	0.28	0.308
Comp D62	61160	MGZD056	10.1	10.8	0.7	D05909	0.7	0.38	0.266	0.266
Comp D62	61160	MGZD056	45.1	45.8	0.7	D05952	0.8	0.32	0.224	0.256
Comp D62	61160	MGZD056	71	72	1.0	D05986	1.01	0.36	0.36	0.3636
Comp D62	61160	MGZD056	75	75.9	0.9	D05990	0.96	0.44	0.396	0.4224
Comp D62	61160	MGZD058	16.2	17	0.8	D06201	0.8	0.5	0.4	0.4
Comp D62	61160	MGZD058	35.1	36	0.9	D06224	0.96	0.26	0.234	0.2496
Comp D62	61160	MGZD058	47.5	48.2	0.7	D06240	0.8	0.46	0.322	0.368
Comp D62	61160	MGZD110	32.5	33.2	0.7	D18959	0.81	0.37	0.259	0.2997
Comp D62	61160	MGZD110	38.1	38.8	0.7	D18967	0.75	0.44	0.308	0.33
Comp D62	61160	MGZD111	10	11	1.0	D19543	0.92	0.43	0.43	0.3956
Comp D62	61200	MGZD112	39.3	40	0.7	D19702	0.73	0.41	0.287	0.2993
Comp D62	61200	MGZD112	40	40.7	0.7	D19703	0.68	0.42	0.294	0.2856
Comp D62	61200	MGZD112	41.4	42.1	0.7	D19705	0.71	0.31	0.217	0.2201
Comp D62	61200	MGZD112	42.1	42.8	0.7	D19706	0.75	0.27	0.189	0.2025
Comp D62	61200	MGZD113	15.8	16.5	0.7	D19812	0.71	0.47	0.329	0.3337
Comp D62	61200	MGZD114	15.1	15.8	0.7	D19295	0.75	0.43	0.301	0.3225
Comp D62	61200	MGZD114	23.5	24.2	0.7	D19309	0.78	0.32	0.224	0.2496
Comp D62	61200	MGZD114	31.9	32.6	0.7	D19323	0.82	0.33	0.231	0.2706
Comp D63	60880	MGZD175	185.4	186.1	0.7	D39153	0.81	0.54	0.378	0.4374
Comp D63	60880	MGZD175	186.1	186.8	0.7	D39154	0.79	0.64	0.448	0.5056
Comp D63	60880	MGZD175	189.6	190.3	0.7	D39160	0.74	0.71	0.497	0.5254
Comp D63	60880	MGZD175	190.3	191	0.7	D39161	0.83	0.52	0.364	0.4316
Comp D63	60920	MGZD147	158.4	159.1	0.7	D31826	0.86	0.66	0.462	0.5676
Comp D63	60920	MGZD162	162.5	163.2	0.7	D35645	0.77	0.62	0.434	0.4774
Comp D63	60960	MGZD028	182.1	182.8	0.7	D02510	0.94	0.71	0.497	0.6674
Comp D63	60960	MGZD029	113	114	1.0	D02555	1.27	0.71	0.71	0.9017
Comp D63	60960	MGZD029	179.8	180.5	0.7	D02592	0.87	0.65	0.455	0.5655
Comp D63	60960	MGZD048	141.2	142	0.8	D04709	0.83	0.69	0.552	0.5727
Comp D63	60960	MGZD048	157.2	158	0.8	D04730	0.9	0.53	0.424	0.477
Comp D63	60960	MGZD048	158.7	159.4	0.7	D04732	0.79	0.66	0.462	0.5214
Comp D63	60960	MGZD048	163	164	1.0	D04737	1.3	0.65	0.65	0.845
Comp D63	60960	MGZD048	165	166	1.0	D04740	1.23	0.63	0.63	0.7749
Comp D63	60960	MGZD048	167	168	1.0	D04742	1.07	0.74	0.74	0.7918
Comp D63	60960	MGZD062	105	106	1.0	D06502	1.1	0.57	0.57	0.627
Comp D63	60960	MGZD062	113	114	1.0	D06511	1.1	0.52	0.52	0.572
Comp D63	60960	MGZD063	123.8	124.5	0.7	D06393	0.74	0.51	0.357	0.3774
Comp D63	60960	MGZD071	127.3	128	0.7	D07650	0.72	0.68	0.476	0.4896
Comp D63	60960	MGZD145	98	99	1.0	D30519	1.23	0.57	0.57	0.7011
Comp D63	61000	MGZD117	117.9	118.6	0.7	D20215	0.83	0.52	0.364	0.4316
Comp D63	61000	MGZD124	130.9	131.6	0.7	D22331	0.7	0.56	0.392	0.392
Comp D63	61000	MGZD125	95.7	96.4	0.7	D23230	0.7	0.66	0.462	0.462
Comp D63	61000	MGZD125	106.9	107.6	0.7	D23248	0.85	0.65	0.455	0.5525
Comp D63	61000	MGZD125	109	109.7	0.7	D23251	0.8	0.61	0.427	0.488
Comp D63	61000	MGZD125	111.1	111.8	0.7	D23254	0.77	0.62	0.434	0.4774
Comp D63	61000	MGZD125	117.4	118.1	0.7	D23264	0.75	0.53	0.371	0.3975
Comp D63	61000	MGZD127	101.6	102.3	0.7	D25356	0.79	0.65	0.455	0.5135
Comp D63	61000	MGZD127	113	114	1.0	D25369	1.14	0.65	0.65	0.741

D ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp D63	61040	MGZD026	13	14	1.0	D24944	1	0.65	0.65	0.65
Comp D63	61040	MGZD026	86	87	1.0	D02389	1.2	0.6	0.6	0.72
Comp D63	61040	MGZD027	105	105.7	0.7	D02435	0.8	0.67	0.469	0.536
Comp D63	61040	MGZD027	119.7	120.4	0.7	D02459	0.78	0.72	0.504	0.5616
Comp D63	61040	MGZD027	120.4	121.1	0.7	D02460	0.73	0.54	0.378	0.3942
Comp D63	61040	MGZD059	31	32	1.0	D07091	1.19	0.75	0.75	0.8925
Comp D63	61040	MGZD060	89.4	90.1	0.7	D06564	0.5	0.57	0.399	0.285
Comp D63	61040	MGZD067	70.4	71.1	0.7	D07283	0.79	0.73	0.511	0.5767
Comp D63	61040	MGZD067	72	73	1.0	D07285	1.08	0.57	0.57	0.6156
Comp D63	61040	MGZD069	88.1	89	0.9	D07515	1.05	0.51	0.459	0.5355
Comp D63	61040	MGZD104	52.9	53.6	0.7	D16901	0.66	0.66	0.462	0.4356
Comp D63	61040	MGZD104	65.5	66.2	0.7	D16920	0.66	0.74	0.518	0.4884
Comp D63	61040	MGZD104	92.1	92.8	0.7	D16962	0.82	0.54	0.378	0.4428
Comp D63	61040	MGZD104	93.5	94.2	0.7	D16964	0.78	0.51	0.357	0.3978
Comp D63	61080	MGZD024	70	70.7	0.7	D02227	0.8	0.65	0.455	0.52
Comp D63	61080	MGZD024	70.7	71.4	0.7	D02228	0.8	0.56	0.392	0.448
Comp D63	61080	MGZD025	26	27	1.0	D04082	1.1	0.65	0.65	0.715
Comp D63	61080	MGZD025	45.5	46.3	0.8	D02272	0.7	0.61	0.488	0.427
Comp D63	61080	MGZD025	46.3	47	0.7	D02273	0.7	0.51	0.357	0.357
Comp D63	61080	MGZD025	47	47.7	0.7	D02274	0.6	0.55	0.385	0.33
Comp D63	61080	MGZD032	49.7	50.4	0.7	D02753	0.7	0.62	0.434	0.434
Comp D63	61080	MGZD032	55.1	56	0.9	D02761	1	0.55	0.495	0.55
Comp D63	61080	MGZD053	62.2	63	0.8	D06049	0.97	0.52	0.416	0.5044
Comp D63	61080	MGZD105	14	14.7	0.7	D19033	1.38	0.73	0.511	1.0074
Comp D63	61080	MGZD105	20.3	21	0.7	D19043	0.78	0.59	0.413	0.4602
Comp D63	61080	MGZD106	36.5	37.2	0.7	D18822	0.86	0.67	0.469	0.5762
Comp D63	61080	MGZD109	51	51.7	0.7	D19463	0.98	0.6	0.42	0.588
Comp D63	61080	MGZD109	52.4	53.1	0.7	D19465	0.92	0.7	0.49	0.644
Comp D63	61080	MGZD116	61	62	1.0	D20363	2.16	0.66	0.66	1.4256
Comp D63	61080	MGZD116	62	63	1.0	D20364	2.21	0.73	0.73	1.6133
Comp D63	61080	MGZD118	54.1	54.8	0.7	D20437	1.24	0.6	0.42	0.744
Comp D63	61080	MGZD118	55.5	56.2	0.7	D20440	1.45	0.75	0.525	1.0875
Comp D63	61080	MGZD118	97.4	98.1	0.7	D20500	1.34	0.6	0.42	0.804
Comp D63	61120	MGZD019	37.4	38.1	0.7	D01540	0.66	0.56	0.392	0.3696
Comp D63	61120	MGZD019	78	79	1.0	D01584	1.1	0.69	0.69	0.759
Comp D63	61120	MGZD023	56.1	56.8	0.7	D02153	0.6	0.65	0.455	0.39
Comp D63	61120	MGZD023	70.7	71.4	0.7	D02172	0.7	0.52	0.364	0.364
Comp D63	61120	MGZD051	19	19.7	0.7	D05814	0.84	0.63	0.441	0.5292
Comp D63	61120	MGZD051	76	77	1.0	D05883	1.24	0.54	0.54	0.6696
Comp D63	61120	MGZD051	79.8	80.5	0.7	D05888	0.9	0.71	0.497	0.639
Comp D63	61120	MGZD054	56.4	57.1	0.7	D06351	1.02	0.74	0.518	0.7548
Comp D63	61120	MGZD054	57.1	58	0.9	D06352	0.91	0.65	0.585	0.5915
Comp D63	61120	MGZD054	68	69	1.0	D06365	1.33	0.59	0.59	0.7847
Comp D63	61120	MGZD055	53.4	54.1	0.7	D06155	0.73	0.64	0.448	0.4672
Comp D63	61120	MGZD055	66	66.7	0.7	D06173	0.88	0.65	0.455	0.572
Comp D63	61120	MGZD141	58	59	1.0	D29573	1.16	0.63	0.63	0.7308
Comp D63	61120	MGZD141	60	61	1.0	D29575	1.38	0.61	0.61	0.8418
Comp D63	61160	MGZD056	12.2	13	0.8	D05912	0.77	0.65	0.52	0.5005
Comp D63	61160	MGZD056	50.1	51	0.9	D05960	0.95	0.68	0.612	0.646
Comp D63	61160	MGZD056	51.7	52.4	0.7	D05962	0.69	0.6	0.42	0.414
Comp D63	61160	MGZD056	73	74	1.0	D05988	1.09	0.75	0.75	0.8175
Comp D63	61160	MGZD056	74	75	1.0	D05989	1.18	0.63	0.63	0.7434
Comp D63	61160	MGZD058	14.8	15.5	0.7	D06199	0.8	0.66	0.462	0.528
Comp D63	61160	MGZD058	33.7	34.4	0.7	D06220	0.77	0.62	0.434	0.4774
Comp D63	61160	MGZD058	34.4	35.1	0.7	D06222	0.77	0.67	0.469	0.5159
Comp D63	61160	MGZD058	49	50	1.0	D06242	1.1	0.58	0.58	0.638

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Comp D63	61160	MGZD110	9.5	10.2	0.7	D18924	0.68	0.63	0.441	0.4284
Comp D63	61160	MGZD110	13	13.7	0.7	D18929	0.71	0.56	0.392	0.3976
Comp D63	61160	MGZD110	33.2	33.9	0.7	D18960	0.79	0.59	0.413	0.4661
Comp D63	61160	MGZD110	33.9	34.6	0.7	D18961	0.78	0.57	0.399	0.4446
Comp D63	61160	MGZD110	38.8	39.5	0.7	D18968	0.78	0.71	0.497	0.5538
Comp D63	61160	MGZD111	16	17	1.0	D19550	1.36	0.63	0.63	0.8568
Comp D63	61160	MGZD111	21.4	22.1	0.7	D19556	1.42	0.72	0.504	1.0224
Comp D63	61160	MGZD111	29.1	29.8	0.7	D19568	0.66	0.68	0.476	0.4488
Comp D63	61160	MGZD111	32.6	33.3	0.7	D19574	0.75	0.65	0.455	0.4875
Comp D63	61160	MGZD111	33.3	34	0.7	D19575	0.87	0.53	0.371	0.4611
Comp D63	61200	MGZD113	27	27.7	0.7	D19830	0.73	0.74	0.518	0.5402
Comp D63	61200	MGZD114	24.2	24.9	0.7	D19310	0.85	0.54	0.378	0.459
Comp D63	61200	MGZD114	26.3	27	0.7	D19313	0.87	0.71	0.497	0.6177
Comp D63	61200	MGZD114	29.8	30.5	0.7	D19319	0.87	0.65	0.455	0.5655
Comp D63	61200	MGZD114	31.2	31.9	0.7	D19322	0.73	0.65	0.455	0.4745
Comp D64	60880	MGZD175	192.4	193.1	0.7	D39164	0.8	0.97	0.679	0.776
Comp D64	60920	MGZD147	156.3	157	0.7	D31823	0.77	0.9	0.63	0.693
Comp D64	60920	MGZD162	152	152.7	0.7	D35629	0.93	0.78	0.546	0.7254
Comp D64	60920	MGZD162	153.4	154.1	0.7	D35631	0.86	0.84	0.588	0.7224
Comp D64	60920	MGZD162	163.2	163.9	0.7	D35647	0.8	0.96	0.672	0.768
Comp D64	60960	MGZD022	153.8	154.5	0.7	D01868	0.89	0.96	0.672	0.8544
Comp D64	60960	MGZD022	155.2	155.9	0.7	D01870	0.93	0.96	0.672	0.8928
Comp D64	60960	MGZD022	157.3	158	0.7	D01875	0.89	0.85	0.595	0.7565
Comp D64	60960	MGZD028	185.6	186.3	0.7	D02515	1.08	0.79	0.553	0.8532
Comp D64	60960	MGZD029	110.1	111	0.9	D02552	1.06	1	0.9	1.06
Comp D64	60960	MGZD029	112	113	1.0	D02554	1.36	0.85	0.85	1.156
Comp D64	60960	MGZD048	129	129.7	0.7	D04690	0.73	0.83	0.581	0.6059
Comp D64	60960	MGZD048	159.4	160.1	0.7	D04733	0.96	0.78	0.546	0.7488
Comp D64	60960	MGZD063	124.5	125.2	0.7	D06394	0.68	0.84	0.588	0.5712
Comp D64	60960	MGZD063	129	129.7	0.7	D06400	0.8	0.87	0.609	0.696
Comp D64	60960	MGZD063	137.8	138.5	0.7	D06412	0.81	0.92	0.644	0.7452
Comp D64	60960	MGZD063	139.2	140	0.8	D06414	0.83	0.78	0.624	0.6474
Comp D64	60960	MGZD063	146.1	146.8	0.7	D06424	0.73	0.85	0.595	0.6205
Comp D64	60960	MGZD071	125.9	126.6	0.7	D07647	0.83	0.83	0.581	0.6889
Comp D64	60960	MGZD071	128	128.7	0.7	D07651	0.82	0.88	0.616	0.7216
Comp D64	60960	MGZD145	96	97	1.0	D30516	1.14	0.84	0.84	0.9576
Comp D64	61000	MGZD117	113.7	114.4	0.7	D20209	0.75	0.79	0.553	0.5925
Comp D64	61000	MGZD117	115.1	115.8	0.7	D20211	0.78	0.8	0.56	0.624
Comp D64	61000	MGZD117	116.5	117.2	0.7	D20213	0.83	1	0.7	0.83
Comp D64	61000	MGZD125	93.6	94.3	0.7	D23227	0.69	0.77	0.539	0.5313
Comp D64	61000	MGZD125	95	95.7	0.7	D23229	0.67	0.98	0.686	0.6566
Comp D64	61000	MGZD125	106.2	106.9	0.7	D23247	0.79	0.83	0.581	0.6557
Comp D64	61000	MGZD125	107.6	108.3	0.7	D23249	0.85	0.78	0.546	0.663
Comp D64	61000	MGZD125	115.3	116	0.7	D23261	0.79	0.84	0.588	0.6636
Comp D64	61000	MGZD127	103	104	1.0	D25359	1.15	0.79	0.79	0.9085
Comp D64	61000	MGZD127	106	107	1.0	D25362	1.15	0.81	0.81	0.9315
Comp D64	61000	MGZD127	107	108	1.0	D25363	1.19	0.8	0.8	0.952
Comp D64	61000	MGZD127	111	112	1.0	D25367	1.1	0.99	0.99	1.089
Comp D64	61040	MGZD027	123.9	124.6	0.7	D02465	0.77	0.82	0.574	0.6314
Comp D64	61040	MGZD027	126	126.7	0.7	D02468	0.84	0.83	0.581	0.6972
Comp D64	61040	MGZD027	138.4	139.1	0.7	D02484	1	0.99	0.693	0.99
Comp D64	61040	MGZD067	66	66.7	0.7	D07277	0.84	0.89	0.623	0.7476
Comp D64	61040	MGZD067	69	69.7	0.7	D07281	0.81	0.84	0.588	0.6804
Comp D64	61040	MGZD067	69.7	70.4	0.7	D07282	0.8	0.92	0.644	0.736
Comp D64	61040	MGZD104	66.2	66.9	0.7	D16922	0.63	0.92	0.644	0.5796
Comp D64	61080	MGZD025	41.4	42.4	1.0	D02266	1.1	0.83	0.83	0.913

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Comp D64	61080	MGZD032	53.7	54.4	0.7	D02759	0.8	0.8	0.56	0.64
Comp D64	61080	MGZD053	68.7	69.4	0.7	D06057	0.74	1	0.7	0.74
Comp D64	61080	MGZD053	75.1	75.8	0.7	D06067	0.82	0.82	0.574	0.6724
Comp D64	61080	MGZD105	14.7	15.4	0.7	D19034	0.87	0.82	0.574	0.7134
Comp D64	61080	MGZD105	15.4	16.1	0.7	D19035	0.69	0.99	0.693	0.6831
Comp D64	61080	MGZD105	17.5	18.2	0.7	D19039	0.65	0.94	0.658	0.611
Comp D64	61080	MGZD105	18.2	18.9	0.7	D19040	0.72	0.76	0.532	0.5472
Comp D64	61080	MGZD105	21	21.7	0.7	D19044	0.62	0.87	0.609	0.5394
Comp D64	61080	MGZD105	21.7	22.4	0.7	D19045	0.75	0.91	0.637	0.6825
Comp D64	61080	MGZD106	34.4	35.1	0.7	D18817	0.76	0.89	0.623	0.6764
Comp D64	61080	MGZD108	63	63.7	0.7	D19216	0.57	0.79	0.553	0.4503
Comp D64	61080	MGZD118	58.3	59	0.7	D20444	1.31	0.81	0.567	1.0611
Comp D64	61120	MGZD018	49.7	50.4	0.7	D01480	0.7	0.89	0.623	0.623
Comp D64	61120	MGZD019	36.7	37.4	0.7	D01539	0.65	0.76	0.532	0.494
Comp D64	61120	MGZD019	75	76	1.0	D01581	1	1	1	1
Comp D64	61120	MGZD019	87	88	1.0	D01594	1.2	0.8	0.8	0.96
Comp D64	61120	MGZD019	102	103	1.0	D01611	1.15	0.84	0.84	0.966
Comp D64	61120	MGZD023	32.7	33.4	0.7	D02125	0.7	0.97	0.679	0.679
Comp D64	61120	MGZD023	62.1	63.1	1.0	D02162	1	0.98	0.98	0.98
Comp D64	61120	MGZD023	71.4	72.1	0.7	D02174	0.8	0.87	0.609	0.696
Comp D64	61120	MGZD051	23.7	24.4	0.7	D05822	0.75	0.92	0.644	0.69
Comp D64	61120	MGZD051	77.7	78.4	0.7	D05885	0.85	0.98	0.686	0.833
Comp D64	61120	MGZD054	55	55.7	0.7	D06349	0.79	0.95	0.665	0.7505
Comp D64	61120	MGZD055	36.7	37.4	0.7	D06132	0.77	0.97	0.679	0.7469
Comp D64	61120	MGZD055	37.4	38.1	0.7	D06134	0.83	0.82	0.574	0.6806
Comp D64	61120	MGZD055	47.7	48.4	0.7	D06147	0.75	0.99	0.693	0.7425
Comp D64	61120	MGZD141	61	62	1.0	D29576	1.21	0.79	0.79	0.9559
Comp D64	61120	MGZD141	62	63	1.0	D29577	1.33	0.77	0.77	1.0241
Comp D64	61160	MGZD056	11.5	12.2	0.7	D05911	0.76	1	0.7	0.76
Comp D64	61160	MGZD056	69	70	1.0	D05984	1.21	0.8	0.8	0.968
Comp D64	61160	MGZD058	13.4	14.1	0.7	D06197	0.7	0.96	0.672	0.672
Comp D64	61160	MGZD058	37	38	1.0	D06226	1.13	1	1	1.13
Comp D64	61160	MGZD058	46.1	46.8	0.7	D06237	0.8	0.98	0.686	0.784
Comp D64	61160	MGZD110	11.6	12.3	0.7	D18927	0.64	0.83	0.581	0.5312
Comp D64	61160	MGZD110	15.8	16.5	0.7	D18933	0.66	0.82	0.574	0.5412
Comp D64	61160	MGZD111	15	16	1.0	D19549	1.25	0.78	0.78	0.975
Comp D64	61160	MGZD111	19	20	1.0	D19553	1.69	1	1	1.69
Comp D64	61200	MGZD114	17.2	17.9	0.7	D19300	0.86	0.86	0.602	0.7396
Comp D64	61200	MGZD114	25.6	26.3	0.7	D19312	0.67	0.88	0.616	0.5896
Comp D64	61200	MGZD114	27	27.7	0.7	D19314	0.85	0.78	0.546	0.663
Comp D64	61200	MGZD114	30.5	31.2	0.7	D19320	0.79	0.76	0.532	0.6004
Comp D65	60880	MGZD175	174	175	1.0	D39136	1.1	1.04	1.04	1.144
Comp D65	60880	MGZD175	184.7	185.4	0.7	D39152	0.79	1.03	0.721	0.8137
Comp D65	60880	MGZD175	186.8	187.5	0.7	D39155	0.76	1.01	0.707	0.7676
Comp D65	60920	MGZD147	151.4	152.1	0.7	D31814	0.81	1.27	0.889	1.0287
Comp D65	60920	MGZD147	157	157.7	0.7	D31824	0.78	1.13	0.791	0.8814
Comp D65	60960	MGZD022	151	151.7	0.7	D01864	0.74	1.08	0.756	0.7992
Comp D65	60960	MGZD022	151.7	152.4	0.7	D01865	0.9	1.24	0.868	1.116
Comp D65	60960	MGZD022	152.4	153.1	0.7	D01866	0.84	1.02	0.714	0.8568
Comp D65	60960	MGZD022	155.9	156.6	0.7	D01872	0.9	1.08	0.756	0.972
Comp D65	60960	MGZD028	182.8	183.5	0.7	D02511	0.76	1.08	0.756	0.8208
Comp D65	60960	MGZD028	187	187.7	0.7	D02517	0.91	1.3	0.91	1.183
Comp D65	60960	MGZD028	200.7	201.4	0.7	D02535	0.87	1.06	0.742	0.9222
Comp D65	60960	MGZD029	114	115	1.0	D02556	1.24	1.07	1.07	1.3268
Comp D65	60960	MGZD029	181.9	182.6	0.7	D02597	0.79	1.07	0.749	0.8453

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Comp D65	60960	MGZD048	117	117.7	0.7	D04673	0.75	1.23	0.861	0.9225
Comp D65	60960	MGZD048	128	129	1.0	D04689	1.03	1.09	1.09	1.1227
Comp D65	60960	MGZD048	130.4	131.1	0.7	D04692	0.72	1.28	0.896	0.9216
Comp D65	60960	MGZD048	137	137.7	0.7	D04702	0.71	1.3	0.91	0.923
Comp D65	60960	MGZD048	137.7	138.4	0.7	D04703	0.72	1.19	0.833	0.8568
Comp D65	60960	MGZD048	166	167	1.0	D04741	1.18	1.03	1.03	1.2154
Comp D65	60960	MGZD062	111	112	1.0	D06509	1.1	1.2	1.2	1.32
Comp D65	60960	MGZD063	120	121	1.0	D06387	1.07	1.09	1.09	1.1663
Comp D65	60960	MGZD063	133	134	1.0	D06406	1.04	1.08	1.08	1.1232
Comp D65	60960	MGZD063	147.5	148.2	0.7	D06426	0.78	1.18	0.826	0.9204
Comp D65	60960	MGZD071	128.7	129.4	0.7	D07652	0.82	1.06	0.742	0.8692
Comp D65	60960	MGZD071	130.8	131.5	0.7	D07655	0.79	1.05	0.735	0.8295
Comp D65	61000	MGZD117	101.1	101.8	0.7	D20189	0.66	1.17	0.819	0.7722
Comp D65	61000	MGZD119	88.3	89	0.7	D20631	0.84	1.04	0.728	0.8736
Comp D65	61000	MGZD124	85	86	1.0	D22269	0.95	1.15	1.15	1.0925
Comp D65	61000	MGZD125	94.3	95	0.7	D23228	0.77	1.04	0.728	0.8008
Comp D65	61000	MGZD125	112.5	113.2	0.7	D23256	0.72	1.04	0.728	0.7488
Comp D65	61000	MGZD125	116	116.7	0.7	D23262	0.88	1.16	0.812	1.0208
Comp D65	61000	MGZD127	102.3	103	0.7	D25357	0.7	1.12	0.784	0.784
Comp D65	61040	MGZD026	87.7	88.4	0.7	D02391	0.7	1.11	0.777	0.777
Comp D65	61040	MGZD026	89.8	90.5	0.7	D02394	0.8	1.1	0.77	0.88
Comp D65	61040	MGZD027	112.7	113.4	0.7	D02448	0.79	1.14	0.798	0.9006
Comp D65	61040	MGZD027	124.6	125.3	0.7	D02466	0.89	1.23	0.861	1.0947
Comp D65	61040	MGZD067	60	61	1.0	D07269	1.02	1.16	1.16	1.1832
Comp D65	61040	MGZD067	68.1	69	0.9	D07280	1	1.01	0.909	1.01
Comp D65	61080	MGZD025	44	44.7	0.7	D02269	0.7	1.02	0.714	0.714
Comp D65	61080	MGZD032	59	60	1.0	D02765	1.2	1.18	1.18	1.416
Comp D65	61080	MGZD032	80.3	81	0.7	D02793	0.82	1.29	0.903	1.0578
Comp D65	61080	MGZD053	31.7	32.4	0.7	D06010	0.67	1.09	0.763	0.7303
Comp D65	61080	MGZD053	33.1	34	0.9	D06012	1	1.19	1.071	1.19
Comp D65	61080	MGZD053	70.8	71.5	0.7	D06061	0.71	1.3	0.91	0.923
Comp D65	61080	MGZD053	73.7	74.4	0.7	D06065	0.64	1.06	0.742	0.6784
Comp D65	61080	MGZD105	18.9	19.6	0.7	D19041	0.81	1.1	0.77	0.891
Comp D65	61080	MGZD105	19.6	20.3	0.7	D19042	0.85	1.13	0.791	0.9605
Comp D65	61080	MGZD105	22.4	23.1	0.7	D19047	0.72	1.01	0.707	0.7272
Comp D65	61080	MGZD106	35.1	35.8	0.7	D18819	0.71	1.21	0.847	0.8591
Comp D65	61080	MGZD118	94	95	1.0	D20494	2.37	1.02	1.02	2.4174
Comp D65	61120	MGZD018	48	49	1.0	D01478	1.1	1.06	1.06	1.166
Comp D65	61120	MGZD019	39	39.7	0.7	D01542	0.74	1.27	0.889	0.9398
Comp D65	61120	MGZD023	23	24	1.0	D02112	1.2	1.09	1.09	1.308
Comp D65	61120	MGZD023	24	25	1.0	D02114	0.9	1.07	1.07	0.963
Comp D65	61120	MGZD023	72.8	73.5	0.7	D02176	0.9	1.26	0.882	1.134
Comp D65	61120	MGZD033	42.7	43.4	0.7	D02830	0.78	1.08	0.756	0.8424
Comp D65	61120	MGZD051	14	14.7	0.7	D05808	0.89	1.29	0.903	1.1481
Comp D65	61120	MGZD055	25.7	26.4	0.7	D06117	0.9	1.17	0.819	1.053
Comp D65	61160	MGZD034	43	43.7	0.7	D02890	0.76	1.14	0.798	0.8664
Comp D65	61160	MGZD034	61	62	1.0	D02914	1.23	1.19	1.19	1.4637
Comp D65	61160	MGZD034	63	64	1.0	D02916	1.21	1.21	1.21	1.4641
Comp D65	61160	MGZD056	8	8.7	0.7	D05905	0.84	1.1	0.77	0.924
Comp D65	61160	MGZD056	10.8	11.5	0.7	D05910	0.72	1.16	0.812	0.8352
Comp D65	61160	MGZD056	42	43	1.0	D05948	1.11	1.16	1.16	1.2876
Comp D65	61160	MGZD056	52.4	53.1	0.7	D05963	0.82	1.04	0.728	0.8528
Comp D65	61160	MGZD058	33	33.7	0.7	D06219	0.83	1.21	0.847	1.0043
Comp D65	61160	MGZD110	14.4	15.1	0.7	D18931	0.72	1.09	0.763	0.7848
Comp D65	61160	MGZD111	9	10	1.0	D19542	0.97	1.02	1.02	0.9894

D ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp D65	61160	MGZD111	11	12	1.0	D19544	1.16	1.08	1.08	1.2528
Comp D65	61160	MGZD111	12	13	1.0	D19545	1.31	1.28	1.28	1.6768
Comp D65	61160	MGZD111	37.4	38.1	0.7	D19581	0.79	1.02	0.714	0.8058
Comp D65	61200	MGZD112	40.7	41.4	0.7	D19704	0.82	1.12	0.784	0.9184
Comp D65	61200	MGZD112	42.8	43.5	0.7	D19707	0.69	1.1	0.77	0.759
Comp D65	61200	MGZD113	15.1	15.8	0.7	D19811	0.73	1.04	0.728	0.7592
Comp D65	61200	MGZD113	22.8	23.5	0.7	D19824	0.77	1.02	0.714	0.7854
Comp D65	61200	MGZD113	24.9	25.6	0.7	D19827	0.68	1.15	0.805	0.782
Comp D65	61200	MGZD114	22.1	22.8	0.7	D19307	0.78	1.2	0.84	0.936
Comp D65	61200	MGZD114	50.8	51.5	0.7	D19352	0.67	1.29	0.903	0.8643
Comp D66	60920	MGZD162	152.7	153.4	0.7	D35630	0.87	1.6	1.12	1.392
Comp D66	60920	MGZD162	163.9	164.6	0.7	D35648	0.83	1.46	1.022	1.2118
Comp D66	60960	MGZD022	154.5	155.2	0.7	D01869	0.91	1.44	1.008	1.3104
Comp D66	60960	MGZD028	181.4	182.1	0.7	D02509	0.81	1.49	1.043	1.2069
Comp D66	60960	MGZD028	186.3	187	0.7	D02516	0.85	1.44	1.008	1.224
Comp D66	60960	MGZD029	103	104	1.0	D25513	0.95	1.46	1.46	1.387
Comp D66	60960	MGZD048	112	113	1.0	D04666	1.02	1.75	1.75	1.785
Comp D66	60960	MGZD048	115.4	116.1	0.7	D04670	0.74	1.37	0.959	1.0138
Comp D66	60960	MGZD048	124.5	125.2	0.7	D04684	0.65	1.51	1.057	0.9815
Comp D66	60960	MGZD048	125.9	126.6	0.7	D04686	0.8	1.6	1.12	1.28
Comp D66	60960	MGZD048	129.7	130.4	0.7	D04691	0.72	1.52	1.064	1.0944
Comp D66	60960	MGZD048	131.8	132.5	0.7	D04695	0.72	1.56	1.092	1.1232
Comp D66	60960	MGZD048	138.4	139.1	0.7	D04704	0.69	1.33	0.931	0.9177
Comp D66	60960	MGZD048	139.1	139.8	0.7	D04705	0.71	1.46	1.022	1.0366
Comp D66	60960	MGZD048	139.8	140.5	0.7	D04706	0.72	1.66	1.162	1.1952
Comp D66	60960	MGZD048	140.5	141.2	0.7	D04707	0.72	1.66	1.162	1.1952
Comp D66	60960	MGZD048	146	146.7	0.7	D04714	0.76	1.31	0.917	0.9956
Comp D66	60960	MGZD048	146.7	147.4	0.7	D04715	0.72	1.42	0.994	1.0224
Comp D66	60960	MGZD048	152	153	1.0	D04722	1.16	1.63	1.63	1.8908
Comp D66	60960	MGZD048	154.4	155.1	0.7	D04726	0.65	1.64	1.148	1.066
Comp D66	60960	MGZD062	112	113	1.0	D06510	1	1.7	1.7	1.7
Comp D66	60960	MGZD063	137.1	137.8	0.7	D06411	0.73	1.6	1.12	1.168
Comp D66	60960	MGZD063	142	143	1.0	D06417	1.08	1.32	1.32	1.4256
Comp D66	60960	MGZD063	146.8	147.5	0.7	D06425	0.76	1.32	0.924	1.0032
Comp D66	60960	MGZD071	131.5	132.2	0.7	D07656	0.59	1.6	1.12	0.944
Comp D66	60960	MGZD071	132.2	132.9	0.7	D07657	1.04	1.75	1.225	1.82
Comp D66	60960	MGZD145	95	96	1.0	D30515	1.07	1.34	1.34	1.4338
Comp D66	61000	MGZD117	120	121	1.0	D20219	1.3	1.67	1.67	2.171
Comp D66	61000	MGZD119	91.1	91.8	0.7	D20635	0.74	1.42	0.994	1.0508
Comp D66	61000	MGZD125	110.4	111.1	0.7	D23253	0.79	1.44	1.008	1.1376
Comp D66	61000	MGZD125	114.6	115.3	0.7	D23260	0.81	1.59	1.113	1.2879
Comp D66	61040	MGZD026	11	12	1.0	D24942	1	1.46	1.46	1.46
Comp D66	61040	MGZD026	89.1	89.8	0.7	D02393	0.8	1.59	1.113	1.272
Comp D66	61040	MGZD027	109.2	109.9	0.7	D02441	0.76	1.55	1.085	1.178
Comp D66	61040	MGZD027	112	112.7	0.7	D02447	0.74	1.74	1.218	1.2876
Comp D66	61040	MGZD027	117.6	118.3	0.7	D02455	0.79	1.43	1.001	1.1297
Comp D66	61040	MGZD027	119	119.7	0.7	D02457	0.82	1.43	1.001	1.1726
Comp D66	61040	MGZD027	123.2	123.9	0.7	D02464	0.88	1.48	1.036	1.3024
Comp D66	61040	MGZD059	32	33	1.0	D07092	1.23	1.32	1.32	1.6236
Comp D66	61040	MGZD059	130	131	1.0	D07151	1.27	1.55	1.55	1.9685
Comp D66	61040	MGZD067	58	59	1.0	D07267	1.02	1.62	1.62	1.6524
Comp D66	61040	MGZD067	59	60	1.0	D07268	1.01	1.32	1.32	1.3332
Comp D66	61040	MGZD067	71.1	72	0.9	D07284	1.03	1.61	1.449	1.6583
Comp D66	61040	MGZD067	74	75	1.0	D07287	1.07	1.38	1.38	1.4766
Comp D66	61040	MGZD067	77	78	1.0	D07291	0.89	1.69	1.69	1.5041

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Comp D66	61040	MGZD067	80	80.7	0.7	D07294	0.83	1.61	1.127	1.3363
Comp D66	61040	MGZD067	86	87	1.0	D07302	1.22	1.46	1.46	1.7812
Comp D66	61040	MGZD104	52.2	52.9	0.7	D16900	0.65	1.38	0.966	0.897
Comp D66	61040	MGZD104	90	90.7	0.7	D16959	0.84	1.5	1.05	1.26
Comp D66	61040	MGZD104	94.2	94.9	0.7	D16965	0.79	1.44	1.008	1.1376
Comp D66	61040	MGZD138	56.4	57.1	0.7	D29107	0.84	1.72	1.204	1.4448
Comp D66	61080	MGZD025	28	29	1.0	D04084	1.1	1.51	1.51	1.661
Comp D66	61080	MGZD025	51.2	51.9	0.7	D02281	0.7	1.56	1.092	1.092
Comp D66	61080	MGZD032	52	53	1.0	D02756	1.2	1.59	1.59	1.908
Comp D66	61080	MGZD032	60	61	1.0	D02766	1.1	1.38	1.38	1.518
Comp D66	61080	MGZD053	31	31.7	0.7	D06009	0.64	1.58	1.106	1.0112
Comp D66	61080	MGZD053	77.9	78.6	0.7	D06072	0.84	1.72	1.204	1.4448
Comp D66	61080	MGZD106	35.8	36.5	0.7	D18820	0.73	1.35	0.945	0.9855
Comp D66	61080	MGZD108	33.1	33.8	0.7	D19175	0.78	1.4	0.98	1.092
Comp D66	61080	MGZD116	60	61	1.0	D20362	2.19	1.37	1.37	3.0003
Comp D66	61080	MGZD116	68	69	1.0	D20370	2.13	1.67	1.67	3.5571
Comp D66	61080	MGZD118	43	44	1.0	D20423	2.18	1.49	1.49	3.2482
Comp D66	61080	MGZD118	45	45.7	0.7	D20425	1.6	1.43	1.001	2.288
Comp D66	61080	MGZD118	68.8	69.5	0.7	D20461	1.38	1.46	1.022	2.0148
Comp D66	61080	MGZD118	74.4	75.1	0.7	D20469	1.47	1.71	1.197	2.5137
Comp D66	61080	MGZD118	75.8	76.5	0.7	D20472	1.6	1.31	0.917	2.096
Comp D66	61120	MGZD018	23.7	24.7	1.0	D01449	1.1	1.39	1.39	1.529
Comp D66	61120	MGZD018	42	42.7	0.7	D01470	0.7	1.53	1.071	1.071
Comp D66	61120	MGZD019	26.7	27.4	0.7	D01526	0.45	1.34	0.938	0.603
Comp D66	61120	MGZD023	26.7	27.4	0.7	D02117	0.7	1.38	0.966	0.966
Comp D66	61120	MGZD023	84	85	1.0	D02190	1.2	1.72	1.72	2.064
Comp D66	61120	MGZD051	77	77.7	0.7	D05884	0.82	1.4	0.98	1.148
Comp D66	61120	MGZD054	34.4	35.1	0.7	D06322	0.85	1.7	1.19	1.445
Comp D66	61120	MGZD055	32	32.7	0.7	D06126	0.84	1.58	1.106	1.3272
Comp D66	61120	MGZD055	33.4	34.1	0.7	D06128	0.82	1.74	1.218	1.4268
Comp D66	61120	MGZD055	104	105	1.0	D07223	1.13	1.6	1.6	1.808
Comp D66	61160	MGZD056	8.7	9.4	0.7	D05906	0.64	1.54	1.078	0.9856
Comp D66	61160	MGZD058	1	2	1.0	D06181	1	1.62	1.62	1.62
Comp D66	61160	MGZD058	12.7	13.4	0.7	D06195	0.7	1.75	1.225	1.225
Comp D66	61160	MGZD058	39.7	40.4	0.7	D06229	0.89	1.75	1.225	1.5575
Comp D66	61160	MGZD058	46.8	47.5	0.7	D06239	0.7	1.34	0.938	0.938
Comp D66	61160	MGZD058	48.2	49	0.8	D06241	0.9	1.75	1.4	1.575
Comp D66	61160	MGZD110	10.2	10.9	0.7	D18925	0.68	1.65	1.155	1.122
Comp D66	61160	MGZD110	31.1	31.8	0.7	D18956	0.91	1.54	1.078	1.4014
Comp D66	61160	MGZD110	39.5	40.2	0.7	D18969	0.73	1.58	1.106	1.1534
Comp D66	61160	MGZD110	40.9	41.6	0.7	D18972	0.79	1.37	0.959	1.0823
Comp D66	61160	MGZD111	13	14	1.0	D19547	2.69	1.39	1.39	3.7391
Comp D66	61160	MGZD111	27.7	28.4	0.7	D19566	0.81	1.56	1.092	1.2636
Comp D66	61160	MGZD111	34	35	1.0	D19576	1.27	1.33	1.33	1.6891
Comp D66	61200	MGZD114	14.4	15.1	0.7	D19294	0.79	1.4	0.98	1.106
Comp D66	61200	MGZD114	32.6	33.3	0.7	D19324	0.87	1.43	1.001	1.2441
Comp D66	61200	MGZD114	48.7	49.4	0.7	D19349	0.87	1.32	0.924	1.1484
Comp D66	61200	MGZD114	50.1	50.8	0.7	D19351	0.89	1.59	1.113	1.4151
Comp D67	60880	MGZD164	200	201	1.0	D36356	1.17	2.46	2.46	2.8782
Comp D67	60880	MGZD175	201	202	1.0	D39176	1.11	2.08	2.08	2.3088
Comp D67	60920	MGZD142	190.2	191	0.8	D29922	0.89	2.33	1.864	2.0737
Comp D67	60920	MGZD147	140.2	140.9	0.7	D31797	0.8	1.89	1.323	1.512
Comp D67	60920	MGZD147	150.7	151.4	0.7	D31813	0.82	1.92	1.344	1.5744
Comp D67	60920	MGZD147	152.1	152.8	0.7	D31815	0.77	1.85	1.295	1.4245
Comp D67	60920	MGZD147	154.2	154.9	0.7	D31819	0.78	2.34	1.638	1.8252

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Comp D67	60920	MGZD147	154.9	155.6	0.7	D31820	0.78	2.02	1.414	1.5756
Comp D67	60960	MGZD022	156.6	157.3	0.7	D01874	0.89	2.49	1.743	2.2161
Comp D67	60960	MGZD028	184.2	184.9	0.7	D02513	0.83	2.23	1.561	1.8509
Comp D67	60960	MGZD028	184.9	185.6	0.7	D02514	1.07	2.24	1.568	2.3968
Comp D67	60960	MGZD028	188.4	189.1	0.7	D02520	0.83	1.88	1.316	1.5604
Comp D67	60960	MGZD028	201.4	202.1	0.7	D02536	0.75	1.99	1.393	1.4925
Comp D67	60960	MGZD029	108	108.7	0.7	D02549	0.82	2.15	1.505	1.763
Comp D67	60960	MGZD029	108.7	109.4	0.7	D02550	0.8	2.12	1.484	1.696
Comp D67	60960	MGZD048	114	114.7	0.7	D04668	0.7	1.99	1.393	1.393
Comp D67	60960	MGZD048	116.1	117	0.9	D04672	0.9	1.95	1.755	1.755
Comp D67	60960	MGZD048	121.7	122.4	0.7	D04680	0.72	2.5	1.75	1.8
Comp D67	60960	MGZD048	153.7	154.4	0.7	D04725	0.63	1.85	1.295	1.1655
Comp D67	60960	MGZD048	156.5	157.2	0.7	D04729	0.81	2.42	1.694	1.9602
Comp D67	60960	MGZD063	121	121.7	0.7	D06389	0.73	2.29	1.603	1.6717
Comp D67	60960	MGZD063	121.7	122.4	0.7	D06390	0.69	2.34	1.638	1.6146
Comp D67	60960	MGZD063	141	142	1.0	D06416	1.12	2.1	2.1	2.352
Comp D67	60960	MGZD063	144.7	145.4	0.7	D06422	0.75	2.21	1.547	1.6575
Comp D67	60960	MGZD071	123.8	124.5	0.7	D07643	0.71	2.46	1.722	1.7466
Comp D67	61000	MGZD119	89.7	90.4	0.7	D20633	0.75	2.39	1.673	1.7925
Comp D67	61000	MGZD122	112.1	113	0.9	D21839	0.96	2.26	2.034	2.1696
Comp D67	61000	MGZD124	129.5	130.2	0.7	D22329	0.71	1.95	1.365	1.3845
Comp D67	61000	MGZD125	104.8	105.5	0.7	D23244	0.84	1.78	1.246	1.4952
Comp D67	61000	MGZD125	111.8	112.5	0.7	D23255	0.92	2.27	1.589	2.0884
Comp D67	61000	MGZD125	118.8	119.5	0.7	D23266	0.79	1.88	1.316	1.4852
Comp D67	61040	MGZD026	10	11	1.0	D24941	1	2.27	2.27	2.27
Comp D67	61040	MGZD027	113.4	114.1	0.7	D02449	0.84	2.49	1.743	2.0916
Comp D67	61040	MGZD027	114.8	115.5	0.7	D02451	0.74	2.49	1.743	1.8426
Comp D67	61040	MGZD027	115.5	116.2	0.7	D02452	0.69	1.78	1.246	1.2282
Comp D67	61040	MGZD027	116.2	116.9	0.7	D02453	0.79	2.36	1.652	1.8644
Comp D67	61040	MGZD027	118.3	119	0.7	D02456	0.82	2.38	1.666	1.9516
Comp D67	61040	MGZD027	121.1	121.8	0.7	D02461	0.81	2.17	1.519	1.7577
Comp D67	61040	MGZD027	125.3	126	0.7	D02467	0.83	2.48	1.736	2.0584
Comp D67	61040	MGZD061	57	58	1.0	D06681	1.1	2.48	2.48	2.728
Comp D67	61040	MGZD067	76	77	1.0	D07290	1.24	2.28	2.28	2.8272
Comp D67	61040	MGZD067	99.7	100.4	0.7	D07317	0.85	2.42	1.694	2.057
Comp D67	61040	MGZD067	120.7	121.4	0.7	D07342	0.79	2.33	1.631	1.8407
Comp D67	61040	MGZD067	121.4	122.1	0.7	D07343	0.81	1.83	1.281	1.4823
Comp D67	61040	MGZD104	51.5	52.2	0.7	D16899	0.63	2.46	1.722	1.5498
Comp D67	61040	MGZD104	90.7	91.4	0.7	D16960	0.83	1.95	1.365	1.6185
Comp D67	61040	MGZD138	57.1	57.8	0.7	D29108	0.83	2.48	1.736	2.0584
Comp D67	61080	MGZD024	64.4	65.1	0.7	D02219	0.7	2.42	1.694	1.694
Comp D67	61080	MGZD024	65.8	66.5	0.7	D02222	0.6	2.2	1.54	1.32
Comp D67	61080	MGZD025	44.7	45.5	0.8	D02270	0.8	1.86	1.488	1.488
Comp D67	61080	MGZD025	49.8	50.5	0.7	D02279	0.7	1.99	1.393	1.393
Comp D67	61080	MGZD025	50.5	51.2	0.7	D02280	0.7	2.48	1.736	1.736
Comp D67	61080	MGZD025	86.1	87	0.9	D02322	0.9	2.09	1.881	1.881
Comp D67	61080	MGZD032	81.7	82.4	0.7	D02795	0.74	2.07	1.449	1.5318
Comp D67	61080	MGZD053	60.1	60.8	0.7	D06045	0.81	1.8	1.26	1.458
Comp D67	61080	MGZD106	24.5	25.2	0.7	D18805	0.69	2.31	1.617	1.5939
Comp D67	61080	MGZD106	25.2	25.9	0.7	D18806	0.79	2.29	1.603	1.8091
Comp D67	61080	MGZD106	37.9	38.6	0.7	D18824	0.85	1.82	1.274	1.547
Comp D67	61080	MGZD109	51.7	52.4	0.7	D19464	0.94	2.3	1.61	2.162
Comp D67	61080	MGZD118	45.7	46.4	0.7	D20426	1.58	1.79	1.253	2.8282
Comp D67	61080	MGZD118	54.8	55.5	0.7	D20439	1.49	2.1	1.47	3.129
Comp D67	61080	MGZD118	59	59.7	0.7	D20445	1.36	1.91	1.337	2.5976

D ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp D67	61080	MGZD118	73.7	74.4	0.7	D20468	1.35	1.87	1.309	2.5245
Comp D67	61120	MGZD018	21.7	22.8	1.1	D01447	1.2	1.99	2.189	2.388
Comp D67	61120	MGZD019	27.4	28.1	0.7	D01527	0.74	1.79	1.253	1.3246
Comp D67	61120	MGZD019	31.3	32	0.7	D01533	0.74	2.16	1.512	1.5984
Comp D67	61120	MGZD019	39.7	40.4	0.7	D01544	0.64	2.01	1.407	1.2864
Comp D67	61120	MGZD019	72.1	73	0.9	D01578	1.1	1.77	1.593	1.947
Comp D67	61120	MGZD019	83	84	1.0	D01590	1.1	1.97	1.97	2.167
Comp D67	61120	MGZD019	84	85	1.0	D01591	1.1	1.76	1.76	1.936
Comp D67	61120	MGZD019	86	87	1.0	D01593	1.2	2	2	2.4
Comp D67	61120	MGZD023	22	23	1.0	D02111	0.9	2.08	2.08	1.872
Comp D67	61120	MGZD023	57.5	58.2	0.7	D02155	0.8	1.97	1.379	1.576
Comp D67	61120	MGZD023	74.2	74.9	0.7	D02178	0.6	2.14	1.498	1.284
Comp D67	61120	MGZD033	43.4	44.1	0.7	D02831	0.69	1.95	1.365	1.3455
Comp D67	61120	MGZD051	19.7	20.4	0.7	D05815	0.76	2.26	1.582	1.7176
Comp D67	61120	MGZD054	33.7	34.4	0.7	D06320	0.86	2.04	1.428	1.7544
Comp D67	61120	MGZD055	68.1	69	0.9	D06176	1.15	1.86	1.674	2.139
Comp D67	61120	MGZD055	106	107	1.0	D07225	1.04	2.44	2.44	2.5376
Comp D67	61120	MGZD141	59	60	1.0	D29574	1.29	1.86	1.86	2.3994
Comp D67	61160	MGZD034	43.7	44.4	0.7	D02891	0.81	1.88	1.316	1.5228
Comp D67	61160	MGZD034	46.5	47.2	0.7	D02897	0.84	1.76	1.232	1.4784
Comp D67	61160	MGZD034	47.2	48	0.8	D02898	0.95	2.44	1.952	2.318
Comp D67	61160	MGZD056	51	51.7	0.7	D05961	0.8	2.31	1.617	1.848
Comp D67	61160	MGZD058	2	3	1.0	D06182	1.5	2.46	2.46	3.69
Comp D67	61160	MGZD110	10.9	11.6	0.7	D18926	0.63	1.99	1.393	1.2537
Comp D67	61160	MGZD110	15.1	15.8	0.7	D18932	0.74	2.4	1.68	1.776
Comp D67	61160	MGZD111	17	18	1.0	D19551	1.28	1.94	1.94	2.4832
Comp D67	61160	MGZD111	20	20.7	0.7	D19554	1.37	2.25	1.575	3.0825
Comp D67	61200	MGZD113	23.5	24.2	0.7	D19825	0.71	2.23	1.561	1.5833
Comp D67	61200	MGZD113	25.6	26.3	0.7	D19828	0.7	2.07	1.449	1.449
Comp D67	61200	MGZD113	26.3	27	0.7	D19829	0.74	2.09	1.463	1.5466
Comp D67	61200	MGZD114	15.8	16.5	0.7	D19297	0.85	1.83	1.281	1.5555
Comp D67	61200	MGZD114	16.5	17.2	0.7	D19299	0.7	1.86	1.302	1.302
Comp D67	61200	MGZD114	24.9	25.6	0.7	D19311	0.76	2.41	1.687	1.8316
Comp D68	60880	MGZD175	191	191.7	0.7	D39162	0.78	2.78	1.946	2.1684
Comp D68	60880	MGZD175	196.6	197.3	0.7	D39170	0.77	2.99	2.093	2.3023
Comp D68	60880	MGZD175	202	203	1.0	D39177	1.22	3.14	3.14	3.8308
Comp D68	60920	MGZD142	188.1	188.8	0.7	D29917	0.82	3.49	2.443	2.8618
Comp D68	60920	MGZD147	140.9	141.6	0.7	D31799	0.8	2.69	1.883	2.152
Comp D68	60920	MGZD147	142.3	143	0.7	D31801	0.79	3.06	2.142	2.4174
Comp D68	60920	MGZD147	143.7	144.4	0.7	D31803	0.85	2.81	1.967	2.3885
Comp D68	60920	MGZD147	144.4	145.1	0.7	D31804	0.65	2.95	2.065	1.9175
Comp D68	60920	MGZD147	152.8	153.5	0.7	D31816	0.77	3.24	2.268	2.4948
Comp D68	60920	MGZD147	155.6	156.3	0.7	D31822	0.75	3.29	2.303	2.4675
Comp D68	60920	MGZD162	151	152	1.0	D35628	1.28	3	3	3.84
Comp D68	60960	MGZD028	180.7	181.4	0.7	D02508	0.84	3.14	2.198	2.6376
Comp D68	60960	MGZD029	181.2	181.9	0.7	D02595	0.79	3.37	2.359	2.6623
Comp D68	60960	MGZD048	125.2	125.9	0.7	D04685	0.69	3.32	2.324	2.2908
Comp D68	60960	MGZD048	153	153.7	0.7	D04724	0.71	2.64	1.848	1.8744
Comp D68	60960	MGZD048	155.1	155.8	0.7	D04727	0.67	2.76	1.932	1.8492
Comp D68	60960	MGZD062	102	103	1.0	D06499	1.2	2.85	2.85	3.42
Comp D68	60960	MGZD063	143	144	1.0	D06419	1.08	2.87	2.87	3.0996
Comp D68	60960	MGZD063	148.2	149.2	1.0	D06427	1.06	2.72	2.72	2.8832
Comp D68	60960	MGZD071	123.1	123.8	0.7	D07642	0.75	3.44	2.408	2.58
Comp D68	61000	MGZD117	100.4	101.1	0.7	D20188	0.67	3.05	2.135	2.0435
Comp D68	61000	MGZD122	93.1	93.8	0.7	D21814	0.75	2.96	2.072	2.22

D ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp D68	61000	MGZD122	110.7	111.4	0.7	D21836	0.69	2.58	1.806	1.7802
Comp D68	61000	MGZD124	132.3	133	0.7	D22333	0.74	2.85	1.995	2.109
Comp D68	61000	MGZD127	105	106	1.0	D25361	1.12	2.63	2.63	2.9456
Comp D68	61040	MGZD026	90.5	91.2	0.7	D02395	0.8	2.52	1.764	2.016
Comp D68	61040	MGZD027	101.4	102.1	0.7	D02430	0.8	3.34	2.338	2.672
Comp D68	61040	MGZD027	114.1	114.8	0.7	D02450	0.79	3.31	2.317	2.6149
Comp D68	61040	MGZD027	116.9	117.6	0.7	D02454	0.85	2.99	2.093	2.5415
Comp D68	61040	MGZD027	121.8	122.5	0.7	D02462	1	2.88	2.016	2.88
Comp D68	61040	MGZD027	137.7	138.4	0.7	D02483	0.9	3.23	2.261	2.907
Comp D68	61040	MGZD061	58	59	1.0	D06682	1.1	2.99	2.99	3.289
Comp D68	61040	MGZD067	54.7	55.7	1.0	D07263	1.04	2.87	2.87	2.9848
Comp D68	61040	MGZD067	87	88	1.0	D07304	1.19	2.55	2.55	3.0345
Comp D68	61040	MGZD067	89	90	1.0	D07306	1.26	3.3	3.3	4.158
Comp D68	61040	MGZD067	119	119.7	0.7	D07340	0.86	2.64	1.848	2.2704
Comp D68	61040	MGZD067	119.7	120.7	1.0	D07341	1.03	3.1	3.1	3.193
Comp D68	61040	MGZD069	90	91	1.0	D07517	1.25	3.21	3.21	4.0125
Comp D68	61040	MGZD104	66.9	67.6	0.7	D16923	0.57	3.06	2.142	1.7442
Comp D68	61040	MGZD138	69.7	70.4	0.7	D29128	0.74	2.94	2.058	2.1756
Comp D68	61080	MGZD024	71.4	72.4	1.0	D02229	1	2.53	2.53	2.53
Comp D68	61080	MGZD025	42.4	43.1	0.7	D02267	0.7	3.15	2.205	2.205
Comp D68	61080	MGZD025	76	77	1.0	D02310	1	2.91	2.91	2.91
Comp D68	61080	MGZD032	73	74	1.0	D02782	1.07	2.52	2.52	2.6964
Comp D68	61080	MGZD053	60.8	61.5	0.7	D06047	0.79	2.84	1.988	2.2436
Comp D68	61080	MGZD053	68	68.7	0.7	D06056	0.72	3.18	2.226	2.2896
Comp D68	61080	MGZD053	71.5	72.2	0.7	D06062	0.84	2.81	1.967	2.3604
Comp D68	61080	MGZD053	77.2	77.9	0.7	D06070	0.76	2.84	1.988	2.1584
Comp D68	61080	MGZD053	79.3	80	0.7	D06075	0.93	2.57	1.799	2.3901
Comp D68	61080	MGZD105	16.1	16.8	0.7	D19036	0.74	3.13	2.191	2.3162
Comp D68	61120	MGZD018	21	21.7	0.7	D01445	0.8	3.26	2.282	2.608
Comp D68	61120	MGZD018	22.8	23.7	0.9	D01448	1	2.73	2.457	2.73
Comp D68	61120	MGZD019	70.7	71.4	0.7	D01576	0.7	2.87	2.009	2.009
Comp D68	61120	MGZD019	100	101	1.0	D01609	1.04	2.77	2.77	2.8808
Comp D68	61120	MGZD023	26	26.7	0.7	D02116	0.6	3.22	2.254	1.932
Comp D68	61120	MGZD023	33.4	34.2	0.8	D02126	0.8	2.85	2.28	2.28
Comp D68	61120	MGZD023	75.6	76.3	0.7	D02180	0.9	2.75	1.925	2.475
Comp D68	61120	MGZD033	44.1	44.8	0.7	D02832	0.74	2.97	2.079	2.1978
Comp D68	61120	MGZD051	23	23.7	0.7	D05820	0.81	2.85	1.995	2.3085
Comp D68	61120	MGZD055	25	25.7	0.7	D06116	0.83	2.79	1.953	2.3157
Comp D68	61120	MGZD055	32.7	33.4	0.7	D06127	0.82	2.97	2.079	2.4354
Comp D68	61120	MGZD055	52.7	53.4	0.7	D06154	0.73	2.95	2.065	2.1535
Comp D68	61120	MGZD055	58.8	59.5	0.7	D06162	0.85	3.13	2.191	2.6605
Comp D68	61160	MGZD056	48	48.7	0.7	D05957	0.99	2.72	1.904	2.6928
Comp D68	61160	MGZD056	65.7	66.4	0.7	D05979	0.91	2.82	1.974	2.5662
Comp D68	61160	MGZD110	12.3	13	0.7	D18928	0.72	3.47	2.429	2.4984
Comp D68	61160	MGZD110	40.2	40.9	0.7	D18970	0.68	2.78	1.946	1.8904
Comp D68	61200	MGZD113	20.7	21.4	0.7	D19820	0.74	2.96	2.072	2.1904
Comp D68	61200	MGZD113	24.2	24.9	0.7	D19826	0.71	2.62	1.834	1.8602
Comp D68	61200	MGZD113	27.7	28.4	0.7	D19831	0.76	2.56	1.792	1.9456
Comp D68	61200	MGZD114	49.4	50.1	0.7	D19350	0.53	2.74	1.918	1.4522
Comp D69	60920	MGZD142	187.4	188.1	0.7	D29916	0.85	4.04	2.828	3.434
Comp D69	60920	MGZD162	156.9	157.6	0.7	D35636	0.83	4.9	3.43	4.067
Comp D69	60920	MGZD162	161.1	161.8	0.7	D35643	0.76	3.98	2.786	3.0248
Comp D69	60920	MGZD162	167	168	1.0	D35652	1.31	4.24	4.24	5.5544
Comp D69	60960	MGZD028	183.5	184.2	0.7	D02512	0.94	4.67	3.269	4.3898
Comp D69	60960	MGZD029	180.5	181.2	0.7	D02594	0.87	4.54	3.178	3.9498

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Comp D69	60960	MGZD048	123.1	123.8	0.7	D04682	0.67	3.88	2.716	2.5996
Comp D69	60960	MGZD048	127.3	128	0.7	D04688	0.76	3.53	2.471	2.6828
Comp D69	60960	MGZD048	131.1	131.8	0.7	D04694	0.73	3.85	2.695	2.8105
Comp D69	60960	MGZD048	158	158.7	0.7	D04731	0.83	3.91	2.737	3.2453
Comp D69	60960	MGZD062	107	108	1.0	D06504	1.1	4.55	4.55	5.005
Comp D69	60960	MGZD063	128	129	1.0	D06399	0.98	4.89	4.89	4.7922
Comp D69	60960	MGZD063	144	144.7	0.7	D06420	0.75	4.02	2.814	3.015
Comp D69	60960	MGZD071	130.1	130.8	0.7	D07654	0.93	4.52	3.164	4.2036
Comp D69	60960	MGZD071	132.9	133.6	0.7	D07658	0.73	4.17	2.919	3.0441
Comp D69	61000	MGZD122	92.4	93.1	0.7	D21813	0.71	4.65	3.255	3.3015
Comp D69	61000	MGZD125	90.1	90.8	0.7	D23222	0.65	4.55	3.185	2.9575
Comp D69	61000	MGZD125	90.8	91.5	0.7	D23223	0.67	4.75	3.325	3.1825
Comp D69	61040	MGZD026	104	105	1.0	D02412	1.1	4.36	4.36	4.796
Comp D69	61040	MGZD027	122.5	123.2	0.7	D02463	0.81	4.2	2.94	3.402
Comp D69	61040	MGZD067	56.4	57.1	0.7	D07265	0.76	3.76	2.632	2.8576
Comp D69	61040	MGZD067	57.1	58	0.9	D07266	0.97	3.77	3.393	3.6569
Comp D69	61040	MGZD067	66.7	67.4	0.7	D07278	0.71	3.86	2.702	2.7406
Comp D69	61040	MGZD067	100.4	101.1	0.7	D07319	0.84	4.87	3.409	4.0908
Comp D69	61040	MGZD069	87.4	88.1	0.7	D07514	0.7	4.89	3.423	3.423
Comp D69	61040	MGZD104	64.8	65.5	0.7	D16919	0.71	4.17	2.919	2.9607
Comp D69	61040	MGZD138	57.8	58.5	0.7	D29109	0.88	3.99	2.793	3.5112
Comp D69	61040	MGZD138	70.4	71.1	0.7	D29129	0.75	4.13	2.891	3.0975
Comp D69	61040	MGZD138	71.1	71.8	0.7	D29130	0.8	3.55	2.485	2.84
Comp D69	61080	MGZD032	75.4	76.1	0.7	D02785	0.81	4.65	3.255	3.7665
Comp D69	61080	MGZD032	81	81.7	0.7	D02794	0.81	3.67	2.569	2.9727
Comp D69	61080	MGZD053	53	54	1.0	D06036	1.22	3.63	3.63	4.4286
Comp D69	61080	MGZD053	73	73.7	0.7	D06064	0.73	4.68	3.276	3.4164
Comp D69	61080	MGZD105	16.8	17.5	0.7	D19037	0.5	3.66	2.562	1.83
Comp D69	61080	MGZD108	32.4	33.1	0.7	D19174	0.72	3.86	2.702	2.7792
Comp D69	61080	MGZD108	79.7	80.4	0.7	D19239	0.83	4.11	2.877	3.4113
Comp D69	61080	MGZD118	56.2	56.9	0.7	D20441	1.42	3.75	2.625	5.325
Comp D69	61080	MGZD118	75.1	75.8	0.7	D20470	1.5	3.69	2.583	5.535
Comp D69	61120	MGZD019	70	70.7	0.7	D01575	0.7	4.57	3.199	3.199
Comp D69	61120	MGZD019	77	78	1.0	D01583	1	3.56	3.56	3.56
Comp D69	61120	MGZD020	63	63.7	0.7	D01669	0.75	4	2.8	3
Comp D69	61120	MGZD023	70	70.7	0.7	D02170	0.9	3.91	2.737	3.519
Comp D69	61120	MGZD033	33.7	34.4	0.7	D02819	1.18	3.77	2.639	4.4486
Comp D69	61120	MGZD051	14.7	15.4	0.7	D05809	0.87	3.97	2.779	3.4539
Comp D69	61120	MGZD051	15.4	16.1	0.7	D05810	0.81	4.89	3.423	3.9609
Comp D69	61120	MGZD055	47	47.7	0.7	D06145	0.82	3.73	2.611	3.0586
Comp D69	61120	MGZD055	52	52.7	0.7	D06153	0.86	3.51	2.457	3.0186
Comp D69	61120	MGZD055	66.7	67.4	0.7	D06174	0.8	4.64	3.248	3.712
Comp D69	61160	MGZD056	43	43.7	0.7	D05949	0.76	4.64	3.248	3.5264
Comp D69	61160	MGZD056	43.7	44.4	0.7	D05950	0.68	4.75	3.325	3.23
Comp D69	61160	MGZD056	48.7	49.4	0.7	D05958	0.82	4.14	2.898	3.3948
Comp D69	61160	MGZD056	49.4	50.1	0.7	D05959	0.83	4.05	2.835	3.3615
Comp D69	61160	MGZD056	65	65.7	0.7	D05978	0.86	5	3.5	4.3
Comp D69	61160	MGZD058	45.4	46.1	0.7	D06236	0.8	4.67	3.269	3.736
Comp D69	61160	MGZD111	18	19	1.0	D19552	1.34	3.75	3.75	5.025
Comp D69	61160	MGZD111	36.7	37.4	0.7	D19580	0.85	5	3.5	4.25
Comp D69	61200	MGZD113	17.2	17.9	0.7	D19814	0.76	4.68	3.276	3.5568
Comp D70	60880	MGZD175	195.9	196.6	0.7	D39169	0.71	7.93	5.551	5.6303
Comp D70	60920	MGZD147	139.5	140.2	0.7	D31795	0.82	5.91	4.137	4.8462
Comp D70	60920	MGZD147	141.6	142.3	0.7	D31800	0.75	5.45	3.815	4.0875
Comp D70	60920	MGZD162	157.6	158.3	0.7	D35637	0.73	5.98	4.186	4.3654

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Comp D70	60960	MGZD048	109.7	110.4	0.7	D04662	0.76	6.33	4.431	4.8108
Comp D70	60960	MGZD048	110.4	111.1	0.7	D04664	0.7	6.19	4.333	4.333
Comp D70	60960	MGZD048	114.7	115.4	0.7	D04669	0.72	5.35	3.745	3.852
Comp D70	60960	MGZD048	122.4	123.1	0.7	D04681	0.69	6.62	4.634	4.5678
Comp D70	60960	MGZD048	155.8	156.5	0.7	D04728	0.66	6.75	4.725	4.455
Comp D70	60960	MGZD063	119	120	1.0	D06386	1.19	5.31	5.31	6.3189
Comp D70	61000	MGZD119	89	89.7	0.7	D20632	0.79	5.37	3.759	4.2423
Comp D70	61000	MGZD122	116	117	1.0	D21843	1.2	6.19	6.19	7.428
Comp D70	61000	MGZD122	117	118	1.0	D21844	1.1	6.35	6.35	6.985
Comp D70	61000	MGZD124	130.2	130.9	0.7	D22330	0.69	6.18	4.326	4.2642
Comp D70	61000	MGZD124	131.6	132.3	0.7	D22332	0.68	7	4.9	4.76
Comp D70	61000	MGZD124	136.5	137.2	0.7	D22340	0.53	5.88	4.116	3.1164
Comp D70	61000	MGZD125	91.5	92.2	0.7	D23224	0.73	6.96	4.872	5.0808
Comp D70	61000	MGZD127	112	113	1.0	D25368	1.03	5.65	5.65	5.8195
Comp D70	61040	MGZD026	91.2	92.2	1.0	D02397	1.2	5.51	5.51	6.612
Comp D70	61040	MGZD027	100.7	101.4	0.7	D02429	1	7.98	5.586	7.98
Comp D70	61040	MGZD027	102.1	102.8	0.7	D02431	0.8	5.21	3.647	4.168
Comp D70	61040	MGZD027	105.7	106.4	0.7	D02436	0.8	6.84	4.788	5.472
Comp D70	61040	MGZD060	82	83	1.0	D06556	1	7.53	7.53	7.53
Comp D70	61040	MGZD067	88	89	1.0	D07305	1.28	6.05	6.05	7.744
Comp D70	61040	MGZD067	102	103	1.0	D07322	1.21	5.57	5.57	6.7397
Comp D70	61040	MGZD067	110	111	1.0	D07330	1.1	6.31	6.31	6.941
Comp D70	61080	MGZD024	65.1	65.8	0.7	D02220	0.7	5.91	4.137	4.137
Comp D70	61080	MGZD025	51.9	52.6	0.7	D02282	0.8	5.61	3.927	4.488
Comp D70	61080	MGZD025	75	76	1.0	D02309	1.1	5.42	5.42	5.962
Comp D70	61080	MGZD025	84.1	85.1	1.0	D02319	1	6.67	6.67	6.67
Comp D70	61080	MGZD053	58	58.7	0.7	D06041	0.75	5.74	4.018	4.305
Comp D70	61080	MGZD108	62.3	63	0.7	D19215	0.87	5.93	4.151	5.1591
Comp D70	61080	MGZD118	44	45	1.0	D20424	2.28	6.08	6.08	13.8624
Comp D70	61080	MGZD118	73	73.7	0.7	D20467	1.6	6.57	4.599	10.512
Comp D70	61120	MGZD019	85	86	1.0	D01592	1.4	6.03	6.03	8.442
Comp D70	61120	MGZD019	101	102	1.0	D01610	1.05	5.52	5.52	5.796
Comp D70	61120	MGZD019	115	116	1.0	D24562	0.84	6.11	6.11	5.1324
Comp D70	61120	MGZD023	56.8	57.5	0.7	D02154	0.7	7.35	5.145	5.145
Comp D70	61160	MGZD034	44.4	45.1	0.7	D02892	0.84	6.44	4.508	5.4096
Comp D70	61160	MGZD052	39.7	40.4	0.7	D06293	0.77	5.34	3.738	4.1118
Comp D70	61160	MGZD110	35.3	36	0.7	D18963	0.78	5.4	3.78	4.212
Comp D70	61200	MGZD114	28.4	29.1	0.7	D19316	0.86	5.14	3.598	4.4204
Comp D71	60880	MGZD164	198	199	1.0	D36354	1.22	8.18	8.18	9.9796
Comp D71	60880	MGZD175	177.7	178.4	0.7	D39141	0.85	8.72	6.104	7.412
Comp D71	60920	MGZD147	143	143.7	0.7	D31802	0.74	30.8	21.56	22.792
Comp D71	60920	MGZD147	153.5	154.2	0.7	D31817	0.72	9.16	6.412	6.5952
Comp D71	60920	MGZD162	156.2	156.9	0.7	D35635	0.76	16	11.2	12.16
Comp D71	60920	MGZD162	158.3	159	0.7	D35639	0.73	12.7	8.89	9.271
Comp D71	60920	MGZD162	161.8	162.5	0.7	D35644	0.73	9.17	6.419	6.6941
Comp D71	60960	MGZD028	187.7	188.4	0.7	D02519	0.98	8.19	5.733	8.0262
Comp D71	60960	MGZD028	200	200.7	0.7	D02534	0.78	13.7	9.59	10.686
Comp D71	60960	MGZD029	179.1	179.8	0.7	D02591	0.87	12	8.4	10.44
Comp D71	60960	MGZD048	109	109.7	0.7	D04661	0.75	11	7.7	8.25
Comp D71	60960	MGZD048	123.8	124.5	0.7	D04683	0.68	8.52	5.964	5.7936
Comp D71	60960	MGZD048	126.6	127.3	0.7	D04687	0.74	12.3	8.61	9.102
Comp D71	60960	MGZD063	134	135	1.0	D06407	1.15	11.7	11.7	13.455
Comp D71	60960	MGZD071	124.5	125.2	0.7	D07644	0.85	8.53	5.971	7.2505
Comp D71	60960	MGZD071	129.4	130.1	0.7	D07653	0.88	9.15	6.405	8.052
Comp D71	61000	MGZD117	112.3	113	0.7	D20207	0.78	24.3	17.01	18.954

D ZONE Grade Composite	Section	HOLE_ID	Meters From	To	Interval m	SAMPLE_NO	G&T Weight (kg)	Drill Core Assay Au g/t	Grade x Thickness g Au/t x m	Grade x Sample Wt g Au/t x kg
Comp D71	61000	MGZD117	114.4	115.1	0.7	D20210	0.85	11.1	7.77	9.435
Comp D71	61000	MGZD124	83	84	1.0	D22267	1.06	24.4	24.4	25.864
Comp D71	61000	MGZD124	138.6	139.3	0.7	D22343	0.73	9.82	6.874	7.1686
Comp D71	61000	MGZD125	113.2	113.9	0.7	D23257	0.79	17.7	12.39	13.983
Comp D71	61000	MGZD125	113.9	114.6	0.7	D23259	0.76	13.5	9.45	10.26
Comp D71	61040	MGZD027	99	100	1.0	D02426	1.2	12.2	12.2	14.64
Comp D71	61040	MGZD059	129	130	1.0	D07150	1.21	26	26	31.46
Comp D71	61040	MGZD060	88.7	89.4	0.7	D06563	0.8	12.7	8.89	10.16
Comp D71	61040	MGZD067	55.7	56.4	0.7	D07264	0.78	9.93	6.951	7.7454
Comp D71	61040	MGZD067	73	74	1.0	D07286	1.16	10.5	10.5	12.18
Comp D71	61040	MGZD067	101.1	102	0.9	D07320	1.17	15.3	13.77	17.901
Comp D71	61040	MGZD067	109	110	1.0	D07329	1.1	10.8	10.8	11.88
Comp D71	61040	MGZD067	111	112	1.0	D07331	0.98	12.2	12.2	11.956
Comp D71	61040	MGZD070	73	73.7	0.7	D07608	0.78	8.54	5.978	6.6612
Comp D71	61040	MGZD070	73.7	74.4	0.7	D07609	0.78	8.78	6.146	6.8484
Comp D71	61040	MGZD104	63.4	64.1	0.7	D16916	0.58	8.27	5.789	4.7966
Comp D71	61080	MGZD024	66.5	67.2	0.7	D02223	0.8	13	9.1	10.4
Comp D71	61080	MGZD024	67.2	67.9	0.7	D02224	0.7	8.32	5.824	5.824
Comp D71	61080	MGZD025	85.1	86.1	1.0	D02320	1	12.3	12.3	12.3
Comp D71	61080	MGZD053	52	53	1.0	D06035	1.12	11	11	12.32
Comp D71	61080	MGZD053	61.5	62.2	0.7	D06048	0.78	13.5	9.45	10.53
Comp D71	61080	MGZD053	63	63.7	0.7	D06050	0.71	16.5	11.55	11.715
Comp D71	61080	MGZD053	72.2	73	0.8	D06063	0.96	8.87	7.096	8.5152
Comp D71	61080	MGZD053	75.8	76.5	0.7	D06068	0.75	11.1	7.77	8.325
Comp D71	61080	MGZD053	76.5	77.2	0.7	D06069	0.74	9.34	6.538	6.9116
Comp D71	61080	MGZD053	78.6	79.3	0.7	D06074	0.64	30.2	21.14	19.328
Comp D71	61080	MGZD053	80	80.7	0.7	D06076	0.84	9.64	6.748	8.0976
Comp D71	61080	MGZD116	67	68	1.0	D20369	2.06	8.61	8.61	17.7366
Comp D71	61080	MGZD118	49.2	50	0.8	D20431	1.73	34.9	27.92	60.377
Comp D71	61080	MGZD118	69.5	70.2	0.7	D20462	1.44	8.3	5.81	11.952
Comp D71	61120	MGZD019	71.4	72.1	0.7	D01577	0.8	27	18.9	21.6
Comp D71	61120	MGZD019	76	77	1.0	D01582	1	15	15	15
Comp D71	61120	MGZD023	54.7	55.4	0.7	D02151	0.8	21.2	14.84	16.96
Comp D71	61120	MGZD023	61.4	62.1	0.7	D02161	0.7	12.6	8.82	8.82
Comp D71	61120	MGZD023	63.1	63.9	0.8	D02163	0.8	11	8.8	8.8
Comp D71	61120	MGZD023	73.5	74.2	0.7	D02177	0.6	38.5	26.95	23.1
Comp D71	61120	MGZD023	82	83	1.0	D02187	1.2	24.7	24.7	29.64
Comp D71	61120	MGZD054	55.7	56.4	0.7	D06350	0.78	8.43	5.901	6.5754
Comp D71	61120	MGZD054	69	70	1.0	D07174	1.18	8.75	8.75	10.325
Comp D71	61120	MGZD055	56	56.7	0.7	D06158	0.79	12.5	8.75	9.875
Comp D71	61160	MGZD034	45.1	45.8	0.7	D02894	0.8	9.65	6.755	7.72
Comp D71	61160	MGZD034	57.7	58.4	0.7	D02910	0.88	14.8	10.36	13.024
Comp D71	61160	MGZD052	40.4	41.1	0.7	D06294	0.82	18.9	13.23	15.498
Comp D71	61160	MGZD056	44.4	45.1	0.7	D05951	0.86	9.09	6.363	7.8174
Comp D71	61160	MGZD110	37.4	38.1	0.7	D18966	0.77	9.71	6.797	7.4767
Comp D71	61160	MGZD110	41.6	42.3	0.7	D18973	0.77	28.1	19.67	21.637

Appendix E

Qualified Persons Certificates

CERTIFICATE OF QUALIFICATIONS

I, Sandy M. Archibald, P. Geo., of 105 Breakwater Drive, Whitby, Ontario, Canada, as an author of this report entitled "Mineral Resource Estimate and Update to a NI43-101 Technical Report for the Handeni Property centered at 37.97°E, 5.744°S, Tanga Province, Handeni District, Tanzania" dated June 11, 2013 prepared for East Africa Metals Inc. (the "Issuer"), do hereby certify that:

1. I am a Principal Consultant Geologist with Aurum Exploration Services.
2. I graduated with an honours B.Sc. degree in Geology from University of Glasgow in 1992, was awarded an M.Sc. degree in Geology from Memorial University of Newfoundland in 1995, and a Ph.D. in Geology/Geochemistry from McGill University, Montréal, Canada in 2002.
3. This certificate applies to the technical report entitled "Mineral Resource Estimate and Update to a NI43-101 Technical Report for the Handeni Property centered at 37.97°E, 5.744°S, Tanga Province, Handeni District, Tanzania" dated June 11, 2013 ("Technical Report") prepared for the Issuer.
4. I have been employed in my profession by Aurum Exploration Services since completing my final postgraduate degree since 2002. My relevant experience includes designing and implementing mineral exploration programmes for a variety of commodities, including orogenic lode-gold exploration in Europe, Africa and North America.
5. I am a member of the European Federation of Geologists (Title No. 873), and I am a Professional Geologist (Title No. 193) associated with the Institute of Geologists of Ireland. I am also a Fellow of the Society of Economic Geologists, and a Member of the Society for Geology Applied to Mineral Deposits.
6. I have read the definitions of "Qualified Person" set out in in National Instrument 43-101 – *Standards of Disclosure for Mineral Projects* ("NI 43-101") and certify that by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I fulfill the requirements to be a "Qualified Person" for the purposes of NI 43-101.
7. I most recently visited the subject property from February 14 to 16, 2012.
8. I am responsible for preparation of all sections of the Technical Report, other than Sections 11, 12 (except for subsection 12.2), 13 and 14.
9. I am independent of the Issuer applying all the tests in Section 1.5 of NI 43-101.
10. I have had prior involvement with the property that is the subject of the Technical Report. The nature of my prior involvement was as the author of the report entitled "NI 43-101 Technical Report on the Handeni Property Centred at 39.97°E, 5.753°S, Tanga Province, Kalindi District, Tanzania" (March 2011).
11. I have read NI 43-101 and NI 43-101F1 and the Technical Report has been prepared in compliance with that instrument and form.
12. As of the effective date of the Technical Report, to the best of my knowledge, information and belief, the Technical Report contains all scientific and technical information that is required to be disclosed to make the Technical Report not misleading.

"Sandy M. Archibald" (signed)

EurGeol Dr. Sandy M. Archibald, P.Geo.

DATED at Whitby, Canada, this 11th day of June, 2013.

CERTIFICATE OF QUALIFICATIONS

I, Ian J. Farrelly, P.Geo., of 32A, Beaubec, Dublin Road, Drogheda, Ireland, as an author of this report entitled "Mineral Resource Estimate and Update to a NI43-101 Technical Report for the Handeni Property centered at 37.97°E, 5.744°S, Tanga Province, Handeni District, Tanzania" dated June 11, 2013 prepared for East Africa Metals Inc. (the "Issuer"), do hereby certify that:

1. I am a Principal Consultant Geologist with Aurum Exploration Services.
2. This certificate applies to the technical report entitled "Mineral Resource Estimate and Update to a NI43-101 Technical Report for the Handeni Property centered at 37.97°E, 5.744°S, Tanga Province, Handeni District, Tanzania" dated June 11, 2013 ("Technical Report") prepared for the Issuer.
3. I graduated with an honours Bachelor of Arts degree in Geology from Trinity College Dublin, Ireland in 1994 and was awarded a Post Graduate Diploma in Statistics from Trinity College Dublin, Ireland in 1995.
4. I have been employed in my profession since 1997; most recently by Aurum Exploration Services since 2003. My relevant experience includes both domestic and international mineral exploration, design and implementation of drilling/sampling programs, independent monitoring of QA/QC data and resource evaluation for a variety of commodities. In addition to this work, I have also taken professional development courses in orogenic lode-gold systems and geostatistics.
5. I am a member of the European Federation of Geologists (Title No. 936), and I am a Professional Geologist (Title No. 210) associated with the Institute of Geologists of Ireland. I am also a Fellow of the Society of Economic Geologists.
6. I have read the definitions of "Qualified Person" set out in National Instrument 43-101 – *Standards of Disclosure for Mineral Projects* ("NI 43-101") and certify that by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I fulfill the requirements to be a "Qualified Person" for the purposes of NI 43-101.
7. I most recently visited the subject property from September 25 to 28, 2011.
8. I am responsible for preparation of sections 11 and 12 of the Technical Report, excepting subsections 12.2 and 12.3.1.
9. I am independent of the Issuer applying all the tests in Section 1.5 of NI 43-101.
10. I have had prior involvement with the property that is the subject of the Technical Report. The nature of my prior involvement is as a geologist and consultant during the review and preparation of reports related to QA/QC procedures at the Handeni property for Canaco Resources Inc.
11. I have read NI 43-101 and NI 43-101F1 and the Technical Report has been prepared in compliance with that instrument and form.
12. As of the effective date of the Technical Report, to the best of my knowledge, information and belief, the Technical Report contains all scientific and technical information that is required to be disclosed to make the Technical Report not misleading.

"Ian J. Farrelly" (signed)
EurGeol Ian J. Farrelly, P.Geo.
DATED at Kells, Ireland this 11th day of June, 2013.

CERTIFICATE OF AUTHOR
James N. Gray

I, James N. Gray, P. Geo., as an author of this report entitled "Mineral Resource Estimate and Update to a NI43-101 Technical Report for the Handeni Property centered at 37.97°E, 5.744°S, Tanga Province, Handeni District, Tanzania" dated June 11, 2013, prepared for East Africa Metals Inc. (the "Issuer"), do hereby certify that:

1. I am a consulting geologist residing at 1051 Bullmoose Trail, Osoyoos, BC.

2. This certificate applies to the entitled "Mineral Resource Estimate and Update to a NI43-101 Technical Report for the Handeni Property centered at 37.97°E, 5.744°S, Tanga Province, Handeni District, Tanzania" dated June 11, 2013 ("Technical Report") prepared for the Issuer.

3. I am a graduate of the University of Waterloo, with a B.Sc. in Geology in 1985. I have practiced my profession continuously since 1985. My experience includes resource estimation work at operating mines as well as base and precious metal projects in North and South America, Europe, Asia and Africa.

4. I am a Professional Geoscientist registered in good standing with the Association of Professional Engineers and Geoscientists of British Columbia (#27022).

5. I have read the definition of "qualified person" set out in National Instrument 43-101 – *Standards of Disclosure for Mineral Projects* ("NI 43-101") and certify that by reason of my education, affiliation with professional associations (as deemed in NI 43-101) and past relevant work experience, I fulfill the requirements to be a "qualified person" (QP) for the purposes of NI 43-101.

6. I visited the subject property from February 14 to 16, 2012.

7. I was responsible for the preparation of Sections 12.3.1 and 14 of the Technical Report.

8. I am independent of the Issuer applying all the tests in Section 1.5 of NI 43-101.

9. I have had prior involvement with the property that is the subject of the Technical Report. The nature of my prior involvement was as the author of the report entitled "NI 43-101 Technical Report and Mineral Resource Estimate for the Handeni Property centered at 37.97°E, 5.744°S, Tanga Province, Handeni District, Tanzania" (June 2012).

10. I have read NI 43-101 and Form 43-101F1, and the Technical Report has been prepared in compliance with that instrument and form.

11. As of the effective date of the Technical Report, to the best of my knowledge, information and belief, the Technical Report contains all scientific and technical information that is required to be disclosed to make the Technical Report not misleading.

Dated this 11th day of June, 2013, in Osoyoos, British Columbia.

"James N. Gray" (signed and sealed)
James N. Gray, P.Geo
Advantage Geoservices Limited

CERTIFICATE OF QUALIFICATIONS

I, James Anthony King, P.Eng., of 6775 Marine Drive, West Vancouver, British Columbia, Canada, as an author of this report entitled “Mineral Resource Estimate and Update to a NI43-101 Technical Report for the Handeni Property centered at 37.97°E, 5.744°S, Tanga Province, Handeni District, Tanzania” dated June 11, 2013 prepared for East Africa Metals Inc. (the “Issuer”), do hereby certify that:

1. I am the Principal of Jim King Consulting Inc.
2. This certificate applies to the technical report entitled “Mineral Resource Estimate and Update to a NI43-101 Technical Report for the Handeni Property centered at 37.97°E, 5.744°S, Tanga Province, Handeni District, Tanzania” dated June 11, 2011 (“Technical Report”) prepared for the Issuer.
3. I graduated with a Bachelor of Science (Eng) degree in Extraction Metallurgy from the Royal School of Mines, London University, UK, in 1963, and was awarded a Doctor of Philosophy in Hydrometallurgy from the Royal School of Mines in 1966.
4. I have been employed in my profession continuously since completing my postgraduate degree in 1966, having worked for Roan Selection Trust, Zambia (1966-1968), Western Mines Ltd. (1968-1970), and Placer Dome Inc. (1970 to 2006). In 2007, I formed the private metallurgical consulting company Jim King Consulting Inc., of which I am the principal.
5. I am a member of The Association of Professional Engineers and Geoscientists of British Columbia, Licence # 7398.
6. I have read the definitions of “Qualified Person” set out in NI 43-101 and certify that by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I fulfill the requirements to be a “Qualified Person” for the purposes of NI 43-101.
7. I most recently visited the subject property from February 14 to 16, 2012.
8. I am responsible for preparation of Section 13 of the Technical Report.
9. I am independent of the Issuer, applying all the tests in Section 1.5 of NI 43-101.
10. I have had prior involvement with the property that is the subject of the Technical Report. The nature of my prior involvement was as the author of the report entitled "NI 43-101 Technical Report and Mineral Resource Estimate for the Handeni Property centered at 37.97°E, 5.744°S, Tanga Province, Handeni District, Tanzania” (June 2012).
11. I have read NI 43-101 and NI 43-101F1 and the technical report has been prepared in compliance with that instrument and form.
12. As of the effective date of the Technical Report, to the best of my knowledge, information and belief, the Technical Report contains all scientific and technical information that is required to be disclosed to make the Technical Report not misleading.

Dated this 11th day of June, 2013, in West Vancouver, British Columbia.

“James A. King” (signed and sealed)
Dr. James Anthony King, P.Eng.